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Next Generation EU

COMUNE DI ALSENO
Provincia di
Piacenza



PIANO NAZIONALE DI RIPRESA E RESILIENZA - PNRR

Finanziato dall'Unione Europea Next Generation EU

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Componente 1 - Potenziamento dell'offerta dei servizi di istruzione: dagli asili nido all'università
Investimento 1.2 "Piano di estensione del tempo pieno e mense"

PROGETTO DEFINITIVO-ESECUTIVO

REALIZZAZIONE NUOVA MENSA SCUOLA SECONDARIA ALSENO

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CUP E95E22000450001

(ISTITUTO COMPRENSIVO CASTELL'ARQUATO)



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OGGETTO

F - ELABORATI STRUTTURALI

ELABORATO N°

F.2

TITOLO

**EDIFICIO MENSA -
RELAZIONE DI CALCOLO**

SCALA

DATA

03.06.2023

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Il presente elaborato è tutelato dalle leggi sul diritto d'autore. E' fatto divieto a chiunque di riprodurlo anche in parte se non per fini autorizzati.

La presente relazione di calcolo è redatta in conformità alle disposizioni della DGR n. 1373/2011 del 26.09.2011: *"Approvazione dell'atto di indirizzo recante l'individuazione della documentazione attinente alla riduzione del rischio sismico necessaria per il rilascio del permesso di costruire e per gli altri titoli edilizi, alla individuazione degli elaborati costitutivi e dei contenuti del progetto esecutivo riguardante le strutture e alla definizione delle modalità di controllo degli stessi, ai sensi dell'art. 12, comma 1 e dell'art. 4, comma 1 della L.R. n. 19 del 2008"*, pubblicata sul BUR n. 153 del 12.10.2011 parte seconda.

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F.2. RELAZIONE DI CALCOLO STRUTTURALE DI DETTAGLIO

Facendo seguito alla "1. *Illustrazione Sintetica degli Elementi Essenziali del Progetto Strutturale*", si riportano in modo analitico i risultati delle verifiche relative agli elementi strutturali dell'intervento in oggetto che prevede la realizzazione di un edificio adibito a **Mensa Scolastica** da realizzarsi in Via Dante Alighieri n.1, in Comune di Alseno – PC.

La presente è da consultarsi congiuntamente agli Elaborati Grafici Esecutivi depositati contestualmente.

2.1 Principali Risultati

Di seguito si riportano i principali risultati più significativi delle analisi svolte, mirati a riassumere il comportamento della struttura.

2.1.1 Risultati Analisi Dinamica Lineare "Modale"

Ciascun caso di carico sismico è caratterizzato da un angolo di ingresso e da una configurazione di masse determinante la forza sismica complessiva.

Nella colonna Note sono riportati i parametri fondamentali che caratterizzano l'azione sismica, in particolare:

| | |
|-------------------------------|---|
| Angolo di ingresso | Angolo di ingresso dell'azione sismica orizzontale |
| Accelerazione a_g | Accelerazione orizzontale massima sul suolo |
| Categoria suolo | Categoria di profilo stratigrafico del suolo di fondazione |
| Fattore di comportamento q | Fattore dipendente dalla tipologia strutturale |
| Fattore di sito S | Fattore dipendente dalla stratigrafia e dal profilo topografico |
| Classe di duttilità CD | Classe di duttilità della struttura – "A" duttilità alta, "B" duttilità media |
| Periodo proprio T_1 | Periodo proprio di vibrazione della struttura |
| Ordinata spettro $S(T_b-T_c)$ | Valore dell' ordinata dello spettro in uso nel tratto costante |
| numero di modi considerati | Numero di modi di vibrare della struttura considerati nell'analisi dinamica |

Per ciascun caso di carico sismico viene riportato l'insieme di dati sotto elencati (le masse sono espresse in unità di forza):

- quota, posizione del centro di massa e massa risultante, posizione del baricentro delle rigidezze;
- frequenza, periodo, accelerazione spettrale, massa eccitata nelle due direzioni globali per tutti i modi massa complessiva ed aliquota di massa complessiva eccitata.

| Id nodo | Longitudine | Latitudine | Distanza |
|---------|-------------|------------|----------|
| | | | Km |
| Loc. | 9.909 | 44.889 | |
| 14934 | 9.894 | 44.881 | 1.436 |
| 14935 | 9.964 | 44.883 | 4.397 |
| 14713 | 9.961 | 44.933 | 6.396 |
| 14712 | 9.891 | 44.931 | 4.877 |

| SL | Pver | Tr | a_g | Fo | T*c |
|-----|------|--------|-------|-------|-------|
| | | Anni | g | | sec |
| SLO | 81.0 | 45.2 | 0.050 | 2.483 | 0.244 |
| SLD | 63.0 | 75.4 | 0.063 | 2.481 | 0.260 |
| SLV | 10.0 | 711.8 | 0.151 | 2.514 | 0.285 |
| SLC | 5.0 | 1462.2 | 0.190 | 2.550 | 0.292 |

| SL | ag | S | Fo | Fv | Tb | Tc | Td |
|-----|-------|-------|-------|-------|-------|-------|-------|
| | g | | | | sec | sec | sec |
| SLO | 0.050 | 1.200 | 2.483 | 0.751 | 0.119 | 0.356 | 1.801 |
| SLD | 0.063 | 1.200 | 2.481 | 0.841 | 0.125 | 0.374 | 1.852 |
| SLV | 0.151 | 1.200 | 2.514 | 1.320 | 0.134 | 0.403 | 2.205 |
| SLC | 0.190 | 1.200 | 2.550 | 1.501 | 0.137 | 0.411 | 2.360 |

2.1.1.1 Tabulati Analisi Dinamica Lineare

Massa sismica totale: $M_{sis.} = 317\ 700\ kg.$

| Quota | M Sismica x g | Pos. GX | Pos. GY | E agg. X-X | E agg. Y-Y | Pos. KX | Pos. KY |
|--------|---------------|---------|---------|------------|------------|---------|---------|
| cm | daN | cm | cm | cm | cm | cm | cm |
| 592.00 | 1.712e+04 | 2190.49 | 1155.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 589.60 | 30.49 | 2852.50 | 1143.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 588.98 | 27.08 | 2852.50 | 1162.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 588.03 | 37.91 | 1280.50 | 1135.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 585.00 | 38.69 | 2852.50 | 1120.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 584.26 | 35.29 | 1280.50 | 1174.25 | 0.0 | 0.0 | 0.0 | 0.0 |
| 583.63 | 38.38 | 1280.50 | 1113.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 580.39 | 77.06 | 2852.50 | 1109.90 | 0.0 | -2.30 | 0.0 | 0.0 |
| 579.93 | 63.60 | 2852.50 | 1180.13 | 0.0 | -1.12 | 0.0 | 0.0 |
| 579.22 | 36.75 | 1280.50 | 1091.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 576.52 | 39.26 | 1280.50 | 1193.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 575.79 | 46.08 | 2852.50 | 1074.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 574.82 | 41.92 | 1280.50 | 1069.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 574.00 | 46.93 | 1280.50 | 1134.72 | 0.0 | -4.15 | 0.0 | 0.0 |
| 571.19 | 43.95 | 2852.50 | 1051.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 570.89 | 44.90 | 2852.50 | 1207.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 570.42 | 40.03 | 1280.50 | 1047.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 568.77 | 36.28 | 1280.50 | 1212.75 | 0.0 | 0.0 | 0.0 | 0.0 |
| 566.59 | 41.82 | 2852.50 | 1028.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 566.02 | 38.51 | 1280.50 | 1025.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 561.98 | 39.45 | 2852.50 | 1005.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 561.84 | 40.83 | 2852.50 | 1230.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 561.61 | 37.69 | 1280.50 | 1003.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 561.03 | 32.46 | 1280.50 | 1232.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 557.38 | 49.76 | 2852.50 | 982.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 557.01 | 43.93 | 1280.50 | 980.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 556.00 | 127.39 | 1280.50 | 1118.57 | 0.0 | -11.44 | 0.0 | 0.0 |
| 555.39 | 213.59 | 2852.50 | 1119.81 | 0.0 | -11.25 | 2852.50 | 1117.50 |
| 553.99 | 34.15 | 1280.50 | 1249.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 552.79 | 97.12 | 2852.50 | 1105.95 | 0.0 | -14.68 | 0.0 | 0.0 |
| 552.41 | 41.85 | 1280.50 | 957.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 547.88 | 48.12 | 2852.50 | 934.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 547.81 | 40.19 | 1280.50 | 934.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 546.96 | 37.41 | 1280.50 | 1267.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 543.74 | 43.43 | 2852.50 | 1275.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 543.20 | 38.42 | 1280.50 | 911.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 542.87 | 46.11 | 2852.50 | 909.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 538.60 | 43.75 | 1280.50 | 888.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 538.00 | 201.24 | 1280.50 | 1092.96 | 0.0 | -17.79 | 1280.50 | 1089.08 |
| 537.87 | 43.28 | 2852.50 | 884.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 537.36 | 48.44 | 1280.50 | 1290.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 534.69 | 52.40 | 2852.50 | 1297.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 534.00 | 41.70 | 1280.50 | 865.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 532.87 | 54.43 | 2852.50 | 859.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 530.39 | 389.47 | 2852.50 | 1084.49 | 0.0 | -19.53 | 2852.50 | 1079.75 |
| 529.40 | 40.04 | 1280.50 | 842.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 527.87 | 51.13 | 2852.50 | 834.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 527.31 | 44.98 | 1280.50 | 1315.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 525.64 | 47.05 | 2852.50 | 1320.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 524.79 | 38.83 | 1280.50 | 819.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 522.86 | 48.62 | 2852.50 | 809.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 520.06 | 47.30 | 1280.50 | 795.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 520.00 | 1823.64 | 745.53 | 1140.17 | 0.0 | -24.83 | 1280.50 | 1067.50 |
| 517.86 | 46.10 | 2852.50 | 784.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 517.25 | 51.03 | 1280.50 | 1340.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 516.59 | 42.62 | 2852.50 | 1342.50 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | M Sismica x g | Pos. GX | Pos. GY | E agg. X-X | E agg. Y-Y | Pos. KX | Pos. KY |
|--------|---------------|---------|---------|------------|------------|---------|---------|
| 516.42 | 763.97 | 101.00 | 1137.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 516.05 | 729.17 | 1280.50 | 1135.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 515.26 | 43.63 | 1280.50 | 771.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 512.86 | 43.28 | 2852.50 | 759.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 512.44 | 800.93 | 101.00 | 1117.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 512.13 | 710.24 | 1280.50 | 1174.25 | 0.0 | 0.0 | 0.0 | 0.0 |
| 511.67 | 766.68 | 1280.50 | 1113.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 511.01 | 891.21 | 101.00 | 1177.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 510.86 | 40.18 | 1280.50 | 749.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 508.46 | 799.33 | 101.00 | 1097.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 507.85 | 50.22 | 2852.50 | 734.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 507.54 | 51.23 | 2852.50 | 1365.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 507.29 | 766.68 | 1280.50 | 1091.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 507.20 | 46.25 | 1280.50 | 1365.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 506.45 | 38.66 | 1280.50 | 727.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 505.39 | 583.22 | 2852.50 | 1055.85 | 0.0 | -29.15 | 2852.50 | 1051.00 |
| 504.47 | 797.56 | 101.00 | 1077.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 504.26 | 710.23 | 1280.50 | 1193.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 503.65 | 43.28 | 2852.50 | 713.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 502.91 | 766.47 | 1280.50 | 1069.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 502.83 | 855.07 | 101.00 | 1197.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 502.05 | 36.99 | 1280.50 | 705.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 500.49 | 786.11 | 101.00 | 1057.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 499.45 | 41.51 | 2852.50 | 692.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 499.00 | 87.74 | 101.00 | 1129.72 | 0.0 | -5.00 | 0.0 | 0.0 |
| 498.53 | 820.85 | 1368.74 | 1066.26 | 0.0 | -17.02 | 0.0 | 0.0 |
| 497.65 | 43.65 | 1280.50 | 683.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 497.14 | 48.29 | 1280.50 | 1390.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 496.71 | 764.04 | 101.00 | 1038.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 496.40 | 717.97 | 1280.50 | 1212.75 | 0.0 | 0.0 | 0.0 | 0.0 |
| 496.06 | 16.98 | 1280.50 | 795.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 496.00 | 352.67 | 1280.50 | 1044.37 | 0.0 | -33.02 | 1280.50 | 1053.45 |
| 495.90 | 14.20 | 1280.50 | 957.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 495.25 | 39.73 | 2852.50 | 671.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 494.66 | 903.85 | 101.00 | 1217.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 494.15 | 774.72 | 1280.50 | 1025.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 493.25 | 41.70 | 1280.50 | 661.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 492.93 | 762.59 | 101.00 | 1019.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 491.04 | 37.96 | 2852.50 | 650.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 489.78 | 783.23 | 1280.50 | 1003.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 489.44 | 41.82 | 2852.50 | 1410.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 489.15 | 761.15 | 101.00 | 1000.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 488.84 | 40.18 | 1280.50 | 639.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 488.64 | 41.26 | 1280.50 | 1412.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 488.53 | 677.40 | 1280.50 | 1232.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 486.84 | 35.95 | 2852.50 | 629.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 485.46 | 952.70 | 101.00 | 1239.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 485.37 | 759.71 | 101.00 | 981.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 485.20 | 800.80 | 1280.50 | 980.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 484.44 | 38.66 | 1280.50 | 617.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 482.64 | 44.43 | 2852.50 | 608.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 481.59 | 758.03 | 101.00 | 962.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 481.38 | 645.13 | 1280.50 | 1249.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 480.62 | 800.59 | 1280.50 | 957.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 480.39 | 782.44 | 2852.50 | 1050.67 | 0.0 | -40.15 | 0.0 | 0.0 |
| 480.04 | 36.98 | 1280.50 | 595.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 479.79 | 39.10 | 1280.50 | 1434.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 478.44 | 42.09 | 2852.50 | 587.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 477.80 | 887.32 | 101.00 | 943.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 476.27 | 960.65 | 101.00 | 1262.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 476.04 | 809.24 | 1280.50 | 934.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 475.64 | 43.64 | 1280.50 | 573.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 475.00 | 262.09 | 101.00 | 1106.10 | 0.0 | -13.88 | 101.00 | 1100.75 |
| 474.22 | 810.89 | 1358.66 | 1232.17 | 0.0 | -35.02 | 0.0 | 0.0 |
| 474.00 | 492.04 | 1280.50 | 1014.24 | 0.0 | -41.93 | 1280.50 | 1008.97 |
| 472.83 | 1005.38 | 101.00 | 918.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 471.46 | 809.28 | 1280.50 | 911.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 471.34 | 43.43 | 2852.50 | 1455.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 471.23 | 42.62 | 1280.50 | 551.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 470.94 | 44.00 | 1280.50 | 1456.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 470.03 | 39.89 | 2852.50 | 545.50 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | M Sismica x g | Pos. GX | Pos. GY | E agg. X-X | E agg. Y-Y | Pos. KX | Pos. KY |
|--------|---------------|---------|---------|------------|------------|---------|---------|
| 467.85 | 1002.88 | 101.00 | 893.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 467.07 | 955.50 | 101.00 | 1284.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 466.89 | 800.59 | 1280.50 | 888.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 466.63 | 41.48 | 1280.50 | 528.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 465.53 | 40.22 | 2852.50 | 523.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 464.48 | 900.08 | 1280.50 | 1290.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 462.88 | 1000.38 | 101.00 | 868.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 462.30 | 853.21 | 1377.04 | 902.76 | 0.0 | -30.62 | 0.0 | 0.0 |
| 462.09 | 79.76 | 1280.50 | 997.53 | 0.0 | -48.60 | 0.0 | 0.0 |
| 460.73 | 52.38 | 2852.50 | 499.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 458.00 | 890.72 | 2852.50 | 993.40 | 0.0 | -46.60 | 2852.50 | 989.00 |
| 457.90 | 1843.37 | 101.00 | 1055.89 | 0.0 | -23.20 | 0.0 | 0.0 |
| 457.73 | 800.67 | 1280.50 | 842.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 457.63 | 37.71 | 1280.50 | 483.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 455.93 | 49.30 | 2852.50 | 475.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 454.26 | 932.03 | 1280.50 | 1315.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 453.25 | 92.84 | 2077.12 | 1500.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 453.12 | 865.03 | 1280.50 | 800.76 | 0.0 | -17.91 | 0.0 | 0.0 |
| 452.93 | 1008.16 | 101.00 | 818.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 452.00 | 595.94 | 1280.50 | 985.10 | 0.0 | -49.73 | 1280.50 | 975.64 |
| 451.12 | 46.99 | 2852.50 | 451.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 451.00 | 439.27 | 101.00 | 1076.91 | 0.0 | -23.20 | 101.00 | 1075.00 |
| 450.72 | 746.37 | 101.00 | 1324.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 448.62 | 42.42 | 1280.50 | 438.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 448.45 | 838.40 | 1280.50 | 795.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 447.95 | 1004.94 | 101.00 | 793.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 446.32 | 44.67 | 2852.50 | 427.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 444.40 | 43.08 | 1280.50 | 1522.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 444.20 | 42.62 | 2852.50 | 1522.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 444.12 | 40.83 | 1280.50 | 416.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 444.04 | 921.30 | 1280.50 | 1340.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 443.67 | 800.51 | 1280.50 | 771.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 443.57 | 849.33 | 101.00 | 1342.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 442.97 | 1002.44 | 101.00 | 768.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 441.52 | 41.96 | 2852.50 | 403.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 439.62 | 38.88 | 1280.50 | 393.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 439.29 | 765.99 | 1280.50 | 749.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 438.00 | 999.93 | 101.00 | 743.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 436.96 | 16.83 | 3103.00 | 1540.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 436.72 | 52.95 | 2852.50 | 379.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 435.35 | 40.42 | 1280.50 | 1544.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 435.12 | 97.35 | 2107.67 | 988.75 | 0.0 | -58.70 | 0.0 | 0.0 |
| 434.91 | 765.90 | 1280.50 | 727.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 434.37 | 951.53 | 101.00 | 1364.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 433.82 | 941.54 | 1280.50 | 1366.09 | 0.0 | -1.25 | 0.0 | 0.0 |
| 433.02 | 2121.49 | 1559.11 | 849.97 | 0.0 | -55.98 | 0.0 | 0.0 |
| 431.91 | 49.78 | 2852.50 | 355.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 430.61 | 43.83 | 1280.50 | 348.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 430.53 | 774.21 | 1280.50 | 705.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 430.00 | 713.43 | 1280.50 | 967.92 | 0.0 | -57.55 | 1280.50 | 955.10 |
| 428.05 | 1007.62 | 101.00 | 693.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 427.11 | 47.46 | 2852.50 | 331.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 427.00 | 614.79 | 101.00 | 1045.00 | 0.0 | -32.33 | 101.00 | 1041.25 |
| 426.30 | 46.67 | 1280.50 | 1567.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 426.11 | 876.93 | 1408.42 | 734.37 | 0.0 | -62.08 | 0.0 | 0.0 |
| 425.18 | 958.96 | 101.00 | 1387.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 423.60 | 852.72 | 1280.50 | 1390.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 423.07 | 1004.49 | 101.00 | 668.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 422.31 | 52.62 | 2888.07 | 307.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 421.78 | 765.99 | 1280.50 | 661.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 421.61 | 42.01 | 1280.50 | 303.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 418.09 | 1001.99 | 101.00 | 643.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 417.51 | 53.66 | 2903.08 | 283.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 417.40 | 765.99 | 1280.50 | 639.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 417.25 | 42.34 | 1280.50 | 1589.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 417.11 | 39.54 | 1280.50 | 281.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 417.05 | 51.08 | 2897.95 | 1590.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 415.98 | 953.64 | 101.00 | 1409.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 414.96 | 794.98 | 1280.50 | 1412.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 413.12 | 999.49 | 101.00 | 618.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 413.02 | 765.89 | 1280.50 | 617.50 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | M Sismica x g | Pos. GX | Pos. GY | E agg. X-X | E agg. Y-Y | Pos. KX | Pos. KY |
|--------|---------------|---------|---------|------------|------------|---------|---------|
| 412.70 | 45.12 | 2880.89 | 259.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 412.60 | 51.55 | 1280.50 | 258.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 408.64 | 775.93 | 1280.50 | 595.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 408.14 | 996.87 | 101.00 | 593.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 408.00 | 3.405e+04 | 2202.46 | 786.61 | 0.0 | -68.85 | 2554.91 | 924.22 |
| 406.79 | 962.02 | 101.00 | 1432.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 405.97 | 821.74 | 1280.50 | 1434.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 404.26 | 767.69 | 1280.50 | 573.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 403.17 | 1007.09 | 101.00 | 568.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 403.00 | 781.30 | 101.00 | 1008.47 | 0.0 | -40.83 | 101.00 | 1001.25 |
| 399.88 | 785.16 | 1280.50 | 551.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 398.19 | 1064.22 | 101.00 | 543.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 397.59 | 956.64 | 101.00 | 1454.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 396.98 | 812.61 | 1280.50 | 1456.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 395.30 | 793.89 | 1280.50 | 528.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 392.62 | 1061.41 | 101.00 | 515.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 390.83 | 785.16 | 1280.50 | 506.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 388.39 | 952.30 | 101.00 | 1477.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 387.98 | 812.84 | 1280.50 | 1478.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 387.64 | 998.75 | 101.00 | 490.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 386.35 | 785.05 | 1280.50 | 483.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 382.67 | 996.26 | 101.00 | 465.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 381.87 | 794.99 | 1280.50 | 461.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 381.00 | 7050.80 | 2265.21 | 925.46 | 0.0 | -68.85 | 2546.65 | 924.19 |
| 379.20 | 960.06 | 101.00 | 1499.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 379.00 | 1788.04 | 643.98 | 1218.97 | 0.0 | -51.75 | 101.00 | 971.00 |
| 377.69 | 1006.19 | 101.00 | 440.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 377.39 | 784.80 | 1280.50 | 438.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 376.00 | 78.90 | 2852.50 | 909.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 372.91 | 784.81 | 1280.50 | 416.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 372.71 | 1003.31 | 101.00 | 415.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 371.15 | 81.23 | 2852.50 | 959.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 370.99 | 81.51 | 2852.50 | 884.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 370.00 | 4593.13 | 677.99 | 1522.00 | 0.0 | 0.0 | 640.25 | 1522.00 |
| 368.43 | 784.81 | 1280.50 | 393.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 367.74 | 1000.81 | 101.00 | 390.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 365.99 | 84.03 | 2852.50 | 859.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 363.96 | 784.81 | 1280.50 | 371.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 362.76 | 898.59 | 101.00 | 365.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 361.90 | 83.20 | 2852.50 | 982.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 360.99 | 86.54 | 2852.50 | 834.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 360.87 | 1.266e+04 | 2191.75 | 0.0 | 0.0 | 0.0 | 2191.58 | 0.0 |
| 359.48 | 784.75 | 1280.50 | 348.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 358.78 | 777.08 | 101.00 | 345.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 355.99 | 89.06 | 2852.50 | 809.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 355.00 | 1.283e+04 | 1372.08 | 754.21 | 0.0 | -68.85 | 2329.56 | 947.86 |
| 352.65 | 88.60 | 2852.50 | 1005.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 350.98 | 92.51 | 2852.50 | 784.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 345.98 | 80.58 | 2852.50 | 759.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 343.40 | 79.38 | 2852.50 | 1028.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 340.98 | 94.42 | 2852.50 | 734.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 336.78 | 71.94 | 2852.50 | 713.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 334.14 | 84.79 | 2852.50 | 1051.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 333.00 | 8853.99 | 1554.95 | 926.52 | 0.0 | -68.85 | 2269.38 | 947.87 |
| 332.57 | 74.12 | 2852.50 | 692.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 328.37 | 66.10 | 2852.50 | 671.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 324.89 | 78.03 | 2852.50 | 1074.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 324.17 | 67.98 | 2852.50 | 650.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 319.97 | 69.75 | 2852.50 | 629.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 316.00 | 2765.00 | 2191.62 | 0.0 | 0.0 | 0.0 | 2191.70 | 0.0 |
| 315.76 | 71.52 | 2852.50 | 608.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 315.64 | 82.40 | 2852.50 | 1097.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 311.56 | 73.62 | 2852.50 | 587.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 311.00 | 8702.14 | 1532.31 | 928.73 | 0.0 | -68.85 | 1921.93 | 947.88 |
| 307.36 | 65.75 | 2852.50 | 566.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 306.39 | 88.01 | 2852.50 | 1120.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 303.16 | 70.00 | 2852.50 | 545.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 298.66 | 44.03 | 2852.50 | 523.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 297.14 | 45.07 | 2852.50 | 1143.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 289.00 | 8576.77 | 1528.44 | 932.44 | 0.0 | -68.85 | 1957.81 | 947.90 |
| 267.00 | 7305.10 | 1549.29 | 948.82 | 0.0 | -68.85 | 2272.93 | 957.53 |

| Quota | M Sismica x g | Pos. GX | Pos. GY | E agg. X-X | E agg. Y-Y | Pos. KX | Pos. KY |
|---------|---------------|---------|---------|------------|------------|---------|---------|
| 244.00 | 5731.32 | 1599.36 | 943.06 | 0.0 | -68.85 | 2273.25 | 957.49 |
| 220.00 | 5853.26 | 1599.36 | 943.06 | 0.0 | -68.85 | 2273.25 | 957.49 |
| 196.00 | 5853.26 | 1599.36 | 943.06 | 0.0 | -68.85 | 2273.25 | 957.49 |
| 172.00 | 5510.21 | 1573.32 | 939.97 | 0.0 | -68.85 | 2255.19 | 954.31 |
| 152.00 | 5167.15 | 1543.81 | 936.46 | 0.0 | -68.85 | 2255.19 | 954.31 |
| 132.00 | 5167.15 | 1543.81 | 936.46 | 0.0 | -68.85 | 2255.19 | 954.31 |
| 112.00 | 5167.15 | 1543.81 | 936.46 | 0.0 | -68.85 | 2255.19 | 954.31 |
| 92.00 | 5970.76 | 1548.60 | 981.05 | 0.0 | -68.85 | 2254.72 | 1011.72 |
| 69.00 | 6774.37 | 1552.25 | 1015.06 | 0.0 | -68.85 | 2254.72 | 1011.72 |
| 46.00 | 6774.37 | 1552.25 | 1015.06 | 0.0 | -68.85 | 2254.72 | 1011.72 |
| 23.00 | 6774.37 | 1552.26 | 1015.06 | 0.0 | -68.85 | 2254.72 | 1011.72 |
| 0.0 | 2.150e+04 | 1667.13 | 781.77 | 0.0 | -80.62 | 1900.03 | 923.97 |
| Risulta | 3.177e+05 | | | | | | |

• **Caso di carico sisma x-x ecc+– SLV**

| CDC | Tipo | Sigla Id | Note |
|-----|------|---|--|
| 9 | Edk | CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +) | |
| | | | categoria suolo: B |
| | | | fattore di sito S = 1.200 |
| | | | ordinata spettro (tratto Tb-Tc) = 0.304 g |
| | | | angolo di ingresso:0.0 |
| | | | eccentricità aggiuntiva: positiva |
| | | | periodo proprio T1: 0.055 sec. |
| | | | fattore q: 1.500 |
| | | | amplificazione ND (non dissipativi): 1.000 |
| | | | fattore per spost. mu d: 3.500 |
| | | | classe di duttilità CD: ND |
| | | | numero di modi considerati:100 |
| | | | combinaz. modale: CQC |

Analisi dinamica e spettro di risposta SLV ecc+

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|------|-----------|---------|----------------|------------------|----------|------------------|----------|------------------|----------|
| | Hz | sec | g | daN | | daN | | daN | |
| 1 | 7.651 | 0.131 | 0.301 | 1.757e+04 | 5.5 | 18.14 | 5.71e-03 | 100.30 | 3.16e-02 |
| 2 | 8.344 | 0.120 | 0.291 | 1.195e+04 | 3.8 | 0.29 | 9.23e-05 | 509.24 | 0.2 |
| 3 | 9.116 | 0.110 | 0.282 | 2.196e+04 | 6.9 | 11.82 | 3.72e-03 | 0.63 | 1.99e-04 |
| 4 | 11.020 | 0.091 | 0.265 | 1222.37 | 0.4 | 1.083e+04 | 3.4 | 500.78 | 0.2 |
| 5 | 11.340 | 0.088 | 0.262 | 122.57 | 3.86e-02 | 1.182e+05 | 37.2 | 154.57 | 4.86e-02 |
| 6 | 11.807 | 0.085 | 0.259 | 3292.50 | 1.0 | 814.84 | 0.3 | 456.60 | 0.1 |
| 7 | 12.623 | 0.079 | 0.254 | 2.861e+04 | 9.0 | 11.67 | 3.67e-03 | 10.36 | 3.26e-03 |
| 8 | 13.434 | 0.074 | 0.250 | 643.49 | 0.2 | 2.699e+04 | 8.5 | 46.15 | 1.45e-02 |
| 9 | 13.983 | 0.072 | 0.247 | 3.545e+04 | 11.2 | 804.83 | 0.3 | 3.08 | 9.70e-04 |
| 10 | 14.774 | 0.068 | 0.244 | 96.86 | 3.05e-02 | 4.307e+04 | 13.6 | 34.62 | 1.09e-02 |
| 11 | 16.418 | 0.061 | 0.237 | 326.65 | 0.1 | 1.348e+04 | 4.2 | 10.60 | 3.34e-03 |
| 12 | 16.663 | 0.060 | 0.237 | 8263.59 | 2.6 | 271.01 | 8.53e-02 | 3.07 | 9.65e-04 |
| 13 | 17.095 | 0.058 | 0.235 | 50.15 | 1.58e-02 | 3998.78 | 1.3 | 13.78 | 4.34e-03 |
| 14 | 17.336 | 0.058 | 0.234 | 4346.96 | 1.4 | 5939.18 | 1.9 | 5.06 | 1.59e-03 |
| 15 | 17.515 | 0.057 | 0.234 | 403.22 | 0.1 | 5608.19 | 1.8 | 6.54 | 2.06e-03 |
| 16 | 18.016 | 0.056 | 0.232 | 348.38 | 0.1 | 1.787e+04 | 5.6 | 0.07 | 2.23e-05 |
| 17 | 18.283 | 0.055 | 0.232 | 4.182e+04 | 13.2 | 131.44 | 4.14e-02 | 13.57 | 4.27e-03 |
| 18 | 18.486 | 0.054 | 0.231 | 414.88 | 0.1 | 5825.20 | 1.8 | 14.51 | 4.57e-03 |
| 19 | 19.064 | 0.052 | 0.230 | 4165.79 | 1.3 | 88.66 | 2.79e-02 | 6.52 | 2.05e-03 |
| 20 | 19.108 | 0.052 | 0.229 | 6912.37 | 2.2 | 1258.77 | 0.4 | 281.44 | 8.86e-02 |
| 21 | 20.176 | 0.050 | 0.227 | 164.76 | 5.18e-02 | 1585.86 | 0.5 | 14.27 | 4.49e-03 |
| 22 | 20.391 | 0.049 | 0.226 | 793.49 | 0.2 | 1565.44 | 0.5 | 1.39 | 4.38e-04 |
| 23 | 20.608 | 0.049 | 0.226 | 34.17 | 1.08e-02 | 1437.37 | 0.5 | 19.11 | 6.01e-03 |
| 24 | 20.995 | 0.048 | 0.225 | 920.03 | 0.3 | 1252.59 | 0.4 | 67.76 | 2.13e-02 |
| 25 | 21.000 | 0.048 | 0.225 | 3926.51 | 1.2 | 2297.39 | 0.7 | 0.40 | 1.26e-04 |
| 26 | 21.736 | 0.046 | 0.224 | 2762.90 | 0.9 | 63.87 | 2.01e-02 | 33.23 | 1.05e-02 |
| 27 | 22.060 | 0.045 | 0.223 | 2466.57 | 0.8 | 196.44 | 6.18e-02 | 42.61 | 1.34e-02 |
| 28 | 22.190 | 0.045 | 0.223 | 753.45 | 0.2 | 1466.64 | 0.5 | 4.60 | 1.45e-03 |
| 29 | 23.518 | 0.043 | 0.221 | 7.62 | 2.40e-03 | 13.78 | 4.34e-03 | 1.70 | 5.36e-04 |
| 30 | 23.769 | 0.042 | 0.220 | 212.67 | 6.69e-02 | 119.06 | 3.75e-02 | 8.90 | 2.80e-03 |
| 31 | 23.901 | 0.042 | 0.220 | 91.96 | 2.89e-02 | 0.40 | 1.25e-04 | 0.68 | 2.13e-04 |
| 32 | 24.054 | 0.042 | 0.220 | 3474.41 | 1.1 | 29.74 | 9.36e-03 | 301.58 | 9.49e-02 |
| 33 | 24.685 | 0.041 | 0.219 | 1296.68 | 0.4 | 87.53 | 2.75e-02 | 63.80 | 2.01e-02 |
| 34 | 24.873 | 0.040 | 0.218 | 547.32 | 0.2 | 308.25 | 9.70e-02 | 6.03 | 1.90e-03 |

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|----------------|-----------|---------|----------------|------------------|----------|------------------|----------|------------------|----------|
| 35 | 25.320 | 0.039 | 0.218 | 16.28 | 5.12e-03 | 1399.45 | 0.4 | 470.80 | 0.1 |
| 36 | 26.198 | 0.038 | 0.217 | 758.52 | 0.2 | 2012.67 | 0.6 | 806.45 | 0.3 |
| 37 | 26.393 | 0.038 | 0.216 | 114.53 | 3.60e-02 | 145.64 | 4.58e-02 | 140.05 | 4.41e-02 |
| 38 | 26.734 | 0.037 | 0.216 | 156.72 | 4.93e-02 | 39.65 | 1.25e-02 | 2.55 | 8.04e-04 |
| 39 | 27.595 | 0.036 | 0.215 | 3010.38 | 0.9 | 394.62 | 0.1 | 5.13 | 1.62e-03 |
| 40 | 27.993 | 0.036 | 0.214 | 334.10 | 0.1 | 21.69 | 6.83e-03 | 3.68 | 1.16e-03 |
| 41 | 28.610 | 0.035 | 0.214 | 3.06 | 9.63e-04 | 76.18 | 2.40e-02 | 129.47 | 4.07e-02 |
| 42 | 28.653 | 0.035 | 0.214 | 60.61 | 1.91e-02 | 70.41 | 2.22e-02 | 598.36 | 0.2 |
| 43 | 28.848 | 0.035 | 0.213 | 2.784e+04 | 8.8 | 65.92 | 2.07e-02 | 667.89 | 0.2 |
| 44 | 29.399 | 0.034 | 0.213 | 1034.95 | 0.3 | 81.11 | 2.55e-02 | 24.40 | 7.68e-03 |
| 45 | 29.952 | 0.033 | 0.212 | 898.65 | 0.3 | 13.66 | 4.30e-03 | 21.89 | 6.89e-03 |
| 46 | 30.151 | 0.033 | 0.212 | 58.17 | 1.83e-02 | 383.61 | 0.1 | 1.19e-05 | 0.0 |
| 47 | 30.254 | 0.033 | 0.212 | 825.81 | 0.3 | 8.18 | 2.57e-03 | 6.77 | 2.13e-03 |
| 48 | 30.762 | 0.033 | 0.211 | 1.89 | 5.96e-04 | 184.16 | 5.80e-02 | 1.885e+04 | 5.9 |
| 49 | 31.190 | 0.032 | 0.211 | 0.03 | 9.14e-06 | 17.08 | 5.37e-03 | 233.52 | 7.35e-02 |
| 50 | 31.598 | 0.032 | 0.211 | 562.44 | 0.2 | 1292.02 | 0.4 | 1.322e+04 | 4.2 |
| 51 | 32.437 | 0.031 | 0.210 | 125.37 | 3.95e-02 | 1810.29 | 0.6 | 1.418e+04 | 4.5 |
| 52 | 33.084 | 0.030 | 0.209 | 99.12 | 3.12e-02 | 99.68 | 3.14e-02 | 1501.88 | 0.5 |
| 53 | 33.579 | 0.030 | 0.209 | 108.51 | 3.41e-02 | 1038.23 | 0.3 | 7566.20 | 2.4 |
| 54 | 34.223 | 0.029 | 0.208 | 1045.68 | 0.3 | 0.20 | 6.40e-05 | 998.98 | 0.3 |
| 55 | 34.825 | 0.029 | 0.208 | 146.12 | 4.60e-02 | 1258.56 | 0.4 | 1936.99 | 0.6 |
| 56 | 35.668 | 0.028 | 0.207 | 150.48 | 4.74e-02 | 1.11 | 3.48e-04 | 26.84 | 8.45e-03 |
| 57 | 36.041 | 0.028 | 0.207 | 289.10 | 9.10e-02 | 16.30 | 5.13e-03 | 72.87 | 2.29e-02 |
| 58 | 36.608 | 0.027 | 0.207 | 7448.87 | 2.3 | 3.25 | 1.02e-03 | 1738.17 | 0.5 |
| 59 | 36.878 | 0.027 | 0.206 | 549.00 | 0.2 | 360.83 | 0.1 | 6135.34 | 1.9 |
| 60 | 37.173 | 0.027 | 0.206 | 35.85 | 1.13e-02 | 1565.05 | 0.5 | 860.65 | 0.3 |
| 61 | 37.453 | 0.027 | 0.206 | 1377.74 | 0.4 | 1.94 | 6.11e-04 | 324.86 | 0.1 |
| 62 | 38.187 | 0.026 | 0.206 | 1.322e+04 | 4.2 | 7.28 | 2.29e-03 | 2401.22 | 0.8 |
| 63 | 38.262 | 0.026 | 0.205 | 42.73 | 1.34e-02 | 147.07 | 4.63e-02 | 0.19 | 6.07e-05 |
| 64 | 38.627 | 0.026 | 0.205 | 12.67 | 3.99e-03 | 15.17 | 4.77e-03 | 534.31 | 0.2 |
| 65 | 38.794 | 0.026 | 0.205 | 1.05 | 3.31e-04 | 231.72 | 7.29e-02 | 309.08 | 9.73e-02 |
| 66 | 39.029 | 0.026 | 0.205 | 1124.05 | 0.4 | 15.09 | 4.75e-03 | 757.13 | 0.2 |
| 67 | 39.447 | 0.025 | 0.205 | 80.31 | 2.53e-02 | 166.52 | 5.24e-02 | 4.103e+04 | 12.9 |
| 68 | 39.491 | 0.025 | 0.205 | 10.34 | 3.25e-03 | 14.58 | 4.59e-03 | 1206.85 | 0.4 |
| 69 | 39.745 | 0.025 | 0.205 | 1109.58 | 0.3 | 67.77 | 2.13e-02 | 693.74 | 0.2 |
| 70 | 39.865 | 0.025 | 0.205 | 2007.58 | 0.6 | 1.42 | 4.48e-04 | 9024.82 | 2.8 |
| 71 | 39.969 | 0.025 | 0.204 | 10.72 | 3.37e-03 | 633.06 | 0.2 | 2421.48 | 0.8 |
| 72 | 40.374 | 0.025 | 0.204 | 162.35 | 5.11e-02 | 692.82 | 0.2 | 140.28 | 4.41e-02 |
| 73 | 40.917 | 0.024 | 0.204 | 21.44 | 6.75e-03 | 1.83 | 5.75e-04 | 1214.40 | 0.4 |
| 74 | 41.602 | 0.024 | 0.204 | 0.02 | 5.54e-06 | 258.42 | 8.13e-02 | 842.16 | 0.3 |
| 75 | 41.861 | 0.024 | 0.203 | 811.94 | 0.3 | 20.88 | 6.57e-03 | 1506.61 | 0.5 |
| 76 | 42.459 | 0.024 | 0.203 | 0.64 | 2.01e-04 | 13.55 | 4.27e-03 | 16.30 | 5.13e-03 |
| 77 | 42.687 | 0.023 | 0.203 | 493.10 | 0.2 | 165.90 | 5.22e-02 | 4417.68 | 1.4 |
| 78 | 42.801 | 0.023 | 0.203 | 816.69 | 0.3 | 381.79 | 0.1 | 9736.04 | 3.1 |
| 79 | 42.865 | 0.023 | 0.203 | 4.20 | 1.32e-03 | 5.40e-04 | 0.0 | 75.37 | 2.37e-02 |
| 80 | 43.319 | 0.023 | 0.203 | 26.36 | 8.29e-03 | 270.20 | 8.50e-02 | 6214.05 | 2.0 |
| 81 | 44.061 | 0.023 | 0.202 | 225.08 | 7.08e-02 | 46.99 | 1.48e-02 | 4607.28 | 1.4 |
| 82 | 44.279 | 0.023 | 0.202 | 124.28 | 3.91e-02 | 9.19 | 2.89e-03 | 267.84 | 8.43e-02 |
| 83 | 44.394 | 0.023 | 0.202 | 2.39 | 7.51e-04 | 656.26 | 0.2 | 0.15 | 4.85e-05 |
| 84 | 44.703 | 0.022 | 0.202 | 69.26 | 2.18e-02 | 108.08 | 3.40e-02 | 357.81 | 0.1 |
| 85 | 44.910 | 0.022 | 0.202 | 7.06 | 2.22e-03 | 3.78 | 1.19e-03 | 158.45 | 4.99e-02 |
| 86 | 45.247 | 0.022 | 0.202 | 9.41 | 2.96e-03 | 89.55 | 2.82e-02 | 3.88 | 1.22e-03 |
| 87 | 45.419 | 0.022 | 0.202 | 43.23 | 1.36e-02 | 236.06 | 7.43e-02 | 2947.57 | 0.9 |
| 88 | 46.181 | 0.022 | 0.201 | 9.27 | 2.92e-03 | 300.76 | 9.47e-02 | 60.91 | 1.92e-02 |
| 89 | 46.323 | 0.022 | 0.201 | 30.58 | 9.62e-03 | 822.95 | 0.3 | 68.17 | 2.15e-02 |
| 90 | 46.533 | 0.021 | 0.201 | 165.55 | 5.21e-02 | 12.88 | 4.05e-03 | 54.62 | 1.72e-02 |
| 91 | 47.453 | 0.021 | 0.201 | 0.55 | 1.74e-04 | 61.06 | 1.92e-02 | 40.11 | 1.26e-02 |
| 92 | 47.783 | 0.021 | 0.201 | 479.08 | 0.2 | 300.68 | 9.46e-02 | 5.50 | 1.73e-03 |
| 93 | 48.095 | 0.021 | 0.201 | 95.67 | 3.01e-02 | 74.18 | 2.33e-02 | 174.43 | 5.49e-02 |
| 94 | 48.416 | 0.021 | 0.200 | 144.51 | 4.55e-02 | 152.09 | 4.79e-02 | 1180.96 | 0.4 |
| 95 | 48.474 | 0.021 | 0.200 | 10.00 | 3.15e-03 | 1.06 | 3.33e-04 | 80.43 | 2.53e-02 |
| 96 | 49.030 | 0.020 | 0.200 | 55.39 | 1.74e-02 | 27.72 | 8.73e-03 | 132.09 | 4.16e-02 |
| 97 | 49.470 | 0.020 | 0.200 | 846.19 | 0.3 | 1.91 | 6.03e-04 | 203.05 | 6.39e-02 |
| 98 | 49.830 | 0.020 | 0.200 | 123.09 | 3.87e-02 | 1.57e-03 | 0.0 | 413.92 | 0.1 |
| 99 | 50.825 | 0.020 | 0.200 | 55.46 | 1.75e-02 | 1.10 | 3.48e-04 | 1167.30 | 0.4 |
| 100 | 51.012 | 0.020 | 0.200 | 11.56 | 3.64e-03 | 0.58 | 1.83e-04 | 345.82 | 0.1 |
| Risulta | | | | 2.749e+05 | | 2.840e+05 | | 1.681e+05 | |
| In percentuale | | | | 86.52 | | 89.38 | | 52.90 | |

• **Caso di carico sisma x-x ecc⁻ SLV**

| CDC | Tipo | Sigla Id | Note |
|-----|------|---|--|
| 10 | Edk | CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -) | |
| | | | categoria suolo: B |
| | | | fattore di sito S = 1.200 |
| | | | ordinata spettro (tratto Tb-Tc) = 0.304 g |
| | | | angolo di ingresso:0.0 |
| | | | eccentricità aggiuntiva: negativa |
| | | | periodo proprio T1: 0.072 sec. |
| | | | fattore q: 1.500 |
| | | | amplificazione ND (non dissipativi): 1.000 |
| | | | fattore per spost. mu d: 3.500 |
| | | | classe di duttilità CD: ND |
| | | | numero di modi considerati:100 |
| | | | combinaz. modale: CQC |

Analisi dinamica e spettro di risposta SLV ecc⁻

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X | % | M efficace Y | % | M efficace Z | % |
|------|-----------|---------|----------------|--------------|----------|--------------|----------|--------------|----------|
| | Hz | sec | g | x g | | x g | | x g | |
| | | | | daN | | daN | | daN | |
| 1 | 7.627 | 0.131 | 0.302 | 1.599e+04 | 5.0 | 12.39 | 3.90e-03 | 132.01 | 4.15e-02 |
| 2 | 8.369 | 0.119 | 0.291 | 1.408e+04 | 4.4 | 0.23 | 7.29e-05 | 467.33 | 0.1 |
| 3 | 9.121 | 0.110 | 0.282 | 2.123e+04 | 6.7 | 12.05 | 3.79e-03 | 0.59 | 1.85e-04 |
| 4 | 10.971 | 0.091 | 0.265 | 972.82 | 0.3 | 9176.71 | 2.9 | 402.71 | 0.1 |
| 5 | 11.339 | 0.088 | 0.262 | 14.75 | 4.64e-03 | 1.182e+05 | 37.2 | 163.02 | 5.13e-02 |
| 6 | 11.561 | 0.087 | 0.261 | 2872.60 | 0.9 | 2414.60 | 0.8 | 522.13 | 0.2 |
| 7 | 12.496 | 0.080 | 0.255 | 2.657e+04 | 8.4 | 18.72 | 5.89e-03 | 8.28 | 2.60e-03 |
| 8 | 13.433 | 0.074 | 0.250 | 852.80 | 0.3 | 2.698e+04 | 8.5 | 45.70 | 1.44e-02 |
| 9 | 13.926 | 0.072 | 0.247 | 3.723e+04 | 11.7 | 835.50 | 0.3 | 7.56 | 2.38e-03 |
| 10 | 14.775 | 0.068 | 0.244 | 25.45 | 8.01e-03 | 4.314e+04 | 13.6 | 35.32 | 1.11e-02 |
| 11 | 16.426 | 0.061 | 0.237 | 7.82 | 2.46e-03 | 1.368e+04 | 4.3 | 9.37 | 2.95e-03 |
| 12 | 16.687 | 0.060 | 0.236 | 7678.83 | 2.4 | 5.44 | 1.71e-03 | 1.02 | 3.22e-04 |
| 13 | 17.108 | 0.058 | 0.235 | 97.73 | 3.08e-02 | 4578.41 | 1.4 | 14.95 | 4.71e-03 |
| 14 | 17.398 | 0.057 | 0.234 | 1630.35 | 0.5 | 8576.65 | 2.7 | 2.36 | 7.44e-04 |
| 15 | 17.573 | 0.057 | 0.234 | 891.72 | 0.3 | 1991.90 | 0.6 | 9.12 | 2.87e-03 |
| 16 | 18.038 | 0.055 | 0.232 | 247.92 | 7.80e-02 | 1.824e+04 | 5.7 | 4.64 | 1.46e-03 |
| 17 | 18.092 | 0.055 | 0.232 | 2.040e+04 | 6.4 | 140.84 | 4.43e-02 | 59.49 | 1.87e-02 |
| 18 | 18.489 | 0.054 | 0.231 | 188.90 | 5.94e-02 | 6581.91 | 2.1 | 15.54 | 4.89e-03 |
| 19 | 18.853 | 0.053 | 0.230 | 2.003e+04 | 6.3 | 30.77 | 9.68e-03 | 11.30 | 3.56e-03 |
| 20 | 19.269 | 0.052 | 0.229 | 1.382e+04 | 4.3 | 389.02 | 0.1 | 306.48 | 9.65e-02 |
| 21 | 20.190 | 0.050 | 0.227 | 492.51 | 0.2 | 1297.23 | 0.4 | 4.88 | 1.53e-03 |
| 22 | 20.385 | 0.049 | 0.226 | 1198.49 | 0.4 | 1983.13 | 0.6 | 2.56 | 8.07e-04 |
| 23 | 20.607 | 0.049 | 0.226 | 35.07 | 1.10e-02 | 1585.66 | 0.5 | 13.92 | 4.38e-03 |
| 24 | 20.943 | 0.048 | 0.225 | 6197.31 | 2.0 | 3168.70 | 1.0 | 16.47 | 5.18e-03 |
| 25 | 21.163 | 0.047 | 0.225 | 254.33 | 8.00e-02 | 291.63 | 9.18e-02 | 20.44 | 6.43e-03 |
| 26 | 21.676 | 0.046 | 0.224 | 500.70 | 0.2 | 43.55 | 1.37e-02 | 10.11 | 3.18e-03 |
| 27 | 21.968 | 0.046 | 0.223 | 4488.16 | 1.4 | 30.13 | 9.48e-03 | 34.22 | 1.08e-02 |
| 28 | 22.182 | 0.045 | 0.223 | 271.24 | 8.54e-02 | 1608.31 | 0.5 | 18.61 | 5.86e-03 |
| 29 | 23.516 | 0.043 | 0.221 | 0.51 | 1.60e-04 | 10.54 | 3.32e-03 | 1.65 | 5.20e-04 |
| 30 | 23.694 | 0.042 | 0.220 | 122.65 | 3.86e-02 | 102.54 | 3.23e-02 | 0.94 | 2.94e-04 |
| 31 | 23.905 | 0.042 | 0.220 | 0.90 | 2.84e-04 | 8.87 | 2.79e-03 | 5.17 | 1.63e-03 |
| 32 | 24.741 | 0.040 | 0.219 | 427.35 | 0.1 | 317.06 | 9.98e-02 | 10.46 | 3.29e-03 |
| 33 | 24.859 | 0.040 | 0.218 | 135.38 | 4.26e-02 | 206.59 | 6.50e-02 | 0.98 | 3.07e-04 |
| 34 | 25.284 | 0.040 | 0.218 | 482.51 | 0.2 | 1038.15 | 0.3 | 11.28 | 3.55e-03 |
| 35 | 25.433 | 0.039 | 0.218 | 1207.72 | 0.4 | 280.52 | 8.83e-02 | 1111.43 | 0.3 |
| 36 | 26.202 | 0.038 | 0.217 | 525.59 | 0.2 | 2000.20 | 0.6 | 923.59 | 0.3 |
| 37 | 26.394 | 0.038 | 0.216 | 87.31 | 2.75e-02 | 108.56 | 3.42e-02 | 170.31 | 5.36e-02 |
| 38 | 26.727 | 0.037 | 0.216 | 336.81 | 0.1 | 69.76 | 2.20e-02 | 2.85 | 8.96e-04 |
| 39 | 27.516 | 0.036 | 0.215 | 671.86 | 0.2 | 33.64 | 1.06e-02 | 5.48 | 1.72e-03 |
| 40 | 27.661 | 0.036 | 0.215 | 1130.36 | 0.4 | 442.99 | 0.1 | 3.12 | 9.82e-04 |
| 41 | 28.590 | 0.035 | 0.214 | 54.56 | 1.72e-02 | 58.88 | 1.85e-02 | 281.04 | 8.84e-02 |
| 42 | 28.654 | 0.035 | 0.214 | 132.14 | 4.16e-02 | 76.75 | 2.42e-02 | 569.16 | 0.2 |
| 43 | 28.913 | 0.035 | 0.213 | 12.16 | 3.83e-03 | 1.50 | 4.71e-04 | 17.50 | 5.51e-03 |
| 44 | 29.373 | 0.034 | 0.213 | 102.77 | 3.23e-02 | 110.34 | 3.47e-02 | 4.46 | 1.41e-03 |
| 45 | 30.095 | 0.033 | 0.212 | 16.05 | 5.05e-03 | 333.19 | 0.1 | 6.02 | 1.90e-03 |
| 46 | 30.571 | 0.033 | 0.212 | 8672.95 | 2.7 | 0.03 | 8.23e-06 | 3167.78 | 1.0 |
| 47 | 30.940 | 0.032 | 0.211 | 2324.08 | 0.7 | 428.94 | 0.1 | 2.427e+04 | 7.6 |
| 48 | 31.229 | 0.032 | 0.211 | 1327.61 | 0.4 | 240.66 | 7.57e-02 | 2030.44 | 0.6 |
| 49 | 31.817 | 0.031 | 0.210 | 1.154e+04 | 3.6 | 642.09 | 0.2 | 197.86 | 6.23e-02 |
| 50 | 32.067 | 0.031 | 0.210 | 1.226e+04 | 3.9 | 899.65 | 0.3 | 79.07 | 2.49e-02 |

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|----------------|-----------|---------|----------------|---------------------|----------|---------------------|----------|---------------------|----------|
| 51 | 32.630 | 0.031 | 0.210 | 221.70 | 6.98e-02 | 1156.94 | 0.4 | 1.352e+04 | 4.3 |
| 52 | 32.904 | 0.030 | 0.209 | 636.21 | 0.2 | 6.42e-03 | 2.02e-06 | 378.19 | 0.1 |
| 53 | 33.096 | 0.030 | 0.209 | 5344.24 | 1.7 | 63.40 | 2.00e-02 | 455.67 | 0.1 |
| 54 | 33.229 | 0.030 | 0.209 | 1.627e+04 | 5.1 | 85.92 | 2.70e-02 | 2339.48 | 0.7 |
| 55 | 33.641 | 0.030 | 0.209 | 1909.44 | 0.6 | 892.77 | 0.3 | 1.201e+04 | 3.8 |
| 56 | 34.848 | 0.029 | 0.208 | 207.61 | 6.53e-02 | 1338.04 | 0.4 | 3050.44 | 1.0 |
| 57 | 35.670 | 0.028 | 0.207 | 186.95 | 5.88e-02 | 0.32 | 1.01e-04 | 200.17 | 6.30e-02 |
| 58 | 36.050 | 0.028 | 0.207 | 2.39 | 7.53e-04 | 9.22 | 2.90e-03 | 8.36 | 2.63e-03 |
| 59 | 36.410 | 0.027 | 0.207 | 742.74 | 0.2 | 33.70 | 1.06e-02 | 138.96 | 4.37e-02 |
| 60 | 36.669 | 0.027 | 0.207 | 642.77 | 0.2 | 19.56 | 6.16e-03 | 4617.70 | 1.5 |
| 61 | 37.116 | 0.027 | 0.206 | 0.06 | 1.81e-05 | 1876.42 | 0.6 | 0.11 | 3.37e-05 |
| 62 | 37.648 | 0.027 | 0.206 | 1293.23 | 0.4 | 6.38 | 2.01e-03 | 3.17 | 9.97e-04 |
| 63 | 38.259 | 0.026 | 0.206 | 46.63 | 1.47e-02 | 151.45 | 4.77e-02 | 39.79 | 1.25e-02 |
| 64 | 38.597 | 0.026 | 0.205 | 448.11 | 0.1 | 2.18 | 6.87e-04 | 501.45 | 0.2 |
| 65 | 38.684 | 0.026 | 0.205 | 866.06 | 0.3 | 62.10 | 1.95e-02 | 1175.33 | 0.4 |
| 66 | 38.805 | 0.026 | 0.205 | 13.07 | 4.11e-03 | 179.08 | 5.64e-02 | 0.23 | 7.30e-05 |
| 67 | 38.981 | 0.026 | 0.205 | 52.82 | 1.66e-02 | 33.71 | 1.06e-02 | 1840.80 | 0.6 |
| 68 | 39.476 | 0.025 | 0.205 | 290.88 | 9.15e-02 | 164.70 | 5.18e-02 | 4.894e+04 | 15.4 |
| 69 | 39.934 | 0.025 | 0.204 | 10.16 | 3.20e-03 | 714.18 | 0.2 | 1624.16 | 0.5 |
| 70 | 40.001 | 0.025 | 0.204 | 80.17 | 2.52e-02 | 3.90 | 1.23e-03 | 5620.03 | 1.8 |
| 71 | 40.250 | 0.025 | 0.204 | 209.85 | 6.60e-02 | 496.98 | 0.2 | 707.78 | 0.2 |
| 72 | 40.976 | 0.024 | 0.204 | 892.09 | 0.3 | 539.57 | 0.2 | 1320.47 | 0.4 |
| 73 | 41.584 | 0.024 | 0.204 | 10.98 | 3.46e-03 | 3.43 | 1.08e-03 | 404.19 | 0.1 |
| 74 | 42.403 | 0.024 | 0.203 | 60.90 | 1.92e-02 | 32.17 | 1.01e-02 | 0.12 | 3.88e-05 |
| 75 | 42.633 | 0.023 | 0.203 | 522.12 | 0.2 | 316.34 | 9.96e-02 | 8953.23 | 2.8 |
| 76 | 42.750 | 0.023 | 0.203 | 130.73 | 4.11e-02 | 206.56 | 6.50e-02 | 6756.18 | 2.1 |
| 77 | 42.866 | 0.023 | 0.203 | 0.53 | 1.65e-04 | 2.34 | 7.36e-04 | 7.46 | 2.35e-03 |
| 78 | 43.351 | 0.023 | 0.203 | 121.10 | 3.81e-02 | 219.38 | 6.90e-02 | 7590.36 | 2.4 |
| 79 | 43.984 | 0.023 | 0.202 | 7.21 | 2.27e-03 | 11.68 | 3.68e-03 | 2427.42 | 0.8 |
| 80 | 44.302 | 0.023 | 0.202 | 15.06 | 4.74e-03 | 121.11 | 3.81e-02 | 563.67 | 0.2 |
| 81 | 44.546 | 0.022 | 0.202 | 6.33 | 1.99e-03 | 677.54 | 0.2 | 52.01 | 1.64e-02 |
| 82 | 44.901 | 0.022 | 0.202 | 463.04 | 0.1 | 47.99 | 1.51e-02 | 607.11 | 0.2 |
| 83 | 44.997 | 0.022 | 0.202 | 593.79 | 0.2 | 38.31 | 1.21e-02 | 220.02 | 6.92e-02 |
| 84 | 45.243 | 0.022 | 0.202 | 19.00 | 5.98e-03 | 27.86 | 8.77e-03 | 334.05 | 0.1 |
| 85 | 45.476 | 0.022 | 0.202 | 38.61 | 1.22e-02 | 426.75 | 0.1 | 2085.35 | 0.7 |
| 86 | 45.810 | 0.022 | 0.202 | 5.30 | 1.67e-03 | 20.89 | 6.57e-03 | 10.31 | 3.24e-03 |
| 87 | 45.933 | 0.022 | 0.202 | 14.62 | 4.60e-03 | 22.46 | 7.07e-03 | 78.70 | 2.48e-02 |
| 88 | 46.176 | 0.022 | 0.201 | 100.11 | 3.15e-02 | 355.89 | 0.1 | 144.57 | 4.55e-02 |
| 89 | 46.254 | 0.022 | 0.201 | 1.38 | 4.33e-04 | 10.65 | 3.35e-03 | 4.10 | 1.29e-03 |
| 90 | 46.434 | 0.022 | 0.201 | 1013.16 | 0.3 | 1.22 | 3.83e-04 | 84.11 | 2.65e-02 |
| 91 | 46.534 | 0.021 | 0.201 | 43.38 | 1.37e-02 | 515.62 | 0.2 | 36.54 | 1.15e-02 |
| 92 | 47.562 | 0.021 | 0.201 | 306.18 | 9.64e-02 | 266.87 | 8.40e-02 | 87.01 | 2.74e-02 |
| 93 | 48.047 | 0.021 | 0.201 | 7.16 | 2.25e-03 | 20.31 | 6.39e-03 | 185.18 | 5.83e-02 |
| 94 | 48.175 | 0.021 | 0.201 | 31.24 | 9.83e-03 | 170.29 | 5.36e-02 | 697.62 | 0.2 |
| 95 | 48.268 | 0.021 | 0.201 | 170.04 | 5.35e-02 | 43.33 | 1.36e-02 | 500.63 | 0.2 |
| 96 | 48.388 | 0.021 | 0.200 | 19.87 | 6.25e-03 | 132.80 | 4.18e-02 | 572.50 | 0.2 |
| 97 | 48.523 | 0.021 | 0.200 | 4.92 | 1.55e-03 | 2.19 | 6.90e-04 | 34.80 | 1.10e-02 |
| 98 | 50.927 | 0.020 | 0.200 | 22.78 | 7.17e-03 | 1.42 | 4.47e-04 | 275.83 | 8.68e-02 |
| 99 | 50.995 | 0.020 | 0.200 | 19.36 | 6.09e-03 | 0.10 | 3.19e-05 | 741.76 | 0.2 |
| 100 | 51.061 | 0.020 | 0.199 | 67.51 | 2.12e-02 | 0.89 | 2.80e-04 | 355.80 | 0.1 |
| Risulta | | | | 2.740e+05 | | 2.840e+05 | | 1.675e+05 | |
| In percentuale | | | | 86.24 | | 89.38 | | 52.72 | |

• **Caso di carico sisma y-y ecc+ – SLV**

| CDC | Tipo | Sigla Id | Note |
|-----|------|---|--|
| 11 | Edk | CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +) | |
| | | | categoria suolo: B |
| | | | fattore di sito S = 1.200 |
| | | | ordinata spettro (tratto Tb-Tc) = 0.304 g |
| | | | angolo di ingresso:90.00 |
| | | | eccentricità aggiuntiva: positiva |
| | | | periodo proprio T1: 0.088 sec. |
| | | | fattore q: 1.500 |
| | | | amplificazione ND (non dissipativi): 1.000 |
| | | | fattore per spost. mu d: 3.279 |
| | | | classe di duttilità CD: ND |
| | | | numero di modi considerati:100 |
| | | | combinaz. modale: CQC |

Analisi dinamica e spettro di risposta SLV ecc+

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|------|-----------|---------|----------------|------------------|----------|------------------|----------|------------------|----------|
| | Hz | sec | g | daN | | daN | | daN | |
| 1 | 7.645 | 0.131 | 0.301 | 1.640e+04 | 5.2 | 16.03 | 5.05e-03 | 122.68 | 3.86e-02 |
| 2 | 8.325 | 0.120 | 0.292 | 1.312e+04 | 4.1 | 6.15e-03 | 1.93e-06 | 483.10 | 0.2 |
| 3 | 9.115 | 0.110 | 0.282 | 2.174e+04 | 6.8 | 1.14e-06 | 0.0 | 0.74 | 2.34e-04 |
| 4 | 10.988 | 0.091 | 0.265 | 1127.52 | 0.4 | 1.089e+04 | 3.4 | 428.62 | 0.1 |
| 5 | 11.312 | 0.088 | 0.263 | 58.93 | 1.85e-02 | 1.106e+05 | 34.8 | 179.69 | 5.66e-02 |
| 6 | 11.675 | 0.086 | 0.260 | 2931.39 | 0.9 | 1550.55 | 0.5 | 484.56 | 0.2 |
| 7 | 12.567 | 0.080 | 0.254 | 2.779e+04 | 8.7 | 45.19 | 1.42e-02 | 10.85 | 3.42e-03 |
| 8 | 13.073 | 0.076 | 0.252 | 129.26 | 4.07e-02 | 1.982e+04 | 6.2 | 35.80 | 1.13e-02 |
| 9 | 13.949 | 0.072 | 0.247 | 3.675e+04 | 11.6 | 158.30 | 4.98e-02 | 2.40 | 7.54e-04 |
| 10 | 14.853 | 0.067 | 0.243 | 49.94 | 1.57e-02 | 4.367e+04 | 13.7 | 40.21 | 1.27e-02 |
| 11 | 15.823 | 0.063 | 0.239 | 542.87 | 0.2 | 2.721e+04 | 8.6 | 11.71 | 3.69e-03 |
| 12 | 16.397 | 0.061 | 0.237 | 2948.33 | 0.9 | 24.43 | 7.69e-03 | 2.34 | 7.38e-04 |
| 13 | 16.808 | 0.059 | 0.236 | 4681.53 | 1.5 | 203.09 | 6.39e-02 | 0.59 | 1.87e-04 |
| 14 | 16.900 | 0.059 | 0.236 | 5.37 | 1.69e-03 | 734.83 | 0.2 | 4.45 | 1.40e-03 |
| 15 | 17.286 | 0.058 | 0.235 | 399.91 | 0.1 | 3.061e+04 | 9.6 | 7.55 | 2.38e-03 |
| 16 | 17.496 | 0.057 | 0.234 | 2861.80 | 0.9 | 1562.59 | 0.5 | 13.63 | 4.29e-03 |
| 17 | 18.201 | 0.055 | 0.232 | 3.210e+04 | 10.1 | 23.87 | 7.51e-03 | 32.19 | 1.01e-02 |
| 18 | 18.944 | 0.053 | 0.230 | 1.265e+04 | 4.0 | 101.97 | 3.21e-02 | 17.59 | 5.54e-03 |
| 19 | 19.168 | 0.052 | 0.229 | 8101.58 | 2.5 | 3038.02 | 1.0 | 188.30 | 5.93e-02 |
| 20 | 19.542 | 0.051 | 0.228 | 372.70 | 0.1 | 1950.56 | 0.6 | 54.70 | 1.72e-02 |
| 21 | 19.551 | 0.051 | 0.228 | 2557.71 | 0.8 | 7784.45 | 2.4 | 74.47 | 2.34e-02 |
| 22 | 20.226 | 0.049 | 0.227 | 788.13 | 0.2 | 395.65 | 0.1 | 0.17 | 5.34e-05 |
| 23 | 20.295 | 0.049 | 0.227 | 2405.56 | 0.8 | 1213.25 | 0.4 | 11.12 | 3.50e-03 |
| 24 | 20.943 | 0.048 | 0.225 | 844.99 | 0.3 | 3027.92 | 1.0 | 36.77 | 1.16e-02 |
| 25 | 21.494 | 0.047 | 0.224 | 2985.88 | 0.9 | 52.03 | 1.64e-02 | 21.72 | 6.84e-03 |
| 26 | 21.666 | 0.046 | 0.224 | 522.12 | 0.2 | 69.97 | 2.20e-02 | 24.62 | 7.75e-03 |
| 27 | 21.915 | 0.046 | 0.223 | 1885.88 | 0.6 | 3.23 | 1.01e-03 | 56.66 | 1.78e-02 |
| 28 | 22.153 | 0.045 | 0.223 | 801.45 | 0.3 | 50.02 | 1.57e-02 | 34.38 | 1.08e-02 |
| 29 | 22.726 | 0.044 | 0.222 | 1242.48 | 0.4 | 133.51 | 4.20e-02 | 0.06 | 1.97e-05 |
| 30 | 24.092 | 0.042 | 0.220 | 230.41 | 7.25e-02 | 159.78 | 5.03e-02 | 32.71 | 1.03e-02 |
| 31 | 24.522 | 0.041 | 0.219 | 1820.70 | 0.6 | 31.09 | 9.78e-03 | 0.49 | 1.53e-04 |
| 32 | 24.613 | 0.041 | 0.219 | 609.54 | 0.2 | 2.82 | 8.88e-04 | 50.41 | 1.59e-02 |
| 33 | 24.757 | 0.040 | 0.219 | 915.99 | 0.3 | 23.75 | 7.48e-03 | 402.35 | 0.1 |
| 34 | 25.058 | 0.040 | 0.218 | 485.88 | 0.2 | 385.90 | 0.1 | 172.17 | 5.42e-02 |
| 35 | 25.445 | 0.039 | 0.218 | 6.18 | 1.94e-03 | 1089.99 | 0.3 | 66.94 | 2.11e-02 |
| 36 | 25.635 | 0.039 | 0.217 | 123.38 | 3.88e-02 | 1138.34 | 0.4 | 496.84 | 0.2 |
| 37 | 26.541 | 0.038 | 0.216 | 0.27 | 8.60e-05 | 0.29 | 9.04e-05 | 22.47 | 7.07e-03 |
| 38 | 28.046 | 0.036 | 0.214 | 174.87 | 5.50e-02 | 27.11 | 8.53e-03 | 345.18 | 0.1 |
| 39 | 28.217 | 0.035 | 0.214 | 921.05 | 0.3 | 215.22 | 6.77e-02 | 27.31 | 8.60e-03 |
| 40 | 28.345 | 0.035 | 0.214 | 1126.20 | 0.4 | 1.82 | 5.73e-04 | 24.04 | 7.57e-03 |
| 41 | 28.430 | 0.035 | 0.214 | 0.08 | 2.39e-05 | 9.84 | 3.10e-03 | 4.91 | 1.54e-03 |
| 42 | 28.552 | 0.035 | 0.214 | 0.47 | 1.48e-04 | 24.60 | 7.74e-03 | 804.24 | 0.3 |
| 43 | 29.344 | 0.034 | 0.213 | 54.15 | 1.70e-02 | 502.42 | 0.2 | 55.71 | 1.75e-02 |
| 44 | 29.842 | 0.034 | 0.212 | 2.573e+04 | 8.1 | 1.07 | 3.38e-04 | 2866.94 | 0.9 |
| 45 | 30.467 | 0.033 | 0.212 | 712.08 | 0.2 | 2240.33 | 0.7 | 6763.82 | 2.1 |
| 46 | 30.599 | 0.033 | 0.211 | 36.83 | 1.16e-02 | 112.41 | 3.54e-02 | 7.32 | 2.30e-03 |
| 47 | 30.845 | 0.032 | 0.211 | 2246.87 | 0.7 | 1613.41 | 0.5 | 6727.06 | 2.1 |
| 48 | 31.108 | 0.032 | 0.211 | 884.98 | 0.3 | 1937.73 | 0.6 | 5298.42 | 1.7 |
| 49 | 31.334 | 0.032 | 0.211 | 2636.50 | 0.8 | 2.64 | 8.31e-04 | 2369.80 | 0.7 |
| 50 | 31.979 | 0.031 | 0.210 | 187.96 | 5.92e-02 | 530.93 | 0.2 | 4901.62 | 1.5 |
| 51 | 32.021 | 0.031 | 0.210 | 240.85 | 7.58e-02 | 22.79 | 7.17e-03 | 1.451e+04 | 4.6 |
| 52 | 32.413 | 0.031 | 0.210 | 180.77 | 5.69e-02 | 3.43 | 1.08e-03 | 1229.79 | 0.4 |
| 53 | 33.030 | 0.030 | 0.209 | 10.83 | 3.41e-03 | 307.60 | 9.68e-02 | 3068.12 | 1.0 |
| 54 | 33.493 | 0.030 | 0.209 | 975.19 | 0.3 | 0.50 | 1.59e-04 | 696.45 | 0.2 |
| 55 | 33.717 | 0.030 | 0.209 | 1249.92 | 0.4 | 534.68 | 0.2 | 6747.37 | 2.1 |
| 56 | 34.342 | 0.029 | 0.208 | 3093.18 | 1.0 | 160.81 | 5.06e-02 | 3523.63 | 1.1 |
| 57 | 35.057 | 0.029 | 0.208 | 4512.55 | 1.4 | 5.63 | 1.77e-03 | 191.86 | 6.04e-02 |
| 58 | 35.375 | 0.028 | 0.207 | 988.60 | 0.3 | 76.87 | 2.42e-02 | 47.61 | 1.50e-02 |
| 59 | 35.533 | 0.028 | 0.207 | 1.673e+04 | 5.3 | 2.25 | 7.08e-04 | 2207.28 | 0.7 |
| 60 | 36.762 | 0.027 | 0.206 | 234.09 | 7.37e-02 | 459.41 | 0.1 | 154.95 | 4.88e-02 |
| 61 | 36.951 | 0.027 | 0.206 | 890.45 | 0.3 | 1.66 | 5.22e-04 | 7045.75 | 2.2 |
| 62 | 37.368 | 0.027 | 0.206 | 462.39 | 0.1 | 292.19 | 9.20e-02 | 132.51 | 4.17e-02 |
| 63 | 37.870 | 0.026 | 0.206 | 58.33 | 1.84e-02 | 36.40 | 1.15e-02 | 532.17 | 0.2 |
| 64 | 38.778 | 0.026 | 0.205 | 0.04 | 1.25e-05 | 942.15 | 0.3 | 1.124e+04 | 3.5 |
| 65 | 39.295 | 0.025 | 0.205 | 7.16 | 2.25e-03 | 1238.78 | 0.4 | 1416.24 | 0.4 |
| 66 | 39.498 | 0.025 | 0.205 | 1342.92 | 0.4 | 0.02 | 5.85e-06 | 1033.57 | 0.3 |

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|----------------|-----------|---------|----------------|------------------|----------|------------------|----------|------------------|----------|
| 67 | 39.733 | 0.025 | 0.205 | 11.51 | 3.62e-03 | 362.70 | 0.1 | 3570.32 | 1.1 |
| 68 | 39.903 | 0.025 | 0.205 | 308.45 | 9.71e-02 | 441.05 | 0.1 | 4.007e+04 | 12.6 |
| 69 | 40.273 | 0.025 | 0.204 | 4.75 | 1.50e-03 | 1.50 | 4.71e-04 | 56.38 | 1.77e-02 |
| 70 | 40.927 | 0.024 | 0.204 | 602.14 | 0.2 | 58.49 | 1.84e-02 | 1853.07 | 0.6 |
| 71 | 41.502 | 0.024 | 0.204 | 185.70 | 5.84e-02 | 23.10 | 7.27e-03 | 459.52 | 0.1 |
| 72 | 41.990 | 0.024 | 0.203 | 5.09 | 1.60e-03 | 112.49 | 3.54e-02 | 379.41 | 0.1 |
| 73 | 42.268 | 0.024 | 0.203 | 45.99 | 1.45e-02 | 3.63e-03 | 1.14e-06 | 34.35 | 1.08e-02 |
| 74 | 42.392 | 0.024 | 0.203 | 660.95 | 0.2 | 239.81 | 7.55e-02 | 8310.27 | 2.6 |
| 75 | 42.404 | 0.024 | 0.203 | 859.59 | 0.3 | 205.49 | 6.47e-02 | 7210.98 | 2.3 |
| 76 | 42.728 | 0.023 | 0.203 | 902.66 | 0.3 | 8.09 | 2.55e-03 | 392.95 | 0.1 |
| 77 | 42.759 | 0.023 | 0.203 | 7.10 | 2.23e-03 | 162.83 | 5.12e-02 | 9.77 | 3.07e-03 |
| 78 | 42.879 | 0.023 | 0.203 | 0.23 | 7.08e-05 | 37.56 | 1.18e-02 | 293.86 | 9.25e-02 |
| 79 | 43.185 | 0.023 | 0.203 | 30.35 | 9.55e-03 | 82.11 | 2.58e-02 | 3641.07 | 1.1 |
| 80 | 43.338 | 0.023 | 0.203 | 5.51 | 1.74e-03 | 559.23 | 0.2 | 6818.64 | 2.1 |
| 81 | 43.830 | 0.023 | 0.202 | 273.94 | 8.62e-02 | 160.82 | 5.06e-02 | 1464.36 | 0.5 |
| 82 | 44.542 | 0.022 | 0.202 | 6.85 | 2.15e-03 | 290.40 | 9.14e-02 | 179.52 | 5.65e-02 |
| 83 | 44.690 | 0.022 | 0.202 | 15.60 | 4.91e-03 | 6.67 | 2.10e-03 | 365.40 | 0.1 |
| 84 | 44.913 | 0.022 | 0.202 | 37.82 | 1.19e-02 | 19.64 | 6.18e-03 | 32.22 | 1.01e-02 |
| 85 | 45.006 | 0.022 | 0.202 | 3.30 | 1.04e-03 | 85.25 | 2.68e-02 | 81.88 | 2.58e-02 |
| 86 | 45.249 | 0.022 | 0.202 | 19.04 | 5.99e-03 | 39.52 | 1.24e-02 | 94.99 | 2.99e-02 |
| 87 | 45.483 | 0.022 | 0.202 | 8.06 | 2.54e-03 | 0.43 | 1.34e-04 | 1729.57 | 0.5 |
| 88 | 45.561 | 0.022 | 0.202 | 31.82 | 1.00e-02 | 12.08 | 3.80e-03 | 8.03 | 2.53e-03 |
| 89 | 46.565 | 0.021 | 0.201 | 39.22 | 1.23e-02 | 8.95 | 2.82e-03 | 185.37 | 5.83e-02 |
| 90 | 47.052 | 0.021 | 0.201 | 94.59 | 2.98e-02 | 18.31 | 5.76e-03 | 51.94 | 1.63e-02 |
| 91 | 47.295 | 0.021 | 0.201 | 708.57 | 0.2 | 0.04 | 1.35e-05 | 86.12 | 2.71e-02 |
| 92 | 47.804 | 0.021 | 0.201 | 38.46 | 1.21e-02 | 54.80 | 1.72e-02 | 325.69 | 0.1 |
| 93 | 47.867 | 0.021 | 0.201 | 547.25 | 0.2 | 119.65 | 3.77e-02 | 164.39 | 5.17e-02 |
| 94 | 48.589 | 0.021 | 0.200 | 29.81 | 9.38e-03 | 9.60 | 3.02e-03 | 308.86 | 9.72e-02 |
| 95 | 49.843 | 0.020 | 0.200 | 0.29 | 8.98e-05 | 1231.18 | 0.4 | 659.29 | 0.2 |
| 96 | 49.968 | 0.020 | 0.200 | 0.25 | 7.97e-05 | 0.35 | 1.09e-04 | 1.88 | 5.93e-04 |
| 97 | 50.204 | 0.020 | 0.200 | 120.56 | 3.79e-02 | 77.11 | 2.43e-02 | 41.64 | 1.31e-02 |
| 98 | 50.400 | 0.020 | 0.200 | 0.43 | 1.34e-04 | 0.26 | 8.27e-05 | 1053.97 | 0.3 |
| 99 | 50.788 | 0.020 | 0.200 | 10.26 | 3.23e-03 | 114.48 | 3.60e-02 | 4.64 | 1.46e-03 |
| 100 | 50.807 | 0.020 | 0.200 | 11.21 | 3.53e-03 | 83.51 | 2.63e-02 | 26.31 | 8.28e-03 |
| Risulta | | | | 2.743e+05 | | 2.837e+05 | | 1.676e+05 | |
| In percentuale | | | | 86.33 | | 89.28 | | 52.73 | |

• **Caso di carico sisma y-y ecc- - SLV**

| CDC | Tipo | Sigla Id | Note |
|-----|------|---|--|
| 12 | Edk | CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -) | |
| | | | categoria suolo: B |
| | | | fattore di sito S = 1.200 |
| | | | ordinata spettro (tratto Tb-Tc) = 0.304 g |
| | | | angolo di ingresso:90.00 |
| | | | eccentricità aggiuntiva: negativa |
| | | | periodo proprio T1: 0.089 sec. |
| | | | fattore q: 1.500 |
| | | | amplificazione ND (non dissipativi): 1.000 |
| | | | fattore per spost. mu d: 3.275 |
| | | | classe di duttilità CD: ND |
| | | | numero di modi considerati:100 |
| | | | combinaz. modale: CQC |

Analisi dinamica e spettro di risposta SLV ecc-

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|------|-----------|---------|----------------|------------------|----------|------------------|----------|------------------|----------|
| | Hz | sec | g | daN | | daN | | daN | |
| 1 | 7.648 | 0.131 | 0.301 | 1.687e+04 | 5.3 | 14.80 | 4.66e-03 | 114.23 | 3.60e-02 |
| 2 | 8.387 | 0.119 | 0.291 | 1.312e+04 | 4.1 | 0.93 | 2.94e-04 | 489.07 | 0.2 |
| 3 | 9.121 | 0.110 | 0.282 | 2.142e+04 | 6.7 | 45.11 | 1.42e-02 | 0.50 | 1.57e-04 |
| 4 | 10.995 | 0.091 | 0.265 | 1043.84 | 0.3 | 1.390e+04 | 4.4 | 439.35 | 0.1 |
| 5 | 11.291 | 0.089 | 0.263 | 121.15 | 3.81e-02 | 1.218e+05 | 38.3 | 150.28 | 4.73e-02 |
| 6 | 11.681 | 0.086 | 0.260 | 3103.63 | 1.0 | 670.43 | 0.2 | 516.28 | 0.2 |
| 7 | 12.568 | 0.080 | 0.254 | 2.754e+04 | 8.7 | 11.26 | 3.54e-03 | 8.86 | 2.79e-03 |
| 8 | 13.718 | 0.073 | 0.248 | 3090.92 | 1.0 | 3.877e+04 | 12.2 | 59.11 | 1.86e-02 |
| 9 | 13.969 | 0.072 | 0.247 | 3.400e+04 | 10.7 | 4270.34 | 1.3 | 13.29 | 4.18e-03 |

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|------|-----------|---------|----------------|------------------|----------|------------------|----------|------------------|----------|
| 10 | 14.758 | 0.068 | 0.244 | 89.54 | 2.82e-02 | 3.137e+04 | 9.9 | 19.96 | 6.28e-03 |
| 11 | 16.722 | 0.060 | 0.236 | 7605.53 | 2.4 | 732.27 | 0.2 | 2.13 | 6.70e-04 |
| 12 | 16.742 | 0.060 | 0.236 | 399.73 | 0.1 | 1.241e+04 | 3.9 | 2.04 | 6.42e-04 |
| 13 | 17.080 | 0.059 | 0.235 | 430.41 | 0.1 | 950.64 | 0.3 | 11.02 | 3.47e-03 |
| 14 | 17.474 | 0.057 | 0.234 | 3842.71 | 1.2 | 70.16 | 2.21e-02 | 18.49 | 5.82e-03 |
| 15 | 17.633 | 0.057 | 0.234 | 576.92 | 0.2 | 3305.57 | 1.0 | 3.81 | 1.20e-03 |
| 16 | 17.967 | 0.056 | 0.233 | 3107.48 | 1.0 | 1.087e+04 | 3.4 | 11.33 | 3.57e-03 |
| 17 | 18.241 | 0.055 | 0.232 | 2.725e+04 | 8.6 | 55.68 | 1.75e-02 | 40.94 | 1.29e-02 |
| 18 | 18.936 | 0.053 | 0.230 | 1.513e+04 | 4.8 | 0.06 | 1.91e-05 | 36.82 | 1.16e-02 |
| 19 | 19.157 | 0.052 | 0.229 | 4540.55 | 1.4 | 55.67 | 1.75e-02 | 261.71 | 8.24e-02 |
| 20 | 19.376 | 0.052 | 0.229 | 1535.51 | 0.5 | 715.43 | 0.2 | 0.74 | 2.34e-04 |
| 21 | 19.841 | 0.050 | 0.228 | 30.58 | 9.63e-03 | 2.026e+04 | 6.4 | 6.10 | 1.92e-03 |
| 22 | 20.485 | 0.049 | 0.226 | 848.00 | 0.3 | 519.82 | 0.2 | 1.78 | 5.62e-04 |
| 23 | 20.822 | 0.048 | 0.226 | 7238.09 | 2.3 | 797.10 | 0.3 | 0.98 | 3.07e-04 |
| 24 | 21.239 | 0.047 | 0.225 | 720.86 | 0.2 | 0.52 | 1.63e-04 | 38.61 | 1.22e-02 |
| 25 | 21.475 | 0.047 | 0.224 | 1430.23 | 0.5 | 309.02 | 9.73e-02 | 14.93 | 4.70e-03 |
| 26 | 21.705 | 0.046 | 0.224 | 353.10 | 0.1 | 33.92 | 1.07e-02 | 32.74 | 1.03e-02 |
| 27 | 21.932 | 0.046 | 0.223 | 2707.50 | 0.9 | 109.87 | 3.46e-02 | 50.91 | 1.60e-02 |
| 28 | 22.459 | 0.045 | 0.222 | 93.61 | 2.95e-02 | 33.40 | 1.05e-02 | 9.95 | 3.13e-03 |
| 29 | 23.038 | 0.043 | 0.221 | 37.29 | 1.17e-02 | 840.41 | 0.3 | 18.61 | 5.86e-03 |
| 30 | 23.352 | 0.043 | 0.221 | 78.78 | 2.48e-02 | 116.34 | 3.66e-02 | 1.26 | 3.95e-04 |
| 31 | 23.546 | 0.042 | 0.220 | 123.85 | 3.90e-02 | 967.62 | 0.3 | 0.03 | 1.09e-05 |
| 32 | 24.566 | 0.041 | 0.219 | 1786.71 | 0.6 | 1248.97 | 0.4 | 67.82 | 2.13e-02 |
| 33 | 24.707 | 0.040 | 0.219 | 3239.12 | 1.0 | 3.61 | 1.13e-03 | 330.85 | 0.1 |
| 34 | 24.920 | 0.040 | 0.218 | 571.33 | 0.2 | 247.48 | 7.79e-02 | 594.11 | 0.2 |
| 35 | 25.184 | 0.040 | 0.218 | 8.93 | 2.81e-03 | 1319.76 | 0.4 | 6.66 | 2.10e-03 |
| 36 | 25.833 | 0.039 | 0.217 | 66.42 | 2.09e-02 | 1082.97 | 0.3 | 69.89 | 2.20e-02 |
| 37 | 26.780 | 0.037 | 0.216 | 408.02 | 0.1 | 2286.80 | 0.7 | 902.81 | 0.3 |
| 38 | 27.053 | 0.037 | 0.215 | 22.98 | 7.23e-03 | 17.04 | 5.36e-03 | 5.26 | 1.66e-03 |
| 39 | 27.787 | 0.036 | 0.215 | 194.60 | 6.12e-02 | 1241.96 | 0.4 | 718.26 | 0.2 |
| 40 | 28.432 | 0.035 | 0.214 | 19.35 | 6.09e-03 | 2.62 | 8.24e-04 | 29.11 | 9.16e-03 |
| 41 | 28.548 | 0.035 | 0.214 | 1482.26 | 0.5 | 1.95 | 6.13e-04 | 127.99 | 4.03e-02 |
| 42 | 28.618 | 0.035 | 0.214 | 183.75 | 5.78e-02 | 181.84 | 5.72e-02 | 296.92 | 9.34e-02 |
| 43 | 28.775 | 0.035 | 0.213 | 4.14 | 1.30e-03 | 126.09 | 3.97e-02 | 79.06 | 2.49e-02 |
| 44 | 29.964 | 0.033 | 0.212 | 1.735e+04 | 5.5 | 17.30 | 5.45e-03 | 2939.67 | 0.9 |
| 45 | 30.100 | 0.033 | 0.212 | 5732.79 | 1.8 | 2.31 | 7.28e-04 | 286.35 | 9.01e-02 |
| 46 | 30.609 | 0.033 | 0.211 | 211.67 | 6.66e-02 | 0.45 | 1.41e-04 | 297.82 | 9.37e-02 |
| 47 | 30.824 | 0.032 | 0.211 | 6817.48 | 2.1 | 0.12 | 3.89e-05 | 2611.97 | 0.8 |
| 48 | 30.944 | 0.032 | 0.211 | 1164.63 | 0.4 | 90.16 | 2.84e-02 | 2064.46 | 0.6 |
| 49 | 31.055 | 0.032 | 0.211 | 181.08 | 5.70e-02 | 120.55 | 3.79e-02 | 1.409e+04 | 4.4 |
| 50 | 31.957 | 0.031 | 0.210 | 328.86 | 0.1 | 157.41 | 4.95e-02 | 1.479e+04 | 4.7 |
| 51 | 32.930 | 0.030 | 0.209 | 226.26 | 7.12e-02 | 109.06 | 3.43e-02 | 1.675e+04 | 5.3 |
| 52 | 33.491 | 0.030 | 0.209 | 965.33 | 0.3 | 1.42 | 4.47e-04 | 810.42 | 0.3 |
| 53 | 34.280 | 0.029 | 0.208 | 272.41 | 8.57e-02 | 275.13 | 8.66e-02 | 245.10 | 7.71e-02 |
| 54 | 34.793 | 0.029 | 0.208 | 1904.99 | 0.6 | 2720.24 | 0.9 | 758.83 | 0.2 |
| 55 | 35.116 | 0.028 | 0.208 | 2.016e+04 | 6.3 | 940.33 | 0.3 | 2310.82 | 0.7 |
| 56 | 35.368 | 0.028 | 0.207 | 1671.55 | 0.5 | 375.20 | 0.1 | 640.10 | 0.2 |
| 57 | 35.494 | 0.028 | 0.207 | 984.88 | 0.3 | 691.13 | 0.2 | 1089.67 | 0.3 |
| 58 | 35.658 | 0.028 | 0.207 | 131.99 | 4.15e-02 | 368.35 | 0.1 | 470.72 | 0.1 |
| 59 | 36.126 | 0.028 | 0.207 | 0.41 | 1.30e-04 | 197.89 | 6.23e-02 | 195.02 | 6.14e-02 |
| 60 | 36.725 | 0.027 | 0.207 | 286.89 | 9.03e-02 | 373.30 | 0.1 | 3476.49 | 1.1 |
| 61 | 36.932 | 0.027 | 0.206 | 299.62 | 9.43e-02 | 2.53 | 7.98e-04 | 2419.12 | 0.8 |
| 62 | 36.978 | 0.027 | 0.206 | 349.26 | 0.1 | 225.94 | 7.11e-02 | 2526.44 | 0.8 |
| 63 | 37.099 | 0.027 | 0.206 | 80.91 | 2.55e-02 | 0.40 | 1.25e-04 | 0.16 | 4.93e-05 |
| 64 | 37.281 | 0.027 | 0.206 | 56.51 | 1.78e-02 | 120.52 | 3.79e-02 | 1784.44 | 0.6 |
| 65 | 39.286 | 0.025 | 0.205 | 90.48 | 2.85e-02 | 64.68 | 2.04e-02 | 2.609e+04 | 8.2 |
| 66 | 39.508 | 0.025 | 0.205 | 356.53 | 0.1 | 36.46 | 1.15e-02 | 2.502e+04 | 7.9 |
| 67 | 39.840 | 0.025 | 0.205 | 3136.84 | 1.0 | 0.21 | 6.67e-05 | 1480.99 | 0.5 |
| 68 | 40.266 | 0.025 | 0.204 | 48.36 | 1.52e-02 | 14.59 | 4.59e-03 | 17.80 | 5.60e-03 |
| 69 | 40.402 | 0.025 | 0.204 | 170.43 | 5.36e-02 | 341.78 | 0.1 | 4372.18 | 1.4 |
| 70 | 40.480 | 0.025 | 0.204 | 883.57 | 0.3 | 674.64 | 0.2 | 639.25 | 0.2 |
| 71 | 41.067 | 0.024 | 0.204 | 29.01 | 9.13e-03 | 40.71 | 1.28e-02 | 58.18 | 1.83e-02 |
| 72 | 41.441 | 0.024 | 0.204 | 115.59 | 3.64e-02 | 95.43 | 3.00e-02 | 469.84 | 0.1 |
| 73 | 42.130 | 0.024 | 0.203 | 2.54 | 7.99e-04 | 295.45 | 9.30e-02 | 4628.64 | 1.5 |
| 74 | 42.368 | 0.024 | 0.203 | 0.58 | 1.83e-04 | 9.37 | 2.95e-03 | 18.32 | 5.76e-03 |
| 75 | 42.494 | 0.024 | 0.203 | 152.92 | 4.81e-02 | 483.30 | 0.2 | 7.37 | 2.32e-03 |
| 76 | 42.697 | 0.023 | 0.203 | 1286.68 | 0.4 | 5.32 | 1.68e-03 | 0.03 | 8.14e-06 |
| 77 | 42.844 | 0.023 | 0.203 | 2.19 | 6.89e-04 | 301.59 | 9.49e-02 | 400.49 | 0.1 |
| 78 | 43.094 | 0.023 | 0.203 | 344.50 | 0.1 | 41.55 | 1.31e-02 | 1558.84 | 0.5 |
| 79 | 43.239 | 0.023 | 0.203 | 31.78 | 1.00e-02 | 7.49 | 2.36e-03 | 363.73 | 0.1 |

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|----------------|-----------|---------|----------------|------------------|----------|------------------|----------|------------------|----------|
| 80 | 43.687 | 0.023 | 0.203 | 55.51 | 1.75e-02 | 970.73 | 0.3 | 1.491e+04 | 4.7 |
| 81 | 44.028 | 0.023 | 0.202 | 5.71e-04 | 0.0 | 0.03 | 8.80e-06 | 2691.91 | 0.8 |
| 82 | 44.281 | 0.023 | 0.202 | 162.88 | 5.13e-02 | 195.04 | 6.14e-02 | 613.26 | 0.2 |
| 83 | 44.472 | 0.022 | 0.202 | 63.52 | 2.00e-02 | 483.95 | 0.2 | 2.45 | 7.71e-04 |
| 84 | 44.855 | 0.022 | 0.202 | 0.17 | 5.34e-05 | 0.80 | 2.51e-04 | 930.45 | 0.3 |
| 85 | 45.144 | 0.022 | 0.202 | 70.38 | 2.22e-02 | 191.53 | 6.03e-02 | 104.15 | 3.28e-02 |
| 86 | 45.439 | 0.022 | 0.202 | 32.08 | 1.01e-02 | 279.38 | 8.79e-02 | 1255.05 | 0.4 |
| 87 | 45.485 | 0.022 | 0.202 | 25.93 | 8.16e-03 | 677.03 | 0.2 | 141.08 | 4.44e-02 |
| 88 | 45.570 | 0.022 | 0.202 | 1.63 | 5.12e-04 | 32.37 | 1.02e-02 | 92.75 | 2.92e-02 |
| 89 | 45.760 | 0.022 | 0.202 | 74.19 | 2.33e-02 | 190.82 | 6.01e-02 | 433.38 | 0.1 |
| 90 | 46.518 | 0.021 | 0.201 | 2.09 | 6.57e-04 | 11.66 | 3.67e-03 | 162.39 | 5.11e-02 |
| 91 | 46.756 | 0.021 | 0.201 | 43.83 | 1.38e-02 | 191.97 | 6.04e-02 | 2005.27 | 0.6 |
| 92 | 47.042 | 0.021 | 0.201 | 27.94 | 8.79e-03 | 42.73 | 1.34e-02 | 179.68 | 5.65e-02 |
| 93 | 47.078 | 0.021 | 0.201 | 77.53 | 2.44e-02 | 3.60 | 1.13e-03 | 7.65e-03 | 2.41e-06 |
| 94 | 47.380 | 0.021 | 0.201 | 527.57 | 0.2 | 29.83 | 9.39e-03 | 6.50 | 2.05e-03 |
| 95 | 47.501 | 0.021 | 0.201 | 699.26 | 0.2 | 1.90 | 5.97e-04 | 605.70 | 0.2 |
| 96 | 48.380 | 0.021 | 0.200 | 149.94 | 4.72e-02 | 221.47 | 6.97e-02 | 174.34 | 5.49e-02 |
| 97 | 48.555 | 0.021 | 0.200 | 18.31 | 5.76e-03 | 134.88 | 4.24e-02 | 174.11 | 5.48e-02 |
| 98 | 49.671 | 0.020 | 0.200 | 6.08 | 1.91e-03 | 23.24 | 7.32e-03 | 54.56 | 1.72e-02 |
| 99 | 50.192 | 0.020 | 0.200 | 108.16 | 3.40e-02 | 1.35 | 4.23e-04 | 355.50 | 0.1 |
| 100 | 50.788 | 0.020 | 0.200 | 0.13 | 4.15e-05 | 0.82 | 2.59e-04 | 70.48 | 2.22e-02 |
| Risulta | | | | 2.744e+05 | | 2.846e+05 | | 1.663e+05 | |
| In percentuale | | | | 86.37 | | 89.58 | | 52.33 | |

• **Caso di carico sisma x-x ecc+ - SLD**

| Quota | M Sismica x g | Pos. GX | Pos. GY | E agg. X-X | E agg. Y-Y | Pos. KX | Pos. KY |
|--------|---------------|---------|---------|------------|------------|---------|---------|
| cm | daN | cm | cm | cm | cm | cm | cm |
| 592.00 | 1.712e+04 | 2190.49 | 1155.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 589.60 | 30.49 | 2852.50 | 1143.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 588.98 | 27.08 | 2852.50 | 1162.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 588.03 | 37.91 | 1280.50 | 1135.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 585.00 | 38.69 | 2852.50 | 1120.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 584.26 | 35.29 | 1280.50 | 1174.25 | 0.0 | 0.0 | 0.0 | 0.0 |
| 583.63 | 38.38 | 1280.50 | 1113.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 580.39 | 77.06 | 2852.50 | 1109.90 | 0.0 | -2.30 | 0.0 | 0.0 |
| 579.93 | 63.60 | 2852.50 | 1180.13 | 0.0 | -1.12 | 0.0 | 0.0 |
| 579.22 | 36.75 | 1280.50 | 1091.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 576.52 | 39.26 | 1280.50 | 1193.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 575.79 | 46.08 | 2852.50 | 1074.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 574.82 | 41.92 | 1280.50 | 1069.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 574.00 | 46.93 | 1280.50 | 1134.72 | 0.0 | -4.15 | 0.0 | 0.0 |
| 571.19 | 43.95 | 2852.50 | 1051.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 570.89 | 44.90 | 2852.50 | 1207.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 570.42 | 40.03 | 1280.50 | 1047.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 568.77 | 36.28 | 1280.50 | 1212.75 | 0.0 | 0.0 | 0.0 | 0.0 |
| 566.59 | 41.82 | 2852.50 | 1028.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 566.02 | 38.51 | 1280.50 | 1025.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 561.98 | 39.45 | 2852.50 | 1005.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 561.84 | 40.83 | 2852.50 | 1230.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 561.61 | 37.69 | 1280.50 | 1003.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 561.03 | 32.46 | 1280.50 | 1232.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 557.38 | 49.76 | 2852.50 | 982.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 557.01 | 43.93 | 1280.50 | 980.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 556.00 | 127.39 | 1280.50 | 1118.57 | 0.0 | -11.44 | 0.0 | 0.0 |
| 555.39 | 213.59 | 2852.50 | 1119.81 | 0.0 | -11.25 | 2852.50 | 1117.50 |
| 553.99 | 34.15 | 1280.50 | 1249.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 552.79 | 97.12 | 2852.50 | 1105.95 | 0.0 | -14.68 | 0.0 | 0.0 |
| 552.41 | 41.85 | 1280.50 | 957.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 547.88 | 48.12 | 2852.50 | 934.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 547.81 | 40.19 | 1280.50 | 934.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 546.96 | 37.41 | 1280.50 | 1267.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 543.74 | 43.43 | 2852.50 | 1275.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 543.20 | 38.42 | 1280.50 | 911.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 542.87 | 46.11 | 2852.50 | 909.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 538.60 | 43.75 | 1280.50 | 888.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 538.00 | 201.24 | 1280.50 | 1092.96 | 0.0 | -17.79 | 1280.50 | 1089.08 |
| 537.87 | 43.28 | 2852.50 | 884.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 537.36 | 48.44 | 1280.50 | 1290.85 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | M Sismica x g | Pos. GX | Pos. GY | E agg. X-X | E agg. Y-Y | Pos. KX | Pos. KY |
|--------|---------------|---------|---------|------------|------------|---------|---------|
| 534.69 | 52.40 | 2852.50 | 1297.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 534.00 | 41.70 | 1280.50 | 865.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 532.87 | 54.43 | 2852.50 | 859.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 530.39 | 389.47 | 2852.50 | 1084.49 | 0.0 | -19.53 | 2852.50 | 1079.75 |
| 529.40 | 40.04 | 1280.50 | 842.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 527.87 | 51.13 | 2852.50 | 834.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 527.31 | 44.98 | 1280.50 | 1315.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 525.64 | 47.05 | 2852.50 | 1320.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 524.79 | 38.83 | 1280.50 | 819.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 522.86 | 48.62 | 2852.50 | 809.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 520.06 | 47.30 | 1280.50 | 795.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 520.00 | 1823.64 | 745.53 | 1140.17 | 0.0 | -24.83 | 1280.50 | 1067.50 |
| 517.86 | 46.10 | 2852.50 | 784.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 517.25 | 51.03 | 1280.50 | 1340.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 516.59 | 42.62 | 2852.50 | 1342.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 516.42 | 763.97 | 101.00 | 1137.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 516.05 | 729.17 | 1280.50 | 1135.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 515.26 | 43.63 | 1280.50 | 771.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 512.86 | 43.28 | 2852.50 | 759.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 512.44 | 800.93 | 101.00 | 1117.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 512.13 | 710.24 | 1280.50 | 1174.25 | 0.0 | 0.0 | 0.0 | 0.0 |
| 511.67 | 766.68 | 1280.50 | 1113.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 511.01 | 891.21 | 101.00 | 1177.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 510.86 | 40.18 | 1280.50 | 749.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 508.46 | 799.33 | 101.00 | 1097.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 507.85 | 50.22 | 2852.50 | 734.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 507.54 | 51.23 | 2852.50 | 1365.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 507.29 | 766.68 | 1280.50 | 1091.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 507.20 | 46.25 | 1280.50 | 1365.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 506.45 | 38.66 | 1280.50 | 727.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 505.39 | 583.22 | 2852.50 | 1055.85 | 0.0 | -29.15 | 2852.50 | 1051.00 |
| 504.47 | 797.56 | 101.00 | 1077.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 504.26 | 710.23 | 1280.50 | 1193.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 503.65 | 43.28 | 2852.50 | 713.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 502.91 | 766.47 | 1280.50 | 1069.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 502.83 | 855.07 | 101.00 | 1197.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 502.05 | 36.99 | 1280.50 | 705.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 500.49 | 786.11 | 101.00 | 1057.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 499.45 | 41.51 | 2852.50 | 692.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 499.00 | 87.74 | 101.00 | 1129.72 | 0.0 | -5.00 | 0.0 | 0.0 |
| 498.53 | 820.85 | 1368.74 | 1066.26 | 0.0 | -17.02 | 0.0 | 0.0 |
| 497.65 | 43.65 | 1280.50 | 683.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 497.14 | 48.29 | 1280.50 | 1390.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 496.71 | 764.04 | 101.00 | 1038.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 496.40 | 717.97 | 1280.50 | 1212.75 | 0.0 | 0.0 | 0.0 | 0.0 |
| 496.06 | 16.98 | 1280.50 | 795.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 496.00 | 352.67 | 1280.50 | 1044.37 | 0.0 | -33.02 | 1280.50 | 1053.45 |
| 495.90 | 14.20 | 1280.50 | 957.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 495.25 | 39.73 | 2852.50 | 671.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 494.66 | 903.85 | 101.00 | 1217.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 494.15 | 774.72 | 1280.50 | 1025.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 493.25 | 41.70 | 1280.50 | 661.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 492.93 | 762.59 | 101.00 | 1019.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 491.04 | 37.96 | 2852.50 | 650.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 489.78 | 783.23 | 1280.50 | 1003.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 489.44 | 41.82 | 2852.50 | 1410.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 489.15 | 761.15 | 101.00 | 1000.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 488.84 | 40.18 | 1280.50 | 639.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 488.64 | 41.26 | 1280.50 | 1412.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 488.53 | 677.40 | 1280.50 | 1232.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 486.84 | 35.95 | 2852.50 | 629.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 485.46 | 952.70 | 101.00 | 1239.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 485.37 | 759.71 | 101.00 | 981.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 485.20 | 800.80 | 1280.50 | 980.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 484.44 | 38.66 | 1280.50 | 617.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 482.64 | 44.43 | 2852.50 | 608.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 481.59 | 758.03 | 101.00 | 962.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 481.38 | 645.13 | 1280.50 | 1249.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 480.62 | 800.59 | 1280.50 | 957.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 480.39 | 782.44 | 2852.50 | 1050.67 | 0.0 | -40.15 | 0.0 | 0.0 |
| 480.04 | 36.98 | 1280.50 | 595.50 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | M Sismica x g | Pos. GX | Pos. GY | E agg. X-X | E agg. Y-Y | Pos. KX | Pos. KY |
|--------|---------------|---------|---------|------------|------------|---------|---------|
| 479.79 | 39.10 | 1280.50 | 1434.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 478.44 | 42.09 | 2852.50 | 587.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 477.80 | 887.32 | 101.00 | 943.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 476.27 | 960.65 | 101.00 | 1262.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 476.04 | 809.24 | 1280.50 | 934.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 475.64 | 43.64 | 1280.50 | 573.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 475.00 | 262.09 | 101.00 | 1106.10 | 0.0 | -13.88 | 101.00 | 1100.75 |
| 474.22 | 810.89 | 1358.66 | 1232.17 | 0.0 | -35.02 | 0.0 | 0.0 |
| 474.00 | 492.04 | 1280.50 | 1014.24 | 0.0 | -41.93 | 1280.50 | 1008.97 |
| 472.83 | 1005.38 | 101.00 | 918.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 471.46 | 809.28 | 1280.50 | 911.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 471.34 | 43.43 | 2852.50 | 1455.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 471.23 | 42.62 | 1280.50 | 551.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 470.94 | 44.00 | 1280.50 | 1456.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 470.03 | 39.89 | 2852.50 | 545.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 467.85 | 1002.88 | 101.00 | 893.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 467.07 | 955.50 | 101.00 | 1284.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 466.89 | 800.59 | 1280.50 | 888.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 466.63 | 41.48 | 1280.50 | 528.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 465.53 | 40.22 | 2852.50 | 523.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 464.48 | 900.08 | 1280.50 | 1290.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 462.88 | 1000.38 | 101.00 | 868.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 462.30 | 853.21 | 1377.04 | 902.76 | 0.0 | -30.62 | 0.0 | 0.0 |
| 462.09 | 79.76 | 1280.50 | 997.53 | 0.0 | -48.60 | 0.0 | 0.0 |
| 460.73 | 52.38 | 2852.50 | 499.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 458.00 | 890.72 | 2852.50 | 993.40 | 0.0 | -46.60 | 2852.50 | 989.00 |
| 457.90 | 1843.37 | 101.00 | 1055.89 | 0.0 | -23.20 | 0.0 | 0.0 |
| 457.73 | 800.67 | 1280.50 | 842.15 | 0.0 | 0.0 | 0.0 | 0.0 |
| 457.63 | 37.71 | 1280.50 | 483.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 455.93 | 49.30 | 2852.50 | 475.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 454.26 | 932.03 | 1280.50 | 1315.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 453.25 | 92.84 | 2077.12 | 1500.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 453.12 | 865.03 | 1280.50 | 800.76 | 0.0 | -17.91 | 0.0 | 0.0 |
| 452.93 | 1008.16 | 101.00 | 818.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 452.00 | 595.94 | 1280.50 | 985.10 | 0.0 | -49.73 | 1280.50 | 975.64 |
| 451.12 | 46.99 | 2852.50 | 451.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 451.00 | 439.27 | 101.00 | 1076.91 | 0.0 | -23.20 | 101.00 | 1075.00 |
| 450.72 | 746.37 | 101.00 | 1324.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 448.62 | 42.42 | 1280.50 | 438.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 448.45 | 838.40 | 1280.50 | 795.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 447.95 | 1004.94 | 101.00 | 793.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 446.32 | 44.67 | 2852.50 | 427.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 444.40 | 43.08 | 1280.50 | 1522.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 444.20 | 42.62 | 2852.50 | 1522.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 444.12 | 40.83 | 1280.50 | 416.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 444.04 | 921.30 | 1280.50 | 1340.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 443.67 | 800.51 | 1280.50 | 771.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 443.57 | 849.33 | 101.00 | 1342.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 442.97 | 1002.44 | 101.00 | 768.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 441.52 | 41.96 | 2852.50 | 403.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 439.62 | 38.88 | 1280.50 | 393.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 439.29 | 765.99 | 1280.50 | 749.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 438.00 | 999.93 | 101.00 | 743.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 436.96 | 16.83 | 3103.00 | 1540.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 436.72 | 52.95 | 2852.50 | 379.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 435.35 | 40.42 | 1280.50 | 1544.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 435.12 | 97.35 | 2107.67 | 988.75 | 0.0 | -58.70 | 0.0 | 0.0 |
| 434.91 | 765.90 | 1280.50 | 727.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 434.37 | 951.53 | 101.00 | 1364.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 433.82 | 941.54 | 1280.50 | 1366.09 | 0.0 | -1.25 | 0.0 | 0.0 |
| 433.02 | 2121.49 | 1559.11 | 849.97 | 0.0 | -55.98 | 0.0 | 0.0 |
| 431.91 | 49.78 | 2852.50 | 355.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 430.61 | 43.83 | 1280.50 | 348.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 430.53 | 774.21 | 1280.50 | 705.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 430.00 | 713.43 | 1280.50 | 967.92 | 0.0 | -57.55 | 1280.50 | 955.10 |
| 428.05 | 1007.62 | 101.00 | 693.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 427.11 | 47.46 | 2852.50 | 331.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 427.00 | 614.79 | 101.00 | 1045.00 | 0.0 | -32.33 | 101.00 | 1041.25 |
| 426.30 | 46.67 | 1280.50 | 1567.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 426.11 | 876.93 | 1408.42 | 734.37 | 0.0 | -62.08 | 0.0 | 0.0 |
| 425.18 | 958.96 | 101.00 | 1387.00 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | M Sismica x g | Pos. GX | Pos. GY | E agg. X-X | E agg. Y-Y | Pos. KX | Pos. KY |
|--------|---------------|---------|---------|------------|------------|---------|---------|
| 423.60 | 852.72 | 1280.50 | 1390.85 | 0.0 | 0.0 | 0.0 | 0.0 |
| 423.07 | 1004.49 | 101.00 | 668.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 422.31 | 52.62 | 2888.07 | 307.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 421.78 | 765.99 | 1280.50 | 661.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 421.61 | 42.01 | 1280.50 | 303.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 418.09 | 1001.99 | 101.00 | 643.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 417.51 | 53.66 | 2903.08 | 283.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 417.40 | 765.99 | 1280.50 | 639.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 417.25 | 42.34 | 1280.50 | 1589.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 417.11 | 39.54 | 1280.50 | 281.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 417.05 | 51.08 | 2897.95 | 1590.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 415.98 | 953.64 | 101.00 | 1409.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 414.96 | 794.98 | 1280.50 | 1412.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 413.12 | 999.49 | 101.00 | 618.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 413.02 | 765.89 | 1280.50 | 617.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 412.70 | 45.12 | 2880.89 | 259.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 412.60 | 51.55 | 1280.50 | 258.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 408.64 | 775.93 | 1280.50 | 595.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 408.14 | 996.87 | 101.00 | 593.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 408.00 | 3.405e+04 | 2202.46 | 786.61 | 0.0 | -68.85 | 2554.91 | 924.22 |
| 406.79 | 962.02 | 101.00 | 1432.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 405.97 | 821.74 | 1280.50 | 1434.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 404.26 | 767.69 | 1280.50 | 573.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 403.17 | 1007.09 | 101.00 | 568.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 403.00 | 781.30 | 101.00 | 1008.47 | 0.0 | -40.83 | 101.00 | 1001.25 |
| 399.88 | 785.16 | 1280.50 | 551.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 398.19 | 1064.22 | 101.00 | 543.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 397.59 | 956.64 | 101.00 | 1454.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 396.98 | 812.61 | 1280.50 | 1456.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 395.30 | 793.89 | 1280.50 | 528.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 392.62 | 1061.41 | 101.00 | 515.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 390.83 | 785.16 | 1280.50 | 506.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 388.39 | 952.30 | 101.00 | 1477.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 387.98 | 812.84 | 1280.50 | 1478.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 387.64 | 998.75 | 101.00 | 490.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 386.35 | 785.05 | 1280.50 | 483.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 382.67 | 996.26 | 101.00 | 465.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 381.87 | 794.99 | 1280.50 | 461.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 381.00 | 7050.80 | 2265.21 | 925.46 | 0.0 | -68.85 | 2546.65 | 924.19 |
| 379.20 | 960.06 | 101.00 | 1499.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 379.00 | 1788.04 | 643.98 | 1218.97 | 0.0 | -51.75 | 101.00 | 971.00 |
| 377.69 | 1006.19 | 101.00 | 440.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 377.39 | 784.80 | 1280.50 | 438.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 376.00 | 78.90 | 2852.50 | 909.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 372.91 | 784.81 | 1280.50 | 416.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 372.71 | 1003.31 | 101.00 | 415.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 371.15 | 81.23 | 2852.50 | 959.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 370.99 | 81.51 | 2852.50 | 884.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 370.00 | 4593.13 | 677.99 | 1522.00 | 0.0 | 0.0 | 640.25 | 1522.00 |
| 368.43 | 784.81 | 1280.50 | 393.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 367.74 | 1000.81 | 101.00 | 390.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 365.99 | 84.03 | 2852.50 | 859.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 363.96 | 784.81 | 1280.50 | 371.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 362.76 | 898.59 | 101.00 | 365.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 361.90 | 83.20 | 2852.50 | 982.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 360.99 | 86.54 | 2852.50 | 834.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 360.87 | 1.266e+04 | 2191.75 | 0.0 | 0.0 | 0.0 | 2191.58 | 0.0 |
| 359.48 | 784.75 | 1280.50 | 348.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 358.78 | 777.08 | 101.00 | 345.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 355.99 | 89.06 | 2852.50 | 809.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 355.00 | 1.283e+04 | 1372.08 | 754.21 | 0.0 | -68.85 | 2329.56 | 947.86 |
| 352.65 | 88.60 | 2852.50 | 1005.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 350.98 | 92.51 | 2852.50 | 784.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 345.98 | 80.58 | 2852.50 | 759.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 343.40 | 79.38 | 2852.50 | 1028.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 340.98 | 94.42 | 2852.50 | 734.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 336.78 | 71.94 | 2852.50 | 713.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 334.14 | 84.79 | 2852.50 | 1051.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 333.00 | 8853.99 | 1554.95 | 926.52 | 0.0 | -68.85 | 2269.38 | 947.87 |
| 332.57 | 74.12 | 2852.50 | 692.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 328.37 | 66.10 | 2852.50 | 671.50 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | M Sismica x g | Pos. GX | Pos. GY | E agg. X-X | E agg. Y-Y | Pos. KX | Pos. KY |
|---------|---------------|---------|---------|------------|------------|---------|---------|
| 324.89 | 78.03 | 2852.50 | 1074.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 324.17 | 67.98 | 2852.50 | 650.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 319.97 | 69.75 | 2852.50 | 629.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 316.00 | 2765.00 | 2191.62 | 0.0 | 0.0 | 0.0 | 2191.70 | 0.0 |
| 315.76 | 71.52 | 2852.50 | 608.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 315.64 | 82.40 | 2852.50 | 1097.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 311.56 | 73.62 | 2852.50 | 587.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 311.00 | 8702.14 | 1532.31 | 928.73 | 0.0 | -68.85 | 1921.93 | 947.88 |
| 307.36 | 65.75 | 2852.50 | 566.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 306.39 | 88.01 | 2852.50 | 1120.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 303.16 | 70.00 | 2852.50 | 545.50 | 0.0 | 0.0 | 0.0 | 0.0 |
| 298.66 | 44.03 | 2852.50 | 523.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 297.14 | 45.07 | 2852.50 | 1143.00 | 0.0 | 0.0 | 0.0 | 0.0 |
| 289.00 | 8576.77 | 1528.44 | 932.44 | 0.0 | -68.85 | 1957.81 | 947.90 |
| 267.00 | 7305.10 | 1549.29 | 948.82 | 0.0 | -68.85 | 2272.93 | 957.53 |
| 244.00 | 5731.32 | 1599.36 | 943.06 | 0.0 | -68.85 | 2273.25 | 957.49 |
| 220.00 | 5853.26 | 1599.36 | 943.06 | 0.0 | -68.85 | 2273.25 | 957.49 |
| 196.00 | 5853.26 | 1599.36 | 943.06 | 0.0 | -68.85 | 2273.25 | 957.49 |
| 172.00 | 5510.21 | 1573.32 | 939.97 | 0.0 | -68.85 | 2255.19 | 954.31 |
| 152.00 | 5167.15 | 1543.81 | 936.46 | 0.0 | -68.85 | 2255.19 | 954.31 |
| 132.00 | 5167.15 | 1543.81 | 936.46 | 0.0 | -68.85 | 2255.19 | 954.31 |
| 112.00 | 5167.15 | 1543.81 | 936.46 | 0.0 | -68.85 | 2255.19 | 954.31 |
| 92.00 | 5970.76 | 1548.60 | 981.05 | 0.0 | -68.85 | 2254.72 | 1011.72 |
| 69.00 | 6774.37 | 1552.25 | 1015.06 | 0.0 | -68.85 | 2254.72 | 1011.72 |
| 46.00 | 6774.37 | 1552.25 | 1015.06 | 0.0 | -68.85 | 2254.72 | 1011.72 |
| 23.00 | 6774.37 | 1552.26 | 1015.06 | 0.0 | -68.85 | 2254.72 | 1011.72 |
| 0.0 | 2.150e+04 | 1667.13 | 781.77 | 0.0 | -80.62 | 1900.03 | 923.97 |
| Risulta | 3.177e+05 | | | | | | |

| CDC | Tipo | Sigla Id | Note |
|-----|------|---|---|
| 13 | Edk | CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +) | |
| | | | categoria suolo: B |
| | | | fattore di sito S = 1.200 |
| | | | ordinata spettro (tratto Tb-Tc) = 0.188 g |
| | | | angolo di ingresso:0.0 |
| | | | eccentricità aggiuntiva: positiva |
| | | | periodo proprio T1: 0.055 sec. |
| | | | numero di modi considerati:100 |
| | | | combinaz. modale: CQC |

Analisi Dinamica e Spettro di Risposta x-x ecc⁺ - SLD

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X | % | M efficace Y | % | M efficace Z | % |
|------|-----------|---------|----------------|--------------|----------|--------------|----------|--------------|----------|
| | Hz | sec | g | x g | | x g | | x g | |
| 1 | 7.651 | 0.131 | 0.188 | 1.757e+04 | 5.5 | 18.14 | 5.71e-03 | 100.30 | 3.16e-02 |
| 2 | 8.344 | 0.120 | 0.183 | 1.195e+04 | 3.8 | 0.29 | 9.23e-05 | 509.24 | 0.2 |
| 3 | 9.116 | 0.110 | 0.174 | 2.196e+04 | 6.9 | 11.82 | 3.72e-03 | 0.63 | 1.99e-04 |
| 4 | 11.020 | 0.091 | 0.157 | 1222.37 | 0.4 | 1.083e+04 | 3.4 | 500.78 | 0.2 |
| 5 | 11.340 | 0.088 | 0.155 | 122.57 | 3.86e-02 | 1.182e+05 | 37.2 | 154.57 | 4.86e-02 |
| 6 | 11.807 | 0.085 | 0.151 | 3292.50 | 1.0 | 814.84 | 0.3 | 456.60 | 0.1 |
| 7 | 12.623 | 0.079 | 0.147 | 2.861e+04 | 9.0 | 11.67 | 3.67e-03 | 10.36 | 3.26e-03 |
| 8 | 13.434 | 0.074 | 0.142 | 643.49 | 0.2 | 2.699e+04 | 8.5 | 46.15 | 1.45e-02 |
| 9 | 13.983 | 0.072 | 0.140 | 3.545e+04 | 11.2 | 804.83 | 0.3 | 3.08 | 9.70e-04 |
| 10 | 14.774 | 0.068 | 0.136 | 96.86 | 3.05e-02 | 4.307e+04 | 13.6 | 34.62 | 1.09e-02 |
| 11 | 16.418 | 0.061 | 0.130 | 326.65 | 0.1 | 1.348e+04 | 4.2 | 10.60 | 3.34e-03 |
| 12 | 16.663 | 0.060 | 0.129 | 8263.59 | 2.6 | 271.01 | 8.53e-02 | 3.07 | 9.65e-04 |
| 13 | 17.095 | 0.058 | 0.128 | 50.15 | 1.58e-02 | 3998.78 | 1.3 | 13.78 | 4.34e-03 |
| 14 | 17.336 | 0.058 | 0.127 | 4346.96 | 1.4 | 5939.18 | 1.9 | 5.06 | 1.59e-03 |
| 15 | 17.515 | 0.057 | 0.127 | 403.22 | 0.1 | 5608.19 | 1.8 | 6.54 | 2.06e-03 |
| 16 | 18.016 | 0.056 | 0.125 | 348.38 | 0.1 | 1.787e+04 | 5.6 | 0.07 | 2.23e-05 |
| 17 | 18.283 | 0.055 | 0.125 | 4.182e+04 | 13.2 | 131.44 | 4.14e-02 | 13.57 | 4.27e-03 |
| 18 | 18.486 | 0.054 | 0.124 | 414.88 | 0.1 | 5825.20 | 1.8 | 14.51 | 4.57e-03 |
| 19 | 19.064 | 0.052 | 0.123 | 4165.79 | 1.3 | 88.66 | 2.79e-02 | 6.52 | 2.05e-03 |
| 20 | 19.108 | 0.052 | 0.122 | 6912.37 | 2.2 | 1258.77 | 0.4 | 281.44 | 8.86e-02 |
| 21 | 20.176 | 0.050 | 0.120 | 164.76 | 5.18e-02 | 1585.86 | 0.5 | 14.27 | 4.49e-03 |
| 22 | 20.391 | 0.049 | 0.120 | 793.49 | 0.2 | 1565.44 | 0.5 | 1.39 | 4.38e-04 |
| 23 | 20.608 | 0.049 | 0.119 | 34.17 | 1.08e-02 | 1437.37 | 0.5 | 19.11 | 6.01e-03 |
| 24 | 20.995 | 0.048 | 0.118 | 920.03 | 0.3 | 1252.59 | 0.4 | 67.76 | 2.13e-02 |
| 25 | 21.000 | 0.048 | 0.118 | 3926.51 | 1.2 | 2297.39 | 0.7 | 0.40 | 1.26e-04 |

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|------|-----------|---------|----------------|---------------------|----------|---------------------|----------|---------------------|----------|
| 26 | 21.736 | 0.046 | 0.117 | 2762.90 | 0.9 | 63.87 | 2.01e-02 | 33.23 | 1.05e-02 |
| 27 | 22.060 | 0.045 | 0.116 | 2466.57 | 0.8 | 196.44 | 6.18e-02 | 42.61 | 1.34e-02 |
| 28 | 22.190 | 0.045 | 0.116 | 753.45 | 0.2 | 1466.64 | 0.5 | 4.60 | 1.45e-03 |
| 29 | 23.518 | 0.043 | 0.114 | 7.62 | 2.40e-03 | 13.78 | 4.34e-03 | 1.70 | 5.36e-04 |
| 30 | 23.769 | 0.042 | 0.113 | 212.67 | 6.69e-02 | 119.06 | 3.75e-02 | 8.90 | 2.80e-03 |
| 31 | 23.901 | 0.042 | 0.113 | 91.96 | 2.89e-02 | 0.40 | 1.25e-04 | 0.68 | 2.13e-04 |
| 32 | 24.054 | 0.042 | 0.113 | 3474.41 | 1.1 | 29.74 | 9.36e-03 | 301.58 | 9.49e-02 |
| 33 | 24.685 | 0.041 | 0.112 | 1296.68 | 0.4 | 87.53 | 2.75e-02 | 63.80 | 2.01e-02 |
| 34 | 24.873 | 0.040 | 0.112 | 547.32 | 0.2 | 308.25 | 9.70e-02 | 6.03 | 1.90e-03 |
| 35 | 25.320 | 0.039 | 0.111 | 16.28 | 5.12e-03 | 1399.45 | 0.4 | 470.80 | 0.1 |
| 36 | 26.198 | 0.038 | 0.110 | 758.52 | 0.2 | 2012.67 | 0.6 | 806.45 | 0.3 |
| 37 | 26.393 | 0.038 | 0.110 | 114.53 | 3.60e-02 | 145.64 | 4.58e-02 | 140.05 | 4.41e-02 |
| 38 | 26.734 | 0.037 | 0.109 | 156.72 | 4.93e-02 | 39.65 | 1.25e-02 | 2.55 | 8.04e-04 |
| 39 | 27.595 | 0.036 | 0.108 | 3010.38 | 0.9 | 394.62 | 0.1 | 5.13 | 1.62e-03 |
| 40 | 27.993 | 0.036 | 0.108 | 334.10 | 0.1 | 21.69 | 6.83e-03 | 3.68 | 1.16e-03 |
| 41 | 28.610 | 0.035 | 0.107 | 3.06 | 9.63e-04 | 76.18 | 2.40e-02 | 129.47 | 4.07e-02 |
| 42 | 28.653 | 0.035 | 0.107 | 60.61 | 1.91e-02 | 70.41 | 2.22e-02 | 598.36 | 0.2 |
| 43 | 28.848 | 0.035 | 0.107 | 2.784e+04 | 8.8 | 65.92 | 2.07e-02 | 667.89 | 0.2 |
| 44 | 29.399 | 0.034 | 0.106 | 1034.95 | 0.3 | 81.11 | 2.55e-02 | 24.40 | 7.68e-03 |
| 45 | 29.952 | 0.033 | 0.106 | 898.65 | 0.3 | 13.66 | 4.30e-03 | 21.89 | 6.89e-03 |
| 46 | 30.151 | 0.033 | 0.105 | 58.17 | 1.83e-02 | 383.61 | 0.1 | 1.19e-05 | 0.0 |
| 47 | 30.254 | 0.033 | 0.105 | 825.81 | 0.3 | 8.18 | 2.57e-03 | 6.77 | 2.13e-03 |
| 48 | 30.762 | 0.033 | 0.105 | 1.89 | 5.96e-04 | 184.16 | 5.80e-02 | 1.885e+04 | 5.9 |
| 49 | 31.190 | 0.032 | 0.104 | 0.03 | 9.14e-06 | 17.08 | 5.37e-03 | 233.52 | 7.35e-02 |
| 50 | 31.598 | 0.032 | 0.104 | 562.44 | 0.2 | 1292.02 | 0.4 | 1.322e+04 | 4.2 |
| 51 | 32.437 | 0.031 | 0.103 | 125.37 | 3.95e-02 | 1810.29 | 0.6 | 1.418e+04 | 4.5 |
| 52 | 33.084 | 0.030 | 0.103 | 99.12 | 3.12e-02 | 99.68 | 3.14e-02 | 1501.88 | 0.5 |
| 53 | 33.579 | 0.030 | 0.102 | 108.51 | 3.41e-02 | 1038.23 | 0.3 | 7566.20 | 2.4 |
| 54 | 34.223 | 0.029 | 0.102 | 1045.68 | 0.3 | 0.20 | 6.40e-05 | 998.98 | 0.3 |
| 55 | 34.825 | 0.029 | 0.101 | 146.12 | 4.60e-02 | 1258.56 | 0.4 | 1936.99 | 0.6 |
| 56 | 35.668 | 0.028 | 0.101 | 150.48 | 4.74e-02 | 1.11 | 3.48e-04 | 26.84 | 8.45e-03 |
| 57 | 36.041 | 0.028 | 0.100 | 289.10 | 9.10e-02 | 16.30 | 5.13e-03 | 72.87 | 2.29e-02 |
| 58 | 36.608 | 0.027 | 0.100 | 7448.87 | 2.3 | 3.25 | 1.02e-03 | 1738.17 | 0.5 |
| 59 | 36.878 | 0.027 | 0.100 | 549.00 | 0.2 | 360.83 | 0.1 | 6135.34 | 1.9 |
| 60 | 37.173 | 0.027 | 0.100 | 35.85 | 1.13e-02 | 1565.05 | 0.5 | 860.65 | 0.3 |
| 61 | 37.453 | 0.027 | 0.100 | 1377.74 | 0.4 | 1.94 | 6.11e-04 | 324.86 | 0.1 |
| 62 | 38.187 | 0.026 | 0.099 | 1.322e+04 | 4.2 | 7.28 | 2.29e-03 | 2401.22 | 0.8 |
| 63 | 38.262 | 0.026 | 0.099 | 42.73 | 1.34e-02 | 147.07 | 4.63e-02 | 0.19 | 6.07e-05 |
| 64 | 38.627 | 0.026 | 0.099 | 12.67 | 3.99e-03 | 15.17 | 4.77e-03 | 534.31 | 0.2 |
| 65 | 38.794 | 0.026 | 0.099 | 1.05 | 3.31e-04 | 231.72 | 7.29e-02 | 309.08 | 9.73e-02 |
| 66 | 39.029 | 0.026 | 0.099 | 1124.05 | 0.4 | 15.09 | 4.75e-03 | 757.13 | 0.2 |
| 67 | 39.447 | 0.025 | 0.098 | 80.31 | 2.53e-02 | 166.52 | 5.24e-02 | 4.103e+04 | 12.9 |
| 68 | 39.491 | 0.025 | 0.098 | 10.34 | 3.25e-03 | 14.58 | 4.59e-03 | 1206.85 | 0.4 |
| 69 | 39.745 | 0.025 | 0.098 | 1109.58 | 0.3 | 67.77 | 2.13e-02 | 693.74 | 0.2 |
| 70 | 39.865 | 0.025 | 0.098 | 2007.58 | 0.6 | 1.42 | 4.48e-04 | 9024.82 | 2.8 |
| 71 | 39.969 | 0.025 | 0.098 | 10.72 | 3.37e-03 | 633.06 | 0.2 | 2421.48 | 0.8 |
| 72 | 40.374 | 0.025 | 0.098 | 162.35 | 5.11e-02 | 692.82 | 0.2 | 140.28 | 4.41e-02 |
| 73 | 40.917 | 0.024 | 0.097 | 21.44 | 6.75e-03 | 1.83 | 5.75e-04 | 1214.40 | 0.4 |
| 74 | 41.602 | 0.024 | 0.097 | 0.02 | 5.54e-06 | 258.42 | 8.13e-02 | 842.16 | 0.3 |
| 75 | 41.861 | 0.024 | 0.097 | 811.94 | 0.3 | 20.88 | 6.57e-03 | 1506.61 | 0.5 |
| 76 | 42.459 | 0.024 | 0.097 | 0.64 | 2.01e-04 | 13.55 | 4.27e-03 | 16.30 | 5.13e-03 |
| 77 | 42.687 | 0.023 | 0.097 | 493.10 | 0.2 | 165.90 | 5.22e-02 | 4417.68 | 1.4 |
| 78 | 42.801 | 0.023 | 0.097 | 816.69 | 0.3 | 381.79 | 0.1 | 9736.04 | 3.1 |
| 79 | 42.865 | 0.023 | 0.096 | 4.20 | 1.32e-03 | 5.40e-04 | 0.0 | 75.37 | 2.37e-02 |
| 80 | 43.319 | 0.023 | 0.096 | 26.36 | 8.29e-03 | 270.20 | 8.50e-02 | 6214.05 | 2.0 |
| 81 | 44.061 | 0.023 | 0.096 | 225.08 | 7.08e-02 | 46.99 | 1.48e-02 | 4607.28 | 1.4 |
| 82 | 44.279 | 0.023 | 0.096 | 124.28 | 3.91e-02 | 9.19 | 2.89e-03 | 267.84 | 8.43e-02 |
| 83 | 44.394 | 0.023 | 0.096 | 2.39 | 7.51e-04 | 656.26 | 0.2 | 0.15 | 4.85e-05 |
| 84 | 44.703 | 0.022 | 0.096 | 69.26 | 2.18e-02 | 108.08 | 3.40e-02 | 357.81 | 0.1 |
| 85 | 44.910 | 0.022 | 0.096 | 7.06 | 2.22e-03 | 3.78 | 1.19e-03 | 158.45 | 4.99e-02 |
| 86 | 45.247 | 0.022 | 0.095 | 9.41 | 2.96e-03 | 89.55 | 2.82e-02 | 3.88 | 1.22e-03 |
| 87 | 45.419 | 0.022 | 0.095 | 43.23 | 1.36e-02 | 236.06 | 7.43e-02 | 2947.57 | 0.9 |
| 88 | 46.181 | 0.022 | 0.095 | 9.27 | 2.92e-03 | 300.76 | 9.47e-02 | 60.91 | 1.92e-02 |
| 89 | 46.323 | 0.022 | 0.095 | 30.58 | 9.62e-03 | 822.95 | 0.3 | 68.17 | 2.15e-02 |
| 90 | 46.533 | 0.021 | 0.095 | 165.55 | 5.21e-02 | 12.88 | 4.05e-03 | 54.62 | 1.72e-02 |
| 91 | 47.453 | 0.021 | 0.094 | 0.55 | 1.74e-04 | 61.06 | 1.92e-02 | 40.11 | 1.26e-02 |
| 92 | 47.783 | 0.021 | 0.094 | 479.08 | 0.2 | 300.68 | 9.46e-02 | 5.50 | 1.73e-03 |
| 93 | 48.095 | 0.021 | 0.094 | 95.67 | 3.01e-02 | 74.18 | 2.33e-02 | 174.43 | 5.49e-02 |
| 94 | 48.416 | 0.021 | 0.094 | 144.51 | 4.55e-02 | 152.09 | 4.79e-02 | 1180.96 | 0.4 |
| 95 | 48.474 | 0.021 | 0.094 | 10.00 | 3.15e-03 | 1.06 | 3.33e-04 | 80.43 | 2.53e-02 |

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|----------------|-----------|---------|----------------|---------------------|----------|---------------------|----------|---------------------|----------|
| 96 | 49.030 | 0.020 | 0.094 | 55.39 | 1.74e-02 | 27.72 | 8.73e-03 | 132.09 | 4.16e-02 |
| 97 | 49.470 | 0.020 | 0.094 | 846.19 | 0.3 | 1.91 | 6.03e-04 | 203.05 | 6.39e-02 |
| 98 | 49.830 | 0.020 | 0.094 | 123.09 | 3.87e-02 | 1.57e-03 | 0.0 | 413.92 | 0.1 |
| 99 | 50.825 | 0.020 | 0.093 | 55.46 | 1.75e-02 | 1.10 | 3.48e-04 | 1167.30 | 0.4 |
| 100 | 51.012 | 0.020 | 0.093 | 11.56 | 3.64e-03 | 0.58 | 1.83e-04 | 345.82 | 0.1 |
| Risulta | | | | 2.749e+05 | | 2.840e+05 | | 1.681e+05 | |
| In percentuale | | | | 86.52 | | 89.38 | | 52.90 | |

• **Caso di carico sisma x-x ecc - SLD**

| CDC | Tipo | Sigla Id | Note |
|-----|------|---|---|
| 14 | Eck | CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -) | |
| | | | categoria suolo: B |
| | | | fattore di sito S = 1.200 |
| | | | ordinata spettro (tratto Tb-Tc) = 0.188 g |
| | | | angolo di ingresso:0.0 |
| | | | eccentricità aggiuntiva: negativa |
| | | | periodo proprio T1: 0.072 sec. |
| | | | numero di modi considerati:100 |
| | | | combinaz. modale: CQC |

Analisi Dinamica e Spettro di Risposta x-x ecc- - SLD

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|------|-----------|---------|----------------|---------------------|----------|---------------------|----------|---------------------|----------|
| | Hz | sec | g | daN | | daN | | daN | |
| 1 | 7.627 | 0.131 | 0.188 | 1.599e+04 | 5.0 | 12.39 | 3.90e-03 | 132.01 | 4.15e-02 |
| 2 | 8.369 | 0.119 | 0.183 | 1.408e+04 | 4.4 | 0.23 | 7.29e-05 | 467.33 | 0.1 |
| 3 | 9.121 | 0.110 | 0.174 | 2.123e+04 | 6.7 | 12.05 | 3.79e-03 | 0.59 | 1.85e-04 |
| 4 | 10.971 | 0.091 | 0.157 | 972.82 | 0.3 | 9176.71 | 2.9 | 402.71 | 0.1 |
| 5 | 11.339 | 0.088 | 0.155 | 14.75 | 4.64e-03 | 1.182e+05 | 37.2 | 163.02 | 5.13e-02 |
| 6 | 11.561 | 0.087 | 0.153 | 2872.60 | 0.9 | 2414.60 | 0.8 | 522.13 | 0.2 |
| 7 | 12.496 | 0.080 | 0.147 | 2.657e+04 | 8.4 | 18.72 | 5.89e-03 | 8.28 | 2.60e-03 |
| 8 | 13.433 | 0.074 | 0.142 | 852.80 | 0.3 | 2.698e+04 | 8.5 | 45.70 | 1.44e-02 |
| 9 | 13.926 | 0.072 | 0.140 | 3.723e+04 | 11.7 | 835.50 | 0.3 | 7.56 | 2.38e-03 |
| 10 | 14.775 | 0.068 | 0.136 | 25.45 | 8.01e-03 | 4.314e+04 | 13.6 | 35.32 | 1.11e-02 |
| 11 | 16.426 | 0.061 | 0.130 | 7.82 | 2.46e-03 | 1.368e+04 | 4.3 | 9.37 | 2.95e-03 |
| 12 | 16.687 | 0.060 | 0.129 | 7678.83 | 2.4 | 5.44 | 1.71e-03 | 1.02 | 3.22e-04 |
| 13 | 17.108 | 0.058 | 0.128 | 97.73 | 3.08e-02 | 4578.41 | 1.4 | 14.95 | 4.71e-03 |
| 14 | 17.398 | 0.057 | 0.127 | 1630.35 | 0.5 | 8576.65 | 2.7 | 2.36 | 7.44e-04 |
| 15 | 17.573 | 0.057 | 0.127 | 891.72 | 0.3 | 1991.90 | 0.6 | 9.12 | 2.87e-03 |
| 16 | 18.038 | 0.055 | 0.125 | 247.92 | 7.80e-02 | 1.824e+04 | 5.7 | 4.64 | 1.46e-03 |
| 17 | 18.092 | 0.055 | 0.125 | 2.040e+04 | 6.4 | 140.84 | 4.43e-02 | 59.49 | 1.87e-02 |
| 18 | 18.489 | 0.054 | 0.124 | 188.90 | 5.94e-02 | 6581.91 | 2.1 | 15.54 | 4.89e-03 |
| 19 | 18.853 | 0.053 | 0.123 | 2.003e+04 | 6.3 | 30.77 | 9.68e-03 | 11.30 | 3.56e-03 |
| 20 | 19.269 | 0.052 | 0.122 | 1.382e+04 | 4.3 | 389.02 | 0.1 | 306.48 | 9.65e-02 |
| 21 | 20.190 | 0.050 | 0.120 | 492.51 | 0.2 | 1297.23 | 0.4 | 4.88 | 1.53e-03 |
| 22 | 20.385 | 0.049 | 0.120 | 1198.49 | 0.4 | 1983.13 | 0.6 | 2.56 | 8.07e-04 |
| 23 | 20.607 | 0.049 | 0.119 | 35.07 | 1.10e-02 | 1585.66 | 0.5 | 13.92 | 4.38e-03 |
| 24 | 20.943 | 0.048 | 0.118 | 6197.31 | 2.0 | 3168.70 | 1.0 | 16.47 | 5.18e-03 |
| 25 | 21.163 | 0.047 | 0.118 | 254.33 | 8.00e-02 | 291.63 | 9.18e-02 | 20.44 | 6.43e-03 |
| 26 | 21.676 | 0.046 | 0.117 | 500.70 | 0.2 | 43.55 | 1.37e-02 | 10.11 | 3.18e-03 |
| 27 | 21.968 | 0.046 | 0.116 | 4488.16 | 1.4 | 30.13 | 9.48e-03 | 34.22 | 1.08e-02 |
| 28 | 22.182 | 0.045 | 0.116 | 271.24 | 8.54e-02 | 1608.31 | 0.5 | 18.61 | 5.86e-03 |
| 29 | 23.516 | 0.043 | 0.114 | 0.51 | 1.60e-04 | 10.54 | 3.32e-03 | 1.65 | 5.20e-04 |
| 30 | 23.694 | 0.042 | 0.113 | 122.65 | 3.86e-02 | 102.54 | 3.23e-02 | 0.94 | 2.94e-04 |
| 31 | 23.905 | 0.042 | 0.113 | 0.90 | 2.84e-04 | 8.87 | 2.79e-03 | 5.17 | 1.63e-03 |
| 32 | 24.741 | 0.040 | 0.112 | 427.35 | 0.1 | 317.06 | 9.98e-02 | 10.46 | 3.29e-03 |
| 33 | 24.859 | 0.040 | 0.112 | 135.38 | 4.26e-02 | 206.59 | 6.50e-02 | 0.98 | 3.07e-04 |
| 34 | 25.284 | 0.040 | 0.111 | 482.51 | 0.2 | 1038.15 | 0.3 | 11.28 | 3.55e-03 |
| 35 | 25.433 | 0.039 | 0.111 | 1207.72 | 0.4 | 280.52 | 8.83e-02 | 1111.43 | 0.3 |
| 36 | 26.202 | 0.038 | 0.110 | 525.59 | 0.2 | 2000.20 | 0.6 | 923.59 | 0.3 |
| 37 | 26.394 | 0.038 | 0.110 | 87.31 | 2.75e-02 | 108.56 | 3.42e-02 | 170.31 | 5.36e-02 |
| 38 | 26.727 | 0.037 | 0.109 | 336.81 | 0.1 | 69.76 | 2.20e-02 | 2.85 | 8.96e-04 |
| 39 | 27.516 | 0.036 | 0.108 | 671.86 | 0.2 | 33.64 | 1.06e-02 | 5.48 | 1.72e-03 |
| 40 | 27.661 | 0.036 | 0.108 | 1130.36 | 0.4 | 442.99 | 0.1 | 3.12 | 9.82e-04 |
| 41 | 28.590 | 0.035 | 0.107 | 54.56 | 1.72e-02 | 58.88 | 1.85e-02 | 281.04 | 8.84e-02 |
| 42 | 28.654 | 0.035 | 0.107 | 132.14 | 4.16e-02 | 76.75 | 2.42e-02 | 569.16 | 0.2 |
| 43 | 28.913 | 0.035 | 0.107 | 12.16 | 3.83e-03 | 1.50 | 4.71e-04 | 17.50 | 5.51e-03 |

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|----------------|-----------|---------|----------------|------------------|----------|------------------|----------|------------------|----------|
| 44 | 29.373 | 0.034 | 0.106 | 102.77 | 3.23e-02 | 110.34 | 3.47e-02 | 4.46 | 1.41e-03 |
| 45 | 30.095 | 0.033 | 0.105 | 16.05 | 5.05e-03 | 333.19 | 0.1 | 6.02 | 1.90e-03 |
| 46 | 30.571 | 0.033 | 0.105 | 8672.95 | 2.7 | 0.03 | 8.23e-06 | 3167.78 | 1.0 |
| 47 | 30.940 | 0.032 | 0.105 | 2324.08 | 0.7 | 428.94 | 0.1 | 2.427e+04 | 7.6 |
| 48 | 31.229 | 0.032 | 0.104 | 1327.61 | 0.4 | 240.66 | 7.57e-02 | 2030.44 | 0.6 |
| 49 | 31.817 | 0.031 | 0.104 | 1.154e+04 | 3.6 | 642.09 | 0.2 | 197.86 | 6.23e-02 |
| 50 | 32.067 | 0.031 | 0.104 | 1.226e+04 | 3.9 | 899.65 | 0.3 | 79.07 | 2.49e-02 |
| 51 | 32.630 | 0.031 | 0.103 | 221.70 | 6.98e-02 | 1156.94 | 0.4 | 1.352e+04 | 4.3 |
| 52 | 32.904 | 0.030 | 0.103 | 636.21 | 0.2 | 6.42e-03 | 2.02e-06 | 378.19 | 0.1 |
| 53 | 33.096 | 0.030 | 0.103 | 5344.24 | 1.7 | 63.40 | 2.00e-02 | 455.67 | 0.1 |
| 54 | 33.229 | 0.030 | 0.103 | 1.627e+04 | 5.1 | 85.92 | 2.70e-02 | 2339.48 | 0.7 |
| 55 | 33.641 | 0.030 | 0.102 | 1909.44 | 0.6 | 892.77 | 0.3 | 1.201e+04 | 3.8 |
| 56 | 34.848 | 0.029 | 0.101 | 207.61 | 6.53e-02 | 1338.04 | 0.4 | 3050.44 | 1.0 |
| 57 | 35.670 | 0.028 | 0.101 | 186.95 | 5.88e-02 | 0.32 | 1.01e-04 | 200.17 | 6.30e-02 |
| 58 | 36.050 | 0.028 | 0.100 | 2.39 | 7.53e-04 | 9.22 | 2.90e-03 | 8.36 | 2.63e-03 |
| 59 | 36.410 | 0.027 | 0.100 | 742.74 | 0.2 | 33.70 | 1.06e-02 | 138.96 | 4.37e-02 |
| 60 | 36.669 | 0.027 | 0.100 | 642.77 | 0.2 | 19.56 | 6.16e-03 | 4617.70 | 1.5 |
| 61 | 37.116 | 0.027 | 0.100 | 0.06 | 1.81e-05 | 1876.42 | 0.6 | 0.11 | 3.37e-05 |
| 62 | 37.648 | 0.027 | 0.099 | 1293.23 | 0.4 | 6.38 | 2.01e-03 | 3.17 | 9.97e-04 |
| 63 | 38.259 | 0.026 | 0.099 | 46.63 | 1.47e-02 | 151.45 | 4.77e-02 | 39.79 | 1.25e-02 |
| 64 | 38.597 | 0.026 | 0.099 | 448.11 | 0.1 | 2.18 | 6.87e-04 | 501.45 | 0.2 |
| 65 | 38.684 | 0.026 | 0.099 | 866.06 | 0.3 | 62.10 | 1.95e-02 | 1175.33 | 0.4 |
| 66 | 38.805 | 0.026 | 0.099 | 13.07 | 4.11e-03 | 179.08 | 5.64e-02 | 0.23 | 7.30e-05 |
| 67 | 38.981 | 0.026 | 0.099 | 52.82 | 1.66e-02 | 33.71 | 1.06e-02 | 1840.80 | 0.6 |
| 68 | 39.476 | 0.025 | 0.098 | 290.88 | 9.15e-02 | 164.70 | 5.18e-02 | 4.894e+04 | 15.4 |
| 69 | 39.934 | 0.025 | 0.098 | 10.16 | 3.20e-03 | 714.18 | 0.2 | 1624.16 | 0.5 |
| 70 | 40.001 | 0.025 | 0.098 | 80.17 | 2.52e-02 | 3.90 | 1.23e-03 | 5620.03 | 1.8 |
| 71 | 40.250 | 0.025 | 0.098 | 209.85 | 6.60e-02 | 496.98 | 0.2 | 707.78 | 0.2 |
| 72 | 40.976 | 0.024 | 0.097 | 892.09 | 0.3 | 539.57 | 0.2 | 1320.47 | 0.4 |
| 73 | 41.584 | 0.024 | 0.097 | 10.98 | 3.46e-03 | 3.43 | 1.08e-03 | 404.19 | 0.1 |
| 74 | 42.403 | 0.024 | 0.097 | 60.90 | 1.92e-02 | 32.17 | 1.01e-02 | 0.12 | 3.88e-05 |
| 75 | 42.633 | 0.023 | 0.097 | 522.12 | 0.2 | 316.34 | 9.96e-02 | 8953.23 | 2.8 |
| 76 | 42.750 | 0.023 | 0.097 | 130.73 | 4.11e-02 | 206.56 | 6.50e-02 | 6756.18 | 2.1 |
| 77 | 42.866 | 0.023 | 0.096 | 0.53 | 1.65e-04 | 2.34 | 7.36e-04 | 7.46 | 2.35e-03 |
| 78 | 43.351 | 0.023 | 0.096 | 121.10 | 3.81e-02 | 219.38 | 6.90e-02 | 7590.36 | 2.4 |
| 79 | 43.984 | 0.023 | 0.096 | 7.21 | 2.27e-03 | 11.68 | 3.68e-03 | 2427.42 | 0.8 |
| 80 | 44.302 | 0.023 | 0.096 | 15.06 | 4.74e-03 | 121.11 | 3.81e-02 | 563.67 | 0.2 |
| 81 | 44.546 | 0.022 | 0.096 | 6.33 | 1.99e-03 | 677.54 | 0.2 | 52.01 | 1.64e-02 |
| 82 | 44.901 | 0.022 | 0.096 | 463.04 | 0.1 | 47.99 | 1.51e-02 | 607.11 | 0.2 |
| 83 | 44.997 | 0.022 | 0.096 | 593.79 | 0.2 | 38.31 | 1.21e-02 | 220.02 | 6.92e-02 |
| 84 | 45.243 | 0.022 | 0.095 | 19.00 | 5.98e-03 | 27.86 | 8.77e-03 | 334.05 | 0.1 |
| 85 | 45.476 | 0.022 | 0.095 | 38.61 | 1.22e-02 | 426.75 | 0.1 | 2085.35 | 0.7 |
| 86 | 45.810 | 0.022 | 0.095 | 5.30 | 1.67e-03 | 20.89 | 6.57e-03 | 10.31 | 3.24e-03 |
| 87 | 45.933 | 0.022 | 0.095 | 14.62 | 4.60e-03 | 22.46 | 7.07e-03 | 78.70 | 2.48e-02 |
| 88 | 46.176 | 0.022 | 0.095 | 100.11 | 3.15e-02 | 355.89 | 0.1 | 144.57 | 4.55e-02 |
| 89 | 46.254 | 0.022 | 0.095 | 1.38 | 4.33e-04 | 10.65 | 3.35e-03 | 4.10 | 1.29e-03 |
| 90 | 46.434 | 0.022 | 0.095 | 1013.16 | 0.3 | 1.22 | 3.83e-04 | 84.11 | 2.65e-02 |
| 91 | 46.534 | 0.021 | 0.095 | 43.38 | 1.37e-02 | 515.62 | 0.2 | 36.54 | 1.15e-02 |
| 92 | 47.562 | 0.021 | 0.094 | 306.18 | 9.64e-02 | 266.87 | 8.40e-02 | 87.01 | 2.74e-02 |
| 93 | 48.047 | 0.021 | 0.094 | 7.16 | 2.25e-03 | 20.31 | 6.39e-03 | 185.18 | 5.83e-02 |
| 94 | 48.175 | 0.021 | 0.094 | 31.24 | 9.83e-03 | 170.29 | 5.36e-02 | 697.62 | 0.2 |
| 95 | 48.268 | 0.021 | 0.094 | 170.04 | 5.35e-02 | 43.33 | 1.36e-02 | 500.63 | 0.2 |
| 96 | 48.388 | 0.021 | 0.094 | 19.87 | 6.25e-03 | 132.80 | 4.18e-02 | 572.50 | 0.2 |
| 97 | 48.523 | 0.021 | 0.094 | 4.92 | 1.55e-03 | 2.19 | 6.90e-04 | 34.80 | 1.10e-02 |
| 98 | 50.927 | 0.020 | 0.093 | 22.78 | 7.17e-03 | 1.42 | 4.47e-04 | 275.83 | 8.68e-02 |
| 99 | 50.995 | 0.020 | 0.093 | 19.36 | 6.09e-03 | 0.10 | 3.19e-05 | 741.76 | 0.2 |
| 100 | 51.061 | 0.020 | 0.093 | 67.51 | 2.12e-02 | 0.89 | 2.80e-04 | 355.80 | 0.1 |
| Risulta | | | | 2.740e+05 | | 2.840e+05 | | 1.675e+05 | |
| In percentuale | | | | 86.24 | | 89.38 | | 52.72 | |

• **Caso di carico sisma y-y ecc+– SLD**

| CDC | Tipo | Sigla Id | Note |
|-----|------|---|---|
| 15 | Edk | CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +) | |
| | | | categoria suolo: B |
| | | | fattore di sito S = 1.200 |
| | | | ordinata spettro (tratto Tb-Tc) = 0.188 g |
| | | | angolo di ingresso:90.00 |
| | | | eccentricità aggiuntiva: positiva |
| | | | periodo proprio T1: 0.088 sec. |
| | | | numero di modi considerati:100 |
| | | | combinaz. modale: CQC |

Analisi Dinamica e Spettro di Risposta y-y ecc+ - SLD

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|------|-----------|---------|----------------|------------------|----------|------------------|----------|------------------|----------|
| | Hz | sec | g | daN | | daN | | daN | |
| 1 | 7.645 | 0.131 | 0.188 | 1.640e+04 | 5.2 | 16.03 | 5.05e-03 | 122.68 | 3.86e-02 |
| 2 | 8.325 | 0.120 | 0.183 | 1.312e+04 | 4.1 | 6.15e-03 | 1.93e-06 | 483.10 | 0.2 |
| 3 | 9.115 | 0.110 | 0.174 | 2.174e+04 | 6.8 | 1.14e-06 | 0.0 | 0.74 | 2.34e-04 |
| 4 | 10.988 | 0.091 | 0.157 | 1127.52 | 0.4 | 1.089e+04 | 3.4 | 428.62 | 0.1 |
| 5 | 11.312 | 0.088 | 0.155 | 58.93 | 1.85e-02 | 1.106e+05 | 34.8 | 179.69 | 5.66e-02 |
| 6 | 11.675 | 0.086 | 0.152 | 2931.39 | 0.9 | 1550.55 | 0.5 | 484.56 | 0.2 |
| 7 | 12.567 | 0.080 | 0.147 | 2.779e+04 | 8.7 | 45.19 | 1.42e-02 | 10.85 | 3.42e-03 |
| 8 | 13.073 | 0.076 | 0.144 | 129.26 | 4.07e-02 | 1.982e+04 | 6.2 | 35.80 | 1.13e-02 |
| 9 | 13.949 | 0.072 | 0.140 | 3.675e+04 | 11.6 | 158.30 | 4.98e-02 | 2.40 | 7.54e-04 |
| 10 | 14.853 | 0.067 | 0.136 | 49.94 | 1.57e-02 | 4.367e+04 | 13.7 | 40.21 | 1.27e-02 |
| 11 | 15.823 | 0.063 | 0.132 | 542.87 | 0.2 | 2.721e+04 | 8.6 | 11.71 | 3.69e-03 |
| 12 | 16.397 | 0.061 | 0.130 | 2948.33 | 0.9 | 24.43 | 7.69e-03 | 2.34 | 7.38e-04 |
| 13 | 16.808 | 0.059 | 0.129 | 4681.53 | 1.5 | 203.09 | 6.39e-02 | 0.59 | 1.87e-04 |
| 14 | 16.900 | 0.059 | 0.129 | 5.37 | 1.69e-03 | 734.83 | 0.2 | 4.45 | 1.40e-03 |
| 15 | 17.286 | 0.058 | 0.127 | 399.91 | 0.1 | 3.061e+04 | 9.6 | 7.55 | 2.38e-03 |
| 16 | 17.496 | 0.057 | 0.127 | 2861.80 | 0.9 | 1562.59 | 0.5 | 13.63 | 4.29e-03 |
| 17 | 18.201 | 0.055 | 0.125 | 3.210e+04 | 10.1 | 23.87 | 7.51e-03 | 32.19 | 1.01e-02 |
| 18 | 18.944 | 0.053 | 0.123 | 1.265e+04 | 4.0 | 101.97 | 3.21e-02 | 17.59 | 5.54e-03 |
| 19 | 19.168 | 0.052 | 0.122 | 8101.58 | 2.5 | 3038.02 | 1.0 | 188.30 | 5.93e-02 |
| 20 | 19.542 | 0.051 | 0.121 | 372.70 | 0.1 | 1950.56 | 0.6 | 54.70 | 1.72e-02 |
| 21 | 19.551 | 0.051 | 0.121 | 2557.71 | 0.8 | 7784.45 | 2.4 | 74.47 | 2.34e-02 |
| 22 | 20.226 | 0.049 | 0.120 | 788.13 | 0.2 | 395.65 | 0.1 | 0.17 | 5.34e-05 |
| 23 | 20.295 | 0.049 | 0.120 | 2405.56 | 0.8 | 1213.25 | 0.4 | 11.12 | 3.50e-03 |
| 24 | 20.943 | 0.048 | 0.118 | 844.99 | 0.3 | 3027.92 | 1.0 | 36.77 | 1.16e-02 |
| 25 | 21.494 | 0.047 | 0.117 | 2985.88 | 0.9 | 52.03 | 1.64e-02 | 21.72 | 6.84e-03 |
| 26 | 21.666 | 0.046 | 0.117 | 522.12 | 0.2 | 69.97 | 2.20e-02 | 24.62 | 7.75e-03 |
| 27 | 21.915 | 0.046 | 0.116 | 1885.88 | 0.6 | 3.23 | 1.01e-03 | 56.66 | 1.78e-02 |
| 28 | 22.153 | 0.045 | 0.116 | 801.45 | 0.3 | 50.02 | 1.57e-02 | 34.38 | 1.08e-02 |
| 29 | 22.726 | 0.044 | 0.115 | 1242.48 | 0.4 | 133.51 | 4.20e-02 | 0.06 | 1.97e-05 |
| 30 | 24.092 | 0.042 | 0.113 | 230.41 | 7.25e-02 | 159.78 | 5.03e-02 | 32.71 | 1.03e-02 |
| 31 | 24.522 | 0.041 | 0.112 | 1820.70 | 0.6 | 31.09 | 9.78e-03 | 0.49 | 1.53e-04 |
| 32 | 24.613 | 0.041 | 0.112 | 609.54 | 0.2 | 2.82 | 8.88e-04 | 50.41 | 1.59e-02 |
| 33 | 24.757 | 0.040 | 0.112 | 915.99 | 0.3 | 23.75 | 7.48e-03 | 402.35 | 0.1 |
| 34 | 25.058 | 0.040 | 0.111 | 485.88 | 0.2 | 385.90 | 0.1 | 172.17 | 5.42e-02 |
| 35 | 25.445 | 0.039 | 0.111 | 6.18 | 1.94e-03 | 1089.99 | 0.3 | 66.94 | 2.11e-02 |
| 36 | 25.635 | 0.039 | 0.111 | 123.38 | 3.88e-02 | 1138.34 | 0.4 | 496.84 | 0.2 |
| 37 | 26.541 | 0.038 | 0.109 | 0.27 | 8.60e-05 | 0.29 | 9.04e-05 | 22.47 | 7.07e-03 |
| 38 | 28.046 | 0.036 | 0.108 | 174.87 | 5.50e-02 | 27.11 | 8.53e-03 | 345.18 | 0.1 |
| 39 | 28.217 | 0.035 | 0.107 | 921.05 | 0.3 | 215.22 | 6.77e-02 | 27.31 | 8.60e-03 |
| 40 | 28.345 | 0.035 | 0.107 | 1126.20 | 0.4 | 1.82 | 5.73e-04 | 24.04 | 7.57e-03 |
| 41 | 28.430 | 0.035 | 0.107 | 0.08 | 2.39e-05 | 9.84 | 3.10e-03 | 4.91 | 1.54e-03 |
| 42 | 28.552 | 0.035 | 0.107 | 0.47 | 1.48e-04 | 24.60 | 7.74e-03 | 804.24 | 0.3 |
| 43 | 29.344 | 0.034 | 0.106 | 54.15 | 1.70e-02 | 502.42 | 0.2 | 55.71 | 1.75e-02 |
| 44 | 29.842 | 0.034 | 0.106 | 2.573e+04 | 8.1 | 1.07 | 3.38e-04 | 2866.94 | 0.9 |
| 45 | 30.467 | 0.033 | 0.105 | 712.08 | 0.2 | 2240.33 | 0.7 | 6763.82 | 2.1 |
| 46 | 30.599 | 0.033 | 0.105 | 36.83 | 1.16e-02 | 112.41 | 3.54e-02 | 7.32 | 2.30e-03 |
| 47 | 30.845 | 0.032 | 0.105 | 2246.87 | 0.7 | 1613.41 | 0.5 | 6727.06 | 2.1 |
| 48 | 31.108 | 0.032 | 0.104 | 884.98 | 0.3 | 1937.73 | 0.6 | 5298.42 | 1.7 |
| 49 | 31.334 | 0.032 | 0.104 | 2636.50 | 0.8 | 2.64 | 8.31e-04 | 2369.80 | 0.7 |
| 50 | 31.979 | 0.031 | 0.104 | 187.96 | 5.92e-02 | 530.93 | 0.2 | 4901.62 | 1.5 |
| 51 | 32.021 | 0.031 | 0.104 | 240.85 | 7.58e-02 | 22.79 | 7.17e-03 | 1.451e+04 | 4.6 |
| 52 | 32.413 | 0.031 | 0.103 | 180.77 | 5.69e-02 | 3.43 | 1.08e-03 | 1229.79 | 0.4 |

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|----------------|-----------|---------|----------------|------------------|----------|------------------|----------|------------------|----------|
| 53 | 33.030 | 0.030 | 0.103 | 10.83 | 3.41e-03 | 307.60 | 9.68e-02 | 3068.12 | 1.0 |
| 54 | 33.493 | 0.030 | 0.102 | 975.19 | 0.3 | 0.50 | 1.59e-04 | 696.45 | 0.2 |
| 55 | 33.717 | 0.030 | 0.102 | 1249.92 | 0.4 | 534.68 | 0.2 | 6747.37 | 2.1 |
| 56 | 34.342 | 0.029 | 0.102 | 3093.18 | 1.0 | 160.81 | 5.06e-02 | 3523.63 | 1.1 |
| 57 | 35.057 | 0.029 | 0.101 | 4512.55 | 1.4 | 5.63 | 1.77e-03 | 191.86 | 6.04e-02 |
| 58 | 35.375 | 0.028 | 0.101 | 988.60 | 0.3 | 76.87 | 2.42e-02 | 47.61 | 1.50e-02 |
| 59 | 35.533 | 0.028 | 0.101 | 1.673e+04 | 5.3 | 2.25 | 7.08e-04 | 2207.28 | 0.7 |
| 60 | 36.762 | 0.027 | 0.100 | 234.09 | 7.37e-02 | 459.41 | 0.1 | 154.95 | 4.88e-02 |
| 61 | 36.951 | 0.027 | 0.100 | 890.45 | 0.3 | 1.66 | 5.22e-04 | 7045.75 | 2.2 |
| 62 | 37.368 | 0.027 | 0.100 | 462.39 | 0.1 | 292.19 | 9.20e-02 | 132.51 | 4.17e-02 |
| 63 | 37.870 | 0.026 | 0.099 | 58.33 | 1.84e-02 | 36.40 | 1.15e-02 | 532.17 | 0.2 |
| 64 | 38.778 | 0.026 | 0.099 | 0.04 | 1.25e-05 | 942.15 | 0.3 | 1.124e+04 | 3.5 |
| 65 | 39.295 | 0.025 | 0.098 | 7.16 | 2.25e-03 | 1238.78 | 0.4 | 1416.24 | 0.4 |
| 66 | 39.498 | 0.025 | 0.098 | 1342.92 | 0.4 | 0.02 | 5.85e-06 | 1033.57 | 0.3 |
| 67 | 39.733 | 0.025 | 0.098 | 11.51 | 3.62e-03 | 362.70 | 0.1 | 3570.32 | 1.1 |
| 68 | 39.903 | 0.025 | 0.098 | 308.45 | 9.71e-02 | 441.05 | 0.1 | 4.007e+04 | 12.6 |
| 69 | 40.273 | 0.025 | 0.098 | 4.75 | 1.50e-03 | 1.50 | 4.71e-04 | 56.38 | 1.77e-02 |
| 70 | 40.927 | 0.024 | 0.097 | 602.14 | 0.2 | 58.49 | 1.84e-02 | 1853.07 | 0.6 |
| 71 | 41.502 | 0.024 | 0.097 | 185.70 | 5.84e-02 | 23.10 | 7.27e-03 | 459.52 | 0.1 |
| 72 | 41.990 | 0.024 | 0.097 | 5.09 | 1.60e-03 | 112.49 | 3.54e-02 | 379.41 | 0.1 |
| 73 | 42.268 | 0.024 | 0.097 | 45.99 | 1.45e-02 | 3.63e-03 | 1.14e-06 | 34.35 | 1.08e-02 |
| 74 | 42.392 | 0.024 | 0.097 | 660.95 | 0.2 | 239.81 | 7.55e-02 | 8310.27 | 2.6 |
| 75 | 42.404 | 0.024 | 0.097 | 859.59 | 0.3 | 205.49 | 6.47e-02 | 7210.98 | 2.3 |
| 76 | 42.728 | 0.023 | 0.097 | 902.66 | 0.3 | 8.09 | 2.55e-03 | 392.95 | 0.1 |
| 77 | 42.759 | 0.023 | 0.097 | 7.10 | 2.23e-03 | 162.83 | 5.12e-02 | 9.77 | 3.07e-03 |
| 78 | 42.879 | 0.023 | 0.096 | 0.23 | 7.08e-05 | 37.56 | 1.18e-02 | 293.86 | 9.25e-02 |
| 79 | 43.185 | 0.023 | 0.096 | 30.35 | 9.55e-03 | 82.11 | 2.58e-02 | 3641.07 | 1.1 |
| 80 | 43.338 | 0.023 | 0.096 | 5.51 | 1.74e-03 | 559.23 | 0.2 | 6818.64 | 2.1 |
| 81 | 43.830 | 0.023 | 0.096 | 273.94 | 8.62e-02 | 160.82 | 5.06e-02 | 1464.36 | 0.5 |
| 82 | 44.542 | 0.022 | 0.096 | 6.85 | 2.15e-03 | 290.40 | 9.14e-02 | 179.52 | 5.65e-02 |
| 83 | 44.690 | 0.022 | 0.096 | 15.60 | 4.91e-03 | 6.67 | 2.10e-03 | 365.40 | 0.1 |
| 84 | 44.913 | 0.022 | 0.096 | 37.82 | 1.19e-02 | 19.64 | 6.18e-03 | 32.22 | 1.01e-02 |
| 85 | 45.006 | 0.022 | 0.096 | 3.30 | 1.04e-03 | 85.25 | 2.68e-02 | 81.88 | 2.58e-02 |
| 86 | 45.249 | 0.022 | 0.095 | 19.04 | 5.99e-03 | 39.52 | 1.24e-02 | 94.99 | 2.99e-02 |
| 87 | 45.483 | 0.022 | 0.095 | 8.06 | 2.54e-03 | 0.43 | 1.34e-04 | 1729.57 | 0.5 |
| 88 | 45.561 | 0.022 | 0.095 | 31.82 | 1.00e-02 | 12.08 | 3.80e-03 | 8.03 | 2.53e-03 |
| 89 | 46.565 | 0.021 | 0.095 | 39.22 | 1.23e-02 | 8.95 | 2.82e-03 | 185.37 | 5.83e-02 |
| 90 | 47.052 | 0.021 | 0.095 | 94.59 | 2.98e-02 | 18.31 | 5.76e-03 | 51.94 | 1.63e-02 |
| 91 | 47.295 | 0.021 | 0.095 | 708.57 | 0.2 | 0.04 | 1.35e-05 | 86.12 | 2.71e-02 |
| 92 | 47.804 | 0.021 | 0.094 | 38.46 | 1.21e-02 | 54.80 | 1.72e-02 | 325.69 | 0.1 |
| 93 | 47.867 | 0.021 | 0.094 | 547.25 | 0.2 | 119.65 | 3.77e-02 | 164.39 | 5.17e-02 |
| 94 | 48.589 | 0.021 | 0.094 | 29.81 | 9.38e-03 | 9.60 | 3.02e-03 | 308.86 | 9.72e-02 |
| 95 | 49.843 | 0.020 | 0.094 | 0.29 | 8.98e-05 | 1231.18 | 0.4 | 659.29 | 0.2 |
| 96 | 49.968 | 0.020 | 0.094 | 0.25 | 7.97e-05 | 0.35 | 1.09e-04 | 1.88 | 5.93e-04 |
| 97 | 50.204 | 0.020 | 0.093 | 120.56 | 3.79e-02 | 77.11 | 2.43e-02 | 41.64 | 1.31e-02 |
| 98 | 50.400 | 0.020 | 0.093 | 0.43 | 1.34e-04 | 0.26 | 8.27e-05 | 1053.97 | 0.3 |
| 99 | 50.788 | 0.020 | 0.093 | 10.26 | 3.23e-03 | 114.48 | 3.60e-02 | 4.64 | 1.46e-03 |
| 100 | 50.807 | 0.020 | 0.093 | 11.21 | 3.53e-03 | 83.51 | 2.63e-02 | 26.31 | 8.28e-03 |
| Risulta | | | | 2.743e+05 | | 2.837e+05 | | 1.676e+05 | |
| In percentuale | | | | 86.33 | | 89.28 | | 52.73 | |

• **Caso di carico sisma y-y ecc- - SLD**

| CDC | Tipo | Sigla Id | Note |
|-----|------|---|---|
| 16 | Edk | CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -) | |
| | | | categoria suolo: B |
| | | | fattore di sito S = 1.200 |
| | | | ordinata spettro (tratto Tb-Tc) = 0.188 g |
| | | | angolo di ingresso:90.00 |
| | | | eccentricità aggiuntiva: negativa |
| | | | periodo proprio T1: 0.088 sec. |
| | | | numero di modi considerati:100 |
| | | | combinaz. modale: CQC |

Analisi Dinamica e Spettro di Risposta y-y ecc- - SLD

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X | % | M efficace Y | % | M efficace Z | % |
|------|-----------|---------|----------------|--------------|----------|--------------|----------|--------------|----------|
| | Hz | sec | g | x g | | x g | | x g | |
| | | | daN | | | daN | | daN | |
| 1 | 7.627 | 0.131 | 0.188 | 1.599e+04 | 5.0 | 12.39 | 3.90e-03 | 132.01 | 4.15e-02 |
| 2 | 8.369 | 0.119 | 0.183 | 1.408e+04 | 4.4 | 0.23 | 7.29e-05 | 467.33 | 0.1 |
| 3 | 9.121 | 0.110 | 0.174 | 2.123e+04 | 6.7 | 12.05 | 3.79e-03 | 0.59 | 1.85e-04 |
| 4 | 10.971 | 0.091 | 0.157 | 972.82 | 0.3 | 9176.71 | 2.9 | 402.71 | 0.1 |
| 5 | 11.339 | 0.088 | 0.155 | 14.75 | 4.64e-03 | 1.182e+05 | 37.2 | 163.02 | 5.13e-02 |
| 6 | 11.561 | 0.087 | 0.153 | 2872.60 | 0.9 | 2414.60 | 0.8 | 522.13 | 0.2 |
| 7 | 12.496 | 0.080 | 0.147 | 2.657e+04 | 8.4 | 18.72 | 5.89e-03 | 8.28 | 2.60e-03 |
| 8 | 13.433 | 0.074 | 0.142 | 852.80 | 0.3 | 2.698e+04 | 8.5 | 45.70 | 1.44e-02 |
| 9 | 13.926 | 0.072 | 0.140 | 3.723e+04 | 11.7 | 835.50 | 0.3 | 7.56 | 2.38e-03 |
| 10 | 14.775 | 0.068 | 0.136 | 25.45 | 8.01e-03 | 4.314e+04 | 13.6 | 35.32 | 1.11e-02 |
| 11 | 16.426 | 0.061 | 0.130 | 7.82 | 2.46e-03 | 1.368e+04 | 4.3 | 9.37 | 2.95e-03 |
| 12 | 16.687 | 0.060 | 0.129 | 7678.83 | 2.4 | 5.44 | 1.71e-03 | 1.02 | 3.22e-04 |
| 13 | 17.108 | 0.058 | 0.128 | 97.73 | 3.08e-02 | 4578.41 | 1.4 | 14.95 | 4.71e-03 |
| 14 | 17.398 | 0.057 | 0.127 | 1630.35 | 0.5 | 8576.65 | 2.7 | 2.36 | 7.44e-04 |
| 15 | 17.573 | 0.057 | 0.127 | 891.72 | 0.3 | 1991.90 | 0.6 | 9.12 | 2.87e-03 |
| 16 | 18.038 | 0.055 | 0.125 | 247.92 | 7.80e-02 | 1.824e+04 | 5.7 | 4.64 | 1.46e-03 |
| 17 | 18.092 | 0.055 | 0.125 | 2.040e+04 | 6.4 | 140.84 | 4.43e-02 | 59.49 | 1.87e-02 |
| 18 | 18.489 | 0.054 | 0.124 | 188.90 | 5.94e-02 | 6581.91 | 2.1 | 15.54 | 4.89e-03 |
| 19 | 18.853 | 0.053 | 0.123 | 2.003e+04 | 6.3 | 30.77 | 9.68e-03 | 11.30 | 3.56e-03 |
| 20 | 19.269 | 0.052 | 0.122 | 1.382e+04 | 4.3 | 389.02 | 0.1 | 306.48 | 9.65e-02 |
| 21 | 20.190 | 0.050 | 0.120 | 492.51 | 0.2 | 1297.23 | 0.4 | 4.88 | 1.53e-03 |
| 22 | 20.385 | 0.049 | 0.120 | 1198.49 | 0.4 | 1983.13 | 0.6 | 2.56 | 8.07e-04 |
| 23 | 20.607 | 0.049 | 0.119 | 35.07 | 1.10e-02 | 1585.66 | 0.5 | 13.92 | 4.38e-03 |
| 24 | 20.943 | 0.048 | 0.118 | 6197.31 | 2.0 | 3168.70 | 1.0 | 16.47 | 5.18e-03 |
| 25 | 21.163 | 0.047 | 0.118 | 254.33 | 8.00e-02 | 291.63 | 9.18e-02 | 20.44 | 6.43e-03 |
| 26 | 21.676 | 0.046 | 0.117 | 500.70 | 0.2 | 43.55 | 1.37e-02 | 10.11 | 3.18e-03 |
| 27 | 21.968 | 0.046 | 0.116 | 4488.16 | 1.4 | 30.13 | 9.48e-03 | 34.22 | 1.08e-02 |
| 28 | 22.182 | 0.045 | 0.116 | 271.24 | 8.54e-02 | 1608.31 | 0.5 | 18.61 | 5.86e-03 |
| 29 | 23.516 | 0.043 | 0.114 | 0.51 | 1.60e-04 | 10.54 | 3.32e-03 | 1.65 | 5.20e-04 |
| 30 | 23.694 | 0.042 | 0.113 | 122.65 | 3.86e-02 | 102.54 | 3.23e-02 | 0.94 | 2.94e-04 |
| 31 | 23.905 | 0.042 | 0.113 | 0.90 | 2.84e-04 | 8.87 | 2.79e-03 | 5.17 | 1.63e-03 |
| 32 | 24.741 | 0.040 | 0.112 | 427.35 | 0.1 | 317.06 | 9.98e-02 | 10.46 | 3.29e-03 |
| 33 | 24.859 | 0.040 | 0.112 | 135.38 | 4.26e-02 | 206.59 | 6.50e-02 | 0.98 | 3.07e-04 |
| 34 | 25.284 | 0.040 | 0.111 | 482.51 | 0.2 | 1038.15 | 0.3 | 11.28 | 3.55e-03 |
| 35 | 25.433 | 0.039 | 0.111 | 1207.72 | 0.4 | 280.52 | 8.83e-02 | 1111.43 | 0.3 |
| 36 | 26.202 | 0.038 | 0.110 | 525.59 | 0.2 | 2000.20 | 0.6 | 923.59 | 0.3 |
| 37 | 26.394 | 0.038 | 0.110 | 87.31 | 2.75e-02 | 108.56 | 3.42e-02 | 170.31 | 5.36e-02 |
| 38 | 26.727 | 0.037 | 0.109 | 336.81 | 0.1 | 69.76 | 2.20e-02 | 2.85 | 8.96e-04 |
| 39 | 27.516 | 0.036 | 0.108 | 671.86 | 0.2 | 33.64 | 1.06e-02 | 5.48 | 1.72e-03 |
| 40 | 27.661 | 0.036 | 0.108 | 1130.36 | 0.4 | 442.99 | 0.1 | 3.12 | 9.82e-04 |
| 41 | 28.590 | 0.035 | 0.107 | 54.56 | 1.72e-02 | 58.88 | 1.85e-02 | 281.04 | 8.84e-02 |
| 42 | 28.654 | 0.035 | 0.107 | 132.14 | 4.16e-02 | 76.75 | 2.42e-02 | 569.16 | 0.2 |
| 43 | 28.913 | 0.035 | 0.107 | 12.16 | 3.83e-03 | 1.50 | 4.71e-04 | 17.50 | 5.51e-03 |
| 44 | 29.373 | 0.034 | 0.106 | 102.77 | 3.23e-02 | 110.34 | 3.47e-02 | 4.46 | 1.41e-03 |
| 45 | 30.095 | 0.033 | 0.105 | 16.05 | 5.05e-03 | 333.19 | 0.1 | 6.02 | 1.90e-03 |
| 46 | 30.571 | 0.033 | 0.105 | 8672.95 | 2.7 | 0.03 | 8.23e-06 | 3167.78 | 1.0 |
| 47 | 30.940 | 0.032 | 0.105 | 2324.08 | 0.7 | 428.94 | 0.1 | 2.427e+04 | 7.6 |
| 48 | 31.229 | 0.032 | 0.104 | 1327.61 | 0.4 | 240.66 | 7.57e-02 | 2030.44 | 0.6 |
| 49 | 31.817 | 0.031 | 0.104 | 1.154e+04 | 3.6 | 642.09 | 0.2 | 197.86 | 6.23e-02 |
| 50 | 32.067 | 0.031 | 0.104 | 1.226e+04 | 3.9 | 899.65 | 0.3 | 79.07 | 2.49e-02 |
| 51 | 32.630 | 0.031 | 0.103 | 221.70 | 6.98e-02 | 1156.94 | 0.4 | 1.352e+04 | 4.3 |
| 52 | 32.904 | 0.030 | 0.103 | 636.21 | 0.2 | 6.42e-03 | 2.02e-06 | 378.19 | 0.1 |
| 53 | 33.096 | 0.030 | 0.103 | 5344.24 | 1.7 | 63.40 | 2.00e-02 | 455.67 | 0.1 |
| 54 | 33.229 | 0.030 | 0.103 | 1.627e+04 | 5.1 | 85.92 | 2.70e-02 | 2339.48 | 0.7 |
| 55 | 33.641 | 0.030 | 0.102 | 1909.44 | 0.6 | 892.77 | 0.3 | 1.201e+04 | 3.8 |
| 56 | 34.848 | 0.029 | 0.101 | 207.61 | 6.53e-02 | 1338.04 | 0.4 | 3050.44 | 1.0 |
| 57 | 35.670 | 0.028 | 0.101 | 186.95 | 5.88e-02 | 0.32 | 1.01e-04 | 200.17 | 6.30e-02 |
| 58 | 36.050 | 0.028 | 0.100 | 2.39 | 7.53e-04 | 9.22 | 2.90e-03 | 8.36 | 2.63e-03 |
| 59 | 36.410 | 0.027 | 0.100 | 742.74 | 0.2 | 33.70 | 1.06e-02 | 138.96 | 4.37e-02 |
| 60 | 36.669 | 0.027 | 0.100 | 642.77 | 0.2 | 19.56 | 6.16e-03 | 4617.70 | 1.5 |
| 61 | 37.116 | 0.027 | 0.100 | 0.06 | 1.81e-05 | 1876.42 | 0.6 | 0.11 | 3.37e-05 |
| 62 | 37.648 | 0.027 | 0.099 | 1293.23 | 0.4 | 6.38 | 2.01e-03 | 3.17 | 9.97e-04 |
| 63 | 38.259 | 0.026 | 0.099 | 46.63 | 1.47e-02 | 151.45 | 4.77e-02 | 39.79 | 1.25e-02 |
| 64 | 38.597 | 0.026 | 0.099 | 448.11 | 0.1 | 2.18 | 6.87e-04 | 501.45 | 0.2 |
| 65 | 38.684 | 0.026 | 0.099 | 866.06 | 0.3 | 62.10 | 1.95e-02 | 1175.33 | 0.4 |
| 66 | 38.805 | 0.026 | 0.099 | 13.07 | 4.11e-03 | 179.08 | 5.64e-02 | 0.23 | 7.30e-05 |

| Modo | Frequenza | Periodo | Acc. Spettrale | M efficace X x g | % | M efficace Y x g | % | M efficace Z x g | % |
|----------------|-----------|---------|----------------|---------------------|----------|---------------------|----------|---------------------|----------|
| 67 | 38.981 | 0.026 | 0.099 | 52.82 | 1.66e-02 | 33.71 | 1.06e-02 | 1840.80 | 0.6 |
| 68 | 39.476 | 0.025 | 0.098 | 290.88 | 9.15e-02 | 164.70 | 5.18e-02 | 4.894e+04 | 15.4 |
| 69 | 39.934 | 0.025 | 0.098 | 10.16 | 3.20e-03 | 714.18 | 0.2 | 1624.16 | 0.5 |
| 70 | 40.001 | 0.025 | 0.098 | 80.17 | 2.52e-02 | 3.90 | 1.23e-03 | 5620.03 | 1.8 |
| 71 | 40.250 | 0.025 | 0.098 | 209.85 | 6.60e-02 | 496.98 | 0.2 | 707.78 | 0.2 |
| 72 | 40.976 | 0.024 | 0.097 | 892.09 | 0.3 | 539.57 | 0.2 | 1320.47 | 0.4 |
| 73 | 41.584 | 0.024 | 0.097 | 10.98 | 3.46e-03 | 3.43 | 1.08e-03 | 404.19 | 0.1 |
| 74 | 42.403 | 0.024 | 0.097 | 60.90 | 1.92e-02 | 32.17 | 1.01e-02 | 0.12 | 3.88e-05 |
| 75 | 42.633 | 0.023 | 0.097 | 522.12 | 0.2 | 316.34 | 9.96e-02 | 8953.23 | 2.8 |
| 76 | 42.750 | 0.023 | 0.097 | 130.73 | 4.11e-02 | 206.56 | 6.50e-02 | 6756.18 | 2.1 |
| 77 | 42.866 | 0.023 | 0.096 | 0.53 | 1.65e-04 | 2.34 | 7.36e-04 | 7.46 | 2.35e-03 |
| 78 | 43.351 | 0.023 | 0.096 | 121.10 | 3.81e-02 | 219.38 | 6.90e-02 | 7590.36 | 2.4 |
| 79 | 43.984 | 0.023 | 0.096 | 7.21 | 2.27e-03 | 11.68 | 3.68e-03 | 2427.42 | 0.8 |
| 80 | 44.302 | 0.023 | 0.096 | 15.06 | 4.74e-03 | 121.11 | 3.81e-02 | 563.67 | 0.2 |
| 81 | 44.546 | 0.022 | 0.096 | 6.33 | 1.99e-03 | 677.54 | 0.2 | 52.01 | 1.64e-02 |
| 82 | 44.901 | 0.022 | 0.096 | 463.04 | 0.1 | 47.99 | 1.51e-02 | 607.11 | 0.2 |
| 83 | 44.997 | 0.022 | 0.096 | 593.79 | 0.2 | 38.31 | 1.21e-02 | 220.02 | 6.92e-02 |
| 84 | 45.243 | 0.022 | 0.095 | 19.00 | 5.98e-03 | 27.86 | 8.77e-03 | 334.05 | 0.1 |
| 85 | 45.476 | 0.022 | 0.095 | 38.61 | 1.22e-02 | 426.75 | 0.1 | 2085.35 | 0.7 |
| 86 | 45.810 | 0.022 | 0.095 | 5.30 | 1.67e-03 | 20.89 | 6.57e-03 | 10.31 | 3.24e-03 |
| 87 | 45.933 | 0.022 | 0.095 | 14.62 | 4.60e-03 | 22.46 | 7.07e-03 | 78.70 | 2.48e-02 |
| 88 | 46.176 | 0.022 | 0.095 | 100.11 | 3.15e-02 | 355.89 | 0.1 | 144.57 | 4.55e-02 |
| 89 | 46.254 | 0.022 | 0.095 | 1.38 | 4.33e-04 | 10.65 | 3.35e-03 | 4.10 | 1.29e-03 |
| 90 | 46.434 | 0.022 | 0.095 | 1013.16 | 0.3 | 1.22 | 3.83e-04 | 84.11 | 2.65e-02 |
| 91 | 46.534 | 0.021 | 0.095 | 43.38 | 1.37e-02 | 515.62 | 0.2 | 36.54 | 1.15e-02 |
| 92 | 47.562 | 0.021 | 0.094 | 306.18 | 9.64e-02 | 266.87 | 8.40e-02 | 87.01 | 2.74e-02 |
| 93 | 48.047 | 0.021 | 0.094 | 7.16 | 2.25e-03 | 20.31 | 6.39e-03 | 185.18 | 5.83e-02 |
| 94 | 48.175 | 0.021 | 0.094 | 31.24 | 9.83e-03 | 170.29 | 5.36e-02 | 697.62 | 0.2 |
| 95 | 48.268 | 0.021 | 0.094 | 170.04 | 5.35e-02 | 43.33 | 1.36e-02 | 500.63 | 0.2 |
| 96 | 48.388 | 0.021 | 0.094 | 19.87 | 6.25e-03 | 132.80 | 4.18e-02 | 572.50 | 0.2 |
| 97 | 48.523 | 0.021 | 0.094 | 4.92 | 1.55e-03 | 2.19 | 6.90e-04 | 34.80 | 1.10e-02 |
| 98 | 50.927 | 0.020 | 0.093 | 22.78 | 7.17e-03 | 1.42 | 4.47e-04 | 275.83 | 8.68e-02 |
| 99 | 50.995 | 0.020 | 0.093 | 19.36 | 6.09e-03 | 0.10 | 3.19e-05 | 741.76 | 0.2 |
| 100 | 51.061 | 0.020 | 0.093 | 67.51 | 2.12e-02 | 0.89 | 2.80e-04 | 355.80 | 0.1 |
| Risulta | | | | 2.740e+05 | | 2.840e+05 | | 1.675e+05 | |
| In percentuale | | | | 86.24 | | 89.38 | | 52.72 | |

2.1.2 Spostamenti della struttura

Si riportano le massime traslazioni assolute, per i **singoli casi di carico** più significativi, a livello dei nodi di impalcato e di testata delle pareti.

2.1.2.1 Traslazioni x-x per singoli casi di carico

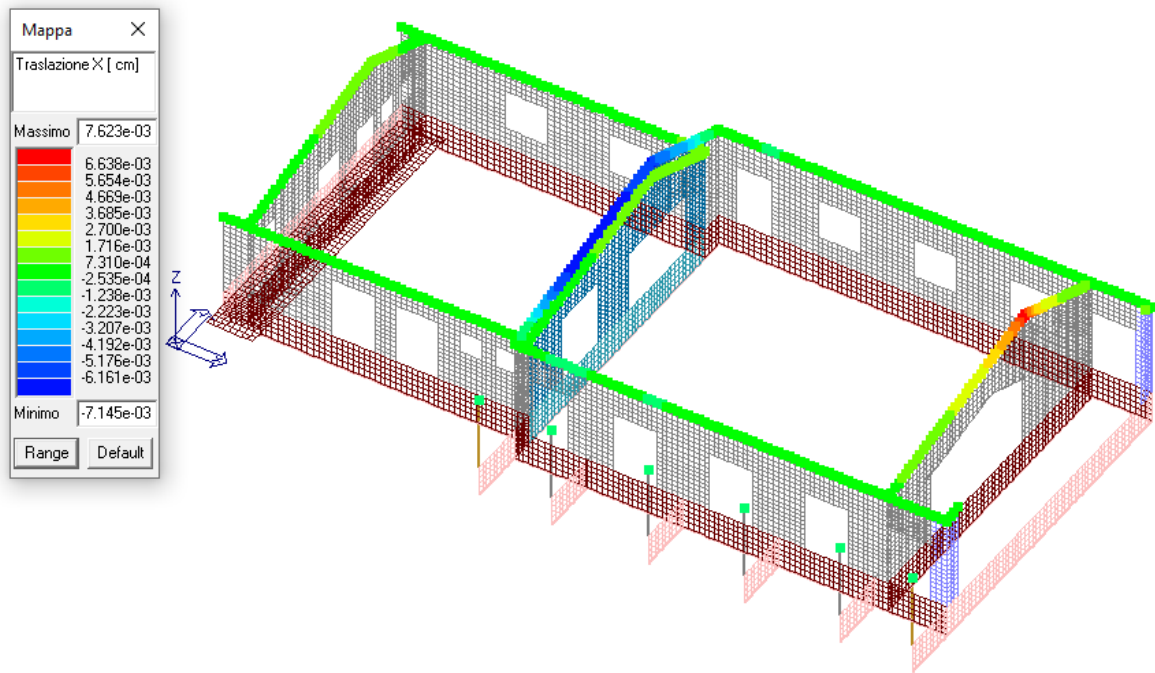


Fig 1. Traslazione x-x per caso di Carico **LC1**: Pesi Propri Strutturali.

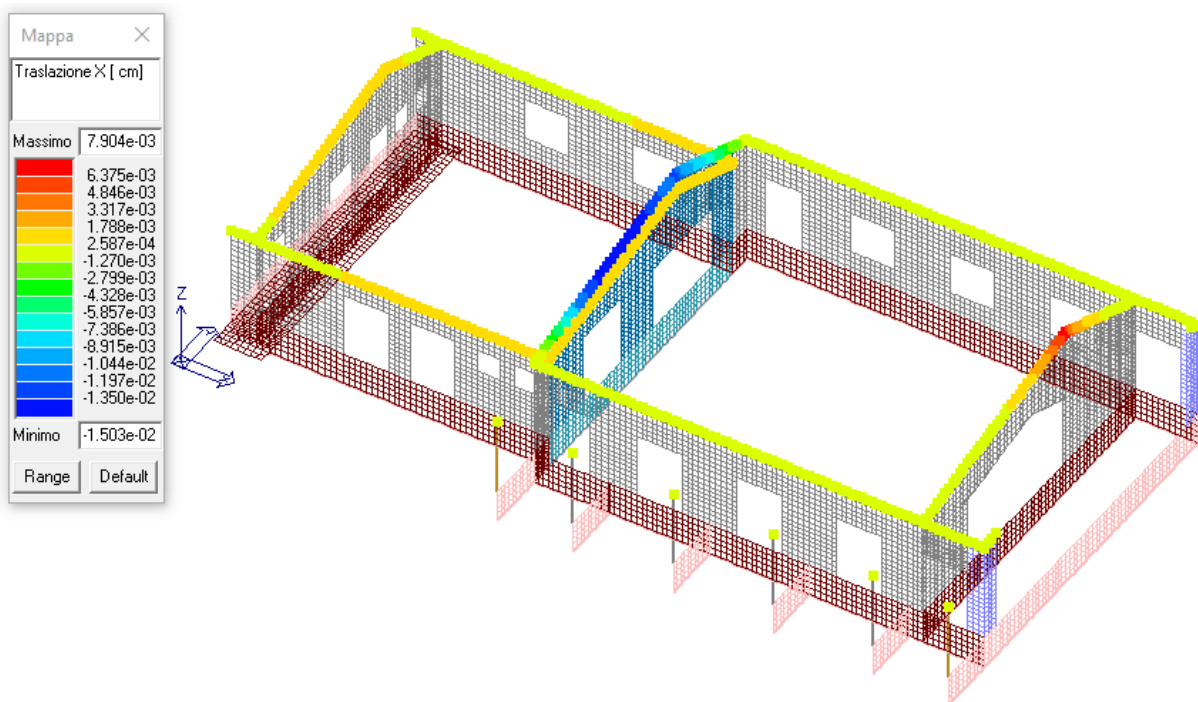


Fig 2. Traslazione x-x per caso di Carico **LC2**: Carichi Perm. Strutturali Copertura.

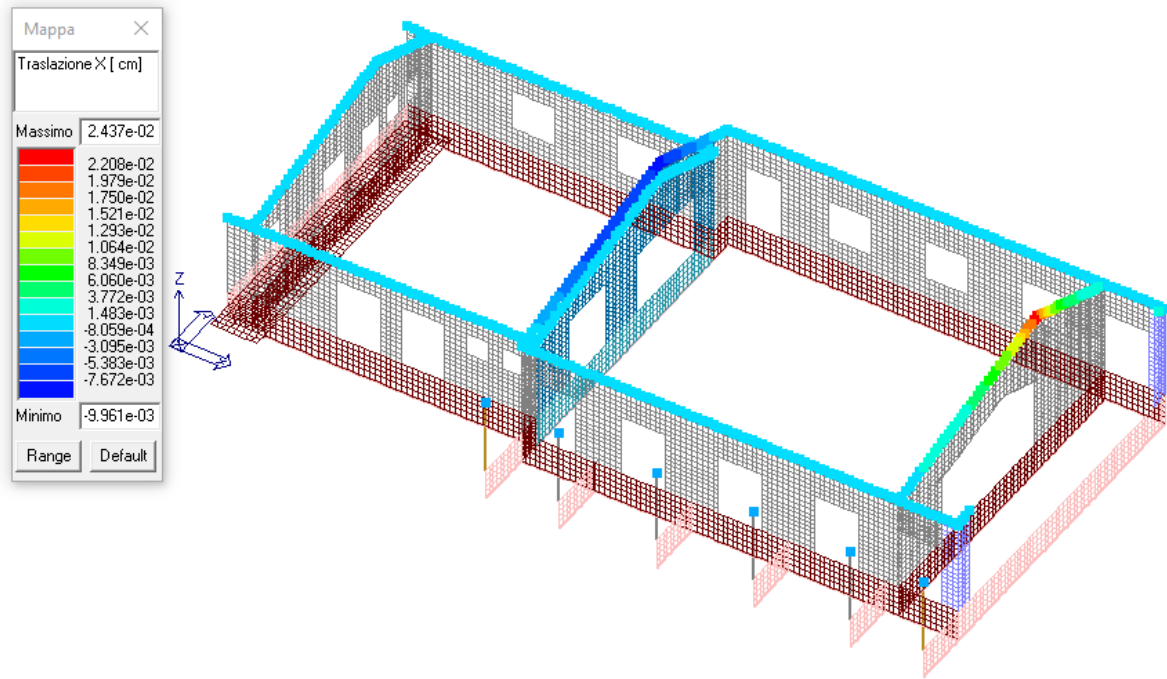


Fig 3. Traslazione x-x per caso di Carico **LC3**: Carichi Perm. copertura n.c.d.

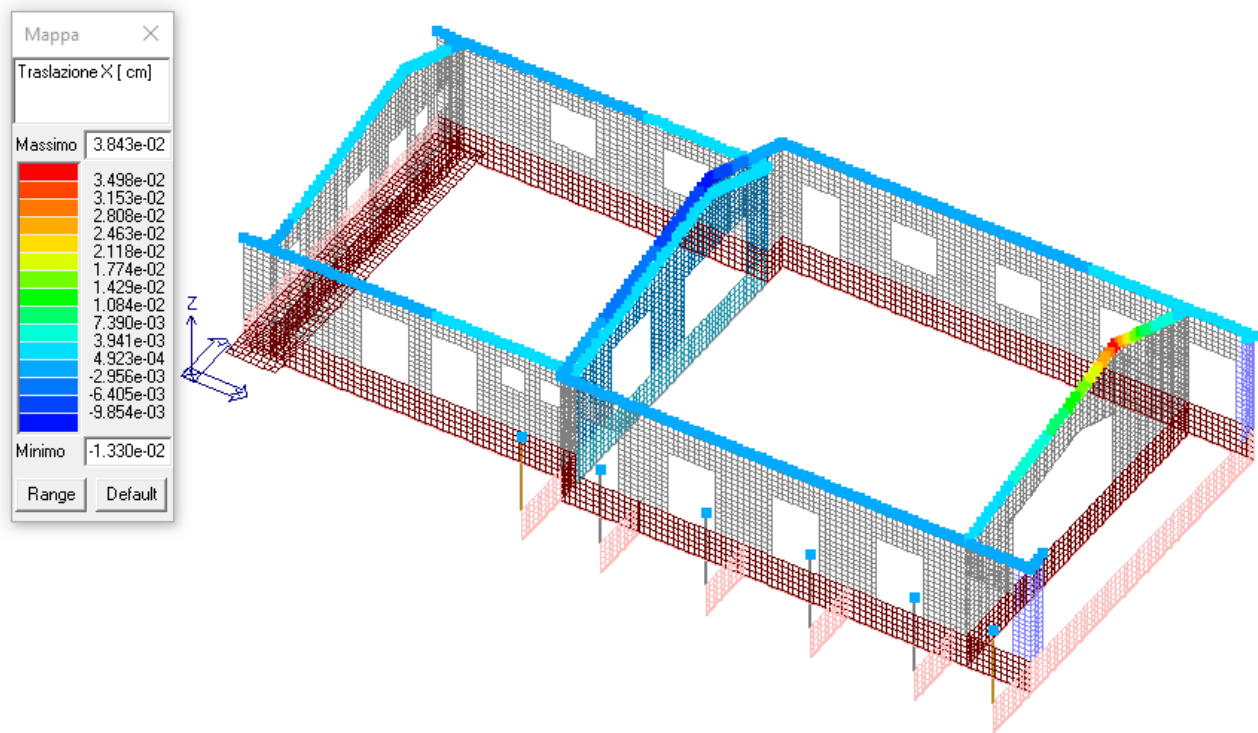


Fig 4. Traslazione x-x per caso di Carico **LC4**: Variabile Neve.

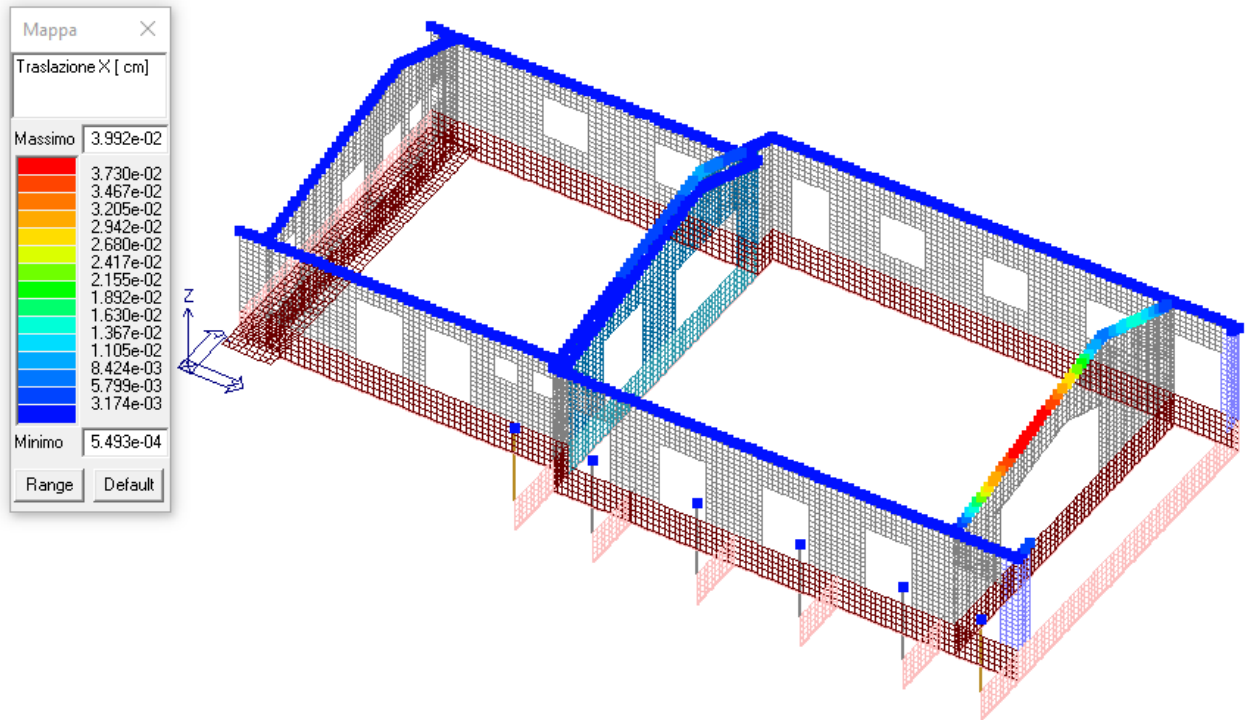


Fig 5. Traslazione x-x per caso di Carico **LC5:** Vento +X

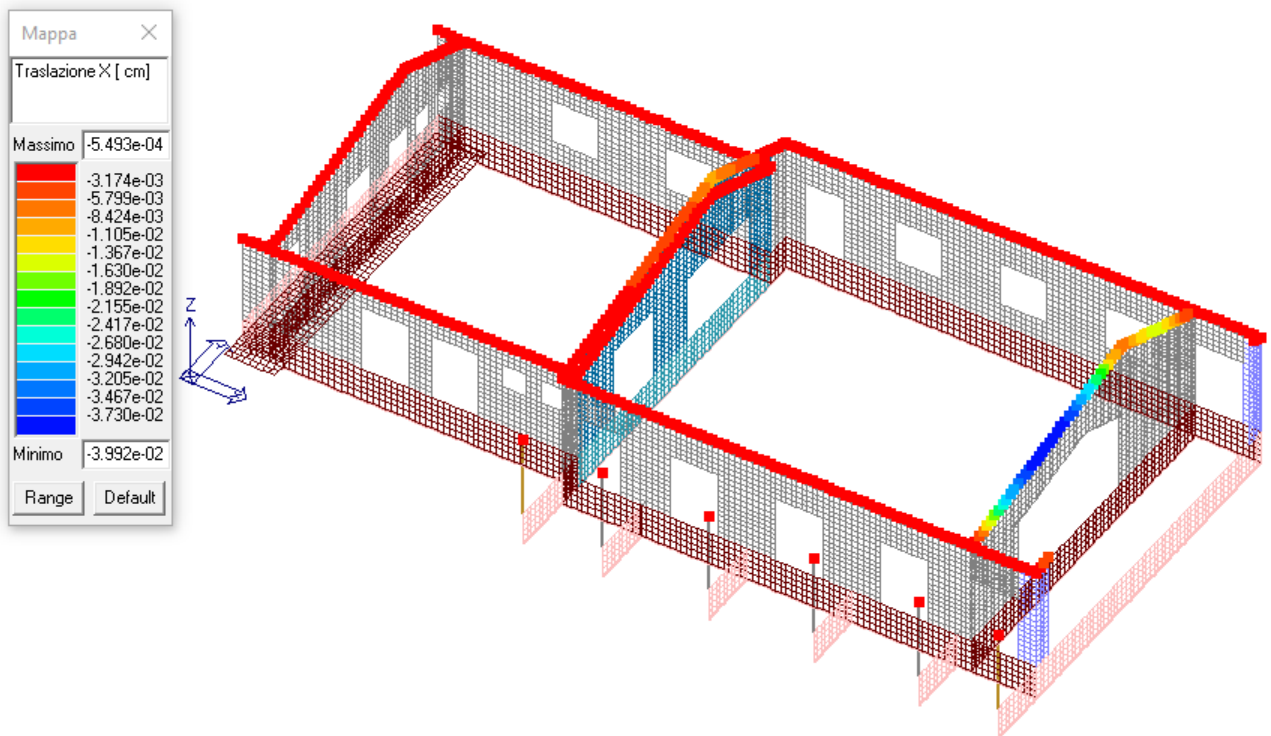


Fig 6. Traslazione x-x per caso di Carico **LC6:** Vento -X.

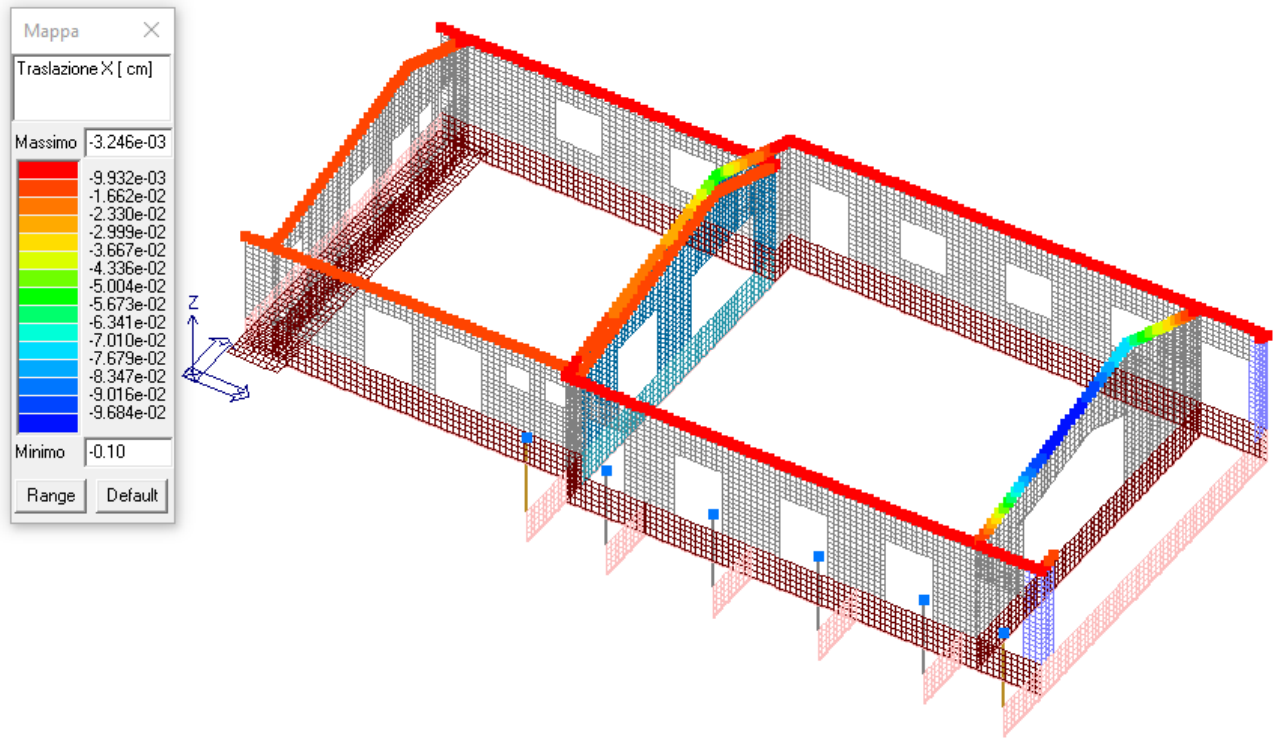


Fig 7. Traslazione x-x per caso di carico sisma x-x SLV ecc.+.

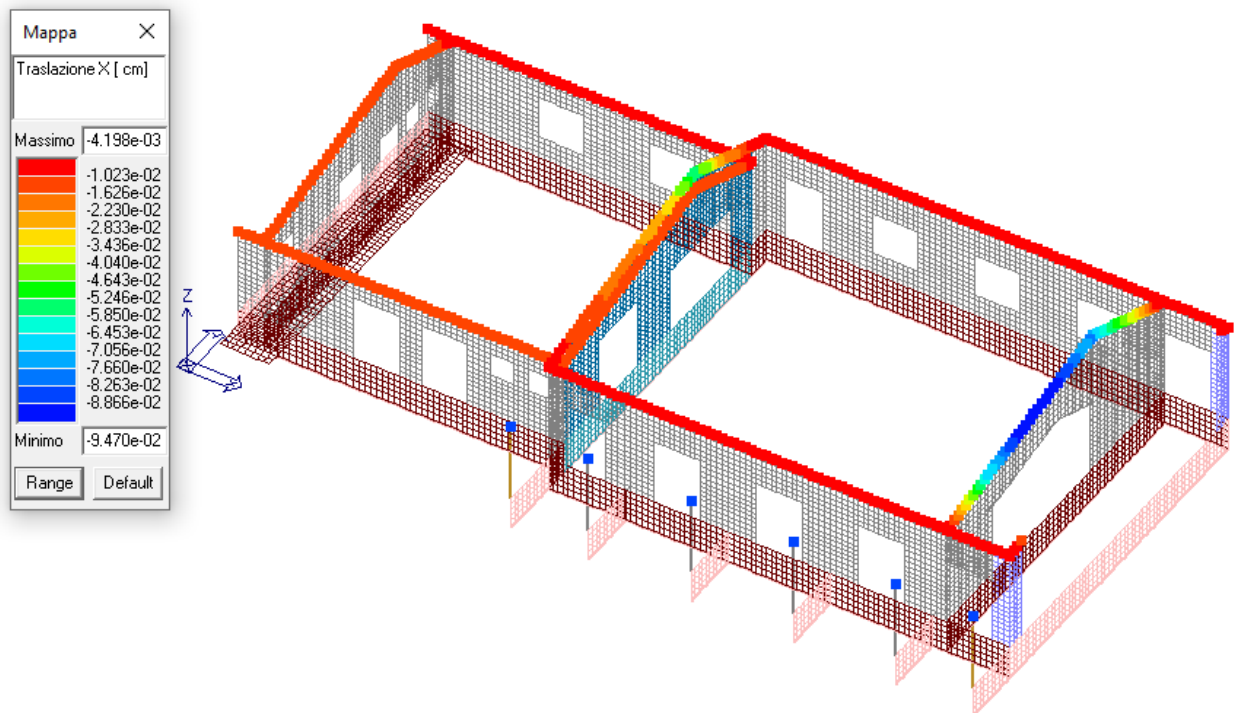


Fig 8. Traslazione x-x per caso di carico sisma x-x SLV ecc.-.

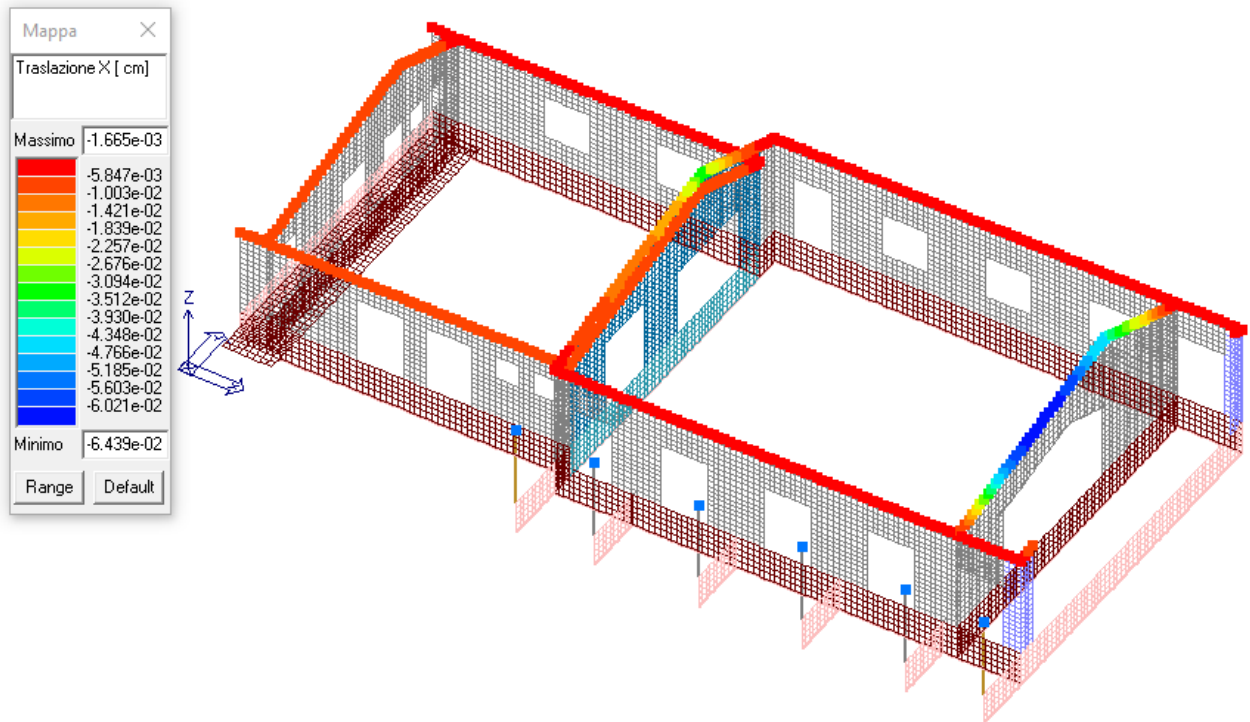


Fig 9. Traslazione x-x per caso di carico sisma x-x SLD Ecc.+.

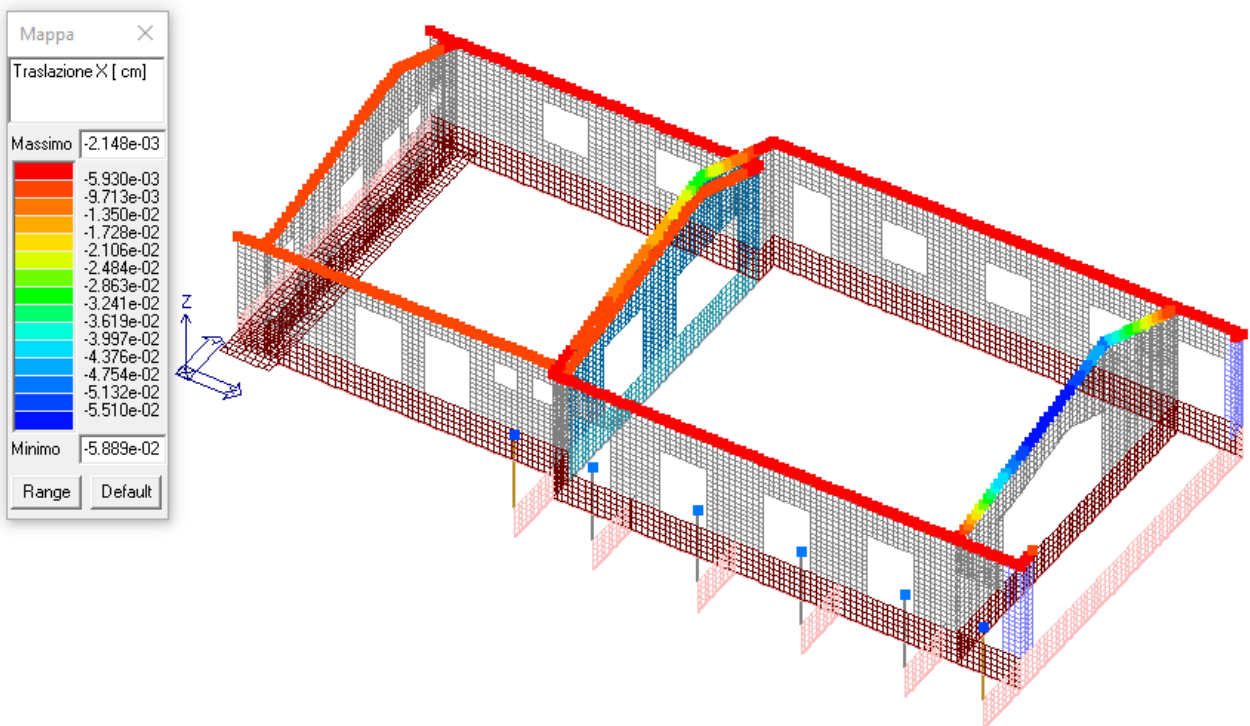


Fig 10. Traslazione x-x per caso di carico sisma x-x SLD Ecc.-.

2.1.2.2 Traslazioni y-y per singoli casi di carico

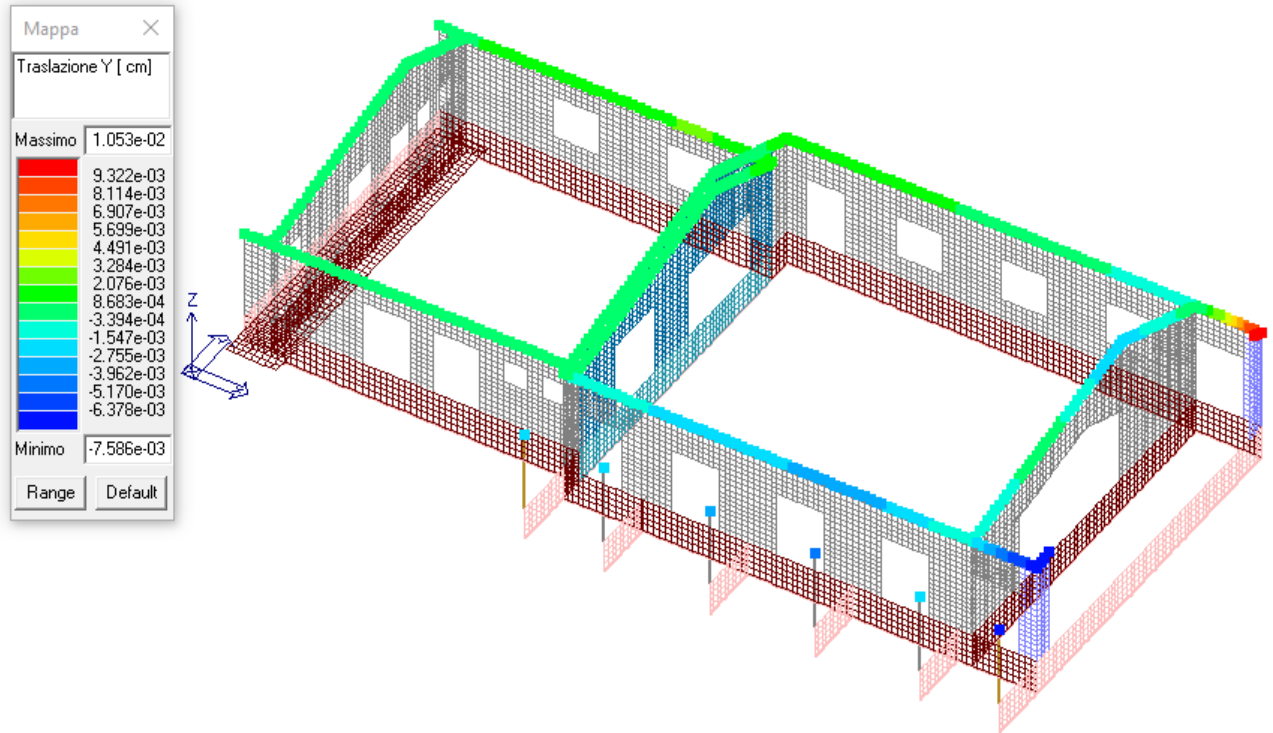


Fig 11. Traslazione y-y per caso di Carico **LC1**: Pesì Propri Strutturali.

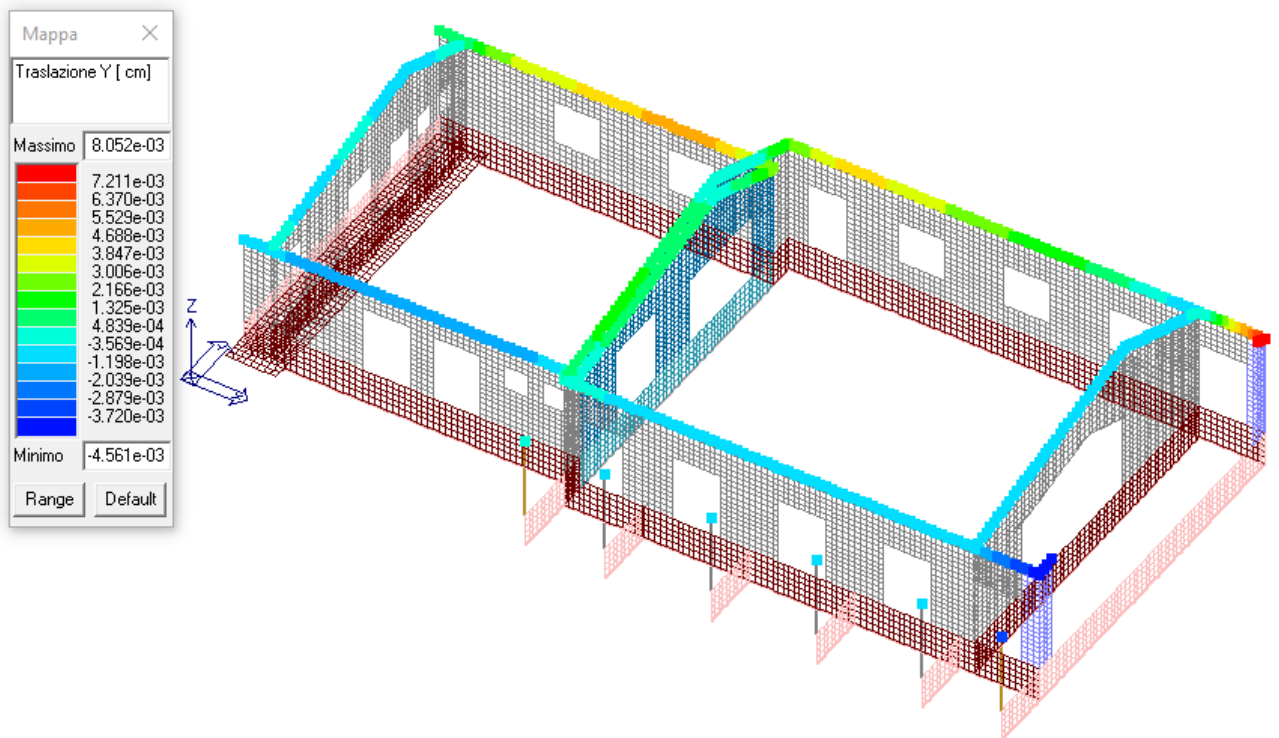


Fig 12. Traslazione y-y per caso di Carico **LC2**: Carichi Perm. Strutturali impalcati.

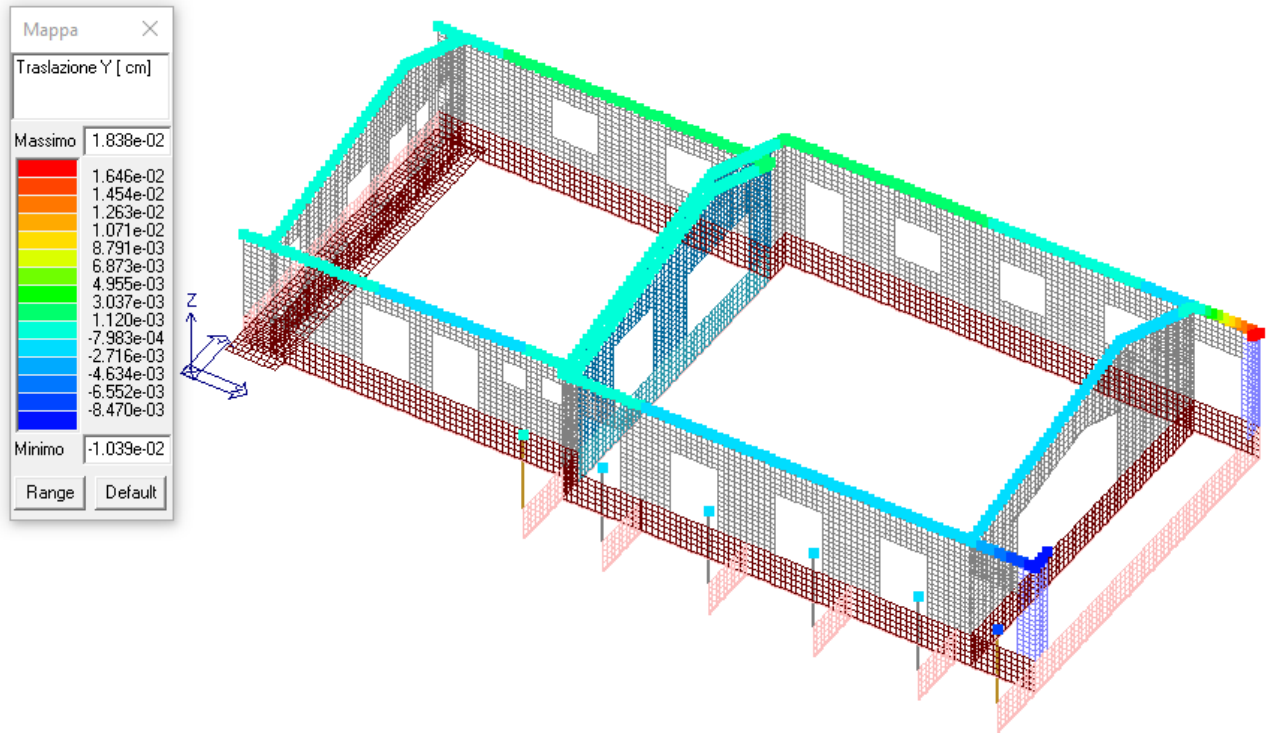


Fig 13. Traslazione y-y per caso di Carico **LC3**: Carichi Perm. impalcati n.c.d.

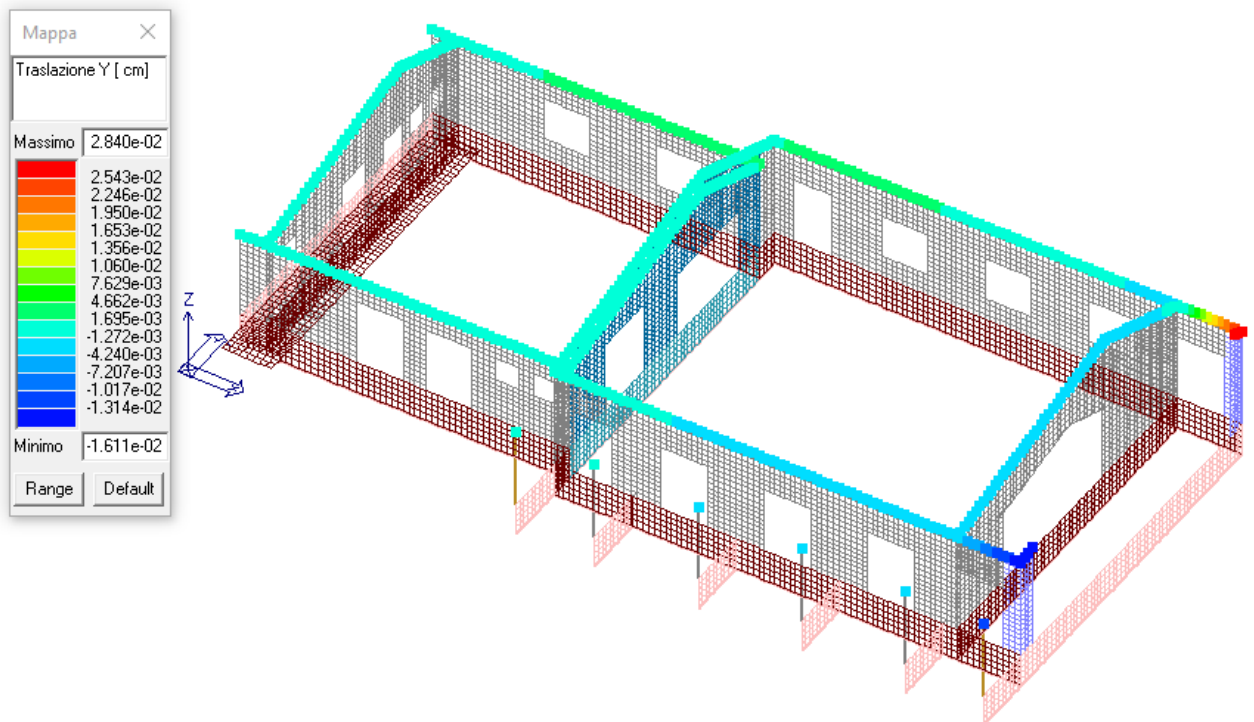


Fig 14. Traslazione y-y per caso di Carico **LC4**: Perm. Variabile Neve..

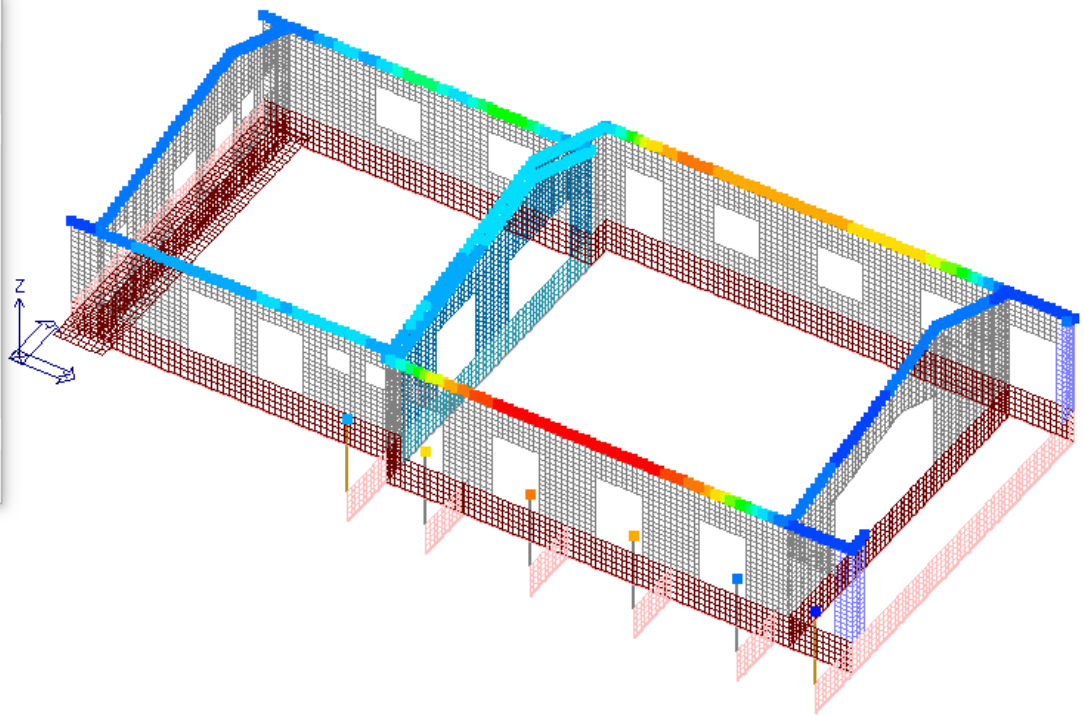
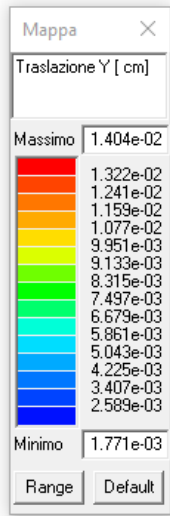


Fig 15. Traslazione y-y per caso di carico vento +y.

Fig 16.

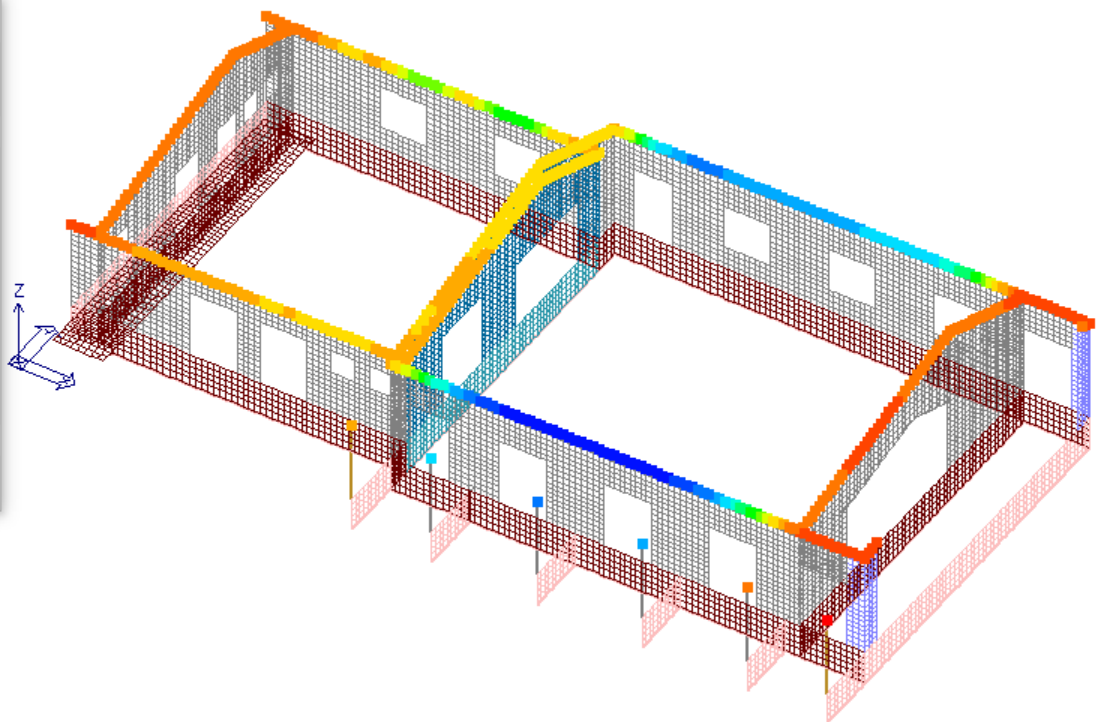
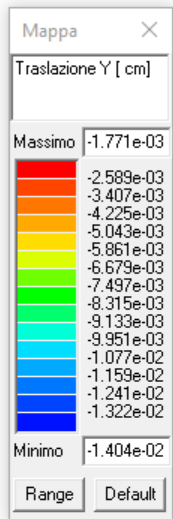


Fig 17. Traslazione y-y per caso di carico vento -y.

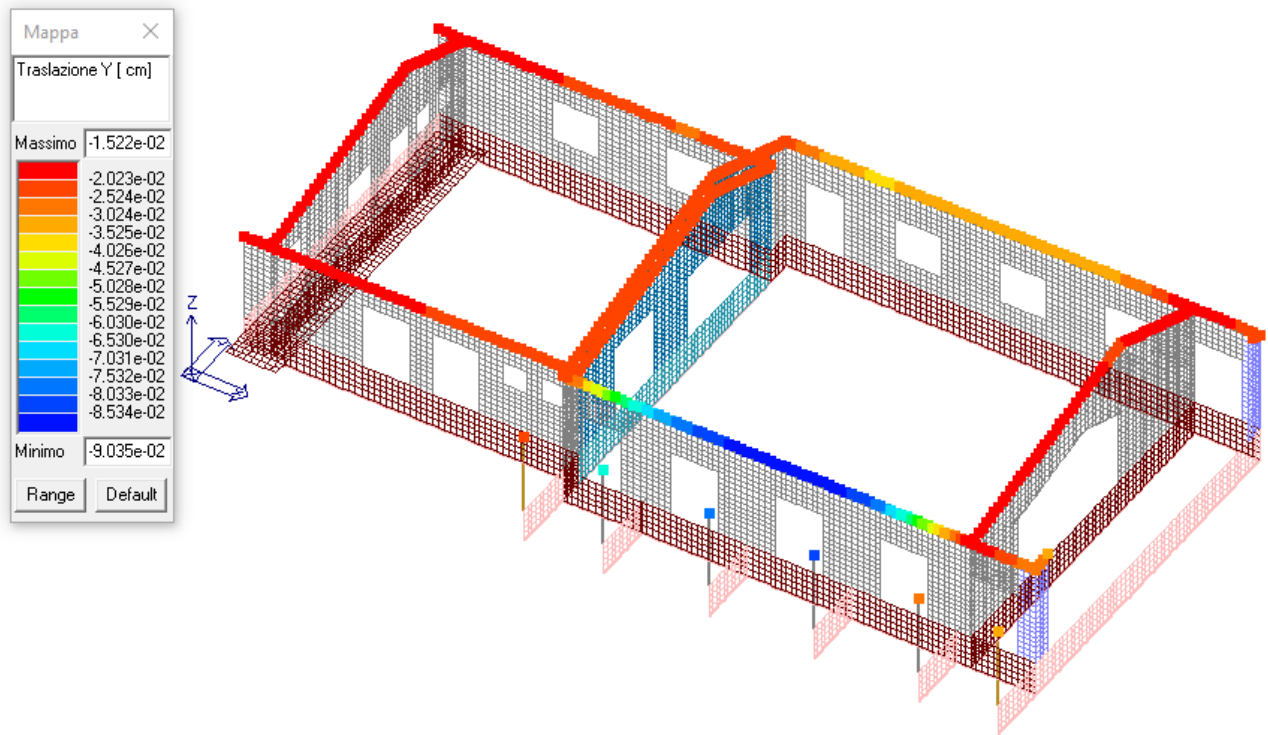


Fig 18. Traslazione y-y per caso di carico sisma y-y – SLV, ecc.+.

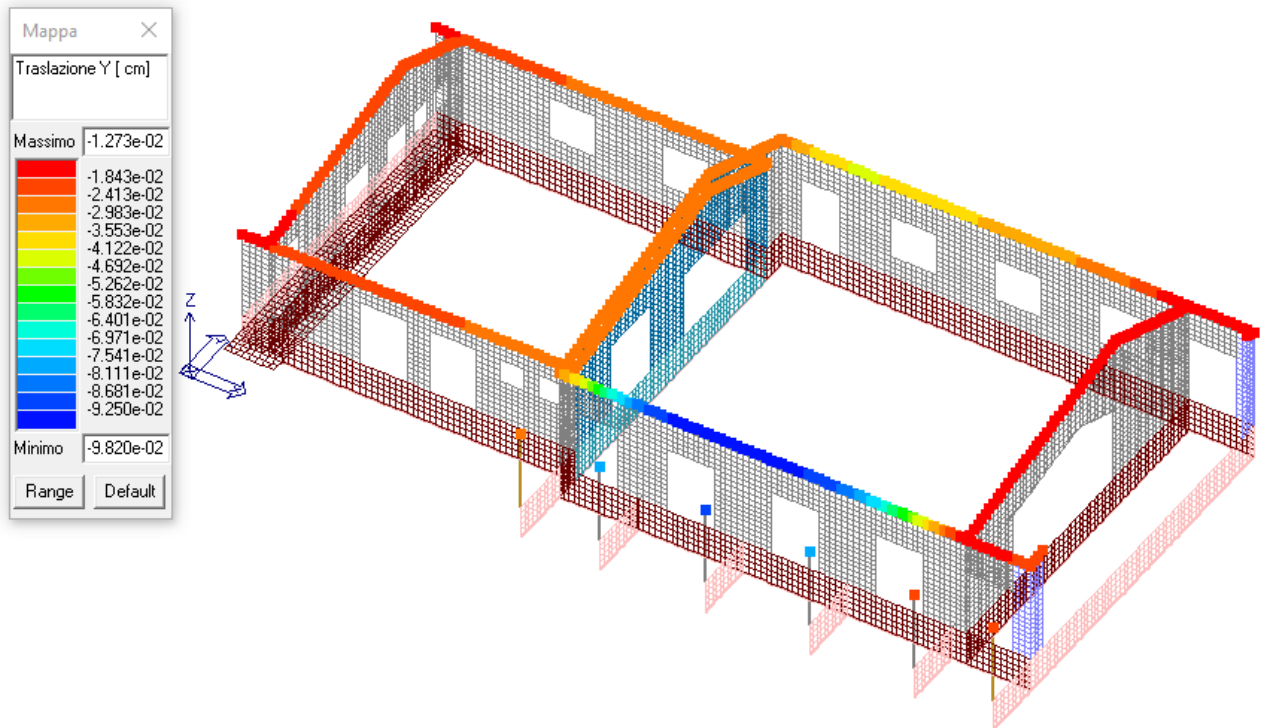


Fig 19. Traslazione y-y per caso di carico sisma y-y – SLV, ecc.-.

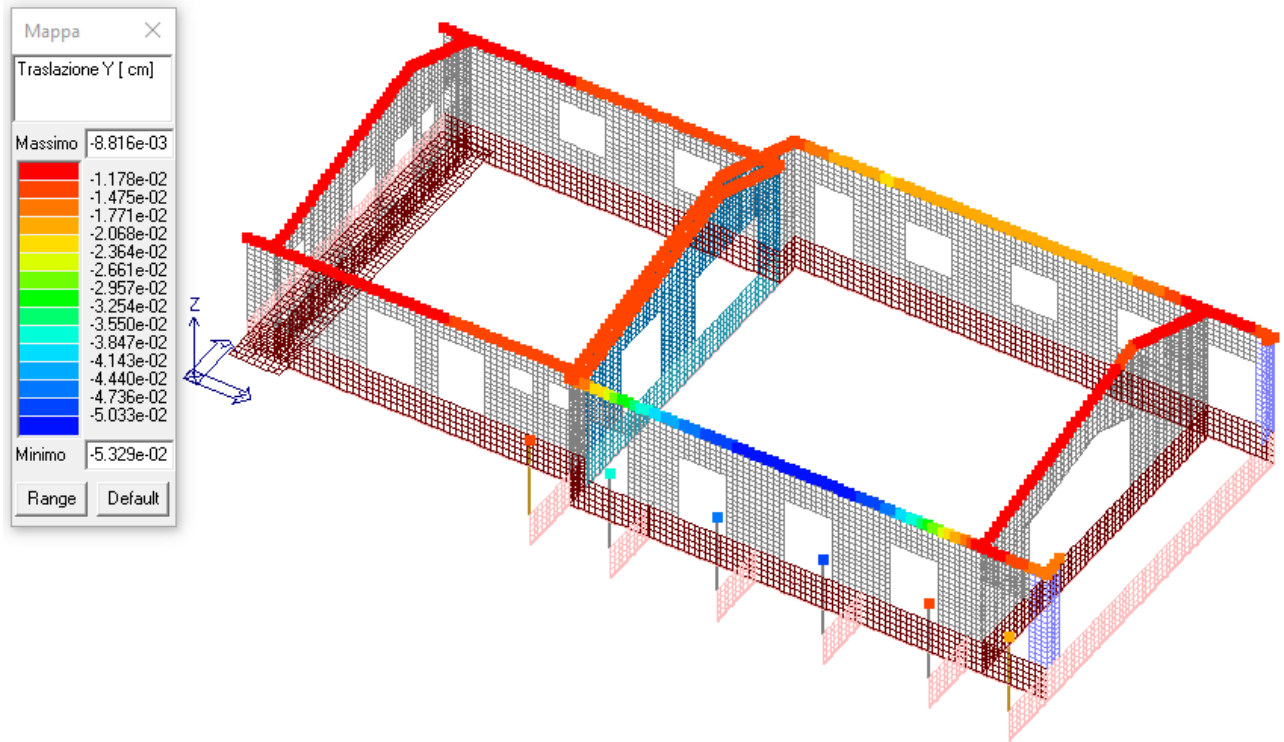


Fig 20. Traslazione y-y per caso di carico sisma y-y – SLD ecc.+.

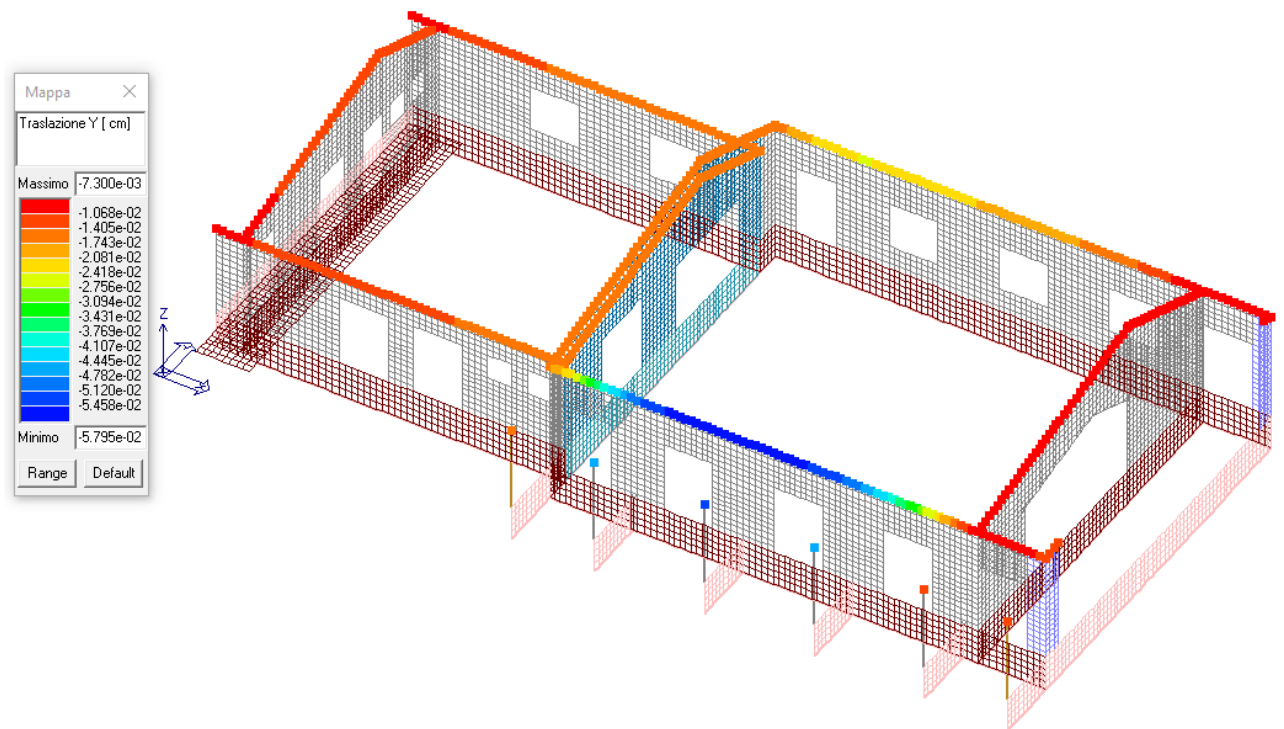


Fig 21. Traslazione y-y per caso di carico sisma y-y – SLD ecc -.

2.1.3 Definizione Spostamenti massimi in cmb. sismiche SLV

Gli spostamenti massimi in cmb. sismiche SLV vengono valutati sulla struttura calcolandoli analiticamente per lo SLV secondo §7.3.3.3 NTC-2018, ossia:

gli spostamenti d_E della struttura sotto l'azione sismica di progetto allo SLV si ottengono moltiplicando per il fattore μ_d i valori d_{Ee} ottenuti dall'analisi lineare dinamica secondo l'espressione seguente:

$$d_E = \mu_d d_{Ee}$$

dove:

$$\begin{aligned} \mu_d &= q && \text{per } T_1 \geq T_C \\ \mu_d &= 1 + (q-1) T_C / T_1 && \text{per } T_1 < T_C; \end{aligned}$$

Nel caso in esame:

- sisma x-x ecc+: $\mu_d = 2.679$;
- sisma x-x ecc-: $\mu_d = 2.781$;
- sisma y-y ecc+: $\mu_d = 3.324$;
- sisma y-y ecc-: $\mu_d = 3.229$.
-

Si riportano gli spostamenti massimi involuppo già amplificati per “ μ_d ” degli elementi strutturali di elevazione per le combinazioni sismiche (SLV).

Spostamenti in Cmb. Sismiche SLV (nodi di testata delle pareti e dei pilastri)

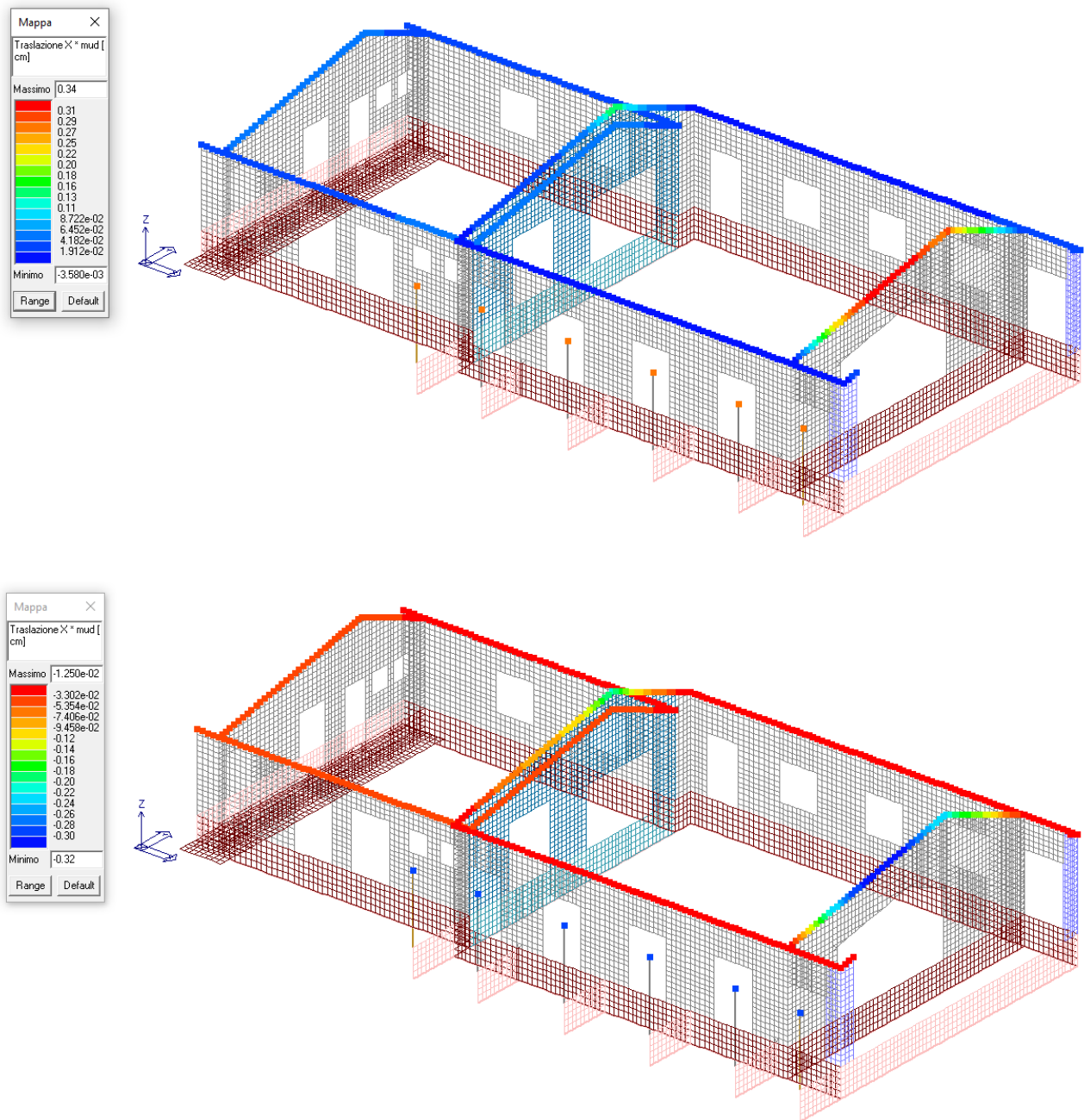


Fig 22. Spostamento max involucro in direzione X-X in cmb. sismica $d_{E,x-x} [= \mu d_{Ee}]$.

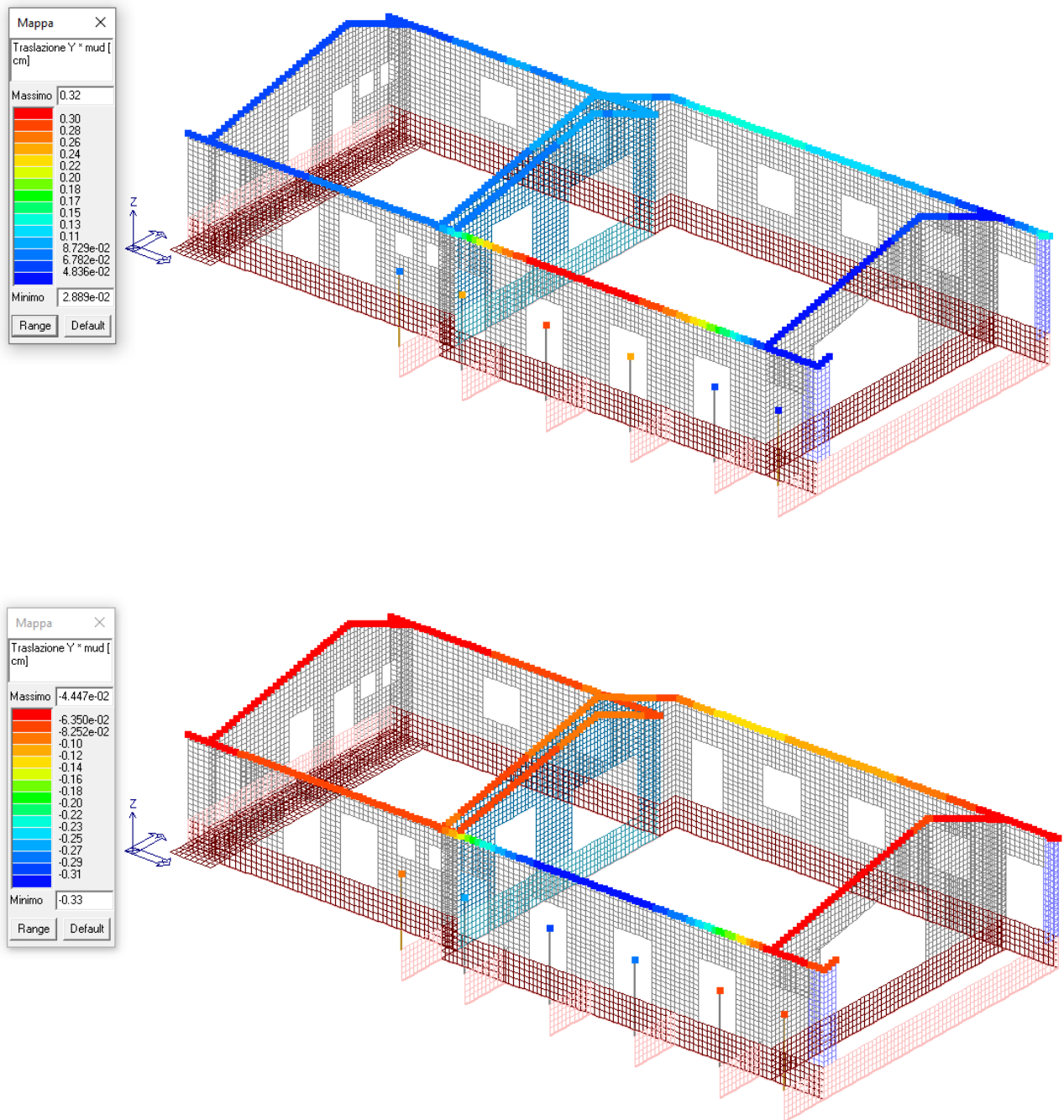


Fig 23. Spostamento max involucro in direzione Y-Y in cmb. sismica $d_{E,Y-Y} [= \mu_d d_{E0}]$.

2.2 Verifiche agli Stati Limite Ultimi

Nella presente sezione si riportano le verifiche agli Stati Limite Ultimi dei vari **ELEMENTI STRUTTURALI** costituenti l'edificio in oggetto, con riferimento al modello di calcolo descritto precedentemente (§1. **“Illustrazione Sintetica degli Elementi Essenziali del progetto Strutturale”**) nel presente documento.

2.2.1 Verifica pareti in Blocchi ISOTEX.

Il progetto e la verifica strutturale delle pareti in blocchi ISOTEX è stato svolto mediante l'ausilio di programma di calcolo Pro-Sap, implementando i risultati delle analisi ottenute dal solutore di calcolo sul modello strutturale delle elevazioni.

Parametri sismici di riferimento e Criteri di Progetto:

- Terreno: Cat. **“B” – T1**
- Comportamento Strutturale: **NON DISSIPATIVO;**
- Fattore di Comportamento: **$q_x=q_y= 1.5$**
- Progettazione ***Non Dissipativa in Campo Sostanzialmente Elastico.***

Materiali:

- Blocchi cassero:

| | | |
|---------------------------|---------------------|---------------------------------|
| Tipologia | HB 20 ISOTEX | |
| Dimensioni blocco singolo | 20x50 cm | |
| Spessore netto | 14 cm | (solo cls) |
| Lunghezza netta | 37 cm | (solo cls) |
| Spessore equivalente | 11.2 cm | (spessore modellato - solo cls) |

| | | |
|---------------------------|---------------------------|---------------------------------|
| Tipologia | HB III38/14 ISOTEX | |
| Dimensioni blocco singolo | 38x50 cm | |
| Spessore netto | 15 cm | (solo cls) |
| Lunghezza netta | 40 cm | (solo cls) |
| Spessore equivalente | 12 cm | (spessore modellato - solo cls) |

- Calcestruzzo **C25/30;**

- Acciaio **B450C.**

2.2.1.1 Legenda Verifiche da Modello di Calcolo

La progettazione viene svolta in **campo sostanzialmente elastico** per **sistemi a comportamento NON DISSIPATIVO** come Pareti Estese Debolmente Armate costituite da elementi D3, in accordo con il DM17.01.2018 e le *Linee Guida per sistemi costruttivi a pannelli portanti basati sull'impiego di blocchi cassero e calcestruzzo debolmente armato gettato in opera*.

Tra le verifiche vengono riportati in mappe cromatiche sintetiche:

- **V N/M** Verifica delle sollecitazioni Normali (momento e sforzo normale) verificato se ≤ 1.0 ;
- **Ver. Nsismica.** Rapporto N_d/N_u (N_u ottenuto considerando $0.25 \cdot f_{cd}$ come resistenza ultima del calcestruzzo in accordo con il §7.3 delle *Linee guida* precedentemente introdotte) per cui, considerato che il codice di calcolo riporta la verifica in accordo con il §7.4.4.5.1 DM17.01.2018 (secondo cui N_u è ottenuto considerando $0.40 \cdot f_{cd}$ trattandosi di pareti progettate in campo non dissipativo), la verifica è da ritenersi soddisfatta se il rapporto **$N_d/N_u \leq 0.25/0.4 = 0.625$** . (Solo Pareti, non pertinente per fasce di piano)
- **Verifica Snellezza** Verifica di snellezza in accordo con il §4.1.2.3.9.2 DM17.01.2018, verificato se ≤ 1.0 . (Solo Pareti, non pertinente per fasce di piano)
- **Verifica V compressione** Verifica a taglio compressione (lato cls).
- **Verifica V trazione** Verifica a taglio trazione (lato acciaio).
- **Af pr+** quantità di armatura richiesta in direzione principale relativa alla faccia positiva (Verticale per setti) (valore derivante da calcolo o minimo normativo) espressa in **cm^2/m** ;
- **Af pr-** quantità di armatura richiesta in direzione principale relativa alla faccia negativa (verticale per setti) (valore derivante da calcolo o minimo normativo) espressa in **cm^2/m** ;
- **Af sec+** quantità di armatura richiesta in direzione secondaria relativa alla faccia positiva (orizzontale per setti) (valore derivante da calcolo o minimo normativo) espressa in **cm^2/m** ;
- **Af sec-** quantità di armatura richiesta in direzione secondaria relativa alla faccia negativa orizzontale per setti) (valore derivante da calcolo o minimo normativo) espressa in **cm^2/m** .

2.2.1.2 Mappe cromatiche sintetiche di verifica da modello di calcolo

Si riportano le mappe cromatiche sintetiche di verifica, in accordo con quanto descritto in precedenza, delle pareti. Nella figura successiva si riporta una vista di insieme del sistema di pareti in blocchi ISOTEX oggetto di verifica.

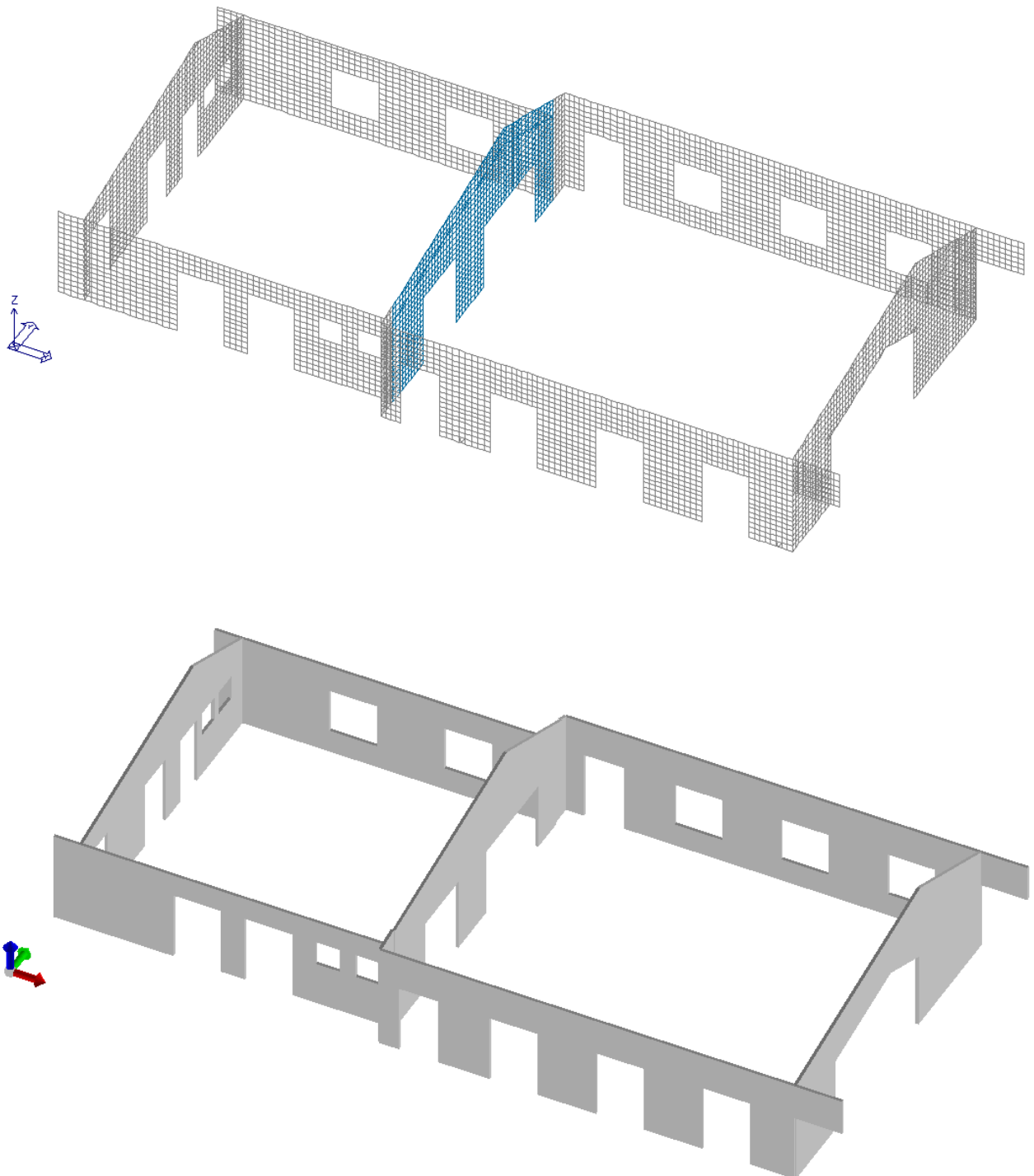


Fig 24. Pareti in ISOTEX oggetto di verifica – Vista Unifilare – Vista solida.

Verifica SLU N/M

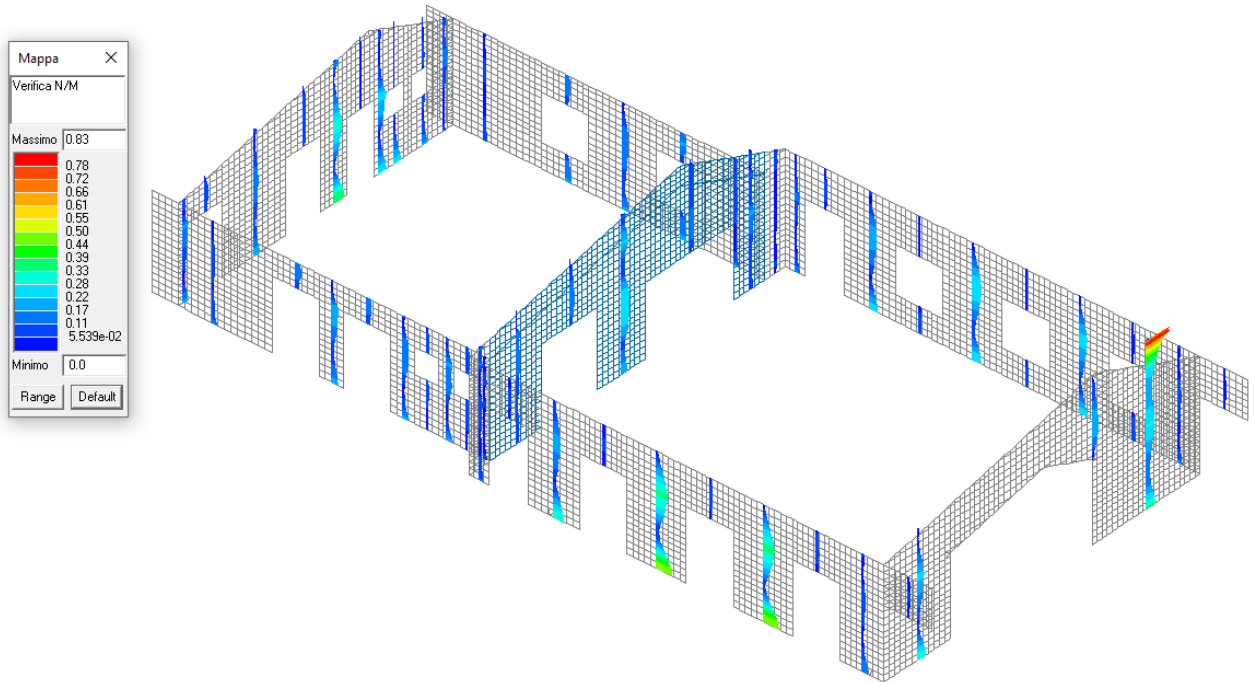


Fig 25. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

Verifica SLU Nsismica

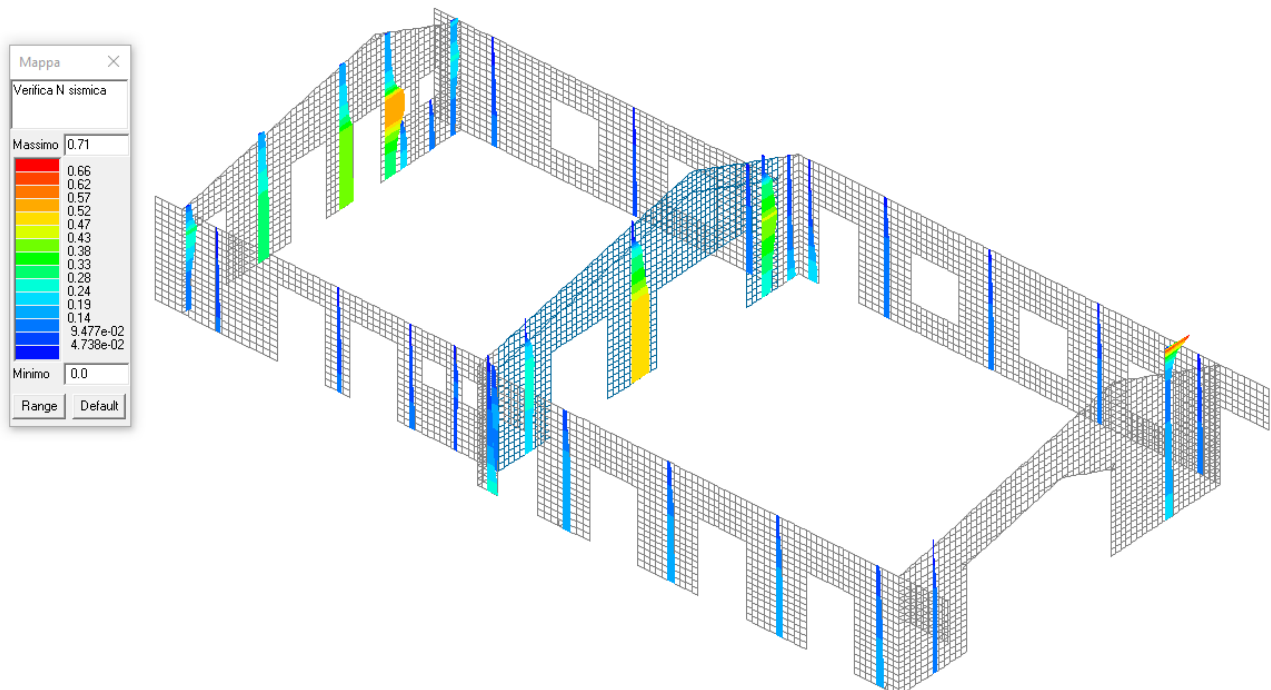


Fig 26. SLU: Mappa di verifica Nsismica – Verifiche soddisfatte ($\rho \leq 0.625$).

Verifiche SLU Snellezza

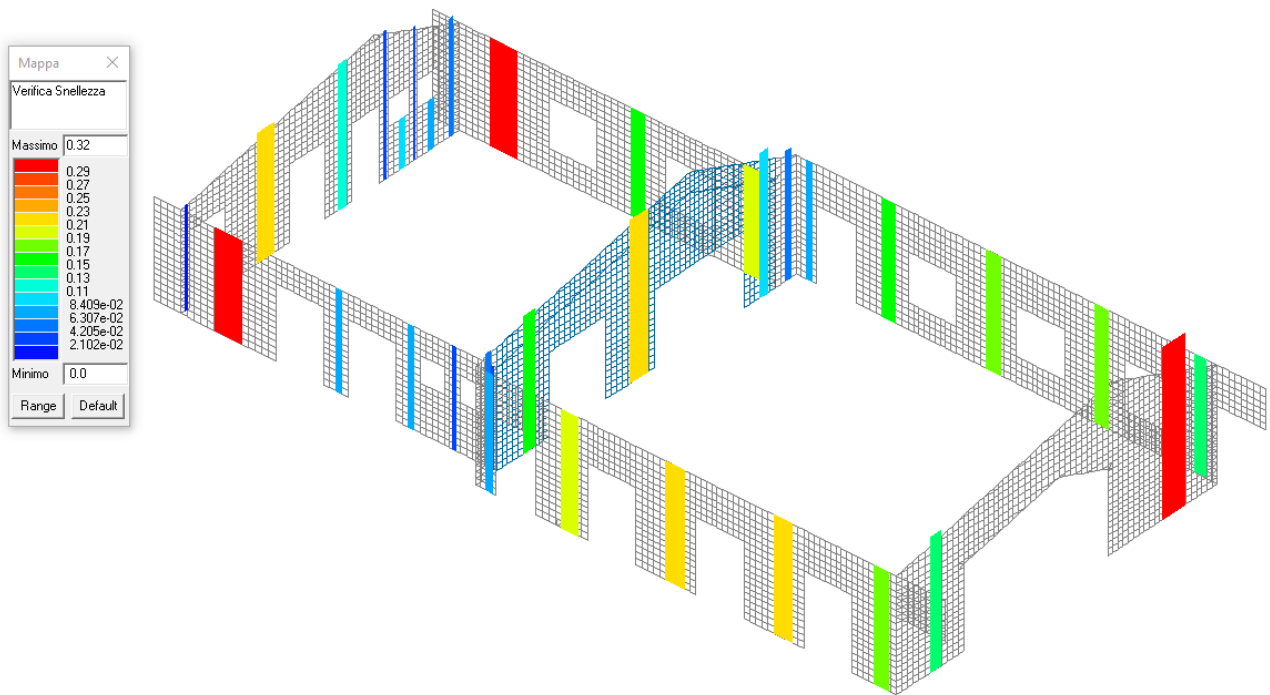


Fig 27. SLU: Mappa di Verifica Snellezza – **Verifiche soddisfatte ($\rho \leq 1$).**

Verifica SLU V compressione

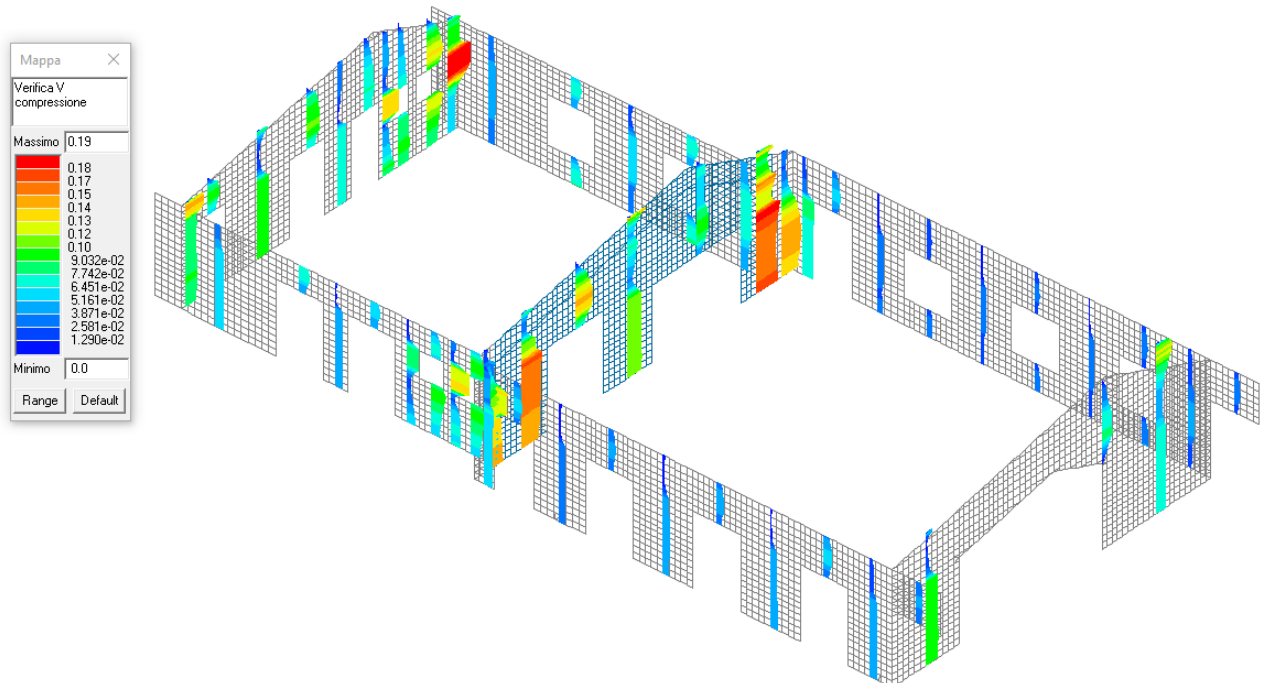


Fig 28. SLU: Mappa di Verifica V compressione – **Verifica soddisfatta ($\rho \leq 1$).**

Verifica SLU V trazione

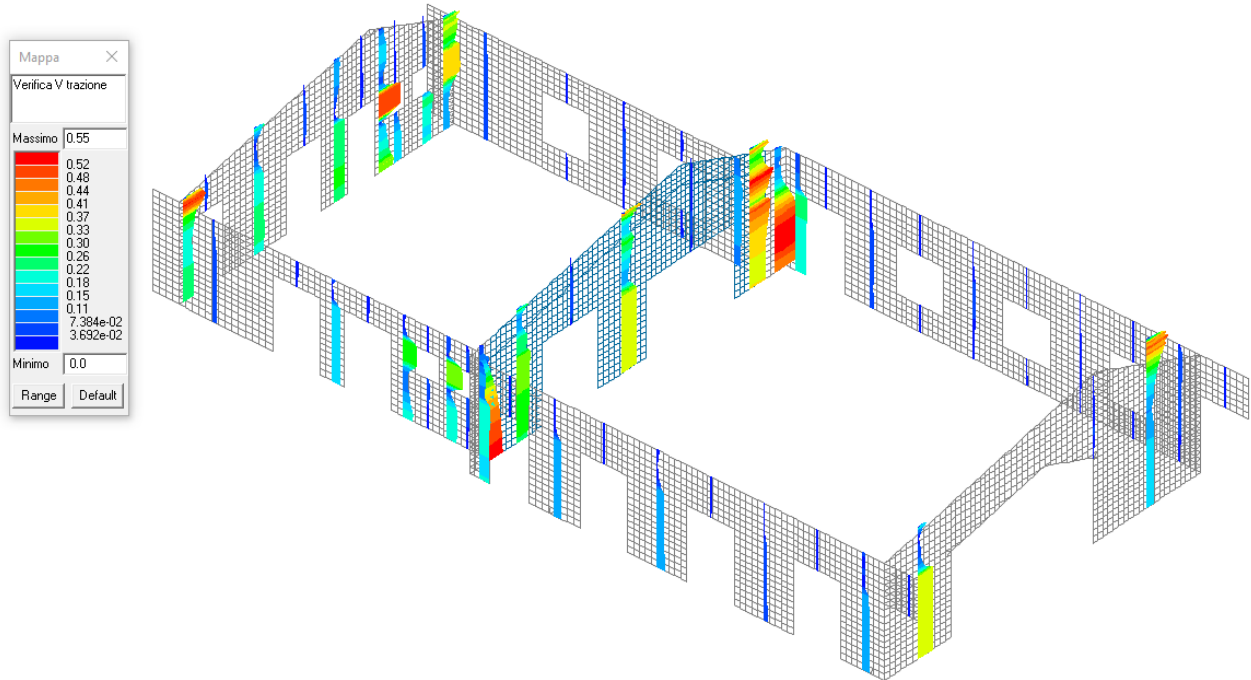


Fig 29. SLU: Mappa di verifica V trazione – Verifiche soddisfatte ($\rho \leq 1$).

Mappa Armatura Verticale di Verifica

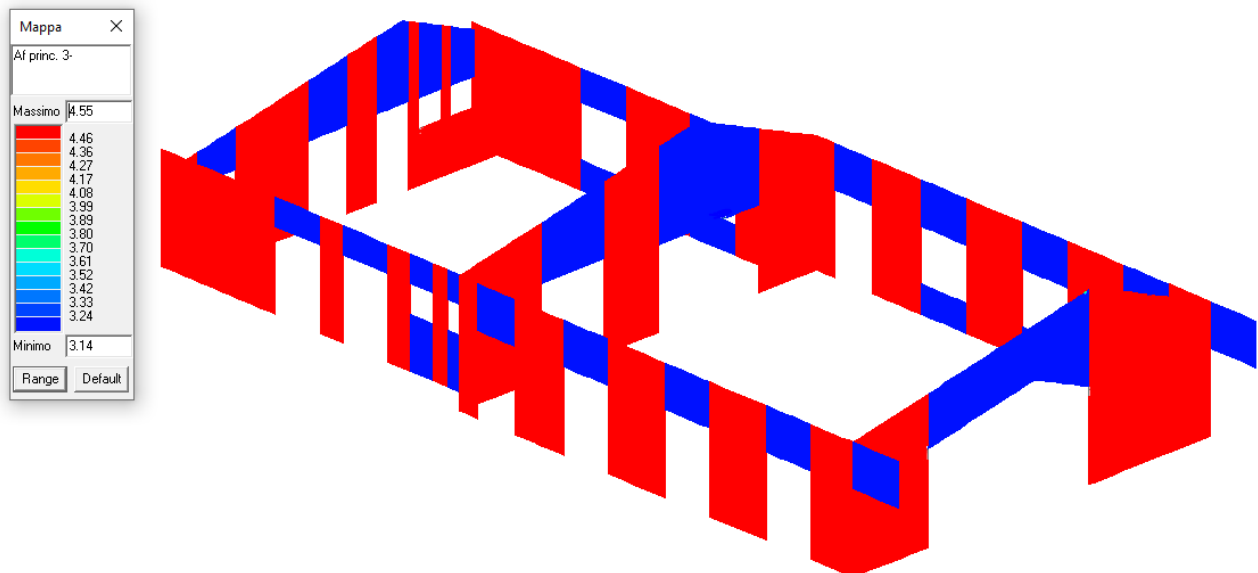


Fig 30. Mappa Armatura Verticale -singolo strato - di Verifica [cm²/m].

Mappa Armatura Orizzontale da Calcolo

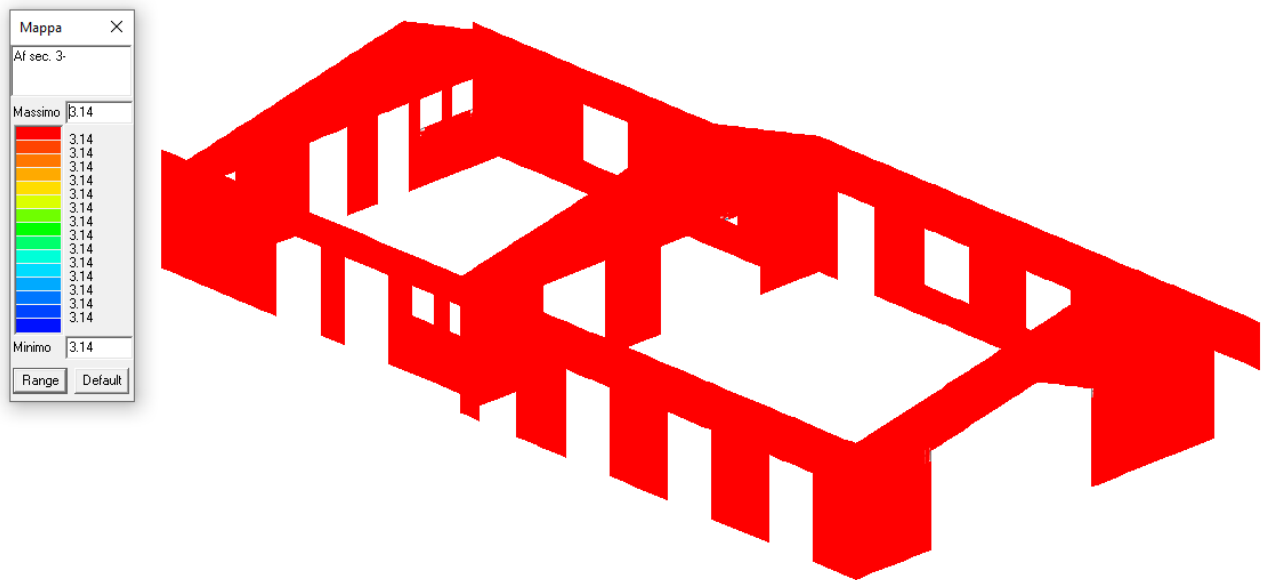


Fig 31. Mappa Armatura Orizzontale – singolo strato - di Verifica [cm^2/m]. .

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

2.2.1.3 Verifiche Analitiche da Modello di Calcolo

Nel seguente paragrafo si riportano le verifiche analitiche dettagliate per ogni parete del fabbricato in oggetto da Modello di Calcolo. Si riporta la legenda dei tabulati di calcolo che sono esposti in seguito.

Per gli elementi con progettazione “Parete Sismica o Parete Debolmente Armata” sono riportate le seguenti tabelle con i simboli di seguito descritti:

| | |
|--------------------|---|
| Parete PDA | Numero della PARETE DEBOLMENTE ARMATA |
| H totale | Altezza complessiva della parete |
| Spessore | Spessore della parete |
| L totale | Larghezza di base della parete |
| Verif. N | Verifica di cui al punto 7.4.4.5.1 compressione semplice |
| Verif. N-M | Verifica di cui al punto 7.4.4.5.1 pressoflessione |
| Fattore V | Fattore di amplificazione del taglio di cui al punto 7.4.4.5.1 |
| Verif. V | Verifica di cui al punto 7.4.4.5.1 taglio (compressione cls, trazione acciaio) |
| Verifica Snellezza | Verifica di cui al punto 7.4.4.5.1 limitazione compressione per prevenire l'instabilità (solo in Parete Debolmente Armata – Non pertinente per elementi fascia) |
| Prog. composta | Sigla per la progettazione composta |

| | |
|------------|---|
| Quota | Ascissa verticale di riferimento |
| Af std | Diametro e passo armatura in zona non confinata (doppia maglia) |
| Af estremi | Diametro dei ferri di estremità del pannello; se posto uguale 0, viene utilizzato il diametro standard |
| Af V (ori) | Diametro e passo armatura orizzontale (doppia maglia) |
| Ver. N | Rapporto tra azione di calcolo e resistenza a compressione (normalizzato a 1 in quanto da confrontare con 40% in CDB). In accordo con il §7.3 delle Linee guida precedentemente introdotte, per le <i>pareti estese debolmente armate in blocchi cassero</i> occorre limitare al 25%, per cui le verifiche sono da intendersi soddisfatte se il rapporto di verifica risulta minore o uguale a 0.625. |
| Ver. N/M | Rapporto tra azione di calcolo e resistenza a pressoflessione |
| Ver. V cls | Rapporto tra azione di calcolo e resistenza a taglio-compressione |
| Ver. V acc | Rapporto tra azione di calcolo e resistenza a taglio-trazione |
| N add | Sforzo assiale di cui al punto 7.4.4.5.1 da sommare e sottrarre nelle verifiche quando q supera 2 |

| | |
|-------------------------------|---|
| Quota | Ascissa verticale di riferimento |
| N v.N | Valore dello sforzo assiale per cui Ver. N attinge il massimo valore |
| N v.M/N, M v.M/N | Valore dello sforzo assiale e momento per cui Ver. N/M attinge il massimo valore |
| N v.M/N, M v.M/N Mo v.M/N | Valore dello sforzo assiale e dei momenti per cui Ver. N/M attinge il massimo valore (per le pareti estese debolmente armate) |
| N v.Vcls, V v.Vcls, | Valore dello sforzo assiale e taglio per cui Ver. V. cls attinge il massimo valore |
| N v.Vacc, M v.Vacc, V v.Vacc, | Valore dello sforzo assiale, momento e taglio per cui Ver. V. acc attinge il massimo valore |
| N v.N | Valore dello sforzo assiale per cui Ver. N attinge il massimo valore |
| N v.M/N, M v.M/N | Valore dello sforzo assiale e momento per cui Ver. N/M attinge il massimo valore |
| N v.M/N, M v.M/N Mo v.M/N | Valore dello sforzo assiale e dei momenti per cui Ver. N/M attinge il massimo valore (per le pareti estese debolmente armate) |
| N v.Vcls, V v.Vcls, | Valore dello sforzo assiale e taglio per cui Ver. V. cls attinge il massimo valore |

| | |
|-----------|---|
| Quota | Ascissa verticale di riferimento |
| CtgT Vcls | Valore di ctg(teta) adottato nella verifica V compressione cls |
| Vrsd Vcls | Valore della resistenza a taglio trazione (armatura di calcolo) |
| Vrcd Vcls | Valore della resistenza a taglio compressione |
| CtgT Vacc | Valore di ctg(teta) adottato nella verifica V trazione armatura |
| Vrsd Vacc | Valore della resistenza a taglio trazione (armatura presente) |
| Vrcd Vacc | Valore della resistenza a taglio compressione |

1.1.1.1.1 Parete Fronte Nord - Ovest

Si riportano le verifiche analitiche dei macroelementi della parete oggetto di verifica identificata nella figura successiva.

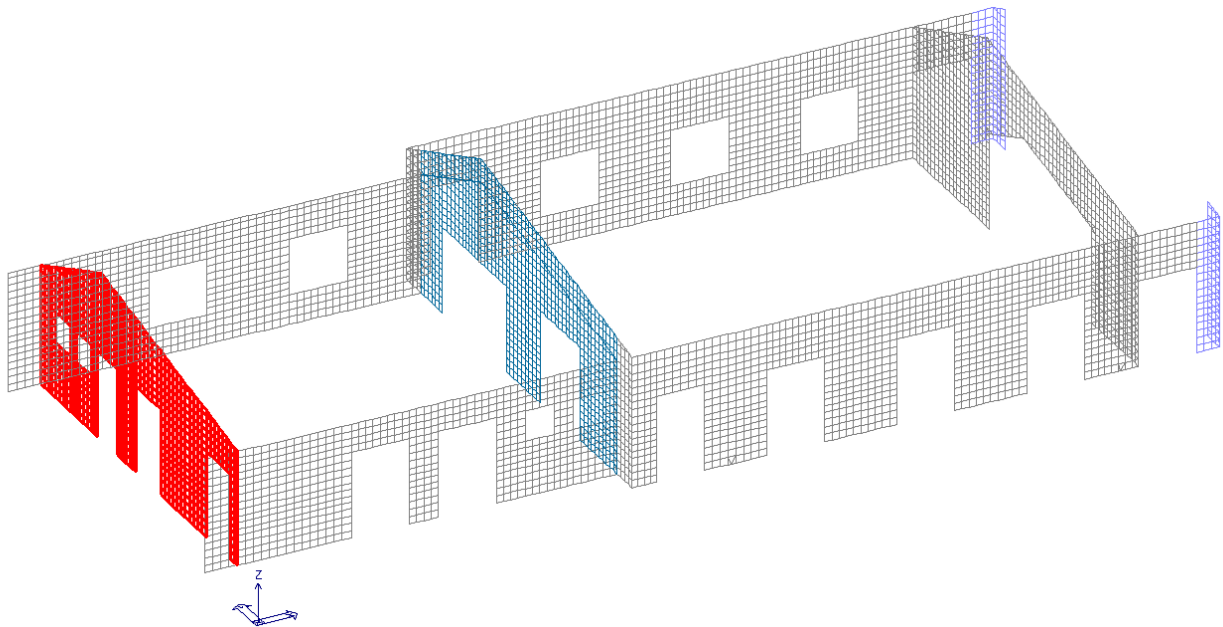


Fig 32. Parete oggetto di verifica (selezione in rosso).

Macrosetti n. 24, 25, 28, 88, 98, 99 [maschi]

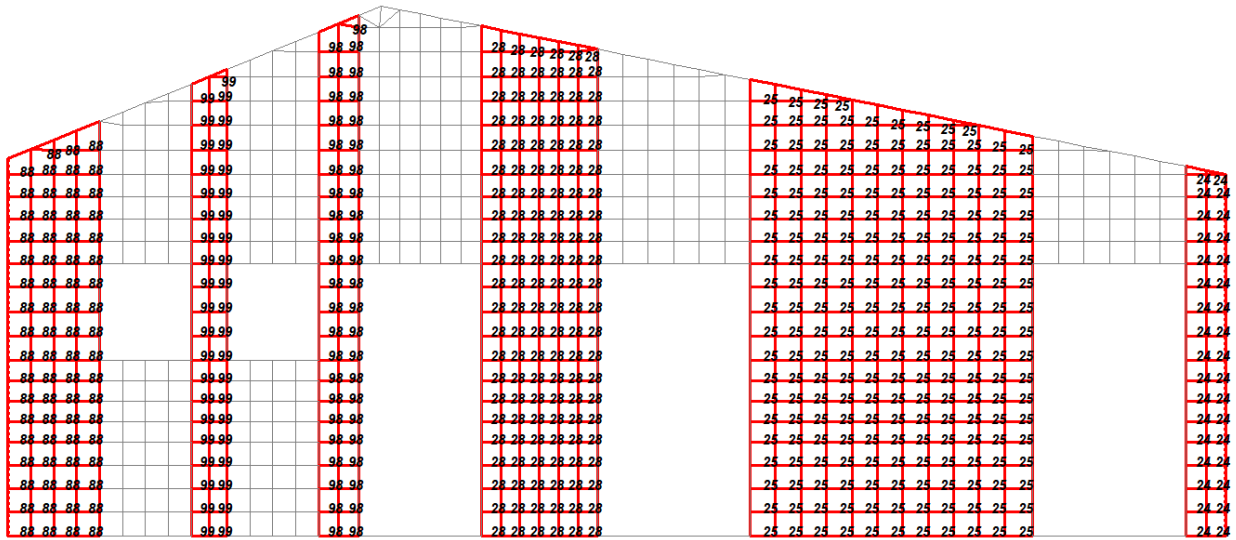


Fig 33. Elemento/i oggetto di verifica (in rosso).

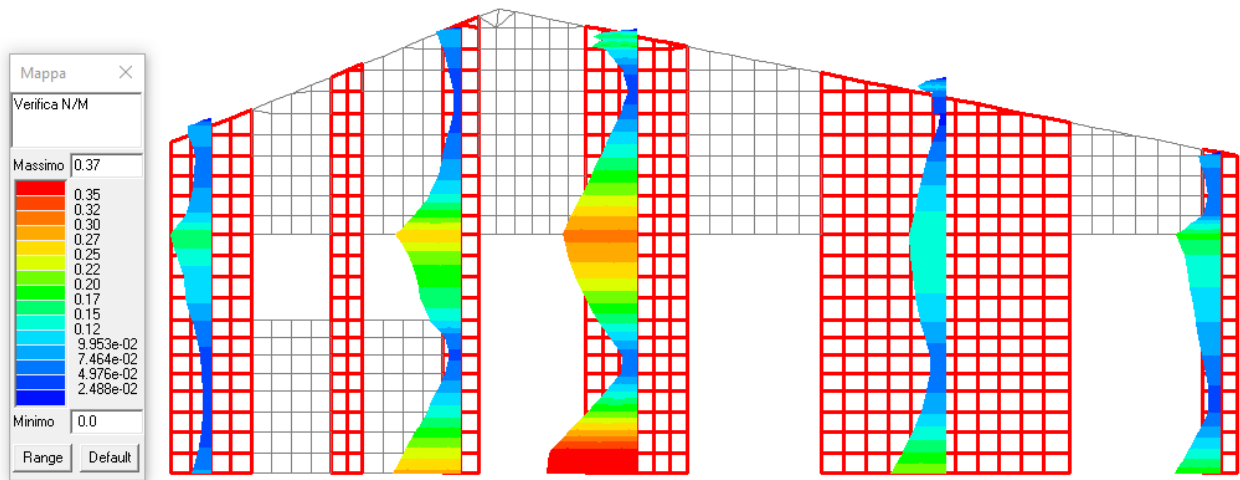


Fig 34. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

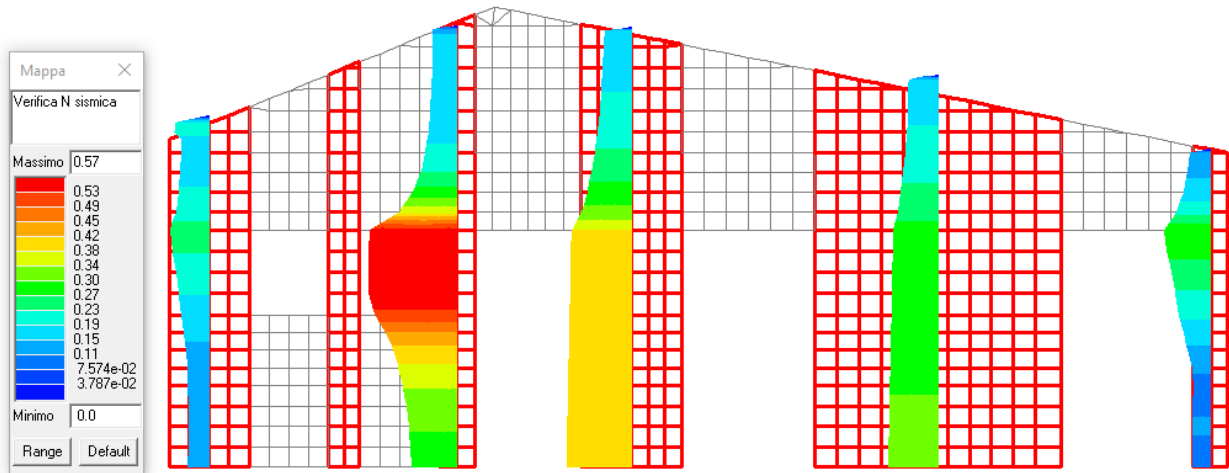


Fig 35. SLU: Mappa di verifica N sismica – **Verifiche soddisfatte ($\rho \leq 0.625$).**

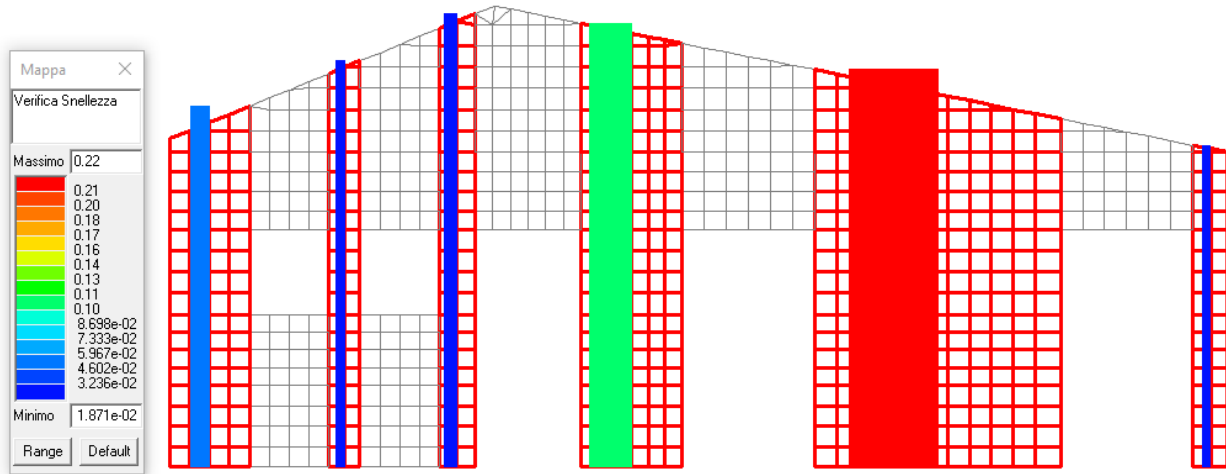


Fig 36. SLU: Mappa di Verifica Snellezza – **Verifiche soddisfatte ($\rho \leq 1$).**

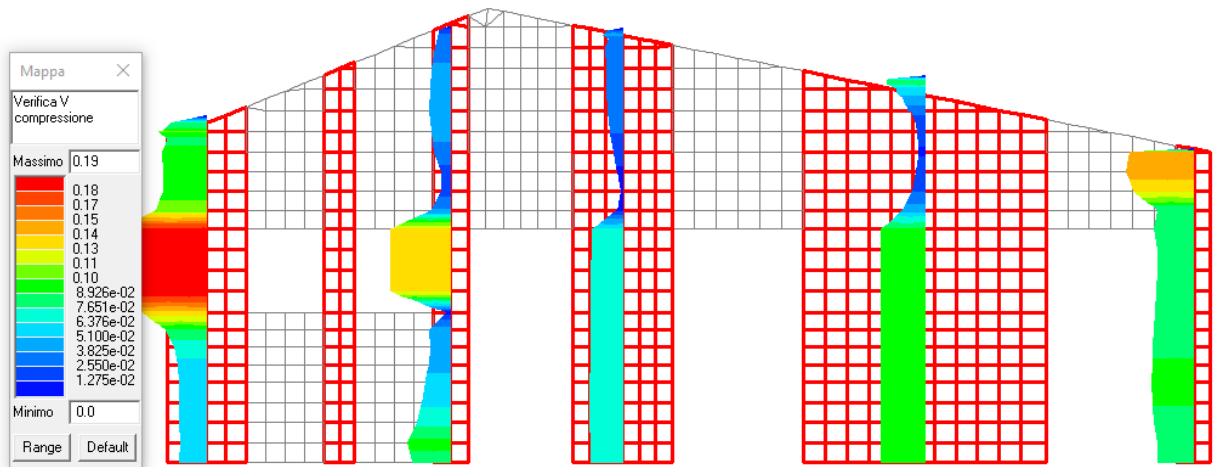


Fig 37. SLU: Mappa di Verifica V compressione – **Verifica soddisfatta ($\rho \leq 1$).**

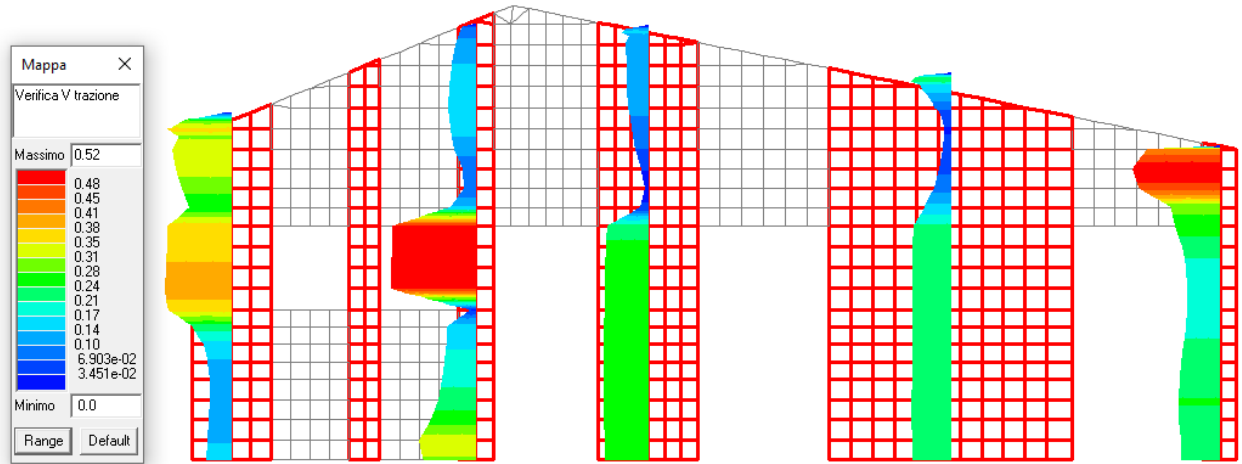


Fig 38. SLU: Mappa di verifica V trazione – Verifiche soddisfatte ($\rho \leq 1$).

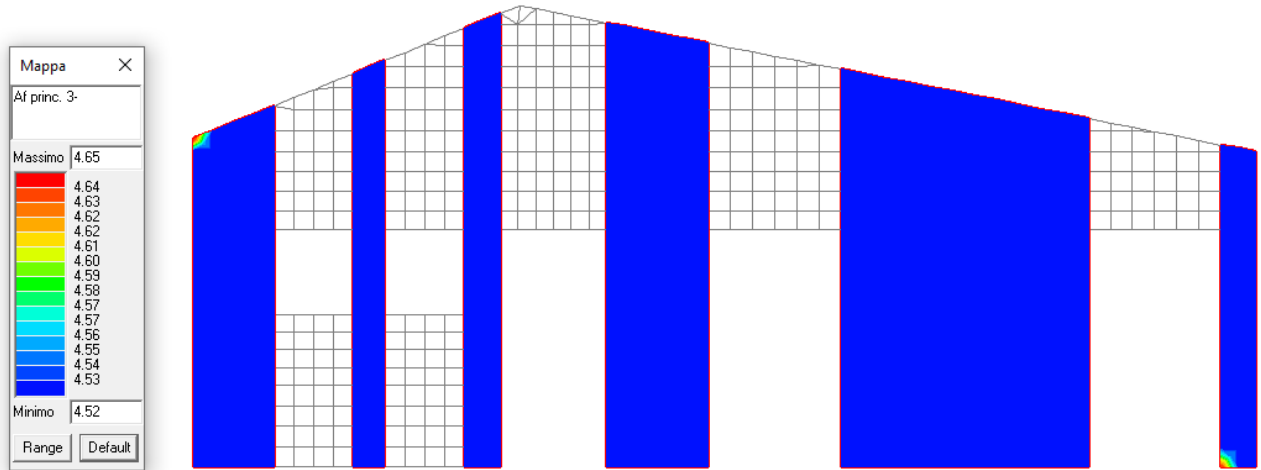


Fig 39. Mappa Armatura Verticale (singolo strato) da Calcolo [cm^2/m].

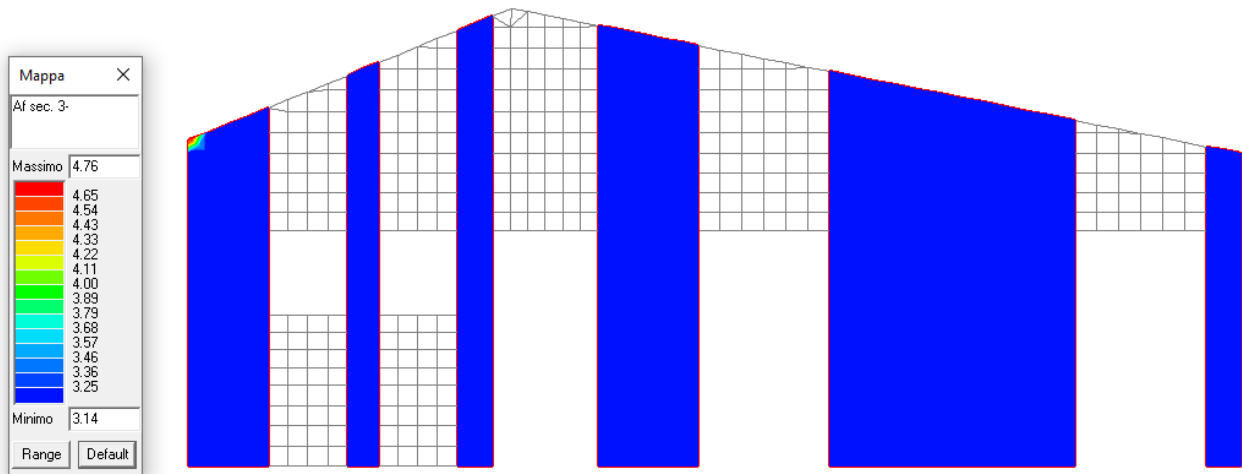


Fig 40. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm^2/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 24 | 362.76 | 12.00 | 39.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.19 | 0.02 | 0.08 | 0.23 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.14 | 0.02 | 0.08 | 0.23 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.09 | 0.02 | 0.09 | 0.24 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.05 | 0.02 | 0.09 | 0.24 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.05 | 0.02 | 0.09 | 0.24 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.06 | 0.02 | 0.09 | 0.22 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.07 | 0.02 | 0.09 | 0.21 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.09 | 0.02 | 0.09 | 0.20 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.20 | 0.10 | 0.02 | 0.08 | 0.19 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.12 | 0.02 | 0.08 | 0.19 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.25 | 0.13 | 0.02 | 0.08 | 0.20 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.28 | 0.15 | 0.02 | 0.08 | 0.22 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.30 | 0.18 | 0.02 | 0.09 | 0.26 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.21 | 0.07 | 0.02 | 0.08 | 0.28 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.05 | 0.02 | 0.13 | 0.47 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.07 | 0.02 | 0.15 | 0.52 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.09 | 0.02 | 0.14 | 0.43 | 0.0 |
| 358.8 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 362.8 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.30 | 0.19 | 0.02 | 0.15 | 0.52 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1823.84 | 296.61 | 2.688e+04 | 256.63 | -911.92 | 1186.18 | 854.66 | 721.68 |
| 23.0 | -1823.84 | 1186.18 | 1.766e+04 | 105.43 | -911.92 | 1186.18 | 854.66 | 721.68 |
| 46.0 | -1920.98 | 792.69 | 1.179e+04 | 78.28 | -911.92 | 792.69 | 927.14 | 752.93 |
| 69.0 | -1832.27 | 245.65 | 6902.31 | 72.06 | -911.92 | 245.65 | 976.19 | 762.28 |
| 92.0 | -1748.62 | -1590.30 | 7819.36 | 47.68 | -911.92 | -456.31 | 990.76 | 740.54 |
| 112.0 | -1936.65 | -1871.95 | 9745.06 | 28.73 | -911.92 | -998.42 | 989.58 | 707.19 |
| 132.0 | -2385.60 | -2335.43 | 1.323e+04 | 16.83 | -911.92 | -1550.20 | 979.02 | 665.60 |
| 152.0 | -2820.49 | -2771.52 | 1.635e+04 | 3.67 | -911.92 | -2053.62 | 963.82 | 624.59 |
| 172.0 | -3245.24 | -3183.01 | 1.906e+04 | 11.23 | -911.92 | -2561.02 | 946.06 | 601.34 |
| 196.0 | -3682.70 | -3589.54 | 2.286e+04 | 35.16 | -911.92 | -3082.05 | 923.37 | 589.60 |
| 220.0 | -4130.16 | -4130.16 | 2.630e+04 | 80.07 | -911.92 | -3718.21 | 906.32 | 619.47 |
| 244.0 | -4552.73 | -4552.73 | 3.069e+04 | 163.83 | -911.92 | -4255.91 | 913.95 | 698.12 |
| 267.0 | -4911.18 | -4829.71 | 3.794e+04 | 1937.26 | -911.92 | -4672.61 | 1004.36 | 830.54 |
| 289.0 | -3538.49 | -3227.51 | 1.284e+04 | 448.65 | -911.92 | -3538.49 | 890.93 | 890.93 |
| 311.0 | -2800.25 | -2800.25 | 9036.41 | 365.23 | -911.92 | -2787.05 | 1485.36 | 1485.36 |
| 333.0 | -2384.92 | -2322.87 | 1.118e+04 | 664.15 | -911.92 | -2016.10 | 1640.23 | 1627.59 |
| 355.0 | -2128.21 | -1876.15 | 1.381e+04 | 1759.46 | -911.92 | -1694.97 | 1559.12 | 1339.20 |
| 358.8 | 0.0 | 0.0 | 0.0 | 0.0 | -911.92 | 0.0 | 0.0 | 0.0 |
| 362.8 | 0.0 | 0.0 | 0.0 | 0.0 | -911.92 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 854.66 | 1.084e+04 | 1.00 | 3143.91 | 1.084e+04 |
| 23.0 | 1.00 | 854.66 | 1.084e+04 | 1.00 | 3143.91 | 1.084e+04 |
| 46.0 | 1.00 | 927.14 | 1.084e+04 | 1.00 | 3143.91 | 1.088e+04 |
| 69.0 | 1.00 | 976.19 | 1.084e+04 | 1.00 | 3143.91 | 1.097e+04 |
| 92.0 | 1.00 | 990.76 | 1.091e+04 | 1.00 | 3143.91 | 1.106e+04 |
| 112.0 | 1.00 | 989.58 | 1.100e+04 | 1.00 | 3143.91 | 1.114e+04 |
| 132.0 | 1.00 | 979.02 | 1.109e+04 | 1.00 | 3143.91 | 1.122e+04 |
| 152.0 | 1.00 | 963.82 | 1.117e+04 | 1.00 | 3143.91 | 1.130e+04 |
| 172.0 | 1.00 | 946.06 | 1.126e+04 | 1.00 | 3143.91 | 1.137e+04 |
| 196.0 | 1.00 | 923.37 | 1.134e+04 | 1.00 | 3143.91 | 1.140e+04 |
| 220.0 | 1.00 | 906.32 | 1.145e+04 | 1.00 | 3143.91 | 1.143e+04 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| 244.0 | 1.00 | 913.95 | 1.153e+04 | 1.00 | 3143.91 | 1.151e+04 |
| 267.0 | 1.00 | 1004.36 | 1.160e+04 | 1.00 | 3143.91 | 1.158e+04 |
| 289.0 | 1.00 | 890.93 | 1.142e+04 | 1.00 | 3143.91 | 1.142e+04 |
| 311.0 | 1.00 | 1485.36 | 1.129e+04 | 1.00 | 3143.91 | 1.129e+04 |
| 333.0 | 1.00 | 1640.23 | 1.117e+04 | 1.00 | 3143.91 | 1.122e+04 |
| 355.0 | 1.00 | 1559.12 | 1.111e+04 | 1.00 | 3143.91 | 1.117e+04 |
| 358.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 362.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 25 | 447.95 | 12.00 | 278.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.31 | 0.22 | 0.22 | 0.09 | 0.22 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.31 | 0.18 | 0.22 | 0.09 | 0.22 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.31 | 0.14 | 0.22 | 0.10 | 0.23 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.30 | 0.10 | 0.22 | 0.10 | 0.22 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.30 | 0.07 | 0.22 | 0.10 | 0.22 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.30 | 0.06 | 0.22 | 0.10 | 0.22 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.30 | 0.06 | 0.22 | 0.10 | 0.22 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.29 | 0.08 | 0.22 | 0.10 | 0.22 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.29 | 0.10 | 0.22 | 0.10 | 0.22 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.29 | 0.12 | 0.22 | 0.09 | 0.22 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.29 | 0.14 | 0.22 | 0.09 | 0.22 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.28 | 0.14 | 0.22 | 0.09 | 0.22 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.28 | 0.15 | 0.22 | 0.09 | 0.22 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.25 | 0.13 | 0.22 | 0.05 | 0.15 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.24 | 0.11 | 0.22 | 0.03 | 0.09 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.09 | 0.22 | 0.02 | 0.06 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.21 | 0.07 | 0.22 | 0.01 | 0.04 | 0.0 |
| 379.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.04 | 0.22 | 0.02 | 0.03 | 0.0 |
| 392.6 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.02 | 0.22 | 0.02 | 0.05 | 0.0 |
| 398.2 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.02 | 0.22 | 0.03 | 0.07 | 0.0 |
| 403.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.02 | 0.22 | 0.03 | 0.08 | 0.0 |
| 403.2 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.05 | 0.22 | 0.04 | 0.09 | 0.0 |
| 408.1 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.04 | 0.22 | 0.04 | 0.10 | 0.0 |
| 413.1 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.05 | 0.22 | 0.05 | 0.12 | 0.0 |
| 418.1 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.05 | 0.22 | 0.05 | 0.13 | 0.0 |
| 423.1 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.05 | 0.22 | 0.06 | 0.17 | 0.0 |
| 427.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.05 | 0.22 | 0.06 | 0.17 | 0.0 |
| 428.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.08 | 0.22 | 0.06 | 0.16 | 0.0 |
| 433.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.11 | 0.22 | 0.08 | 0.22 | 0.0 |
| 438.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.09 | 0.22 | 0.08 | 0.21 | 0.0 |
| 443.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.22 | 0.0 | 0.0 | 0.0 |
| 447.9 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.22 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.31 | 0.22 | 0.22 | 0.10 | 0.23 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|------------|------------|-----------|-----------|------------|------------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -3.652e+04 | -2.224e+04 | 1.183e+05 | 8.458e+04 | -1.826e+04 | -2.462e+04 | 9315.40 | 5986.12 |
| 23.0 | -3.652e+04 | -2.280e+04 | 3.705e+05 | 6.480e+04 | -1.826e+04 | -2.462e+04 | 9315.40 | 5986.12 |
| 46.0 | -3.618e+04 | -2.256e+04 | 3.340e+05 | 4.918e+04 | -1.826e+04 | -2.436e+04 | 9449.18 | 6119.90 |
| 69.0 | -3.585e+04 | -2.230e+04 | 2.974e+05 | 3.402e+04 | -1.826e+04 | -2.410e+04 | 9435.96 | 6106.68 |
| 92.0 | -3.551e+04 | -2.384e+04 | 6.866e+05 | 453.52 | -1.826e+04 | -2.384e+04 | 9421.12 | 6091.84 |
| 112.0 | -3.520e+04 | -2.358e+04 | 5.298e+05 | 3560.47 | -1.826e+04 | -2.358e+04 | 9404.37 | 6075.09 |
| 132.0 | -3.491e+04 | -2.085e+04 | 6815.77 | 2.216e+04 | -1.826e+04 | -2.341e+04 | 9386.08 | 6056.80 |
| 152.0 | -3.462e+04 | -2.063e+04 | 2.208e+04 | 3.082e+04 | -1.826e+04 | -2.315e+04 | 9364.78 | 6035.50 |
| 172.0 | -3.433e+04 | -2.040e+04 | 5.098e+04 | 3.802e+04 | -1.826e+04 | -2.284e+04 | 9340.43 | 6011.15 |
| 196.0 | -3.401e+04 | -2.016e+04 | 8.566e+04 | 4.479e+04 | -1.826e+04 | -2.266e+04 | 9310.23 | 5980.95 |
| 220.0 | -3.366e+04 | -1.989e+04 | 1.203e+05 | 4.954e+04 | -1.826e+04 | -2.227e+04 | 9272.92 | 5943.63 |
| 244.0 | -3.331e+04 | -1.962e+04 | 1.550e+05 | 5.235e+04 | -1.826e+04 | -2.205e+04 | 9231.54 | 5902.25 |
| 267.0 | -3.297e+04 | -1.936e+04 | 1.882e+05 | 5.324e+04 | -1.826e+04 | -2.192e+04 | 9186.88 | 5857.60 |
| 289.0 | -2.981e+04 | -1.849e+04 | 2.725e+05 | 4.490e+04 | -1.826e+04 | -1.977e+04 | 4503.69 | 4113.04 |
| 311.0 | -2.771e+04 | -1.720e+04 | 2.409e+05 | 3.813e+04 | -1.826e+04 | -1.548e+04 | 2463.59 | 2463.59 |
| 333.0 | -2.585e+04 | -1.615e+04 | 2.227e+05 | 3.074e+04 | -1.826e+04 | -1.431e+04 | 1671.38 | 1671.38 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|------------|------------|-----------|-----------|------------|------------|----------|----------|
| 355.0 | -2.423e+04 | -1.518e+04 | 1.958e+05 | 2.285e+04 | -1.826e+04 | -1.346e+04 | 1123.27 | 1123.27 |
| 379.0 | -2.276e+04 | -1.427e+04 | 1.214e+05 | 1.365e+04 | -1.826e+04 | -1.486e+04 | 1514.98 | 885.40 |
| 392.6 | -2.199e+04 | -1.410e+04 | 1.790e+05 | 1667.34 | -1.826e+04 | -1.415e+04 | 2078.27 | 1279.76 |
| 398.2 | -1.989e+04 | -1.298e+04 | 1.268e+05 | 81.08 | -1.826e+04 | -1.298e+04 | 2175.70 | 1533.81 |
| 403.0 | -1.795e+04 | -1.110e+04 | 6.546e+04 | 4224.32 | -1.826e+04 | -1.186e+04 | 2245.23 | 1702.32 |
| 403.2 | -1.759e+04 | -1.027e+04 | 7425.33 | 1.148e+04 | -1.826e+04 | -1.145e+04 | 2576.26 | 1797.06 |
| 408.1 | -1.567e+04 | -9103.38 | 1802.41 | 1.024e+04 | -1.826e+04 | -1.024e+04 | 2453.02 | 1815.50 |
| 413.1 | -1.375e+04 | -7939.53 | 1839.71 | 9008.83 | -1.826e+04 | -9084.34 | 2378.89 | 1819.91 |
| 418.1 | -1.182e+04 | -6775.35 | 3860.88 | 7791.66 | -1.826e+04 | -7892.56 | 2285.13 | 1788.35 |
| 423.1 | -9891.32 | -5652.03 | 7617.92 | 6572.33 | -1.826e+04 | -6687.57 | 2086.85 | 1636.71 |
| 427.0 | -8352.28 | -4781.13 | 1187.16 | 6099.98 | -1.826e+04 | -5733.78 | 1895.88 | 1482.64 |
| 428.0 | -7782.54 | -4409.77 | 4430.90 | 9596.07 | -1.826e+04 | -5203.62 | 1758.63 | 1402.70 |
| 433.0 | -5840.55 | -3234.77 | 2454.71 | 7229.54 | -1.826e+04 | -4013.68 | 1447.18 | 1102.81 |
| 438.0 | -3854.00 | -2111.32 | 1284.72 | 4873.69 | -1.826e+04 | -2695.93 | 1061.85 | 771.25 |
| 443.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1.826e+04 | 0.0 | 0.0 | 0.0 |
| 447.9 | 0.0 | 0.0 | 0.0 | 0.0 | -1.826e+04 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 9315.40 | 9.853e+04 | 1.00 | 2.717e+04 | 9.787e+04 |
| 23.0 | 1.00 | 9315.40 | 9.853e+04 | 1.00 | 2.717e+04 | 9.787e+04 |
| 46.0 | 1.00 | 9449.18 | 9.848e+04 | 1.00 | 2.717e+04 | 9.782e+04 |
| 69.0 | 1.00 | 9435.96 | 9.843e+04 | 1.00 | 2.717e+04 | 9.777e+04 |
| 92.0 | 1.00 | 9421.12 | 9.838e+04 | 1.00 | 2.717e+04 | 9.772e+04 |
| 112.0 | 1.00 | 9404.37 | 9.832e+04 | 1.00 | 2.717e+04 | 9.768e+04 |
| 132.0 | 1.00 | 9386.08 | 9.829e+04 | 1.00 | 2.717e+04 | 9.762e+04 |
| 152.0 | 1.00 | 9364.78 | 9.824e+04 | 1.00 | 2.717e+04 | 9.758e+04 |
| 172.0 | 1.00 | 9340.43 | 9.818e+04 | 1.00 | 2.717e+04 | 9.755e+04 |
| 196.0 | 1.00 | 9310.23 | 9.814e+04 | 1.00 | 2.717e+04 | 9.749e+04 |
| 220.0 | 1.00 | 9272.92 | 9.806e+04 | 1.00 | 2.717e+04 | 9.746e+04 |
| 244.0 | 1.00 | 9231.54 | 9.802e+04 | 1.00 | 2.717e+04 | 9.740e+04 |
| 267.0 | 1.00 | 9186.88 | 9.799e+04 | 1.00 | 2.717e+04 | 9.732e+04 |
| 289.0 | 1.00 | 4503.69 | 9.757e+04 | 1.00 | 2.717e+04 | 9.696e+04 |
| 311.0 | 1.00 | 2463.59 | 9.671e+04 | 1.00 | 2.717e+04 | 9.671e+04 |
| 333.0 | 1.00 | 1671.38 | 9.648e+04 | 1.00 | 2.717e+04 | 9.648e+04 |
| 355.0 | 1.00 | 1123.27 | 9.631e+04 | 1.00 | 2.717e+04 | 9.631e+04 |
| 379.0 | 1.00 | 1514.98 | 9.659e+04 | 1.00 | 2.717e+04 | 9.646e+04 |
| 392.6 | 1.00 | 2078.27 | 9.645e+04 | 1.00 | 2.717e+04 | 9.634e+04 |
| 398.2 | 1.00 | 2175.70 | 8.289e+04 | 1.00 | 2.333e+04 | 8.276e+04 |
| 403.0 | 1.00 | 2245.23 | 7.870e+04 | 1.00 | 2.215e+04 | 7.992e+04 |
| 403.2 | 1.00 | 2576.26 | 6.976e+04 | 1.00 | 1.965e+04 | 6.965e+04 |
| 408.1 | 1.00 | 2453.02 | 6.542e+04 | 1.00 | 1.842e+04 | 6.643e+04 |
| 413.1 | 1.00 | 2378.89 | 5.235e+04 | 1.00 | 1.474e+04 | 5.315e+04 |
| 418.1 | 1.00 | 2285.13 | 4.801e+04 | 1.00 | 1.351e+04 | 4.873e+04 |
| 423.1 | 1.00 | 2086.85 | 3.493e+04 | 1.00 | 9824.73 | 3.545e+04 |
| 427.0 | 1.00 | 1895.88 | 3.150e+04 | 1.00 | 8854.76 | 3.195e+04 |
| 428.0 | 1.00 | 1758.63 | 3.054e+04 | 1.00 | 8596.64 | 3.099e+04 |
| 433.0 | 1.00 | 1447.18 | 1.747e+04 | 1.00 | 4912.36 | 1.771e+04 |
| 438.0 | 1.00 | 1061.85 | 1.310e+04 | 1.00 | 3684.27 | 1.328e+04 |
| 443.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 447.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 28 | 500.49 | 12.00 | 114.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.41 | 0.37 | 0.11 | 0.07 | 0.25 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.41 | 0.37 | 0.11 | 0.07 | 0.25 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.41 | 0.29 | 0.11 | 0.07 | 0.26 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.40 | 0.20 | 0.11 | 0.07 | 0.26 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.40 | 0.12 | 0.11 | 0.07 | 0.26 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.40 | 0.06 | 0.11 | 0.07 | 0.26 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.40 | 0.06 | 0.11 | 0.07 | 0.26 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.39 | 0.11 | 0.11 | 0.07 | 0.26 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.39 | 0.16 | 0.11 | 0.07 | 0.26 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.39 | 0.21 | 0.11 | 0.07 | 0.25 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.39 | 0.25 | 0.11 | 0.07 | 0.25 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.38 | 0.28 | 0.11 | 0.07 | 0.24 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.38 | 0.31 | 0.11 | 0.07 | 0.24 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.32 | 0.27 | 0.11 | 0.01 | 0.04 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.28 | 0.23 | 0.11 | 3.38e-03 | 0.01 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.25 | 0.19 | 0.11 | 0.01 | 0.04 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.23 | 0.15 | 0.11 | 0.02 | 0.07 | 0.0 |
| 379.0 | 1d12 | 1d12/25 | 1d10/25 | 0.21 | 0.11 | 0.11 | 0.03 | 0.09 | 0.0 |
| 403.0 | 1d12 | 1d12/25 | 1d10/25 | 0.20 | 0.06 | 0.11 | 0.03 | 0.11 | 0.0 |
| 427.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.03 | 0.11 | 0.03 | 0.12 | 0.0 |
| 451.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.05 | 0.11 | 0.04 | 0.13 | 0.0 |
| 475.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.13 | 0.11 | 0.04 | 0.13 | 0.0 |
| 477.8 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.18 | 0.11 | 0.04 | 0.13 | 0.0 |
| 481.6 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.16 | 0.11 | 0.03 | 0.12 | 0.0 |
| 485.4 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.14 | 0.11 | 0.03 | 0.11 | 0.0 |
| 489.1 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.18 | 0.11 | 0.04 | 0.15 | 0.0 |
| 492.9 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.13 | 0.11 | 0.04 | 0.13 | 0.0 |
| 496.7 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.11 | 0.0 | 0.0 | 0.0 |
| 500.5 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.11 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.41 | 0.37 | 0.11 | 0.07 | 0.26 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|------------|------------|-----------|-----------|----------|------------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1.982e+04 | -1.401e+04 | 8.087e+04 | 5.825e+04 | -9908.23 | -1.258e+04 | 2337.71 | 2337.71 |
| 23.0 | -1.982e+04 | -1.402e+04 | 8.678e+04 | 5.686e+04 | -9908.23 | -1.258e+04 | 2337.71 | 2337.71 |
| 46.0 | -1.968e+04 | -1.378e+04 | 6.717e+04 | 4.415e+04 | -9908.23 | -1.251e+04 | 2415.14 | 2415.14 |
| 69.0 | -1.954e+04 | -1.354e+04 | 5.488e+04 | 3.116e+04 | -9908.23 | -1.245e+04 | 2411.92 | 2411.92 |
| 92.0 | -1.941e+04 | -1.331e+04 | 4.627e+04 | 1.858e+04 | -9908.23 | -1.238e+04 | 2406.97 | 2406.97 |
| 112.0 | -1.928e+04 | -1.278e+04 | 8.547e+04 | 3857.66 | -9908.23 | -1.231e+04 | 2400.56 | 2400.56 |
| 132.0 | -1.916e+04 | -1.148e+04 | 2428.15 | 8637.00 | -9908.23 | -1.223e+04 | 2393.06 | 2393.06 |
| 152.0 | -1.904e+04 | -1.144e+04 | 2008.61 | 1.611e+04 | -9908.23 | -1.215e+04 | 2383.93 | 2383.93 |
| 172.0 | -1.892e+04 | -1.134e+04 | 7581.67 | 2.371e+04 | -9908.23 | -1.207e+04 | 2373.16 | 2373.16 |
| 196.0 | -1.879e+04 | -1.118e+04 | 1.792e+04 | 3.079e+04 | -9908.23 | -1.194e+04 | 2359.50 | 2359.50 |
| 220.0 | -1.865e+04 | -1.099e+04 | 3.257e+04 | 3.688e+04 | -9908.23 | -1.181e+04 | 2339.83 | 2339.83 |
| 244.0 | -1.850e+04 | -1.058e+04 | 3.752e+04 | 4.080e+04 | -9908.23 | -1.167e+04 | 2255.31 | 2255.32 |
| 267.0 | -1.836e+04 | -1.037e+04 | 4.701e+04 | 4.381e+04 | -9908.23 | -1.153e+04 | 2221.15 | 2221.15 |
| 289.0 | -1.525e+04 | -8799.89 | 3.835e+04 | 3.691e+04 | -9908.23 | -9541.22 | 399.15 | 399.15 |
| 311.0 | -1.353e+04 | -7827.62 | 2.904e+04 | 2.974e+04 | -9908.23 | -8448.84 | 112.89 | 112.89 |
| 333.0 | -1.221e+04 | -7088.83 | 1.943e+04 | 2.378e+04 | -9908.23 | -7591.25 | 349.55 | 349.55 |
| 355.0 | -1.118e+04 | -6511.92 | 1.486e+04 | 1.860e+04 | -9908.23 | -6944.02 | 636.93 | 636.93 |
| 379.0 | -1.030e+04 | -6013.07 | 1.175e+04 | 1.319e+04 | -9908.23 | -6404.28 | 866.09 | 866.09 |
| 403.0 | -9620.34 | -6250.44 | 2984.96 | 7955.64 | -9908.23 | -5988.55 | 1037.01 | 1037.01 |
| 427.0 | -9083.11 | -5859.71 | 1416.61 | 3927.80 | -9908.23 | -5665.02 | 1114.71 | 1114.71 |
| 451.0 | -8667.83 | -5019.41 | 3648.79 | 6514.58 | -9908.23 | -5415.85 | 1166.31 | 1166.31 |
| 475.0 | -8394.12 | -4867.04 | 7009.22 | 1.552e+04 | -9908.23 | -5249.24 | 1218.47 | 1218.47 |
| 477.8 | -8257.23 | -4766.07 | 6057.15 | 2.168e+04 | -9908.23 | -5185.57 | 1180.00 | 1180.00 |
| 481.6 | -6893.63 | -3967.67 | 6219.80 | 1.793e+04 | -9908.23 | -4382.02 | 977.30 | 977.30 |
| 485.4 | -5479.66 | -3130.57 | 4284.78 | 1.419e+04 | -9908.23 | -3537.36 | 794.17 | 794.17 |
| 489.1 | -4041.65 | -2292.45 | 2186.43 | 1.048e+04 | -9908.23 | -2643.55 | 599.85 | 599.85 |
| 492.9 | -2630.45 | -1479.19 | 723.44 | 6841.47 | -9908.23 | -1741.09 | 400.93 | 400.93 |
| 496.7 | 0.0 | 0.0 | 0.0 | 0.0 | -9908.23 | 0.0 | 0.0 | 0.0 |
| 500.5 | 0.0 | 0.0 | 0.0 | 0.0 | -9908.23 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 2337.71 | 3.409e+04 | 1.00 | 9284.37 | 3.409e+04 |
| 23.0 | 1.00 | 2337.71 | 3.409e+04 | 1.00 | 9284.37 | 3.409e+04 |
| 46.0 | 1.00 | 2415.14 | 3.408e+04 | 1.00 | 9284.37 | 3.408e+04 |
| 69.0 | 1.00 | 2411.92 | 3.406e+04 | 1.00 | 9284.37 | 3.406e+04 |
| 92.0 | 1.00 | 2406.97 | 3.405e+04 | 1.00 | 9284.37 | 3.405e+04 |
| 112.0 | 1.00 | 2400.56 | 3.404e+04 | 1.00 | 9284.37 | 3.404e+04 |
| 132.0 | 1.00 | 2393.06 | 3.403e+04 | 1.00 | 9284.37 | 3.403e+04 |
| 152.0 | 1.00 | 2383.93 | 3.402e+04 | 1.00 | 9284.37 | 3.402e+04 |
| 172.0 | 1.00 | 2373.16 | 3.400e+04 | 1.00 | 9284.37 | 3.400e+04 |
| 196.0 | 1.00 | 2359.50 | 3.398e+04 | 1.00 | 9284.37 | 3.398e+04 |
| 220.0 | 1.00 | 2339.83 | 3.396e+04 | 1.00 | 9284.37 | 3.396e+04 |
| 244.0 | 1.00 | 2255.31 | 3.394e+04 | 1.00 | 9284.37 | 3.394e+04 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| 267.0 | 1.00 | 2221.15 | 3.391e+04 | 1.00 | 9284.37 | 3.391e+04 |
| 289.0 | 1.00 | 399.15 | 3.358e+04 | 1.00 | 9284.37 | 3.358e+04 |
| 311.0 | 1.00 | 112.89 | 3.340e+04 | 1.00 | 9284.37 | 3.340e+04 |
| 333.0 | 1.00 | 349.55 | 3.326e+04 | 1.00 | 9284.37 | 3.326e+04 |
| 355.0 | 1.00 | 636.93 | 3.315e+04 | 1.00 | 9284.37 | 3.315e+04 |
| 379.0 | 1.00 | 866.09 | 3.306e+04 | 1.00 | 9284.37 | 3.306e+04 |
| 403.0 | 1.00 | 1037.01 | 3.299e+04 | 1.00 | 9284.37 | 3.299e+04 |
| 427.0 | 1.00 | 1114.71 | 3.294e+04 | 1.00 | 9284.37 | 3.294e+04 |
| 451.0 | 1.00 | 1166.31 | 3.290e+04 | 1.00 | 9284.37 | 3.290e+04 |
| 475.0 | 1.00 | 1218.47 | 3.287e+04 | 1.00 | 9284.37 | 3.287e+04 |
| 477.8 | 1.00 | 1180.00 | 3.286e+04 | 1.00 | 9284.37 | 3.286e+04 |
| 481.6 | 1.00 | 977.30 | 2.957e+04 | 1.00 | 8351.02 | 2.957e+04 |
| 485.4 | 1.00 | 794.17 | 2.627e+04 | 1.00 | 7417.67 | 2.627e+04 |
| 489.1 | 1.00 | 599.85 | 1.426e+04 | 1.00 | 4028.14 | 1.426e+04 |
| 492.9 | 1.00 | 400.93 | 1.096e+04 | 1.00 | 3094.79 | 1.096e+04 |
| 496.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 500.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 88 | 406.79 | 12.00 | 90.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.08 | 0.05 | 0.06 | 0.14 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.05 | 0.05 | 0.06 | 0.14 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.04 | 0.05 | 0.06 | 0.13 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.03 | 0.05 | 0.06 | 0.13 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.03 | 0.05 | 0.06 | 0.13 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.04 | 0.05 | 0.06 | 0.13 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.04 | 0.05 | 0.07 | 0.16 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.06 | 0.05 | 0.09 | 0.22 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.08 | 0.05 | 0.14 | 0.37 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.11 | 0.05 | 0.19 | 0.39 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.21 | 0.11 | 0.05 | 0.19 | 0.38 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.23 | 0.14 | 0.05 | 0.18 | 0.38 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.25 | 0.17 | 0.05 | 0.18 | 0.38 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.21 | 0.10 | 0.05 | 0.11 | 0.25 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.08 | 0.05 | 0.09 | 0.29 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.07 | 0.05 | 0.09 | 0.32 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.07 | 0.05 | 0.10 | 0.35 | 0.0 |
| 370.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.08 | 0.05 | 0.08 | 0.30 | 0.0 |
| 379.0 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.09 | 0.05 | 0.10 | 0.37 | 0.0 |
| 379.2 | 1d12 | 1d12/25 | 1d10/25 | 0.21 | 0.09 | 0.05 | 0.10 | 0.35 | 0.0 |
| 388.4 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.09 | 0.05 | 0.08 | 0.27 | 0.0 |
| 397.6 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.05 | 0.0 | 0.0 | 0.0 |
| 406.8 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.05 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.25 | 0.17 | 0.05 | 0.19 | 0.39 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -5077.20 | -3120.12 | 4011.41 | 8571.72 | -2538.60 | -3788.07 | 1710.34 | 1157.60 |
| 23.0 | -4767.91 | -3224.21 | 1.254e+04 | 5630.12 | -2538.60 | -3637.08 | 1612.94 | 1113.01 |
| 46.0 | -4886.23 | -2352.24 | 1.373e+04 | 3477.59 | -2538.60 | -3614.90 | 1660.56 | 1056.14 |
| 69.0 | -4965.71 | -2621.19 | 2.503e+04 | 814.83 | -2538.60 | -3477.28 | 1653.53 | 1017.12 |
| 92.0 | -5080.15 | -2811.38 | 2.619e+04 | 307.16 | -2538.60 | -3419.15 | 1659.25 | 1018.06 |
| 112.0 | -5272.13 | -3067.87 | 2.936e+04 | 65.19 | -2538.60 | -3388.60 | 1739.18 | 1093.47 |
| 132.0 | -5563.43 | -3380.68 | 3.614e+04 | 264.40 | -2538.60 | -3425.71 | 1968.56 | 1307.19 |
| 152.0 | -6020.33 | -3775.15 | 4.824e+04 | 405.66 | -2538.60 | -3578.16 | 2519.40 | 1804.11 |
| 172.0 | -6643.27 | -4226.87 | 6.614e+04 | 586.80 | -2538.60 | -3867.86 | 3972.72 | 2994.86 |
| 196.0 | -7288.10 | -5291.63 | 9.650e+04 | 1112.50 | -2538.60 | -4033.90 | 5485.06 | 3173.97 |
| 220.0 | -7963.13 | -7319.79 | 9.716e+04 | 5810.82 | -2538.60 | -4968.57 | 5404.34 | 3093.15 |
| 244.0 | -8734.42 | -8734.42 | 1.435e+05 | 338.99 | -2538.60 | -6129.17 | 5374.20 | 3042.12 |
| 267.0 | -9426.21 | -9426.21 | 1.776e+05 | 423.54 | -2538.60 | -7028.20 | 5396.71 | 3050.24 |
| 289.0 | -7923.27 | -7923.27 | 1.022e+05 | 386.51 | -2538.60 | -5809.81 | 3211.98 | 1990.18 |
| 311.0 | -7330.02 | -5344.52 | 7.196e+04 | 1287.99 | -2538.60 | -5344.52 | 2727.94 | 2363.16 |
| 333.0 | -6940.55 | -4978.01 | 5.955e+04 | 1072.41 | -2538.60 | -4978.01 | 2670.51 | 2626.96 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|----------|----------|----------|----------|----------|
| 355.0 | -6725.89 | -6725.89 | 6.141e+04 | 1224.46 | -2538.60 | -6725.89 | 2797.38 | 2797.38 |
| 370.0 | -6534.12 | -5534.58 | 6.190e+04 | 4651.28 | -2538.60 | -6506.74 | 2459.00 | 2459.00 |
| 379.0 | -6308.48 | -3467.48 | 1491.89 | 6138.75 | -2538.60 | -4586.50 | 1696.11 | 1706.43 |
| 379.2 | -6125.92 | -3363.20 | 2459.09 | 6133.04 | -2538.60 | -6125.92 | 1605.54 | 1605.54 |
| 388.4 | -4143.38 | -2298.44 | 168.32 | 5398.24 | -2538.60 | -3015.59 | 964.84 | 944.86 |
| 397.6 | 0.0 | 0.0 | 0.0 | 0.0 | -2538.60 | 0.0 | 0.0 | 0.0 |
| 406.8 | 0.0 | 0.0 | 0.0 | 0.0 | -2538.60 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 1710.34 | 2.863e+04 | 1.00 | 8105.40 | 2.887e+04 |
| 23.0 | 1.00 | 1612.94 | 2.860e+04 | 1.00 | 8105.40 | 2.877e+04 |
| 46.0 | 1.00 | 1660.56 | 2.860e+04 | 1.00 | 8105.40 | 2.879e+04 |
| 69.0 | 1.00 | 1653.53 | 2.858e+04 | 1.00 | 8105.40 | 2.879e+04 |
| 92.0 | 1.00 | 1659.25 | 2.856e+04 | 1.00 | 8105.40 | 2.880e+04 |
| 112.0 | 1.00 | 1739.18 | 2.856e+04 | 1.00 | 8105.40 | 2.883e+04 |
| 132.0 | 1.00 | 1968.56 | 2.857e+04 | 1.00 | 8105.40 | 2.887e+04 |
| 152.0 | 1.00 | 2519.40 | 2.859e+04 | 1.00 | 8105.40 | 2.894e+04 |
| 172.0 | 1.00 | 3972.72 | 2.865e+04 | 1.00 | 8105.40 | 2.904e+04 |
| 196.0 | 1.00 | 5485.06 | 2.868e+04 | 1.00 | 8105.40 | 2.916e+04 |
| 220.0 | 1.00 | 5404.34 | 2.885e+04 | 1.00 | 8105.40 | 2.930e+04 |
| 244.0 | 1.00 | 5374.20 | 2.906e+04 | 1.00 | 8105.40 | 2.954e+04 |
| 267.0 | 1.00 | 5396.71 | 2.923e+04 | 1.00 | 8105.40 | 2.967e+04 |
| 289.0 | 1.00 | 3211.98 | 2.900e+04 | 1.00 | 8105.40 | 2.939e+04 |
| 311.0 | 1.00 | 2727.94 | 2.892e+04 | 1.00 | 8105.40 | 2.928e+04 |
| 333.0 | 1.00 | 2670.51 | 2.885e+04 | 1.00 | 8105.40 | 2.921e+04 |
| 355.0 | 1.00 | 2797.38 | 2.917e+04 | 1.00 | 8105.40 | 2.917e+04 |
| 370.0 | 1.00 | 2459.00 | 2.913e+04 | 1.00 | 8105.40 | 2.913e+04 |
| 379.0 | 1.00 | 1696.11 | 1.637e+04 | 1.00 | 4567.49 | 1.661e+04 |
| 379.2 | 1.00 | 1605.54 | 1.650e+04 | 1.00 | 4543.94 | 1.650e+04 |
| 388.4 | 1.00 | 964.84 | 1.232e+04 | 1.00 | 3438.65 | 1.250e+04 |
| 397.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 406.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 98 | 511.01 | 12.00 | 40.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.29 | 0.28 | 0.03 | 0.08 | 0.31 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.30 | 0.24 | 0.03 | 0.09 | 0.33 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.31 | 0.19 | 0.03 | 0.07 | 0.26 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.32 | 0.14 | 0.03 | 0.06 | 0.22 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.35 | 0.10 | 0.03 | 0.06 | 0.20 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.37 | 0.06 | 0.03 | 0.05 | 0.18 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.41 | 0.04 | 0.03 | 0.04 | 0.17 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.45 | 0.06 | 0.03 | 0.05 | 0.17 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.52 | 0.13 | 0.03 | 8.73e-03 | 0.03 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.57 | 0.17 | 0.03 | 0.13 | 0.50 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.57 | 0.18 | 0.03 | 0.13 | 0.50 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.56 | 0.21 | 0.03 | 0.13 | 0.50 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.56 | 0.27 | 0.03 | 0.13 | 0.49 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.37 | 0.19 | 0.03 | 0.04 | 0.15 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.28 | 0.13 | 0.03 | 0.02 | 0.07 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.23 | 0.09 | 0.03 | 0.02 | 0.07 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.20 | 0.07 | 0.03 | 0.03 | 0.12 | 0.0 |
| 379.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.05 | 0.03 | 0.04 | 0.15 | 0.0 |
| 403.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.03 | 0.03 | 0.05 | 0.16 | 0.0 |
| 427.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.03 | 0.03 | 0.04 | 0.16 | 0.0 |
| 451.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.05 | 0.03 | 0.04 | 0.14 | 0.0 |
| 475.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.07 | 0.03 | 0.03 | 0.12 | 0.0 |
| 494.7 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.10 | 0.03 | 0.02 | 0.09 | 0.0 |
| 499.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.03 | 0.0 | 0.0 | 0.0 |
| 502.8 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.03 | 0.0 | 0.0 | 0.0 |
| 511.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.03 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.57 | 0.28 | 0.03 | 0.13 | 0.50 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|-----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -4940.79 | -3042.65 | 3052.72 | 1.654e+04 | -2470.40 | -4349.82 | 981.80 | 981.80 |
| 23.0 | -5038.68 | -2386.90 | 1285.17 | 1.328e+04 | -2470.40 | -1845.81 | 1062.21 | 1062.21 |
| 46.0 | -5170.06 | -3870.30 | 3441.05 | 1.142e+04 | -2470.40 | -2319.10 | 826.52 | 826.52 |
| 69.0 | -5433.13 | -3963.57 | 3976.57 | 8447.31 | -2470.40 | -2827.92 | 709.74 | 709.74 |
| 92.0 | -5843.91 | -4154.42 | 4994.32 | 5706.64 | -2470.40 | -3336.44 | 636.92 | 636.92 |
| 112.0 | -6294.74 | -4411.58 | 5934.41 | 3360.77 | -2470.40 | -6278.41 | 573.51 | 573.51 |
| 132.0 | -6879.85 | -4588.87 | 8853.69 | 903.49 | -2470.40 | -6865.38 | 544.87 | 544.87 |
| 152.0 | -7673.95 | -4538.85 | 701.79 | 4001.45 | -2470.40 | -4928.27 | 542.59 | 542.59 |
| 172.0 | -8784.13 | -7843.00 | 1.819e+04 | 7178.01 | -2470.40 | -5379.99 | 103.75 | 104.19 |
| 196.0 | -9617.75 | -5624.36 | 1.315e+04 | 9958.34 | -2470.40 | -6801.02 | 1594.71 | 1594.71 |
| 220.0 | -9567.59 | -5585.77 | 4139.08 | 1.218e+04 | -2470.40 | -6788.54 | 1590.13 | 1590.13 |
| 244.0 | -9517.42 | -5621.03 | 7461.89 | 1.401e+04 | -2470.40 | -6711.41 | 1584.42 | 1584.42 |
| 267.0 | -9468.29 | -5465.68 | 1.951e+04 | 1.636e+04 | -2470.40 | -6658.68 | 1578.51 | 1578.51 |
| 289.0 | -6185.92 | -3576.03 | 6610.96 | 1.144e+04 | -2470.40 | -4631.48 | 474.60 | 474.60 |
| 311.0 | -4723.92 | -2734.23 | 2993.36 | 7320.38 | -2470.40 | -3335.47 | 224.68 | 224.68 |
| 333.0 | -3876.86 | -2242.12 | 1324.34 | 5120.62 | -2470.40 | -1856.55 | 236.81 | 236.81 |
| 355.0 | -3361.10 | -2156.58 | 146.05 | 3991.92 | -2470.40 | -1613.21 | 390.11 | 390.11 |
| 379.0 | -3014.75 | -1956.35 | 251.46 | 2822.65 | -2470.40 | -1450.15 | 474.34 | 474.34 |
| 403.0 | -2803.15 | -1819.75 | 363.18 | 1566.70 | -2470.40 | -1353.95 | 506.21 | 506.21 |
| 427.0 | -2673.50 | -1480.62 | 475.37 | 1332.34 | -2470.40 | -1296.02 | 495.93 | 495.93 |
| 451.0 | -2600.49 | -1423.34 | 638.71 | 2524.83 | -2470.40 | -1264.31 | 452.18 | 452.18 |
| 475.0 | -2570.02 | -1224.57 | 851.62 | 3686.76 | -2470.40 | -1253.75 | 378.09 | 378.09 |
| 494.7 | -2563.39 | -1211.80 | 983.42 | 5125.01 | -2470.40 | -1261.95 | 272.11 | 272.11 |
| 499.0 | 0.0 | 0.0 | 0.0 | 0.0 | -2470.40 | 0.0 | 0.0 | 0.0 |
| 502.8 | 0.0 | 0.0 | 0.0 | 0.0 | -2470.40 | 0.0 | 0.0 | 0.0 |
| 511.0 | 0.0 | 0.0 | 0.0 | 0.0 | -2470.40 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 981.80 | 1.171e+04 | 1.00 | 3193.04 | 1.171e+04 |
| 23.0 | 1.00 | 1062.21 | 1.131e+04 | 1.00 | 3193.04 | 1.131e+04 |
| 46.0 | 1.00 | 826.52 | 1.138e+04 | 1.00 | 3193.04 | 1.138e+04 |
| 69.0 | 1.00 | 709.74 | 1.147e+04 | 1.00 | 3193.04 | 1.147e+04 |
| 92.0 | 1.00 | 636.92 | 1.155e+04 | 1.00 | 3193.04 | 1.155e+04 |
| 112.0 | 1.00 | 573.51 | 1.203e+04 | 1.00 | 3193.04 | 1.203e+04 |
| 132.0 | 1.00 | 544.87 | 1.212e+04 | 1.00 | 3193.04 | 1.212e+04 |
| 152.0 | 1.00 | 542.59 | 1.181e+04 | 1.00 | 3193.04 | 1.181e+04 |
| 172.0 | 1.00 | 103.75 | 1.188e+04 | 1.00 | 3193.04 | 1.235e+04 |
| 196.0 | 1.00 | 1594.71 | 1.211e+04 | 1.00 | 3193.04 | 1.211e+04 |
| 220.0 | 1.00 | 1590.13 | 1.211e+04 | 1.00 | 3193.04 | 1.211e+04 |
| 244.0 | 1.00 | 1584.42 | 1.210e+04 | 1.00 | 3193.04 | 1.210e+04 |
| 267.0 | 1.00 | 1578.51 | 1.209e+04 | 1.00 | 3193.04 | 1.209e+04 |
| 289.0 | 1.00 | 474.60 | 1.176e+04 | 1.00 | 3193.04 | 1.176e+04 |
| 311.0 | 1.00 | 224.68 | 1.155e+04 | 1.00 | 3193.04 | 1.155e+04 |
| 333.0 | 1.00 | 236.81 | 1.131e+04 | 1.00 | 3193.04 | 1.131e+04 |
| 355.0 | 1.00 | 390.11 | 1.127e+04 | 1.00 | 3193.04 | 1.127e+04 |
| 379.0 | 1.00 | 474.34 | 1.124e+04 | 1.00 | 3193.04 | 1.124e+04 |
| 403.0 | 1.00 | 506.21 | 1.123e+04 | 1.00 | 3193.04 | 1.123e+04 |
| 427.0 | 1.00 | 495.93 | 1.122e+04 | 1.00 | 3193.04 | 1.122e+04 |
| 451.0 | 1.00 | 452.18 | 1.121e+04 | 1.00 | 3193.04 | 1.121e+04 |
| 475.0 | 1.00 | 378.09 | 1.121e+04 | 1.00 | 3193.04 | 1.121e+04 |
| 494.7 | 1.00 | 272.11 | 1.121e+04 | 1.00 | 3193.04 | 1.121e+04 |
| 499.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 502.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 511.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 99 | 457.87 | 12.00 | 35.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 379.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 403.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 427.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 443.6 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 450.7 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 451.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| 457.9 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.0 | 0.02 | 0.0 | 0.0 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|--------|----------|----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 23.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 46.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 69.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 92.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 112.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 132.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 152.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 172.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 196.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 220.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 244.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 267.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 289.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 311.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 333.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 355.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 379.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 403.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 427.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 443.6 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 450.7 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 451.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |
| 457.9 | 0.0 | 0.0 | 0.0 | 0.0 | -1283.56 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 23.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 46.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 69.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 92.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 112.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 132.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 152.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 172.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 196.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 220.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 244.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 267.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 289.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 311.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 333.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 355.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 379.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 403.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|----------|
| 427.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 443.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 450.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 451.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 457.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Macrosetti n. 98, 92, 95, 90 [fasce di piano]

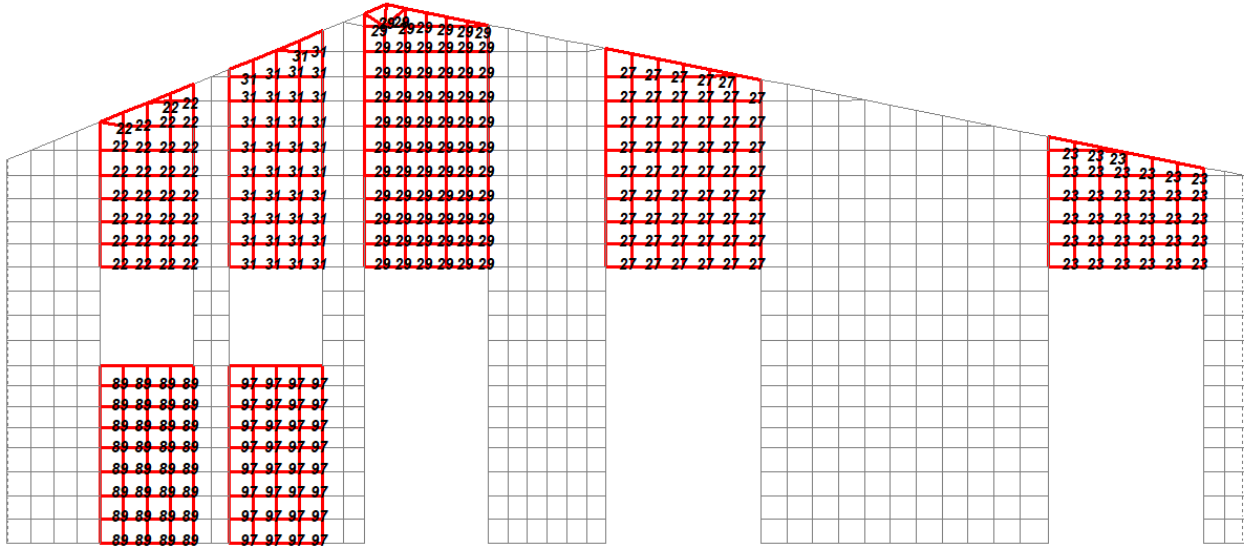


Fig 41. Elemento/i oggetto di verifica (Selezione in rosso).

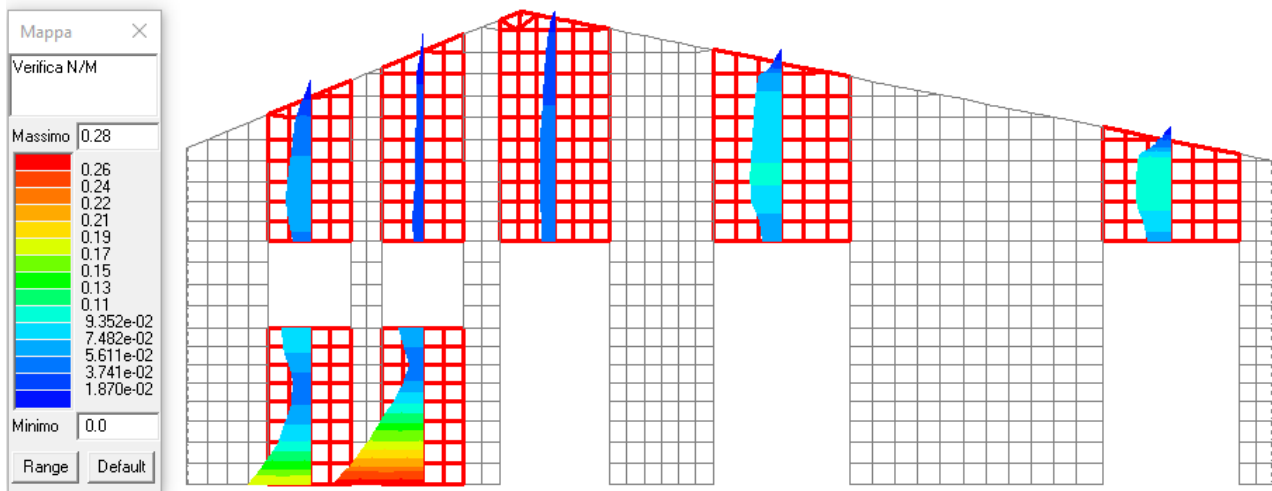


Fig 42. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

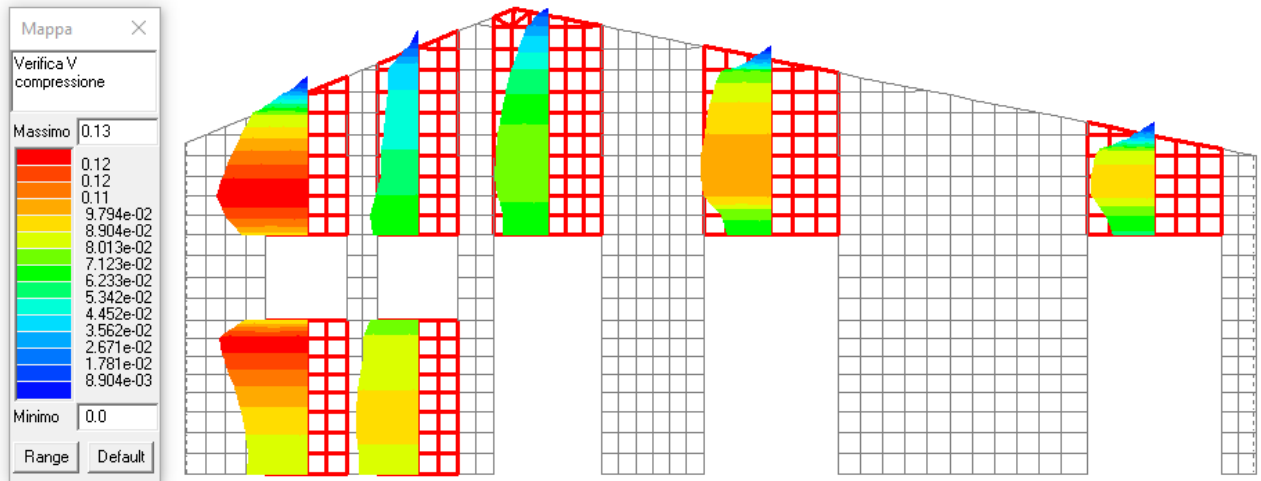


Fig 43. SLU: Mappa di Verifica V compressione – Verifica soddisfatta ($\rho \leq 1$).

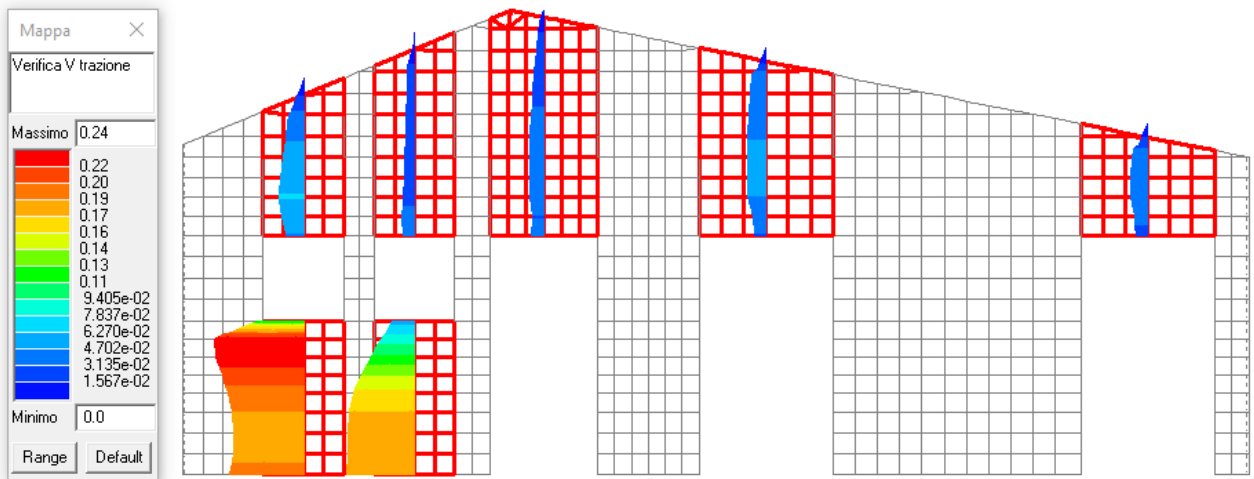


Fig 44. SLU: Mappa di verifica V trazione – Verifiche soddisfatte ($\rho \leq 1$).

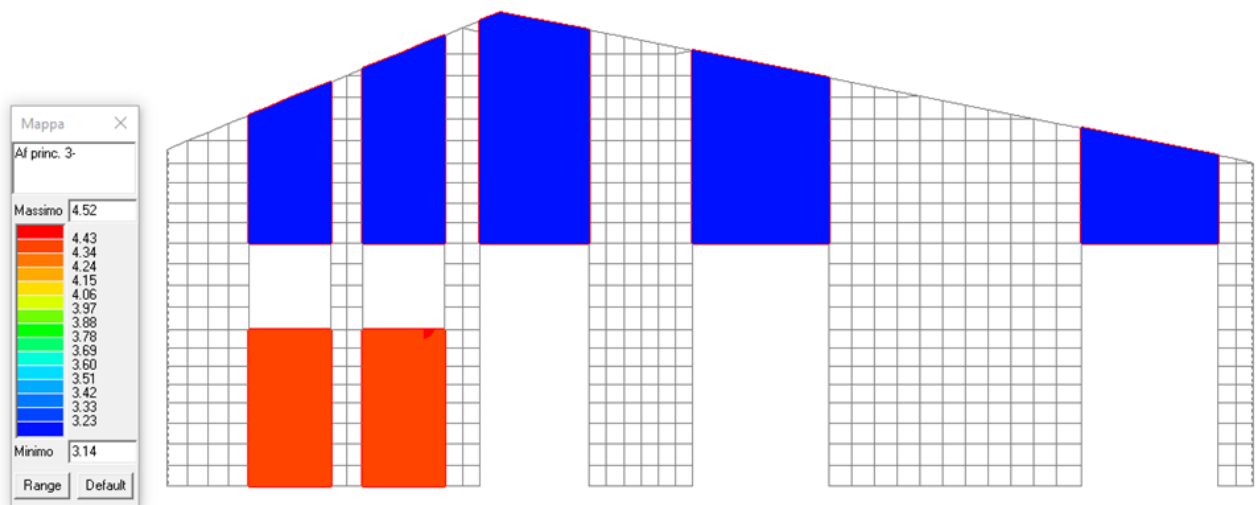


Fig 45. Mappa Armatura Verticale (singolo strato) da Calcolo [cm²/m].

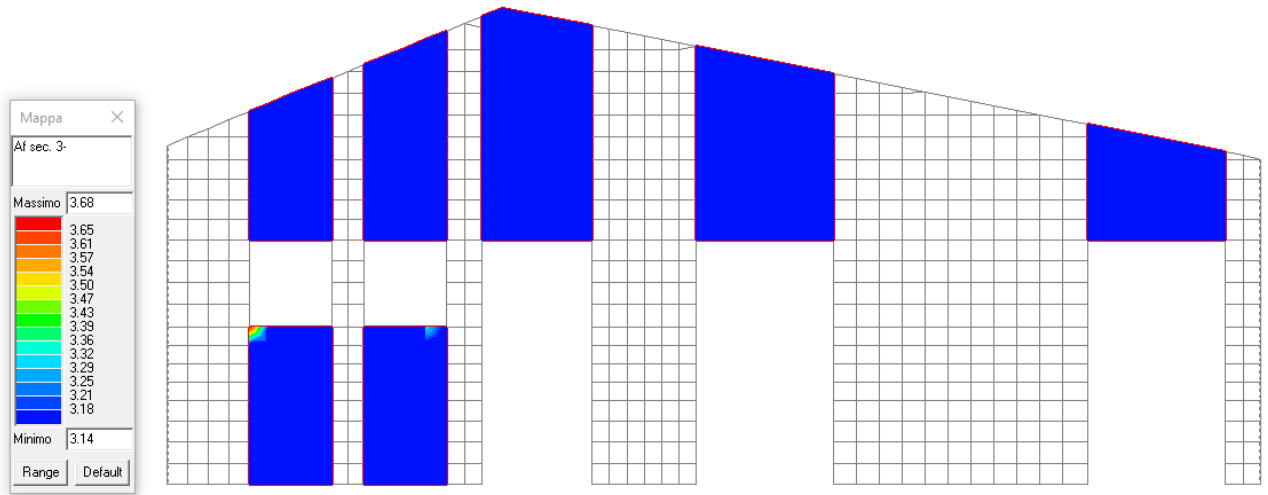


Fig 46. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm²/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 22 | 176.57 | 12.00 | 90.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.10 | 0.05 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.12 | 0.06 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.13 | 0.06 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.12 | 0.06 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.11 | 0.05 | 0.0 |
| 379.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.10 | 0.05 | 0.0 |
| 403.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.08 | 0.04 | 0.0 |
| 406.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.07 | 0.03 | 0.0 |
| 416.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.05 | 0.02 | 0.0 |
| 425.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.03 | 0.02 | 0.0 |
| 427.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.01 | 0.0 | 0.03 | 0.01 | 0.0 |
| 434.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 6.91e-03 | 0.0 | 0.01 | 6.21e-03 | 0.0 |
| 443.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.07 | 0.0 | 0.13 | 0.06 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|--------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 1.980e+05 | 0.0 | 0.0 | 0.0 | 4399.70 | 4399.70 |
| 289.0 | 0.0 | 0.0 | 2.468e+05 | 0.0 | 0.0 | 0.0 | 5485.34 | 5485.34 |
| 311.0 | 0.0 | 0.0 | 2.749e+05 | 0.0 | 0.0 | 0.0 | 6108.17 | 6108.17 |
| 333.0 | 0.0 | 0.0 | 2.543e+05 | 0.0 | 0.0 | 0.0 | 5650.88 | 5650.88 |
| 355.0 | 0.0 | 0.0 | 2.278e+05 | 0.0 | 0.0 | 0.0 | 5062.74 | 5062.74 |
| 379.0 | 0.0 | 0.0 | 1.968e+05 | 0.0 | 0.0 | 0.0 | 4372.83 | 4372.83 |
| 403.0 | 0.0 | 0.0 | 1.637e+05 | 0.0 | 0.0 | 0.0 | 3638.61 | 3638.61 |
| 406.8 | 0.0 | 0.0 | 1.384e+05 | 0.0 | 0.0 | 0.0 | 3075.19 | 3075.19 |
| 416.0 | 0.0 | 0.0 | 1.021e+05 | 0.0 | 0.0 | 0.0 | 2269.51 | 2269.51 |
| 425.2 | 0.0 | 0.0 | 6.598e+04 | 0.0 | 0.0 | 0.0 | 1466.12 | 1466.12 |
| 427.0 | 0.0 | 0.0 | 5.367e+04 | 0.0 | 0.0 | 0.0 | 1192.67 | 1192.67 |
| 434.4 | 0.0 | 0.0 | 2.690e+04 | 0.0 | 0.0 | 0.0 | 597.79 | 597.79 |
| 443.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 4399.70 | 4.573e+04 | 2.50 | 9.620e+04 | 4.573e+04 |
| 289.0 | 2.50 | 5485.34 | 4.573e+04 | 2.50 | 9.620e+04 | 4.573e+04 |
| 311.0 | 2.50 | 6108.17 | 4.573e+04 | 2.50 | 9.620e+04 | 4.573e+04 |
| 333.0 | 2.50 | 5650.88 | 4.573e+04 | 2.50 | 9.620e+04 | 4.573e+04 |
| 355.0 | 2.50 | 5062.74 | 4.573e+04 | 2.50 | 9.620e+04 | 4.573e+04 |
| 379.0 | 2.50 | 4372.83 | 4.573e+04 | 2.50 | 9.620e+04 | 4.573e+04 |
| 403.0 | 2.50 | 3638.61 | 4.573e+04 | 2.50 | 9.620e+04 | 4.573e+04 |
| 406.8 | 2.50 | 3075.19 | 4.573e+04 | 2.50 | 9.620e+04 | 4.573e+04 |
| 416.0 | 2.50 | 2269.51 | 4.573e+04 | 2.50 | 9.620e+04 | 4.573e+04 |
| 425.2 | 2.50 | 1466.12 | 4.573e+04 | 2.50 | 9.620e+04 | 4.573e+04 |
| 427.0 | 2.50 | 1192.67 | 4.573e+04 | 2.50 | 9.620e+04 | 4.573e+04 |
| 434.4 | 2.50 | 597.79 | 4.573e+04 | 2.50 | 9.620e+04 | 4.573e+04 |
| 443.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 23 | 125.62 | 12.00 | 150.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.06 | 0.03 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.07 | 0.03 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.09 | 0.04 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.09 | 0.04 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.09 | 0.04 | 0.0 |
| 362.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.08 | 0.04 | 0.0 |
| 367.7 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.06 | 0.03 | 0.0 |
| 372.7 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| 377.7 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.02 | 0.0 |
| 379.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.02 | 0.0 |
| 382.7 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.02 | 9.85e-03 | 0.0 |
| 387.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.01 | 0.0 | 0.01 | 4.75e-03 | 0.0 |
| 392.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.11 | 0.0 | 0.09 | 0.04 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 1.469e+05 | 0.0 | 0.0 | 0.0 | 1958.15 | 1958.15 |
| 289.0 | 0.0 | 0.0 | 1.736e+05 | 0.0 | 0.0 | 0.0 | 2314.40 | 2314.40 |
| 311.0 | 0.0 | 0.0 | 2.237e+05 | 0.0 | 0.0 | 0.0 | 2983.19 | 2983.19 |
| 333.0 | 0.0 | 0.0 | 2.246e+05 | 0.0 | 0.0 | 0.0 | 2994.46 | 2994.46 |
| 355.0 | 0.0 | 0.0 | 2.100e+05 | 0.0 | 0.0 | 0.0 | 2800.42 | 2800.42 |
| 362.8 | 0.0 | 0.0 | 1.940e+05 | 0.0 | 0.0 | 0.0 | 2586.60 | 2586.60 |
| 367.7 | 0.0 | 0.0 | 1.398e+05 | 0.0 | 0.0 | 0.0 | 1863.91 | 1863.91 |
| 372.7 | 0.0 | 0.0 | 1.023e+05 | 0.0 | 0.0 | 0.0 | 1363.74 | 1363.74 |
| 377.7 | 0.0 | 0.0 | 8.040e+04 | 0.0 | 0.0 | 0.0 | 1071.98 | 1071.98 |
| 379.0 | 0.0 | 0.0 | 7.763e+04 | 0.0 | 0.0 | 0.0 | 1035.00 | 1035.00 |
| 382.7 | 0.0 | 0.0 | 5.027e+04 | 0.0 | 0.0 | 0.0 | 670.31 | 670.31 |
| 387.6 | 0.0 | 0.0 | 2.426e+04 | 0.0 | 0.0 | 0.0 | 323.51 | 323.51 |
| 392.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 1958.15 | 3.235e+04 | 2.50 | 6.804e+04 | 3.235e+04 |
| 289.0 | 2.50 | 2314.40 | 3.235e+04 | 2.50 | 6.804e+04 | 3.235e+04 |
| 311.0 | 2.50 | 2983.19 | 3.235e+04 | 2.50 | 6.804e+04 | 3.235e+04 |
| 333.0 | 2.50 | 2994.46 | 3.235e+04 | 2.50 | 6.804e+04 | 3.235e+04 |
| 355.0 | 2.50 | 2800.42 | 3.235e+04 | 2.50 | 6.804e+04 | 3.235e+04 |
| 362.8 | 2.50 | 2586.60 | 3.235e+04 | 2.50 | 6.804e+04 | 3.235e+04 |
| 367.7 | 2.50 | 1863.91 | 3.235e+04 | 2.50 | 6.804e+04 | 3.235e+04 |
| 372.7 | 2.50 | 1363.74 | 3.235e+04 | 2.50 | 6.804e+04 | 3.235e+04 |
| 377.7 | 2.50 | 1071.98 | 3.235e+04 | 2.50 | 6.804e+04 | 3.235e+04 |
| 379.0 | 2.50 | 1035.00 | 3.235e+04 | 2.50 | 6.804e+04 | 3.235e+04 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| 382.7 | 2.50 | 670.31 | 3.235e+04 | 2.50 | 6.804e+04 | 3.235e+04 |
| 387.6 | 2.50 | 323.51 | 3.235e+04 | 2.50 | 6.804e+04 | 3.235e+04 |
| 392.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 27 | 210.80 | 12.00 | 150.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.07 | 0.03 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.07 | 0.03 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.10 | 0.05 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.10 | 0.05 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.10 | 0.05 | 0.0 |
| 379.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.10 | 0.05 | 0.0 |
| 403.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.09 | 0.04 | 0.0 |
| 427.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.09 | 0.04 | 0.0 |
| 447.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.08 | 0.04 | 0.0 |
| 451.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.07 | 0.03 | 0.0 |
| 452.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.05 | 0.02 | 0.0 |
| 457.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.04 | 0.02 | 0.0 |
| 462.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.03 | 0.01 | 0.0 |
| 467.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.02 | 8.94e-03 | 0.0 |
| 472.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 8.02e-03 | 0.0 | 8.85e-03 | 4.21e-03 | 0.0 |
| 477.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.09 | 0.0 | 0.10 | 0.05 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 2.669e+05 | 0.0 | 0.0 | 0.0 | 3558.97 | 3558.97 |
| 289.0 | 0.0 | 0.0 | 3.016e+05 | 0.0 | 0.0 | 0.0 | 4021.05 | 4021.05 |
| 311.0 | 0.0 | 0.0 | 4.096e+05 | 0.0 | 0.0 | 0.0 | 5461.08 | 5461.08 |
| 333.0 | 0.0 | 0.0 | 4.286e+05 | 0.0 | 0.0 | 0.0 | 5714.24 | 5714.24 |
| 355.0 | 0.0 | 0.0 | 4.236e+05 | 0.0 | 0.0 | 0.0 | 5647.67 | 5647.67 |
| 379.0 | 0.0 | 0.0 | 4.033e+05 | 0.0 | 0.0 | 0.0 | 5376.86 | 5376.86 |
| 403.0 | 0.0 | 0.0 | 3.834e+05 | 0.0 | 0.0 | 0.0 | 5111.71 | 5111.71 |
| 427.0 | 0.0 | 0.0 | 3.513e+05 | 0.0 | 0.0 | 0.0 | 4684.63 | 4684.63 |
| 447.9 | 0.0 | 0.0 | 3.090e+05 | 0.0 | 0.0 | 0.0 | 4119.73 | 4119.73 |
| 451.0 | 0.0 | 0.0 | 2.720e+05 | 0.0 | 0.0 | 0.0 | 3626.72 | 3626.72 |
| 452.9 | 0.0 | 0.0 | 2.106e+05 | 0.0 | 0.0 | 0.0 | 2807.41 | 2807.41 |
| 457.9 | 0.0 | 0.0 | 1.621e+05 | 0.0 | 0.0 | 0.0 | 2160.82 | 2160.82 |
| 462.9 | 0.0 | 0.0 | 1.177e+05 | 0.0 | 0.0 | 0.0 | 1569.83 | 1569.83 |
| 467.9 | 0.0 | 0.0 | 7.717e+04 | 0.0 | 0.0 | 0.0 | 1028.95 | 1028.95 |
| 472.8 | 0.0 | 0.0 | 3.633e+04 | 0.0 | 0.0 | 0.0 | 484.41 | 484.41 |
| 477.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 3558.97 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 289.0 | 2.50 | 4021.05 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 311.0 | 2.50 | 5461.08 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 333.0 | 2.50 | 5714.24 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 355.0 | 2.50 | 5647.67 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 379.0 | 2.50 | 5376.86 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 403.0 | 2.50 | 5111.71 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 427.0 | 2.50 | 4684.63 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 447.9 | 2.50 | 4119.73 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 451.0 | 2.50 | 3626.72 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 452.9 | 2.50 | 2807.41 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 457.9 | 2.50 | 2160.82 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 462.9 | 2.50 | 1569.83 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 467.9 | 2.50 | 1028.95 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 472.8 | 2.50 | 484.41 | 5.473e+04 | 2.50 | 1.151e+05 | 5.473e+04 |
| 477.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 29 | 253.00 | 12.00 | 120.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|
| cm | | | | | | | | |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.07 | 0.03 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.07 | 0.03 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.07 | 0.04 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.08 | 0.04 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.08 | 0.04 |
| 379.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.07 | 0.04 |
| 403.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.07 | 0.03 |
| 427.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.06 | 0.03 |
| 451.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.05 | 0.03 |
| 475.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.04 | 0.02 |
| 499.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.03 | 0.01 |
| 500.5 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.01 | 0.0 | 0.03 | 0.01 |
| 504.5 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.01 | 0.0 | 0.02 | 0.01 |
| 508.5 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.01 | 0.0 | 0.02 | 9.80e-03 |
| 511.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.01 | 0.0 | 0.02 | 8.65e-03 |
| 512.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 9.25e-03 | 0.0 | 0.02 | 7.61e-03 |
| 516.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 5.04e-03 | 0.0 | 8.71e-03 | 4.14e-03 |
| 520.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc |
| | | | | 0.0 | 0.05 | 0.0 | 0.08 | 0.04 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 2.626e+05 | 0.0 | 0.0 | 0.0 | 4376.26 | 4376.26 |
| 289.0 | 0.0 | 0.0 | 2.603e+05 | 0.0 | 0.0 | 0.0 | 4338.45 | 4338.45 |
| 311.0 | 0.0 | 0.0 | 2.921e+05 | 0.0 | 0.0 | 0.0 | 4868.51 | 4868.51 |
| 333.0 | 0.0 | 0.0 | 3.073e+05 | 0.0 | 0.0 | 0.0 | 5122.00 | 5122.00 |
| 355.0 | 0.0 | 0.0 | 3.023e+05 | 0.0 | 0.0 | 0.0 | 5038.05 | 5038.05 |
| 379.0 | 0.0 | 0.0 | 2.924e+05 | 0.0 | 0.0 | 0.0 | 4873.70 | 4873.70 |
| 403.0 | 0.0 | 0.0 | 2.714e+05 | 0.0 | 0.0 | 0.0 | 4522.61 | 4522.61 |
| 427.0 | 0.0 | 0.0 | 2.445e+05 | 0.0 | 0.0 | 0.0 | 4075.53 | 4075.53 |
| 451.0 | 0.0 | 0.0 | 2.115e+05 | 0.0 | 0.0 | 0.0 | 3525.57 | 3525.57 |
| 475.0 | 0.0 | 0.0 | 1.704e+05 | 0.0 | 0.0 | 0.0 | 2840.64 | 2840.64 |
| 499.0 | 0.0 | 0.0 | 1.245e+05 | 0.0 | 0.0 | 0.0 | 2074.63 | 2074.63 |
| 500.5 | 0.0 | 0.0 | 1.020e+05 | 0.0 | 0.0 | 0.0 | 1700.12 | 1700.12 |
| 504.5 | 0.0 | 0.0 | 9.242e+04 | 0.0 | 0.0 | 0.0 | 1540.31 | 1540.31 |
| 508.5 | 0.0 | 0.0 | 8.139e+04 | 0.0 | 0.0 | 0.0 | 1356.44 | 1356.44 |
| 511.0 | 0.0 | 0.0 | 7.183e+04 | 0.0 | 0.0 | 0.0 | 1197.18 | 1197.18 |
| 512.4 | 0.0 | 0.0 | 6.318e+04 | 0.0 | 0.0 | 0.0 | 1052.95 | 1052.95 |
| 516.4 | 0.0 | 0.0 | 3.441e+04 | 0.0 | 0.0 | 0.0 | 573.53 | 573.53 |
| 520.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 4376.26 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 289.0 | 2.50 | 4338.45 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 311.0 | 2.50 | 4868.51 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 333.0 | 2.50 | 5122.00 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 355.0 | 2.50 | 5038.05 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 379.0 | 2.50 | 4873.70 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 403.0 | 2.50 | 4522.61 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 427.0 | 2.50 | 4075.53 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 451.0 | 2.50 | 3525.57 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 475.0 | 2.50 | 2840.64 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 499.0 | 2.50 | 2074.63 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 500.5 | 2.50 | 1700.12 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 504.5 | 2.50 | 1540.31 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 508.5 | 2.50 | 1356.44 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 511.0 | 2.50 | 1197.18 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 512.4 | 2.50 | 1052.95 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 516.4 | 2.50 | 573.53 | 6.582e+04 | 2.50 | 1.384e+05 | 6.582e+04 |
| 520.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 31 | 227.66 | 12.00 | 90.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.07 | 0.03 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.07 | 0.03 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.06 | 0.03 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.06 | 0.03 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.05 | 0.03 | 0.0 |
| 379.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.05 | 0.02 | 0.0 |
| 403.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.05 | 0.02 | 0.0 |
| 427.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.04 | 0.02 | 0.0 |
| 451.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.04 | 0.02 | 0.0 |
| 457.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.04 | 0.02 | 0.0 |
| 467.1 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.01 | 0.0 | 0.03 | 0.01 | 0.0 |
| 475.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 7.92e-03 | 0.0 | 0.02 | 8.85e-03 | 0.0 |
| 476.3 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 5.45e-03 | 0.0 | 0.01 | 6.09e-03 | 0.0 |
| 485.5 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 2.77e-03 | 0.0 | 6.50e-03 | 3.09e-03 | 0.0 |
| 494.7 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.03 | 0.0 | 0.07 | 0.03 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 1.798e+05 | 0.0 | 0.0 | 0.0 | 3996.43 | 3996.43 |
| 289.0 | 0.0 | 0.0 | 1.866e+05 | 0.0 | 0.0 | 0.0 | 4146.77 | 4146.77 |
| 311.0 | 0.0 | 0.0 | 1.673e+05 | 0.0 | 0.0 | 0.0 | 3718.30 | 3718.30 |
| 333.0 | 0.0 | 0.0 | 1.474e+05 | 0.0 | 0.0 | 0.0 | 3274.92 | 3274.92 |
| 355.0 | 0.0 | 0.0 | 1.452e+05 | 0.0 | 0.0 | 0.0 | 3225.73 | 3225.73 |
| 379.0 | 0.0 | 0.0 | 1.367e+05 | 0.0 | 0.0 | 0.0 | 3037.66 | 3037.66 |
| 403.0 | 0.0 | 0.0 | 1.273e+05 | 0.0 | 0.0 | 0.0 | 2828.86 | 2828.86 |
| 427.0 | 0.0 | 0.0 | 1.189e+05 | 0.0 | 0.0 | 0.0 | 2642.39 | 2642.39 |
| 451.0 | 0.0 | 0.0 | 1.154e+05 | 0.0 | 0.0 | 0.0 | 2565.02 | 2565.02 |
| 457.9 | 0.0 | 0.0 | 9.920e+04 | 0.0 | 0.0 | 0.0 | 2204.50 | 2204.50 |
| 467.1 | 0.0 | 0.0 | 7.005e+04 | 0.0 | 0.0 | 0.0 | 1556.59 | 1556.59 |
| 475.0 | 0.0 | 0.0 | 4.953e+04 | 0.0 | 0.0 | 0.0 | 1100.73 | 1100.73 |
| 476.3 | 0.0 | 0.0 | 3.408e+04 | 0.0 | 0.0 | 0.0 | 757.37 | 757.37 |
| 485.5 | 0.0 | 0.0 | 1.732e+04 | 0.0 | 0.0 | 0.0 | 384.82 | 384.82 |
| 494.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 3996.43 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 289.0 | 2.50 | 4146.77 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 311.0 | 2.50 | 3718.30 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 333.0 | 2.50 | 3274.92 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 355.0 | 2.50 | 3225.73 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 379.0 | 2.50 | 3037.66 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 403.0 | 2.50 | 2828.86 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 427.0 | 2.50 | 2642.39 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 451.0 | 2.50 | 2565.02 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 457.9 | 2.50 | 2204.50 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 467.1 | 2.50 | 1556.59 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 475.0 | 2.50 | 1100.73 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 476.3 | 2.50 | 757.37 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 485.5 | 2.50 | 384.82 | 5.916e+04 | 2.50 | 1.244e+05 | 5.916e+04 |
| 494.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 89 | 172.00 | 12.00 | 90.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.19 | 0.07 | 0.09 | 0.19 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.14 | 0.07 | 0.09 | 0.18 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.10 | 0.07 | 0.09 | 0.18 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.07 | 0.07 | 0.10 | 0.19 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.05 | 0.07 | 0.10 | 0.20 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.05 | 0.07 | 0.11 | 0.21 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.06 | 0.07 | 0.12 | 0.23 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.08 | 0.07 | 0.13 | 0.24 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.08 | 0.07 | 0.09 | 0.12 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.13 | 0.19 | 0.07 | 0.13 | 0.24 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -5120.49 | -3363.76 | 7328.48 | 2.039e+04 | -3015.48 | -3055.98 | 2491.42 | 1568.37 |
| 23.0 | -5054.99 | -3318.63 | 8161.25 | 1.488e+04 | -3015.48 | -3015.28 | 2429.27 | 1492.86 |
| 46.0 | -4853.34 | -3173.03 | 9459.72 | 1.019e+04 | -3015.48 | -2745.55 | 2547.35 | 1487.89 |
| 69.0 | -4583.99 | -3287.30 | 1.397e+04 | 7535.46 | -3015.48 | -2544.80 | 2731.32 | 1524.38 |
| 92.0 | -4220.36 | -2997.63 | 1.839e+04 | 5118.84 | -3015.48 | -2243.99 | 2965.20 | 1608.95 |
| 112.0 | -3786.33 | -1923.96 | 3.757e+04 | 372.72 | -3015.48 | -1923.96 | 3227.07 | 1729.58 |
| 132.0 | -3173.02 | -1565.81 | 4.947e+04 | 70.09 | -3015.48 | -1565.81 | 3497.38 | 1875.71 |
| 152.0 | -2242.59 | -1074.07 | 6.159e+04 | 439.71 | -3015.48 | -1074.07 | 3654.00 | 1905.74 |
| 172.0 | -910.47 | -427.39 | 6.069e+04 | 429.24 | -3015.48 | -427.39 | 2564.34 | 949.94 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 2491.42 | 2.850e+04 | 1.00 | 8105.40 | 2.882e+04 |
| 23.0 | 1.00 | 2429.27 | 2.849e+04 | 1.00 | 8105.40 | 2.880e+04 |
| 46.0 | 1.00 | 2547.35 | 2.844e+04 | 1.00 | 8105.40 | 2.876e+04 |
| 69.0 | 1.00 | 2731.32 | 2.840e+04 | 1.00 | 8105.40 | 2.871e+04 |
| 92.0 | 1.00 | 2965.20 | 2.835e+04 | 1.00 | 8105.40 | 2.864e+04 |
| 112.0 | 1.00 | 3227.07 | 2.829e+04 | 1.00 | 8105.40 | 2.856e+04 |
| 132.0 | 1.00 | 3497.38 | 2.822e+04 | 1.00 | 8105.40 | 2.846e+04 |
| 152.0 | 1.00 | 3654.00 | 2.813e+04 | 1.00 | 8105.40 | 2.831e+04 |
| 172.0 | 1.00 | 2564.34 | 2.802e+04 | 1.00 | 8105.40 | 2.809e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 97 | 172.00 | 12.00 | 90.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.20 | 0.28 | 0.09 | 0.09 | 0.18 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.20 | 0.22 | 0.09 | 0.09 | 0.17 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.17 | 0.09 | 0.09 | 0.18 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.13 | 0.09 | 0.09 | 0.17 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.09 | 0.09 | 0.09 | 0.16 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.06 | 0.09 | 0.09 | 0.14 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.04 | 0.09 | 0.08 | 0.11 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.06 | 0.09 | 0.08 | 0.09 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.07 | 0.09 | 0.07 | 0.06 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.20 | 0.28 | 0.09 | 0.09 | 0.18 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -7494.14 | -4831.62 | 1.280e+04 | 3.209e+04 | -4390.08 | -4680.15 | 2542.23 | 1451.41 |
| 23.0 | -7554.85 | -5401.51 | 1.643e+04 | 2.543e+04 | -4390.08 | -4720.85 | 2496.19 | 1415.04 |
| 46.0 | -7387.99 | -5253.93 | 1.684e+04 | 1.991e+04 | -4390.08 | -4355.57 | 2659.28 | 1438.38 |
| 69.0 | -7056.60 | -4989.62 | 1.628e+04 | 1.476e+04 | -4390.08 | -4185.31 | 2650.22 | 1408.53 |
| 92.0 | -6526.99 | -4578.56 | 1.467e+04 | 1.009e+04 | -4390.08 | -3954.98 | 2563.47 | 1304.40 |
| 112.0 | -5845.08 | -4065.84 | 1.786e+04 | 6035.18 | -4390.08 | -3663.02 | 2450.61 | 1139.40 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|----------|----------|----------|----------|----------|
| 132.0 | -4858.87 | -3327.00 | 3.383e+04 | 1191.76 | -4390.08 | -3143.96 | 2345.13 | 920.06 |
| 152.0 | -3373.86 | -2257.02 | 4.593e+04 | 687.39 | -4390.08 | -2257.02 | 2328.16 | 711.35 |
| 172.0 | -1303.42 | -894.41 | 5.451e+04 | 577.92 | -4390.08 | -894.41 | 2020.74 | 470.07 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 2542.23 | 2.880e+04 | 1.00 | 8105.40 | 2.921e+04 |
| 23.0 | 1.00 | 2496.19 | 2.880e+04 | 1.00 | 8105.40 | 2.922e+04 |
| 46.0 | 1.00 | 2659.28 | 2.874e+04 | 1.00 | 8105.40 | 2.919e+04 |
| 69.0 | 1.00 | 2650.22 | 2.871e+04 | 1.00 | 8105.40 | 2.914e+04 |
| 92.0 | 1.00 | 2563.47 | 2.866e+04 | 1.00 | 8105.40 | 2.906e+04 |
| 112.0 | 1.00 | 2450.61 | 2.861e+04 | 1.00 | 8105.40 | 2.894e+04 |
| 132.0 | 1.00 | 2345.13 | 2.851e+04 | 1.00 | 8105.40 | 2.877e+04 |
| 152.0 | 1.00 | 2328.16 | 2.835e+04 | 1.00 | 8105.40 | 2.852e+04 |
| 172.0 | 1.00 | 2020.74 | 2.810e+04 | 1.00 | 8105.40 | 2.816e+04 |

1.1.1.1.2 Pareti Fronte Sud - Ovest

Si riportano le verifiche analitiche dei macroelementi della parete oggetto di verifica identificata nella figura successiva.

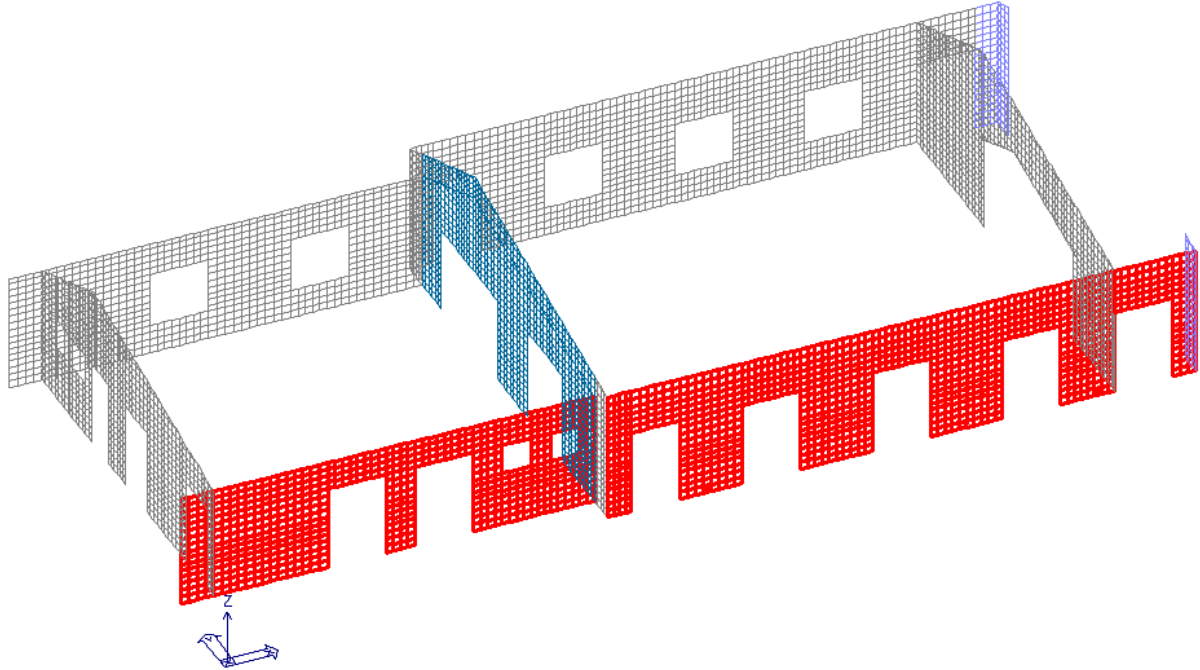


Fig 47. Parete oggetto di verifica (selezione in rosso).

Macrosetti n. 1, 2, 3, 4, 5 [maschi]

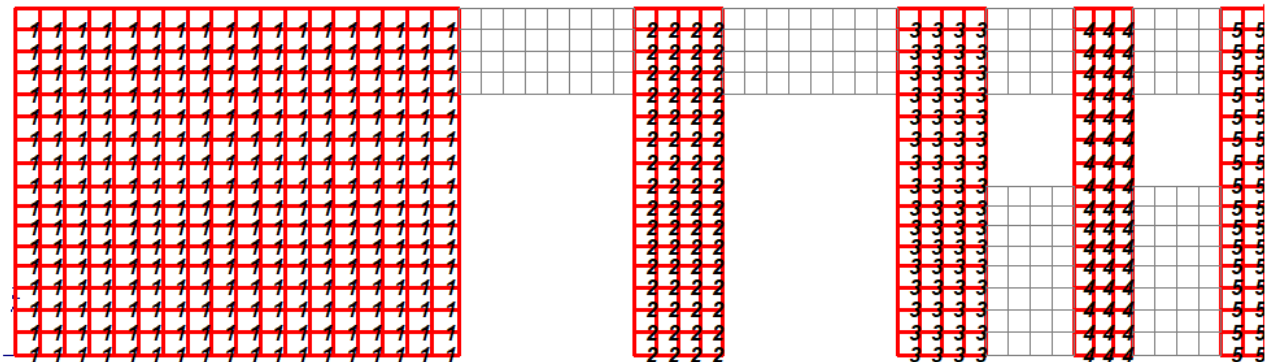


Fig 48. Elemento/i oggetto di verifica (Selezione in rosso).

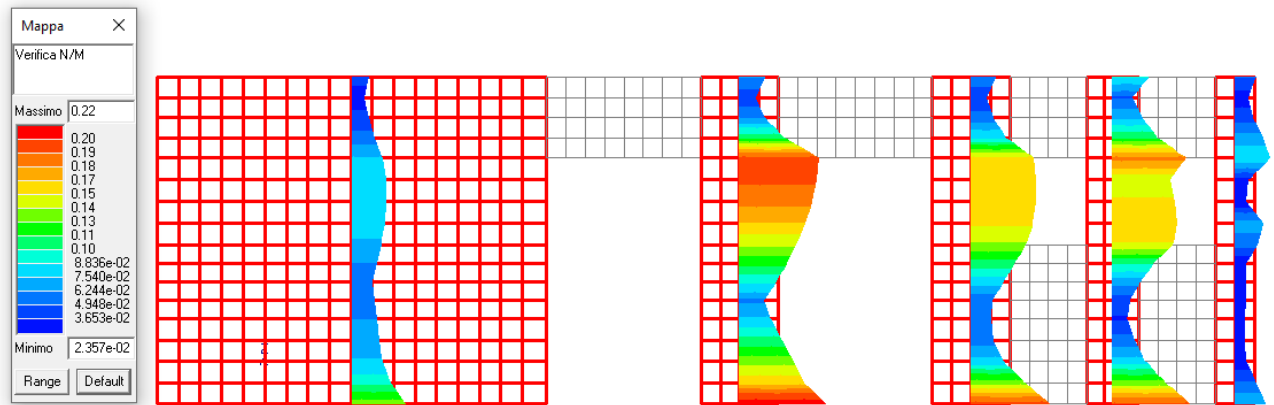


Fig 49. SLU: Mappa di verifica N/M – **Verifiche soddisfatte ($\rho \leq 1$).**

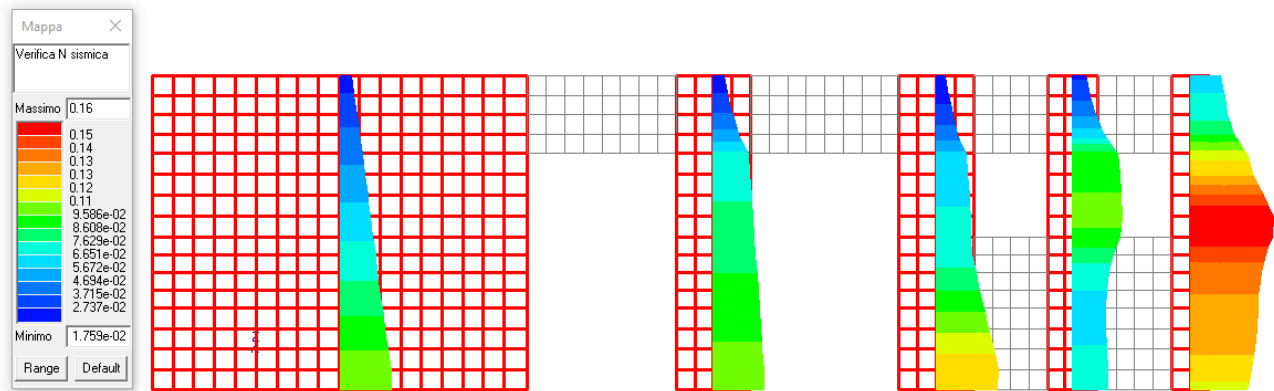


Fig 50. SLU: Mappa di verifica Nsismica – **Verifiche soddisfatte ($\rho \leq 0.625$).**

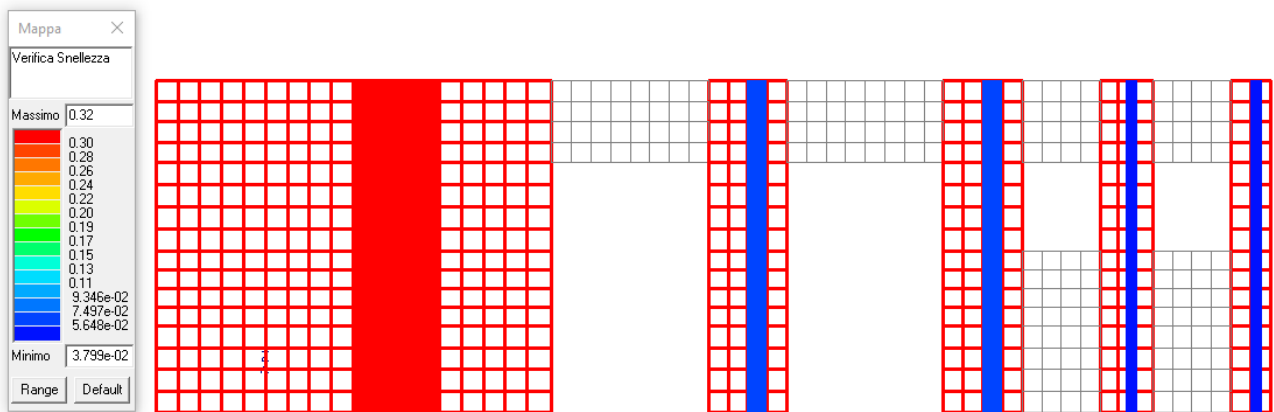


Fig 51. SLU: Mappa di Verifica Snellezza – **Verifiche soddisfatte ($\rho \leq 1$).**

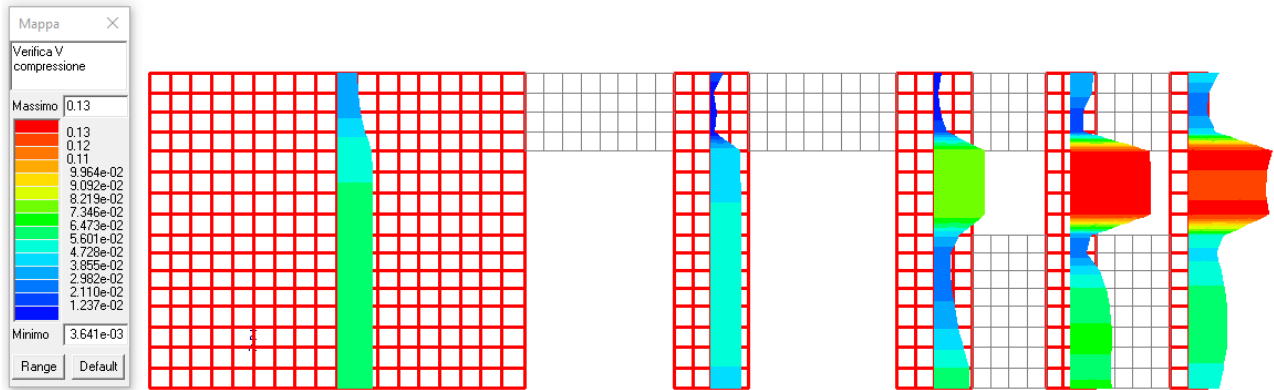


Fig 52. SLU: Mappa di Verifica V compressione – **Verifica soddisfatta ($\rho \leq 1$).**

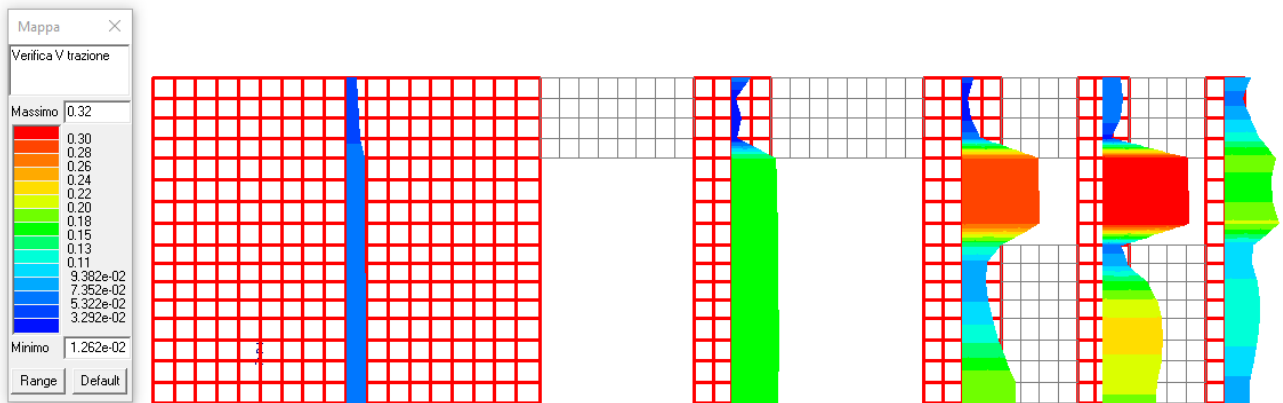


Fig 53. SLU: Mappa di verifica V trazione – **Verifiche soddisfatte ($\rho \leq 1$).**

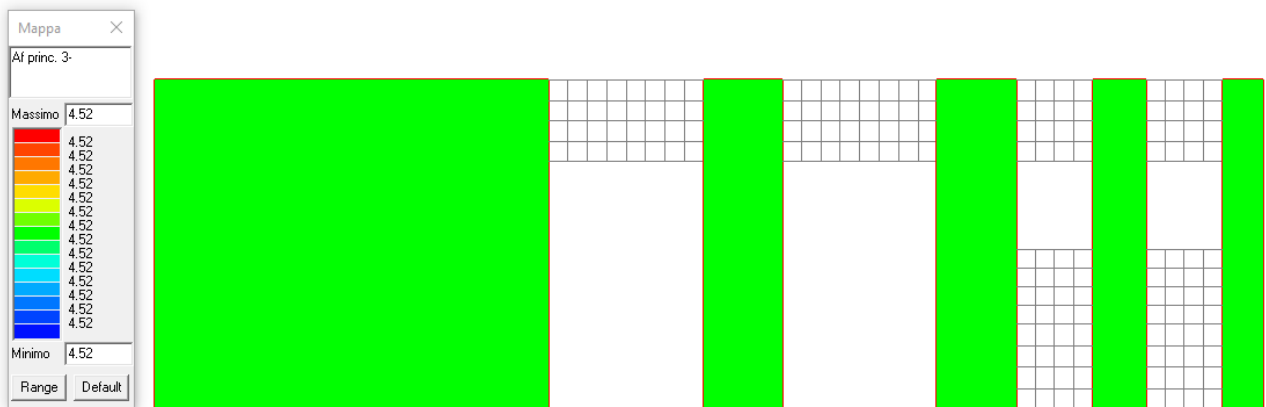


Fig 54. Mappa Armatura Verticale (singolo strato) da Calcolo [cm^2/m].

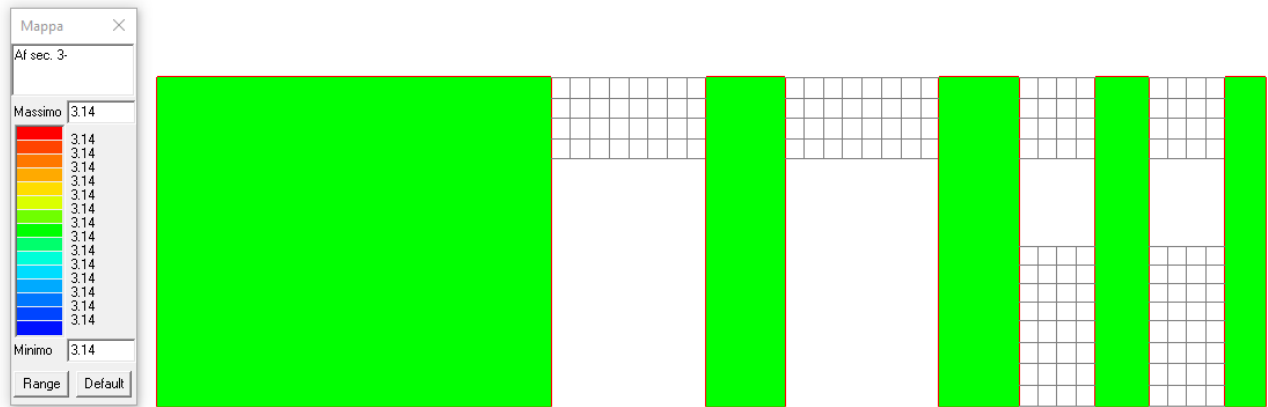


Fig 55. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm²/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 1 | 355.00 | 12.00 | 454.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.14 | 0.32 | 0.06 | 0.07 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.10 | 0.32 | 0.06 | 0.07 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.08 | 0.32 | 0.06 | 0.07 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.07 | 0.32 | 0.06 | 0.07 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.06 | 0.32 | 0.06 | 0.07 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.06 | 0.32 | 0.06 | 0.07 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.05 | 0.32 | 0.06 | 0.07 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.06 | 0.32 | 0.06 | 0.07 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.07 | 0.32 | 0.06 | 0.07 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.08 | 0.32 | 0.06 | 0.07 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.09 | 0.32 | 0.06 | 0.07 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.09 | 0.32 | 0.06 | 0.07 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.08 | 0.32 | 0.06 | 0.06 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.06 | 0.32 | 0.04 | 0.05 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.04 | 0.32 | 0.04 | 0.04 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.03 | 0.32 | 0.03 | 0.04 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.04 | 0.32 | 0.03 | 0.04 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.10 | 0.14 | 0.32 | 0.06 | 0.07 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|------------|------------|-----------|-----------|------------|------------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1.950e+04 | -1.900e+04 | 4.140e+05 | 6.893e+04 | -1.181e+04 | -1.453e+04 | 8564.92 | 2932.19 |
| 23.0 | -1.950e+04 | -1.757e+04 | 1.102e+05 | 4.932e+04 | -1.181e+04 | -1.453e+04 | 8564.92 | 2932.19 |
| 46.0 | -1.840e+04 | -1.378e+04 | 1.417e+06 | 8198.68 | -1.181e+04 | -1.366e+04 | 8683.57 | 2940.63 |
| 69.0 | -1.729e+04 | -1.306e+04 | 1.290e+06 | 5170.20 | -1.181e+04 | -1.277e+04 | 8681.25 | 2942.28 |
| 92.0 | -1.619e+04 | -1.235e+04 | 1.163e+06 | 2343.76 | -1.181e+04 | -1.185e+04 | 8666.95 | 2936.82 |
| 112.0 | -1.518e+04 | -1.165e+04 | 1.044e+06 | 2153.60 | -1.181e+04 | -1.101e+04 | 8646.21 | 2928.22 |
| 132.0 | -1.433e+04 | -1.102e+04 | 9.338e+05 | 5667.87 | -1.181e+04 | -1.018e+04 | 8621.29 | 2918.74 |
| 152.0 | -1.350e+04 | -1.257e+04 | 2.861e+05 | 2.940e+04 | -1.181e+04 | -9355.35 | 8591.23 | 2908.46 |
| 172.0 | -1.265e+04 | -1.164e+04 | 2.675e+05 | 3.441e+04 | -1.181e+04 | -8522.25 | 8535.91 | 2897.33 |
| 196.0 | -1.168e+04 | -1.107e+04 | 2.567e+05 | 3.857e+04 | -1.181e+04 | -7564.05 | 8489.36 | 2883.43 |
| 220.0 | -1.060e+04 | -9651.00 | 2.467e+05 | 4.046e+04 | -1.181e+04 | -6612.94 | 8426.63 | 2864.01 |
| 244.0 | -9500.81 | -8677.70 | 2.419e+05 | 3.968e+04 | -1.181e+04 | -5705.09 | 8388.25 | 2835.55 |
| 267.0 | -8492.23 | -7790.07 | 2.445e+05 | 3.544e+04 | -1.181e+04 | -4793.98 | 8314.25 | 2795.30 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|-----------|------------|----------|----------|----------|
| 289.0 | -7529.85 | -4791.20 | 2.057e+05 | 2.458e+04 | -1.181e+04 | -4350.44 | 6651.45 | 2157.07 |
| 311.0 | -6566.61 | -4280.69 | 2.204e+05 | 1.751e+04 | -1.181e+04 | -3921.69 | 5483.85 | 1828.90 |
| 333.0 | -5443.59 | -3459.32 | 1.917e+05 | 1.273e+04 | -1.181e+04 | -3189.27 | 4906.88 | 1627.39 |
| 355.0 | -4333.23 | -4123.97 | 1.927e+05 | 1.823e+04 | -1.181e+04 | -2655.89 | 4786.67 | 1589.82 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 8564.92 | 1.517e+05 | 1.00 | 4.320e+04 | 1.525e+05 |
| 23.0 | 1.00 | 8564.92 | 1.517e+05 | 1.00 | 4.320e+04 | 1.525e+05 |
| 46.0 | 1.00 | 8683.57 | 1.516e+05 | 1.00 | 4.320e+04 | 1.523e+05 |
| 69.0 | 1.00 | 8681.25 | 1.514e+05 | 1.00 | 4.320e+04 | 1.521e+05 |
| 92.0 | 1.00 | 8666.95 | 1.512e+05 | 1.00 | 4.320e+04 | 1.519e+05 |
| 112.0 | 1.00 | 8646.21 | 1.510e+05 | 1.00 | 4.320e+04 | 1.517e+05 |
| 132.0 | 1.00 | 8621.29 | 1.509e+05 | 1.00 | 4.320e+04 | 1.515e+05 |
| 152.0 | 1.00 | 8591.23 | 1.507e+05 | 1.00 | 4.320e+04 | 1.514e+05 |
| 172.0 | 1.00 | 8535.91 | 1.506e+05 | 1.00 | 4.320e+04 | 1.512e+05 |
| 196.0 | 1.00 | 8489.36 | 1.504e+05 | 1.00 | 4.320e+04 | 1.510e+05 |
| 220.0 | 1.00 | 8426.63 | 1.502e+05 | 1.00 | 4.320e+04 | 1.508e+05 |
| 244.0 | 1.00 | 8388.25 | 1.500e+05 | 1.00 | 4.320e+04 | 1.506e+05 |
| 267.0 | 1.00 | 8314.25 | 1.498e+05 | 1.00 | 4.320e+04 | 1.504e+05 |
| 289.0 | 1.00 | 6651.45 | 1.498e+05 | 1.00 | 4.320e+04 | 1.502e+05 |
| 311.0 | 1.00 | 5483.85 | 1.497e+05 | 1.00 | 4.320e+04 | 1.501e+05 |
| 333.0 | 1.00 | 4906.88 | 1.495e+05 | 1.00 | 4.320e+04 | 1.498e+05 |
| 355.0 | 1.00 | 4786.67 | 1.494e+05 | 1.00 | 4.320e+04 | 1.496e+05 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 2 | 355.00 | 12.00 | 90.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.22 | 0.06 | 0.05 | 0.17 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.16 | 0.06 | 0.05 | 0.17 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.14 | 0.06 | 0.05 | 0.17 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.11 | 0.06 | 0.05 | 0.17 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.08 | 0.06 | 0.05 | 0.17 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.06 | 0.06 | 0.05 | 0.17 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.09 | 0.06 | 0.05 | 0.17 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.12 | 0.06 | 0.05 | 0.17 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.14 | 0.06 | 0.05 | 0.17 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.17 | 0.06 | 0.05 | 0.17 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.18 | 0.06 | 0.05 | 0.16 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.20 | 0.06 | 0.05 | 0.16 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.20 | 0.06 | 0.05 | 0.16 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.11 | 0.06 | 4.86e-03 | 0.02 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.06 | 0.06 | 8.99e-03 | 0.03 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.04 | 0.06 | 3.64e-03 | 0.01 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.06 | 0.06 | 0.02 | 0.07 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.10 | 0.22 | 0.06 | 0.05 | 0.17 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|-----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -3800.77 | -2783.40 | 1.516e+04 | 2.298e+04 | -2301.49 | -2902.50 | 1345.44 | 1345.44 |
| 23.0 | -3800.77 | -2902.50 | 1.325e+05 | 1881.10 | -2301.49 | -2902.50 | 1345.44 | 1345.44 |
| 46.0 | -3692.59 | -2818.90 | 1.098e+05 | 1330.39 | -2301.49 | -2818.90 | 1387.59 | 1387.59 |
| 69.0 | -3584.41 | -2735.29 | 8.632e+04 | 803.19 | -2301.49 | -2735.29 | 1385.83 | 1385.83 |
| 92.0 | -3476.23 | -2651.65 | 6.265e+04 | 291.38 | -2301.49 | -2651.65 | 1382.70 | 1382.70 |
| 112.0 | -3375.11 | -2593.10 | 5346.32 | 6291.69 | -2301.49 | -2573.36 | 1378.31 | 1378.31 |
| 132.0 | -3281.04 | -2520.74 | 2242.48 | 9542.80 | -2301.49 | -2487.39 | 1372.97 | 1372.97 |
| 152.0 | -3186.97 | -2448.38 | 861.36 | 1.231e+04 | -2301.49 | -2426.40 | 1366.28 | 1366.28 |
| 172.0 | -3092.90 | -2198.68 | 2282.93 | 1.468e+04 | -2301.49 | -2309.33 | 1358.24 | 1358.24 |
| 196.0 | -2989.43 | -2119.08 | 4299.30 | 1.706e+04 | -2301.49 | -2251.64 | 1347.93 | 1347.93 |
| 220.0 | -2876.55 | -2072.46 | 7830.33 | 1.884e+04 | -2301.49 | -2188.72 | 1334.87 | 1334.87 |
| 244.0 | -2763.67 | -1985.63 | 1.034e+04 | 1.996e+04 | -2301.49 | -2101.40 | 1320.21 | 1320.21 |
| 267.0 | -2653.14 | -1900.61 | 1.274e+04 | 2.046e+04 | -2301.49 | -2015.93 | 1304.56 | 1304.56 |
| 289.0 | -1924.48 | -1371.08 | 7050.86 | 1.113e+04 | -2301.49 | -1487.31 | 137.02 | 137.02 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|----------|----------|----------|----------|----------|
| 311.0 | -1468.70 | -1149.99 | 4.698e+04 | 628.77 | -2301.49 | -984.64 | 252.84 | 252.84 |
| 333.0 | -1085.48 | -853.20 | 2.952e+04 | 114.09 | -2301.49 | -845.77 | 102.29 | 102.29 |
| 355.0 | -814.99 | -814.99 | 4412.34 | 6207.85 | -2301.49 | -645.06 | 529.03 | 529.03 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 1345.44 | 2.847e+04 | 1.00 | 8105.40 | 2.847e+04 |
| 23.0 | 1.00 | 1345.44 | 2.847e+04 | 1.00 | 8105.40 | 2.847e+04 |
| 46.0 | 1.00 | 1387.59 | 2.845e+04 | 1.00 | 8105.40 | 2.845e+04 |
| 69.0 | 1.00 | 1385.83 | 2.844e+04 | 1.00 | 8105.40 | 2.844e+04 |
| 92.0 | 1.00 | 1382.70 | 2.842e+04 | 1.00 | 8105.40 | 2.842e+04 |
| 112.0 | 1.00 | 1378.31 | 2.841e+04 | 1.00 | 8105.40 | 2.841e+04 |
| 132.0 | 1.00 | 1372.97 | 2.839e+04 | 1.00 | 8105.40 | 2.839e+04 |
| 152.0 | 1.00 | 1366.28 | 2.838e+04 | 1.00 | 8105.40 | 2.838e+04 |
| 172.0 | 1.00 | 1358.24 | 2.836e+04 | 1.00 | 8105.40 | 2.836e+04 |
| 196.0 | 1.00 | 1347.93 | 2.835e+04 | 1.00 | 8105.40 | 2.835e+04 |
| 220.0 | 1.00 | 1334.87 | 2.834e+04 | 1.00 | 8105.40 | 2.834e+04 |
| 244.0 | 1.00 | 1320.21 | 2.832e+04 | 1.00 | 8105.40 | 2.832e+04 |
| 267.0 | 1.00 | 1304.56 | 2.831e+04 | 1.00 | 8105.40 | 2.831e+04 |
| 289.0 | 1.00 | 137.02 | 2.821e+04 | 1.00 | 8105.40 | 2.821e+04 |
| 311.0 | 1.00 | 252.84 | 2.812e+04 | 1.00 | 8105.40 | 2.812e+04 |
| 333.0 | 1.00 | 102.29 | 2.809e+04 | 1.00 | 8105.40 | 2.809e+04 |
| 355.0 | 1.00 | 529.03 | 2.806e+04 | 1.00 | 8105.40 | 2.806e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 3 | 355.00 | 12.00 | 90.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.20 | 0.07 | 0.06 | 0.19 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.14 | 0.07 | 0.06 | 0.19 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.08 | 0.07 | 0.05 | 0.16 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.06 | 0.07 | 0.04 | 0.13 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.05 | 0.07 | 0.03 | 0.11 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.05 | 0.07 | 0.03 | 0.09 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.08 | 0.07 | 0.02 | 0.08 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.11 | 0.07 | 0.03 | 0.09 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.14 | 0.07 | 0.04 | 0.14 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.16 | 0.07 | 0.08 | 0.28 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.16 | 0.07 | 0.08 | 0.28 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.16 | 0.07 | 0.08 | 0.28 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.16 | 0.07 | 0.08 | 0.28 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.09 | 0.07 | 0.02 | 0.07 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.06 | 0.07 | 8.20e-03 | 0.03 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.04 | 0.07 | 4.92e-03 | 0.02 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.06 | 0.07 | 0.01 | 0.04 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.12 | 0.20 | 0.07 | 0.08 | 0.28 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|-----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -4644.95 | -2102.23 | 4577.86 | 2.036e+04 | -2605.64 | 524.84 | 1577.61 | 1577.61 |
| 23.0 | -4664.74 | -2113.65 | 5777.41 | 1.389e+04 | -2605.64 | 505.05 | 1580.15 | 1580.15 |
| 46.0 | -4318.21 | -2014.07 | 5353.18 | 8329.11 | -2605.64 | 271.87 | 1293.16 | 1293.16 |
| 69.0 | -3956.51 | -3035.82 | 2.654e+04 | 4987.74 | -2605.64 | 5.63 | 1061.27 | 1061.27 |
| 92.0 | -3610.43 | -3610.43 | 4.117e+04 | 1029.35 | -2605.64 | -265.33 | 881.80 | 881.80 |
| 112.0 | -3295.18 | -2565.15 | 9230.23 | 5508.24 | -2605.64 | -524.80 | 751.99 | 751.99 |
| 132.0 | -2995.07 | -1970.53 | 6175.21 | 8268.98 | -2605.64 | -803.93 | 680.30 | 680.30 |
| 152.0 | -2714.40 | -1989.65 | 4577.29 | 1.108e+04 | -2605.64 | -1096.77 | 707.23 | 707.23 |
| 172.0 | -2619.41 | -2025.01 | 1119.52 | 1.417e+04 | -2605.64 | -2416.68 | 1127.25 | 1127.25 |
| 196.0 | -2587.87 | -1793.36 | 1886.30 | 1.576e+04 | -2605.64 | -1993.98 | 2304.90 | 2304.90 |
| 220.0 | -2474.98 | -1732.75 | 406.22 | 1.643e+04 | -2605.64 | -1914.30 | 2295.42 | 2295.42 |
| 244.0 | -2362.10 | -1645.92 | 1867.46 | 1.647e+04 | -2605.64 | -1829.80 | 2283.77 | 2283.77 |
| 267.0 | -2251.57 | -1560.90 | 4045.06 | 1.592e+04 | -2605.64 | -1747.37 | 2270.53 | 2270.53 |
| 289.0 | -1595.70 | -1473.87 | 2030.18 | 8858.61 | -2605.64 | -1141.90 | 529.84 | 529.84 |
| 311.0 | -1221.07 | -832.65 | 4.080e+04 | 357.37 | -2605.64 | -950.65 | 230.42 | 230.42 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|---------|---------|-----------|----------|----------|----------|----------|----------|
| 333.0 | -903.10 | -585.29 | 2.798e+04 | 209.67 | -2605.64 | -892.33 | 138.16 | 138.16 |
| 355.0 | -669.97 | -669.97 | 879.79 | 5925.45 | -2605.64 | -404.10 | 322.85 | 322.85 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 1577.61 | 2.794e+04 | 1.00 | 8105.40 | 2.794e+04 |
| 23.0 | 1.00 | 1580.15 | 2.794e+04 | 1.00 | 8105.40 | 2.794e+04 |
| 46.0 | 1.00 | 1293.16 | 2.794e+04 | 1.00 | 8105.40 | 2.794e+04 |
| 69.0 | 1.00 | 1061.27 | 2.794e+04 | 1.00 | 8105.40 | 2.794e+04 |
| 92.0 | 1.00 | 881.80 | 2.799e+04 | 1.00 | 8105.40 | 2.799e+04 |
| 112.0 | 1.00 | 751.99 | 2.803e+04 | 1.00 | 8105.40 | 2.803e+04 |
| 132.0 | 1.00 | 680.30 | 2.809e+04 | 1.00 | 8105.40 | 2.809e+04 |
| 152.0 | 1.00 | 707.23 | 2.814e+04 | 1.00 | 8105.40 | 2.814e+04 |
| 172.0 | 1.00 | 1127.25 | 2.838e+04 | 1.00 | 8105.40 | 2.838e+04 |
| 196.0 | 1.00 | 2304.90 | 2.830e+04 | 1.00 | 8105.40 | 2.830e+04 |
| 220.0 | 1.00 | 2295.42 | 2.829e+04 | 1.00 | 8105.40 | 2.829e+04 |
| 244.0 | 1.00 | 2283.77 | 2.827e+04 | 1.00 | 8105.40 | 2.827e+04 |
| 267.0 | 1.00 | 2270.53 | 2.826e+04 | 1.00 | 8105.40 | 2.826e+04 |
| 289.0 | 1.00 | 529.84 | 2.815e+04 | 1.00 | 8105.40 | 2.815e+04 |
| 311.0 | 1.00 | 230.42 | 2.811e+04 | 1.00 | 8105.40 | 2.811e+04 |
| 333.0 | 1.00 | 138.16 | 2.810e+04 | 1.00 | 8105.40 | 2.810e+04 |
| 355.0 | 1.00 | 322.85 | 2.801e+04 | 1.00 | 8105.40 | 2.801e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 4 | 355.00 | 12.00 | 60.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.20 | 0.04 | 0.07 | 0.19 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.13 | 0.04 | 0.06 | 0.20 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.08 | 0.04 | 0.07 | 0.21 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.06 | 0.04 | 0.07 | 0.22 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.04 | 0.04 | 0.06 | 0.22 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.04 | 0.04 | 0.06 | 0.20 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.07 | 0.04 | 0.05 | 0.16 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.10 | 0.04 | 0.02 | 0.09 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.15 | 0.04 | 0.03 | 0.06 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.16 | 0.04 | 0.13 | 0.32 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.16 | 0.04 | 0.13 | 0.32 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.14 | 0.04 | 0.13 | 0.31 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.19 | 0.04 | 0.13 | 0.31 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.11 | 0.04 | 0.02 | 0.03 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.07 | 0.04 | 0.02 | 0.06 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.05 | 0.04 | 0.03 | 0.07 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.09 | 0.04 | 0.04 | 0.06 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.10 | 0.20 | 0.04 | 0.13 | 0.32 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|-----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1781.65 | -1254.81 | 229.22 | 1.063e+04 | -1221.88 | -1165.65 | 954.23 | 805.87 |
| 23.0 | -1770.09 | -1252.90 | 147.16 | 7277.63 | -1221.88 | -1166.49 | 928.27 | 831.84 |
| 46.0 | -1699.18 | -1591.85 | 16.12 | 4603.81 | -1221.88 | -1123.35 | 951.07 | 891.88 |
| 69.0 | -1653.43 | -1197.31 | 506.36 | 3005.24 | -1221.88 | -1169.45 | 951.98 | 919.61 |
| 92.0 | -1647.76 | -1156.75 | 752.79 | 1910.88 | -1221.88 | -1168.65 | 907.87 | 906.01 |
| 112.0 | -1691.95 | -1634.68 | 1662.05 | 2316.80 | -1221.88 | -1135.42 | 829.86 | 829.86 |
| 132.0 | -1815.73 | -1336.68 | 1979.62 | 3701.40 | -1221.88 | -1194.07 | 665.47 | 665.47 |
| 152.0 | -2047.25 | -1502.82 | 3288.33 | 5614.38 | -1221.88 | -1320.10 | 360.24 | 360.24 |
| 172.0 | -2371.59 | -1639.79 | 3629.27 | 8506.51 | -1221.88 | -1768.40 | 454.46 | 267.55 |
| 196.0 | -2523.18 | -1686.11 | 3251.60 | 9167.47 | -1221.88 | -1899.62 | 1897.52 | 1324.16 |
| 220.0 | -2447.93 | -1628.23 | 3109.51 | 8707.49 | -1221.88 | -1840.02 | 1891.91 | 1318.55 |
| 244.0 | -2372.67 | -1676.14 | 1.133e+04 | 7897.60 | -1221.88 | -1799.56 | 1884.80 | 1311.44 |
| 267.0 | -2298.99 | -1729.78 | 5.143e+04 | 2536.51 | -1221.88 | -1729.78 | 1876.49 | 1303.13 |
| 289.0 | -1577.77 | -1222.48 | 3.021e+04 | 1638.19 | -1221.88 | -1222.48 | 276.70 | 113.34 |
| 311.0 | -1177.31 | -939.87 | 1.908e+04 | 1056.01 | -1221.88 | -939.87 | 268.37 | 263.43 |
| 333.0 | -876.06 | -725.49 | 1.206e+04 | 897.00 | -1221.88 | -725.49 | 480.92 | 287.33 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|---------|---------|---------|----------|----------|----------|----------|----------|
| 355.0 | -665.10 | -639.26 | 2727.25 | 4583.21 | -1221.88 | -549.27 | 514.83 | 266.53 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 954.23 | 1.456e+04 | 1.00 | 4175.51 | 1.457e+04 |
| 23.0 | 1.00 | 928.27 | 1.456e+04 | 1.00 | 4175.51 | 1.457e+04 |
| 46.0 | 1.00 | 951.07 | 1.455e+04 | 1.00 | 4175.51 | 1.457e+04 |
| 69.0 | 1.00 | 951.98 | 1.456e+04 | 1.00 | 4175.51 | 1.455e+04 |
| 92.0 | 1.00 | 907.87 | 1.456e+04 | 1.00 | 4175.51 | 1.455e+04 |
| 112.0 | 1.00 | 829.86 | 1.455e+04 | 1.00 | 4175.51 | 1.455e+04 |
| 132.0 | 1.00 | 665.47 | 1.456e+04 | 1.00 | 4175.51 | 1.456e+04 |
| 152.0 | 1.00 | 360.24 | 1.458e+04 | 1.00 | 4175.51 | 1.458e+04 |
| 172.0 | 1.00 | 454.46 | 1.464e+04 | 1.00 | 4175.51 | 1.472e+04 |
| 196.0 | 1.00 | 1897.52 | 1.466e+04 | 1.00 | 4175.51 | 1.462e+04 |
| 220.0 | 1.00 | 1891.91 | 1.465e+04 | 1.00 | 4175.51 | 1.461e+04 |
| 244.0 | 1.00 | 1884.80 | 1.465e+04 | 1.00 | 4175.51 | 1.460e+04 |
| 267.0 | 1.00 | 1876.49 | 1.464e+04 | 1.00 | 4175.51 | 1.459e+04 |
| 289.0 | 1.00 | 276.70 | 1.457e+04 | 1.00 | 4175.51 | 1.460e+04 |
| 311.0 | 1.00 | 268.37 | 1.453e+04 | 1.00 | 4175.51 | 1.456e+04 |
| 333.0 | 1.00 | 480.92 | 1.449e+04 | 1.00 | 4175.51 | 1.452e+04 |
| 355.0 | 1.00 | 514.83 | 1.447e+04 | 1.00 | 4175.51 | 1.444e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 5 | 355.00 | 12.00 | 46.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.07 | 0.04 | 0.05 | 0.09 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.05 | 0.04 | 0.05 | 0.09 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.03 | 0.04 | 0.06 | 0.11 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.02 | 0.04 | 0.06 | 0.12 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.02 | 0.04 | 0.06 | 0.13 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.02 | 0.04 | 0.06 | 0.13 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.03 | 0.04 | 0.05 | 0.12 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.03 | 0.04 | 0.04 | 0.10 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.05 | 0.04 | 0.06 | 0.10 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.07 | 0.04 | 0.13 | 0.20 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.03 | 0.04 | 0.12 | 0.17 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.03 | 0.04 | 0.13 | 0.17 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.09 | 0.04 | 0.13 | 0.19 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.07 | 0.04 | 0.04 | 0.13 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.04 | 0.04 | 0.03 | 0.09 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.03 | 0.04 | 0.03 | 0.06 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.05 | 0.04 | 0.05 | 0.09 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.16 | 0.09 | 0.04 | 0.13 | 0.20 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -2197.03 | -2074.91 | 6198.01 | 3890.93 | -1643.56 | -1132.87 | 600.58 | 304.46 |
| 23.0 | -2329.36 | -1849.36 | 2687.46 | 2785.94 | -1643.56 | -1194.19 | 670.99 | 313.69 |
| 46.0 | -2491.33 | -1975.21 | 1500.56 | 1434.23 | -1643.56 | -1356.79 | 736.29 | 370.13 |
| 69.0 | -2555.57 | -1793.67 | 4779.48 | 135.93 | -1643.56 | -1583.96 | 758.54 | 411.66 |
| 92.0 | -2600.21 | -1542.78 | 4658.41 | 213.93 | -1643.56 | -1649.04 | 747.39 | 437.05 |
| 112.0 | -2637.12 | -1460.19 | 4915.06 | 168.91 | -1643.56 | -1766.55 | 706.19 | 441.28 |
| 132.0 | -2726.49 | -1382.77 | 5181.83 | 95.94 | -1643.56 | -1944.57 | 635.25 | 412.52 |
| 152.0 | -2891.04 | -2196.95 | 5441.54 | 87.83 | -1643.56 | -2196.95 | 544.23 | 345.93 |
| 172.0 | -3149.96 | -2483.11 | 1.169e+04 | 270.88 | -1643.56 | -2483.11 | 693.52 | 357.96 |
| 196.0 | -3200.18 | -2738.17 | 1.479e+04 | 515.63 | -1643.56 | -2738.17 | 1620.78 | 698.21 |
| 220.0 | -2831.89 | -2647.00 | 1469.99 | 1503.79 | -1643.56 | -2095.22 | 1526.12 | 608.40 |
| 244.0 | -2407.43 | -2242.95 | 3156.26 | 1689.65 | -1643.56 | -1158.78 | 1528.18 | 594.59 |
| 267.0 | -2170.12 | -400.30 | 1.560e+04 | 849.47 | -1643.56 | -400.30 | 1625.90 | 648.40 |
| 289.0 | -1658.86 | -443.97 | 1.221e+04 | 704.88 | -1643.56 | -1652.39 | 508.89 | 436.82 |
| 311.0 | -1423.54 | -380.59 | 7455.01 | 685.78 | -1643.56 | -1414.19 | 341.23 | 320.97 |
| 333.0 | -1315.86 | -417.00 | 4038.63 | 1062.51 | -1643.56 | -417.00 | 361.01 | 223.02 |
| 355.0 | -1156.06 | -447.63 | 438.69 | 2478.31 | -1643.56 | -367.37 | 575.24 | 326.02 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac | Vdd | Vid | [A s.i. | Incli. | Dist.] | Vfd |
|-------|----------|-----------|-----------|---------|----------|-----------|---------|-----|----------|--------|---------|---------|
| cm | | daN | daN | | daN | daN | daN | daN | cm2 | gradi | cm | daN |
| 0.0 | 1.00 | 600.58 | 1.220e+04 | 1.00 | 3487.78 | 1.230e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1267.63 |
| 23.0 | 1.00 | 670.99 | 1.221e+04 | 1.00 | 3487.78 | 1.237e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1261.88 |
| 46.0 | 1.00 | 736.29 | 1.223e+04 | 1.00 | 3487.78 | 1.240e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1224.48 |
| 69.0 | 1.00 | 758.54 | 1.227e+04 | 1.00 | 3487.78 | 1.241e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1262.50 |
| 92.0 | 1.00 | 747.39 | 1.228e+04 | 1.00 | 3487.78 | 1.242e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1276.48 |
| 112.0 | 1.00 | 706.19 | 1.229e+04 | 1.00 | 3487.78 | 1.242e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1291.19 |
| 132.0 | 1.00 | 635.25 | 1.232e+04 | 1.00 | 3487.78 | 1.244e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1351.54 |
| 152.0 | 1.00 | 544.23 | 1.236e+04 | 1.00 | 3487.78 | 1.247e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1457.58 |
| 172.0 | 1.00 | 693.52 | 1.240e+04 | 1.00 | 3487.78 | 1.248e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1613.50 |
| 196.0 | 1.00 | 1620.78 | 1.244e+04 | 1.00 | 3487.78 | 1.225e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1713.48 |
| 220.0 | 1.00 | 1526.12 | 1.235e+04 | 1.00 | 3487.78 | 1.227e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1400.62 |
| 244.0 | 1.00 | 1528.18 | 1.220e+04 | 1.00 | 3487.78 | 1.238e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1255.33 |
| 267.0 | 1.00 | 1625.90 | 1.208e+04 | 1.00 | 3487.78 | 1.231e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1308.36 |
| 289.0 | 1.00 | 508.89 | 1.228e+04 | 1.00 | 3487.78 | 1.223e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1333.23 |
| 311.0 | 1.00 | 341.23 | 1.224e+04 | 1.00 | 3487.78 | 1.220e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1273.73 |
| 333.0 | 1.00 | 361.01 | 1.209e+04 | 1.00 | 3487.78 | 1.219e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1122.62 |
| 355.0 | 1.00 | 575.24 | 1.208e+04 | 1.00 | 3487.78 | 1.219e+04 | 2184.98 | 0.0 | 0.0 | 0.0 | 0.0 | 1070.34 |

Macrosetti n. 15, 16, 44, 45, 49, 107 [maschi]

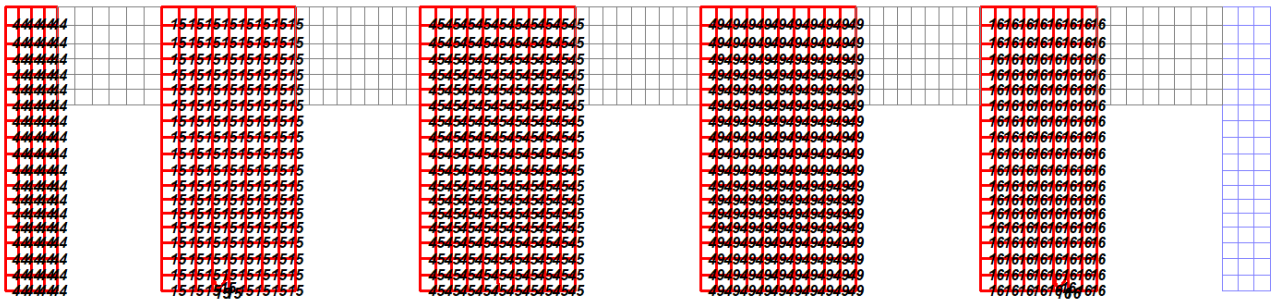


Fig 56. Elemento/i oggetto di verifica (Selezione in rosso).

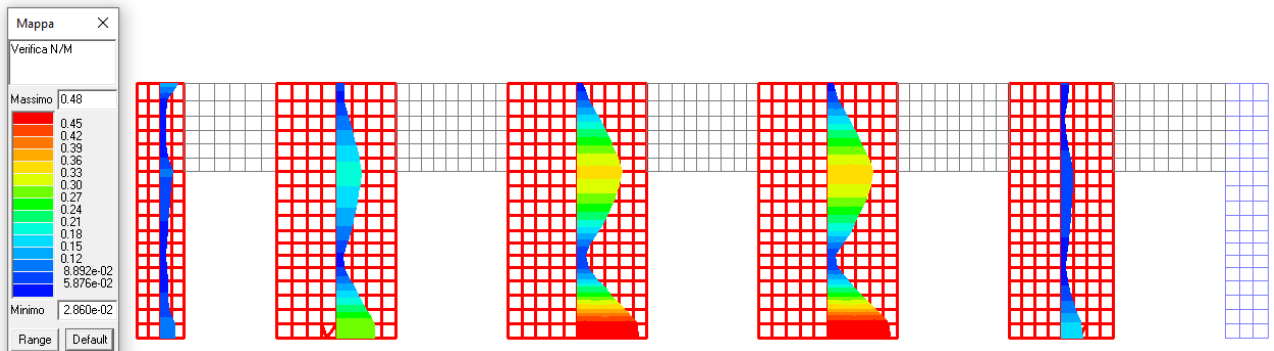


Fig 57. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

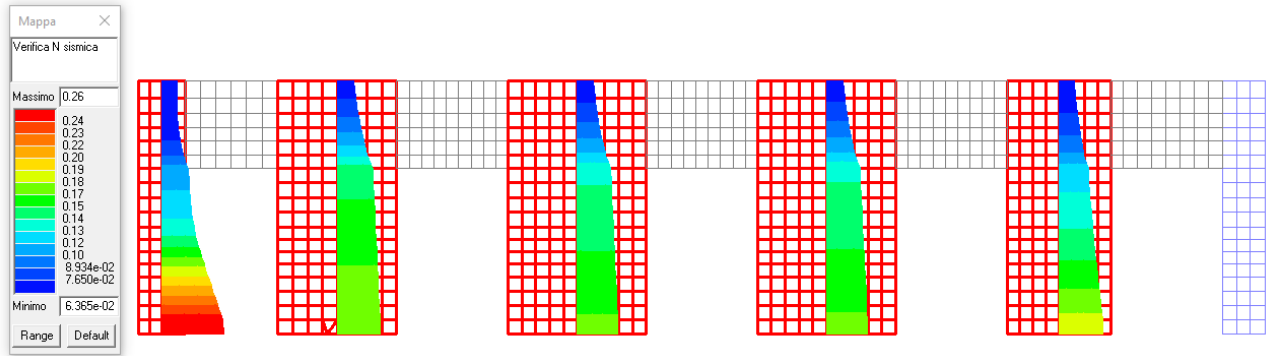


Fig 58. SLU: Mappa di verifica N sismica – **Verifiche soddisfatte ($\rho \leq 0.625$).**

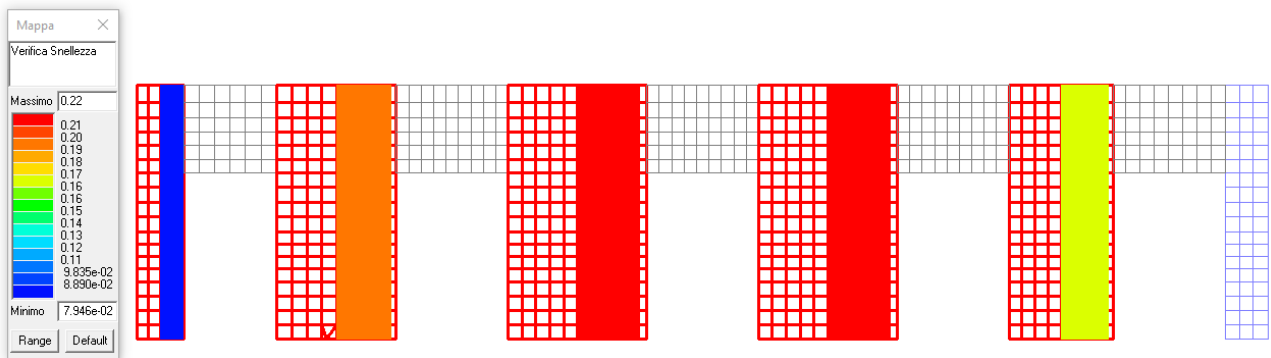


Fig 59. SLU: Mappa di Verifica Snellezza – **Verifiche soddisfatte ($\rho \leq 1$).**

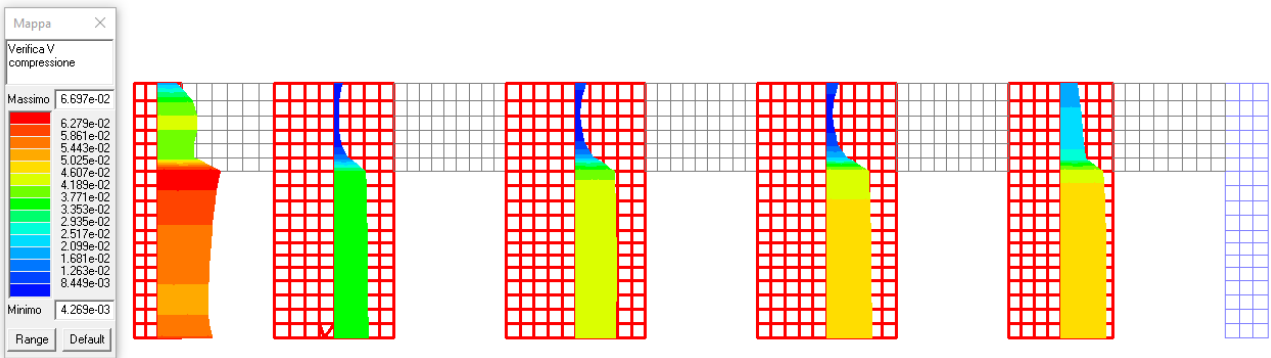


Fig 60. SLU: Mappa di Verifica V compressione – **Verifica soddisfatta ($\rho \leq 1$).**

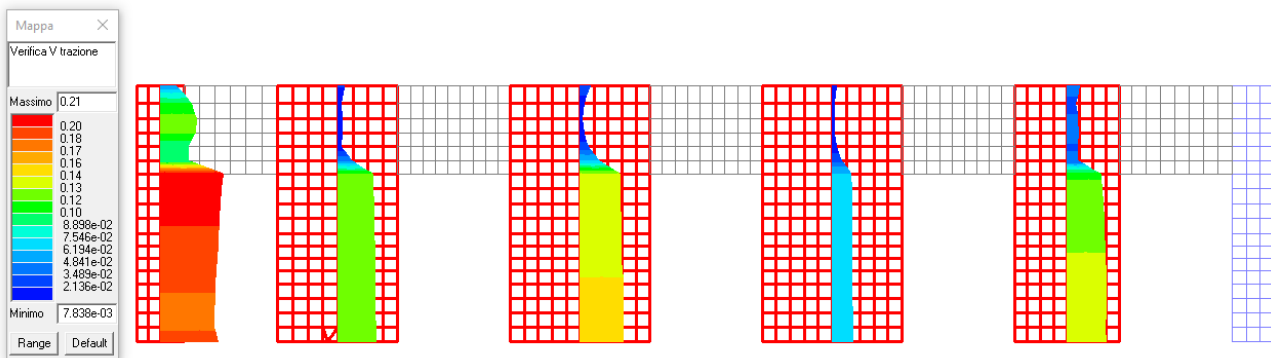


Fig 61. SLU: Mappa di verifica V trazione – **Verifiche soddisfatte ($\rho \leq 1$).**

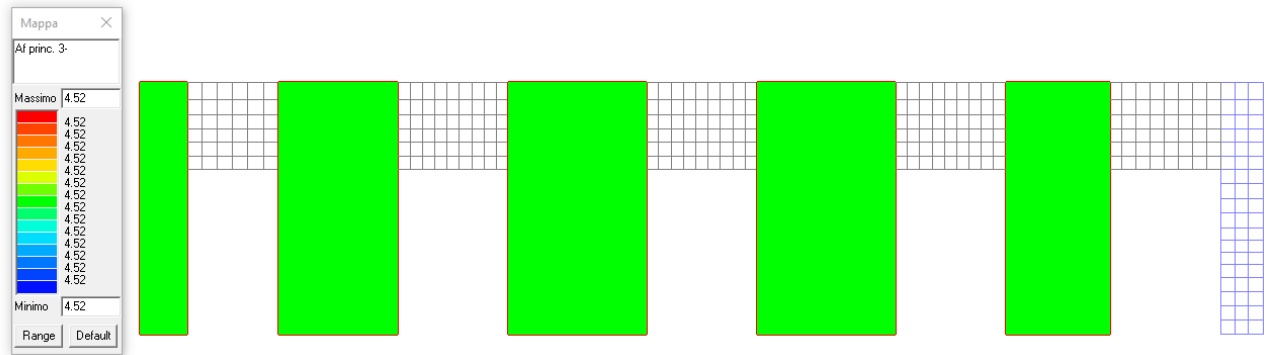


Fig 62. Mappa Armatura Verticale (singolo strato) da Calcolo [cm²/m].

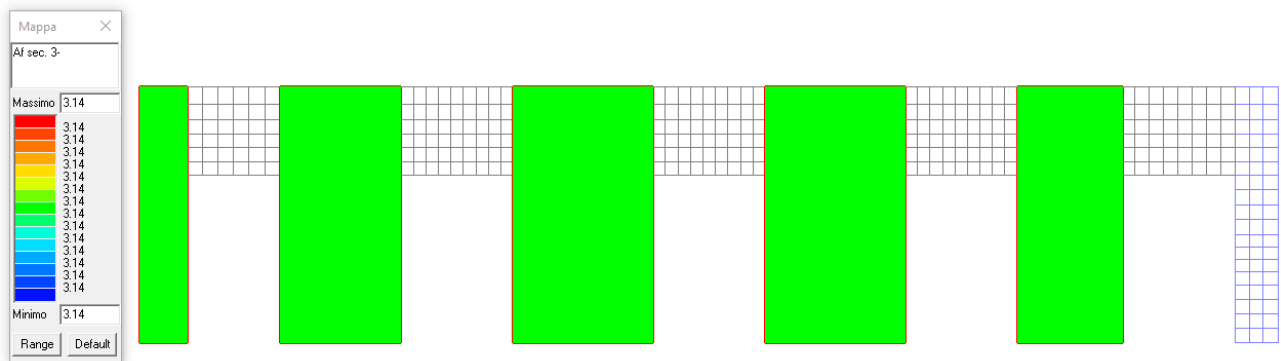


Fig 63. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm²/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| 15 | cm | cm | cm | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.30 | 0.19 | 0.04 | 0.13 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.29 | 0.19 | 0.04 | 0.13 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.23 | 0.19 | 0.04 | 0.13 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.17 | 0.19 | 0.04 | 0.13 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.11 | 0.19 | 0.04 | 0.13 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.06 | 0.19 | 0.04 | 0.13 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.05 | 0.19 | 0.04 | 0.13 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.08 | 0.19 | 0.04 | 0.12 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.11 | 0.19 | 0.04 | 0.12 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.14 | 0.19 | 0.03 | 0.12 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.16 | 0.19 | 0.03 | 0.12 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.18 | 0.19 | 0.03 | 0.12 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.19 | 0.19 | 0.03 | 0.12 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.17 | 0.19 | 0.02 | 0.05 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.15 | 0.19 | 6.70e-03 | 0.01 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.12 | 0.19 | 4.37e-03 | 0.01 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.09 | 0.19 | 4.27e-03 | 0.02 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.06 | 0.19 | 4.47e-03 | 0.01 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.06 | 0.19 | 8.77e-03 | 0.02 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|--------|------------|--------|----------|-------------|------------|------------|-------|
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.18 | 0.30 | 0.19 | 0.04 | 0.13 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|------------|----------|-----------|-----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1.443e+04 | -8302.59 | 1.069e+05 | 6.642e+04 | -9972.41 | -7968.09 | 2332.43 | 2332.43 |
| 23.0 | -1.443e+04 | -7484.27 | 1.038e+05 | 6.469e+04 | -9972.41 | -7990.93 | 2308.03 | 2308.03 |
| 46.0 | -1.427e+04 | -7998.34 | 9.715e+04 | 5.164e+04 | -9972.41 | -7705.31 | 2300.38 | 2300.27 |
| 69.0 | -1.404e+04 | -7939.54 | 7.208e+04 | 3.742e+04 | -9972.41 | -7520.50 | 2290.90 | 2290.78 |
| 92.0 | -1.380e+04 | -6906.19 | 3.931e+04 | 2.357e+04 | -9972.41 | -7362.04 | 2282.02 | 2281.90 |
| 112.0 | -1.359e+04 | -7724.58 | 2.814e+04 | 1.313e+04 | -9972.41 | -7225.07 | 2271.92 | 2271.81 |
| 132.0 | -1.338e+04 | -6664.60 | 4075.37 | 1.154e+04 | -9972.41 | -7070.39 | 2260.66 | 2260.55 |
| 152.0 | -1.318e+04 | -6707.81 | 4794.84 | 1.847e+04 | -9972.41 | -6926.83 | 2247.34 | 2247.22 |
| 172.0 | -1.298e+04 | -6552.64 | 7279.96 | 2.444e+04 | -9972.41 | -6762.46 | 2231.83 | 2231.83 |
| 196.0 | -1.276e+04 | -6381.95 | 1.026e+04 | 3.030e+04 | -9972.41 | -6559.97 | 2212.88 | 2212.76 |
| 220.0 | -1.252e+04 | -6195.74 | 1.324e+04 | 3.476e+04 | -9972.41 | -6376.30 | 2189.73 | 2189.61 |
| 244.0 | -1.228e+04 | -6462.56 | 7.827e+04 | 3.924e+04 | -9972.41 | -6184.05 | 2165.99 | 2165.88 |
| 267.0 | -1.204e+04 | -6209.90 | 9.667e+04 | 4.178e+04 | -9972.41 | -5985.13 | 2146.46 | 2146.35 |
| 289.0 | -1.020e+04 | -5120.79 | 7.264e+04 | 3.678e+04 | -9972.41 | -4971.18 | 957.38 | 824.91 |
| 311.0 | -9058.17 | -4451.43 | 6.024e+04 | 3.081e+04 | -9972.41 | -4304.23 | 423.03 | 211.41 |
| 333.0 | -8034.01 | -3832.70 | 4.804e+04 | 2.457e+04 | -9972.41 | -3771.14 | 275.22 | 260.75 |
| 355.0 | -7122.33 | -3213.05 | 3.691e+04 | 1.796e+04 | -9972.41 | -7100.45 | 271.79 | 271.79 |
| 381.0 | -6236.84 | -2708.29 | 2.632e+04 | 1.105e+04 | -9972.41 | -2798.20 | 280.67 | 237.83 |
| 408.0 | -5577.03 | -2262.49 | 3543.19 | 1.225e+04 | -9972.41 | -2324.47 | 550.50 | 404.50 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 2332.43 | 6.383e+04 | 1.00 | 1.808e+04 | 6.383e+04 |
| 23.0 | 1.00 | 2308.03 | 6.383e+04 | 1.00 | 1.808e+04 | 6.383e+04 |
| 46.0 | 1.00 | 2300.38 | 6.378e+04 | 1.00 | 1.808e+04 | 6.380e+04 |
| 69.0 | 1.00 | 2290.90 | 6.374e+04 | 1.00 | 1.808e+04 | 6.377e+04 |
| 92.0 | 1.00 | 2282.02 | 6.371e+04 | 1.00 | 1.808e+04 | 6.373e+04 |
| 112.0 | 1.00 | 2271.92 | 6.369e+04 | 1.00 | 1.808e+04 | 6.370e+04 |
| 132.0 | 1.00 | 2260.66 | 6.366e+04 | 1.00 | 1.808e+04 | 6.367e+04 |
| 152.0 | 1.00 | 2247.34 | 6.363e+04 | 1.00 | 1.808e+04 | 6.363e+04 |
| 172.0 | 1.00 | 2231.83 | 6.360e+04 | 1.00 | 1.808e+04 | 6.360e+04 |
| 196.0 | 1.00 | 2212.88 | 6.356e+04 | 1.00 | 1.808e+04 | 6.358e+04 |
| 220.0 | 1.00 | 2189.73 | 6.353e+04 | 1.00 | 1.808e+04 | 6.354e+04 |
| 244.0 | 1.00 | 2165.99 | 6.349e+04 | 1.00 | 1.808e+04 | 6.351e+04 |
| 267.0 | 1.00 | 2146.46 | 6.345e+04 | 1.00 | 1.808e+04 | 6.348e+04 |
| 289.0 | 1.00 | 957.38 | 6.326e+04 | 1.00 | 1.808e+04 | 6.329e+04 |
| 311.0 | 1.00 | 423.03 | 6.313e+04 | 1.00 | 1.808e+04 | 6.404e+04 |
| 333.0 | 1.00 | 275.22 | 6.303e+04 | 1.00 | 1.808e+04 | 6.384e+04 |
| 355.0 | 1.00 | 271.79 | 6.366e+04 | 1.00 | 1.808e+04 | 6.366e+04 |
| 381.0 | 1.00 | 280.67 | 6.284e+04 | 1.00 | 1.808e+04 | 6.349e+04 |
| 408.0 | 1.00 | 550.50 | 6.275e+04 | 1.00 | 1.808e+04 | 6.277e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 16 | 408.00 | 12.00 | 167.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.17 | 0.17 | 0.05 | 0.13 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.16 | 0.17 | 0.05 | 0.13 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.11 | 0.17 | 0.05 | 0.13 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.08 | 0.17 | 0.05 | 0.13 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.05 | 0.17 | 0.05 | 0.13 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.04 | 0.17 | 0.05 | 0.13 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.04 | 0.17 | 0.05 | 0.13 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.05 | 0.17 | 0.05 | 0.13 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.07 | 0.17 | 0.05 | 0.13 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.08 | 0.17 | 0.05 | 0.13 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.08 | 0.17 | 0.05 | 0.12 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.09 | 0.17 | 0.05 | 0.12 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.09 | 0.17 | 0.04 | 0.11 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.07 | 0.17 | 0.03 | 0.04 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.05 | 0.17 | 0.02 | 0.03 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.03 | 0.17 | 0.02 | 0.04 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.03 | 0.17 | 0.02 | 0.04 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.05 | 0.17 | 0.02 | 0.03 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.06 | 0.17 | 0.02 | 0.04 | 0.0 |
| | | | | | | | | | |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.18 | 0.17 | 0.17 | 0.05 | 0.13 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|------------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1.296e+04 | -7613.95 | 2.320e+04 | 2.960e+04 | -8668.34 | -9125.87 | 2506.87 | 1900.67 |
| 23.0 | -1.296e+04 | -3021.79 | 8484.62 | 2.462e+04 | -8668.34 | -9146.60 | 2492.74 | 1875.73 |
| 46.0 | -1.240e+04 | -3047.15 | 1.563e+04 | 1.730e+04 | -8668.34 | -8591.21 | 2491.72 | 1887.03 |
| 69.0 | -1.190e+04 | -3590.93 | 8.528e+04 | 1.110e+04 | -8668.34 | -8056.78 | 2502.43 | 1892.78 |
| 92.0 | -1.144e+04 | -3574.88 | 7.968e+04 | 6375.99 | -8668.34 | -7530.11 | 2504.54 | 1892.23 |
| 112.0 | -1.102e+04 | -5630.40 | 8.845e+04 | 62.24 | -8668.34 | -7038.24 | 2499.18 | 1884.69 |
| 132.0 | -1.065e+04 | -4763.32 | 3.362e+04 | 6440.84 | -8668.34 | -6578.47 | 2487.33 | 1871.55 |
| 152.0 | -1.028e+04 | -4648.30 | 3.664e+04 | 8700.39 | -8668.34 | -6154.29 | 2469.71 | 1853.24 |
| 172.0 | -9931.12 | -4539.18 | 3.916e+04 | 1.052e+04 | -8668.34 | -5704.33 | 2446.87 | 1830.26 |
| 196.0 | -9562.97 | -4869.40 | 2.963e+04 | 1.256e+04 | -8668.34 | -5259.41 | 2415.96 | 1799.83 |
| 220.0 | -9185.57 | -4541.49 | 3.361e+04 | 1.366e+04 | -8668.34 | -4765.95 | 2376.38 | 1761.34 |
| 244.0 | -8896.99 | -4228.23 | 3.639e+04 | 1.395e+04 | -8668.34 | -4335.29 | 2333.94 | 1721.44 |
| 267.0 | -8651.07 | -4072.28 | 7.411e+04 | 1.351e+04 | -8668.34 | -3868.23 | 2256.29 | 1638.58 |
| 289.0 | -7379.63 | -3406.61 | 5.081e+04 | 1.079e+04 | -8668.34 | -3406.61 | 1321.36 | 518.98 |
| 311.0 | -6619.06 | -3021.31 | 3.891e+04 | 7683.40 | -8668.34 | -3021.31 | 1221.02 | 493.76 |
| 333.0 | -5982.53 | -3005.65 | 6.485e+04 | 2965.26 | -8668.34 | -2776.07 | 1190.78 | 538.74 |
| 355.0 | -5447.71 | -2667.00 | 5.485e+04 | 2471.50 | -8668.34 | -2482.06 | 1133.59 | 531.18 |
| 381.0 | -4943.49 | -2191.44 | 3.078e+04 | 6957.87 | -8668.34 | -2202.11 | 986.74 | 437.00 |
| 408.0 | -4643.36 | -3757.73 | 9929.18 | 9672.73 | -8668.34 | -1890.01 | 876.90 | 635.85 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 2506.87 | 5.112e+04 | 1.00 | 1.437e+04 | 5.078e+04 |
| 23.0 | 1.00 | 2492.74 | 5.112e+04 | 1.00 | 1.437e+04 | 5.078e+04 |
| 46.0 | 1.00 | 2491.72 | 5.103e+04 | 1.00 | 1.437e+04 | 5.071e+04 |
| 69.0 | 1.00 | 2502.43 | 5.093e+04 | 1.00 | 1.437e+04 | 5.064e+04 |
| 92.0 | 1.00 | 2504.54 | 5.084e+04 | 1.00 | 1.437e+04 | 5.058e+04 |
| 112.0 | 1.00 | 2499.18 | 5.076e+04 | 1.00 | 1.437e+04 | 5.053e+04 |
| 132.0 | 1.00 | 2487.33 | 5.067e+04 | 1.00 | 1.437e+04 | 5.047e+04 |
| 152.0 | 1.00 | 2469.71 | 5.060e+04 | 1.00 | 1.437e+04 | 5.042e+04 |
| 172.0 | 1.00 | 2446.87 | 5.052e+04 | 1.00 | 1.437e+04 | 5.037e+04 |
| 196.0 | 1.00 | 2415.96 | 5.044e+04 | 1.00 | 1.437e+04 | 5.032e+04 |
| 220.0 | 1.00 | 2376.38 | 5.036e+04 | 1.00 | 1.437e+04 | 5.026e+04 |
| 244.0 | 1.00 | 2333.94 | 5.028e+04 | 1.00 | 1.437e+04 | 5.021e+04 |
| 267.0 | 1.00 | 2256.29 | 5.020e+04 | 1.00 | 1.437e+04 | 5.017e+04 |
| 289.0 | 1.00 | 1321.36 | 5.012e+04 | 1.00 | 1.437e+04 | 5.008e+04 |
| 311.0 | 1.00 | 1221.02 | 5.005e+04 | 1.00 | 1.437e+04 | 5.005e+04 |
| 333.0 | 1.00 | 1190.78 | 5.001e+04 | 1.00 | 1.437e+04 | 5.005e+04 |
| 355.0 | 1.00 | 1133.59 | 4.996e+04 | 1.00 | 1.437e+04 | 5.048e+04 |
| 381.0 | 1.00 | 986.74 | 4.991e+04 | 1.00 | 1.437e+04 | 5.038e+04 |
| 408.0 | 1.00 | 876.90 | 4.986e+04 | 1.00 | 1.437e+04 | 4.985e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 44 | 408.00 | 12.00 | 74.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.26 | 0.11 | 0.08 | 0.06 | 0.19 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.25 | 0.11 | 0.08 | 0.06 | 0.18 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.23 | 0.07 | 0.08 | 0.05 | 0.18 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.21 | 0.06 | 0.08 | 0.05 | 0.18 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.05 | 0.08 | 0.05 | 0.19 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.05 | 0.08 | 0.06 | 0.19 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.04 | 0.08 | 0.06 | 0.19 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.05 | 0.08 | 0.06 | 0.19 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.05 | 0.08 | 0.06 | 0.20 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.06 | 0.08 | 0.06 | 0.20 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.07 | 0.08 | 0.06 | 0.20 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.08 | 0.08 | 0.06 | 0.21 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.10 | 0.08 | 0.07 | 0.21 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.06 | 0.08 | 0.04 | 0.09 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.04 | 0.08 | 0.04 | 0.09 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.04 | 0.08 | 0.04 | 0.12 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.04 | 0.08 | 0.04 | 0.12 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.05 | 0.08 | 0.04 | 0.10 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.14 | 0.08 | 0.02 | 0.05 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.26 | 0.14 | 0.08 | 0.07 | 0.21 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -8084.18 | -3939.94 | 4.094e+04 | 4759.92 | -4304.98 | -8084.18 | 1057.43 | 946.07 |
| 23.0 | -7926.34 | 979.15 | 4094.75 | 4812.51 | -4304.98 | -7926.34 | 993.04 | 881.67 |
| 46.0 | -7310.93 | -3567.79 | 2.719e+04 | 1290.66 | -4304.98 | -7310.93 | 958.42 | 882.21 |
| 69.0 | -6690.39 | -2704.79 | 2.300e+04 | 783.15 | -4304.98 | -6690.39 | 956.28 | 892.51 |
| 92.0 | -6080.93 | -2483.46 | 2.060e+04 | 500.46 | -4304.98 | -6080.93 | 966.19 | 906.75 |
| 112.0 | -5576.85 | -128.92 | 1.457e+04 | 1027.17 | -4304.98 | -5527.01 | 976.75 | 919.00 |
| 132.0 | -5060.98 | -306.53 | 1.285e+04 | 1203.57 | -4304.98 | -5057.97 | 987.58 | 931.22 |
| 152.0 | -4563.17 | -4274.27 | 1.938e+04 | 979.44 | -4304.98 | -4556.50 | 998.72 | 943.52 |
| 172.0 | -4202.92 | -4105.96 | 2.259e+04 | 1086.50 | -4304.98 | -3998.93 | 1011.40 | 956.21 |
| 196.0 | -3923.08 | -3914.68 | 2.584e+04 | 1149.77 | -4304.98 | -3460.90 | 1030.41 | 971.75 |
| 220.0 | -3718.34 | -1869.22 | 2.415e+04 | 1705.35 | -4304.98 | -2854.41 | 1056.56 | 987.65 |
| 244.0 | -3546.16 | -2201.20 | 2.967e+04 | 486.84 | -4304.98 | -2319.11 | 1092.31 | 1004.42 |
| 267.0 | -3415.69 | -2252.32 | 3.605e+04 | 894.68 | -4304.98 | -1714.61 | 1143.66 | 1029.88 |
| 289.0 | -2783.46 | -1715.54 | 2.104e+04 | 1007.61 | -4304.98 | -1243.40 | 648.79 | 459.18 |
| 311.0 | -2414.89 | -1461.16 | 1.499e+04 | 972.07 | -4304.98 | -1191.06 | 666.40 | 458.47 |
| 333.0 | -2167.11 | -609.76 | 6473.16 | 2066.22 | -4304.98 | -1188.42 | 713.53 | 574.88 |
| 355.0 | -2028.63 | -589.49 | 4004.34 | 1976.21 | -4304.98 | -1077.02 | 719.03 | 601.79 |
| 381.0 | -2007.21 | -1856.78 | 4351.82 | 2760.70 | -4304.98 | -1013.63 | 629.48 | 507.34 |
| 408.0 | -2078.98 | -1948.12 | 1.104e+04 | 8034.83 | -4304.98 | -792.53 | 340.14 | 262.79 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 1057.43 | 1.793e+04 | 1.00 | 4887.80 | 1.762e+04 |
| 23.0 | 1.00 | 993.04 | 1.791e+04 | 1.00 | 4887.80 | 1.760e+04 |
| 46.0 | 1.00 | 958.42 | 1.782e+04 | 1.00 | 4887.80 | 1.754e+04 |
| 69.0 | 1.00 | 956.28 | 1.774e+04 | 1.00 | 4887.80 | 1.748e+04 |
| 92.0 | 1.00 | 966.19 | 1.766e+04 | 1.00 | 4887.80 | 1.742e+04 |
| 112.0 | 1.00 | 976.75 | 1.759e+04 | 1.00 | 4887.80 | 1.737e+04 |
| 132.0 | 1.00 | 987.58 | 1.752e+04 | 1.00 | 4887.80 | 1.734e+04 |
| 152.0 | 1.00 | 998.72 | 1.746e+04 | 1.00 | 4887.80 | 1.729e+04 |
| 172.0 | 1.00 | 1011.40 | 1.738e+04 | 1.00 | 4887.80 | 1.721e+04 |
| 196.0 | 1.00 | 1030.41 | 1.731e+04 | 1.00 | 4887.80 | 1.716e+04 |
| 220.0 | 1.00 | 1056.56 | 1.723e+04 | 1.00 | 4887.80 | 1.709e+04 |
| 244.0 | 1.00 | 1092.31 | 1.716e+04 | 1.00 | 4887.80 | 1.703e+04 |
| 267.0 | 1.00 | 1143.66 | 1.708e+04 | 1.00 | 4887.80 | 1.698e+04 |
| 289.0 | 1.00 | 648.79 | 1.701e+04 | 1.00 | 4887.80 | 1.706e+04 |
| 311.0 | 1.00 | 666.40 | 1.701e+04 | 1.00 | 4887.80 | 1.717e+04 |
| 333.0 | 1.00 | 713.53 | 1.701e+04 | 1.00 | 4887.80 | 1.714e+04 |
| 355.0 | 1.00 | 719.03 | 1.699e+04 | 1.00 | 4887.80 | 1.712e+04 |
| 381.0 | 1.00 | 629.48 | 1.698e+04 | 1.00 | 4887.80 | 1.712e+04 |
| 408.0 | 1.00 | 340.14 | 1.695e+04 | 1.00 | 4887.80 | 1.694e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 45 | 408.00 | 12.00 | 223.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.47 | 0.22 | 0.04 | 0.15 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.47 | 0.22 | 0.04 | 0.15 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.36 | 0.22 | 0.04 | 0.15 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.26 | 0.22 | 0.04 | 0.14 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.16 | 0.22 | 0.04 | 0.14 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.08 | 0.22 | 0.04 | 0.14 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.06 | 0.22 | 0.04 | 0.14 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.10 | 0.22 | 0.04 | 0.14 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.17 | 0.22 | 0.04 | 0.14 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.23 | 0.22 | 0.04 | 0.14 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.28 | 0.22 | 0.04 | 0.14 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.32 | 0.22 | 0.04 | 0.13 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.34 | 0.22 | 0.04 | 0.13 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.31 | 0.22 | 0.02 | 0.06 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.27 | 0.22 | 9.23e-03 | 0.03 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.22 | 0.22 | 6.03e-03 | 0.01 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.16 | 0.22 | 4.48e-03 | 7.84e-03 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.09 | 0.22 | 4.93e-03 | 0.01 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.04 | 0.22 | 0.01 | 0.03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.17 | 0.47 | 0.22 | 0.04 | 0.15 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|------------|----------|-----------|-----------|------------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1.585e+04 | -8019.85 | 1.477e+05 | 1.078e+05 | -1.107e+04 | -8565.50 | 2946.53 | 2854.28 |
| 23.0 | -1.585e+04 | -8019.58 | 1.437e+05 | 1.069e+05 | -1.107e+04 | -8564.53 | 2946.93 | 2853.96 |
| 46.0 | -1.558e+04 | -7829.08 | 1.218e+05 | 8.287e+04 | -1.107e+04 | -8397.73 | 2956.10 | 2858.93 |
| 69.0 | -1.531e+04 | -7582.69 | 1.021e+05 | 5.897e+04 | -1.107e+04 | -8141.59 | 3047.62 | 2832.18 |
| 92.0 | -1.504e+04 | -7424.65 | 8.242e+04 | 3.619e+04 | -1.107e+04 | -7943.21 | 3035.06 | 2826.38 |
| 112.0 | -1.479e+04 | -7292.36 | 8.128e+04 | 1.827e+04 | -1.107e+04 | -7759.29 | 3022.09 | 2780.39 |
| 132.0 | -1.456e+04 | -7203.47 | 1.278e+04 | 1.348e+04 | -1.107e+04 | -7556.82 | 3008.14 | 2724.25 |
| 152.0 | -1.433e+04 | -6915.07 | 2509.49 | 2.334e+04 | -1.107e+04 | -7386.84 | 2991.86 | 2709.09 |
| 172.0 | -1.409e+04 | -6743.55 | 1667.17 | 3.727e+04 | -1.107e+04 | -7202.76 | 2973.17 | 2691.43 |
| 196.0 | -1.384e+04 | -6535.32 | 8545.14 | 5.069e+04 | -1.107e+04 | -7013.58 | 2949.94 | 2676.95 |
| 220.0 | -1.355e+04 | -6294.07 | 1.620e+04 | 6.257e+04 | -1.107e+04 | -6815.73 | 2921.22 | 2650.96 |
| 244.0 | -1.327e+04 | -6169.17 | 1.144e+04 | 7.096e+04 | -1.107e+04 | -6586.30 | 2889.62 | 2611.63 |
| 267.0 | -1.300e+04 | -5964.83 | 1.440e+04 | 7.573e+04 | -1.107e+04 | -6381.18 | 2857.72 | 2603.82 |
| 289.0 | -1.109e+04 | -4973.09 | 1.387e+04 | 6.778e+04 | -1.107e+04 | -5346.38 | 1349.20 | 1228.62 |
| 311.0 | -9924.96 | -4248.08 | 1.857e+04 | 5.678e+04 | -1.107e+04 | -4690.68 | 630.22 | 538.65 |
| 333.0 | -8878.69 | -3702.90 | 1.548e+04 | 4.547e+04 | -1.107e+04 | -4094.93 | 411.61 | 240.93 |
| 355.0 | -7937.00 | -3216.45 | 2.471e+04 | 3.348e+04 | -1.107e+04 | -3533.64 | 305.00 | 153.44 |
| 381.0 | -6995.78 | -2690.37 | 1.526e+04 | 1.852e+04 | -1.107e+04 | -2989.09 | 335.57 | 273.31 |
| 408.0 | -6283.37 | -2256.92 | 8185.79 | 7436.66 | -1.107e+04 | -2548.63 | 739.67 | 660.20 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 2946.53 | 6.900e+04 | 1.00 | 1.958e+04 | 6.907e+04 |
| 23.0 | 1.00 | 2946.93 | 6.900e+04 | 1.00 | 1.958e+04 | 6.907e+04 |
| 46.0 | 1.00 | 2956.10 | 6.897e+04 | 1.00 | 1.958e+04 | 6.903e+04 |
| 69.0 | 1.00 | 3047.62 | 6.893e+04 | 1.00 | 1.958e+04 | 6.900e+04 |
| 92.0 | 1.00 | 3035.06 | 6.889e+04 | 1.00 | 1.958e+04 | 6.896e+04 |
| 112.0 | 1.00 | 3022.09 | 6.886e+04 | 1.00 | 1.958e+04 | 6.892e+04 |
| 132.0 | 1.00 | 3008.14 | 6.882e+04 | 1.00 | 1.958e+04 | 6.889e+04 |
| 152.0 | 1.00 | 2991.86 | 6.879e+04 | 1.00 | 1.958e+04 | 6.885e+04 |
| 172.0 | 1.00 | 2973.17 | 6.876e+04 | 1.00 | 1.958e+04 | 6.882e+04 |
| 196.0 | 1.00 | 2949.94 | 6.872e+04 | 1.00 | 1.958e+04 | 6.879e+04 |
| 220.0 | 1.00 | 2921.22 | 6.869e+04 | 1.00 | 1.958e+04 | 6.875e+04 |
| 244.0 | 1.00 | 2889.62 | 6.865e+04 | 1.00 | 1.958e+04 | 6.870e+04 |
| 267.0 | 1.00 | 2857.72 | 6.861e+04 | 1.00 | 1.958e+04 | 6.867e+04 |
| 289.0 | 1.00 | 1349.20 | 6.843e+04 | 1.00 | 1.958e+04 | 6.848e+04 |
| 311.0 | 1.00 | 630.22 | 6.831e+04 | 1.00 | 1.958e+04 | 6.836e+04 |
| 333.0 | 1.00 | 411.61 | 6.820e+04 | 1.00 | 1.958e+04 | 6.826e+04 |
| 355.0 | 1.00 | 305.00 | 6.810e+04 | 1.00 | 1.958e+04 | 6.816e+04 |
| 381.0 | 1.00 | 335.57 | 6.801e+04 | 1.00 | 1.958e+04 | 6.805e+04 |
| 408.0 | 1.00 | 739.67 | 6.793e+04 | 1.00 | 1.958e+04 | 6.797e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 49 | 408.00 | 12.00 | 223.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.48 | 0.22 | 0.05 | 0.07 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.48 | 0.22 | 0.05 | 0.07 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.37 | 0.22 | 0.05 | 0.07 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.26 | 0.22 | 0.05 | 0.07 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.16 | 0.22 | 0.05 | 0.07 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.07 | 0.22 | 0.05 | 0.07 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.06 | 0.22 | 0.05 | 0.07 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.12 | 0.22 | 0.05 | 0.07 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.18 | 0.22 | 0.05 | 0.07 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.24 | 0.22 | 0.05 | 0.07 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.29 | 0.22 | 0.05 | 0.06 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.33 | 0.22 | 0.05 | 0.06 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.35 | 0.22 | 0.05 | 0.06 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.31 | 0.22 | 0.02 | 0.03 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.26 | 0.22 | 0.01 | 0.01 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.21 | 0.22 | 8.05e-03 | 8.40e-03 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.15 | 0.22 | 6.08e-03 | 7.85e-03 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.08 | 0.22 | 6.55e-03 | 7.99e-03 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.04 | 0.22 | 0.01 | 0.01 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.17 | 0.48 | 0.22 | 0.05 | 0.07 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|------------|----------|-----------|-----------|------------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1.589e+04 | -8493.19 | 2.141e+05 | 1.110e+05 | -1.111e+04 | -8645.14 | 3316.37 | 1357.63 |
| 23.0 | -1.589e+04 | -8493.56 | 2.084e+05 | 1.101e+05 | -1.111e+04 | -8646.18 | 3316.29 | 1357.30 |
| 46.0 | -1.562e+04 | -8282.09 | 1.762e+05 | 8.463e+04 | -1.111e+04 | -8441.11 | 3303.69 | 1328.60 |
| 69.0 | -1.535e+04 | -8096.81 | 1.443e+05 | 5.939e+04 | -1.111e+04 | -8241.17 | 3294.06 | 1317.09 |
| 92.0 | -1.509e+04 | -7926.06 | 1.132e+05 | 3.555e+04 | -1.111e+04 | -8025.43 | 3283.21 | 1310.57 |
| 112.0 | -1.483e+04 | -7713.02 | 8.610e+04 | 1.661e+04 | -1.111e+04 | -7839.89 | 3270.67 | 1305.24 |
| 132.0 | -1.460e+04 | -7393.59 | 264.70 | 1.343e+04 | -1.111e+04 | -7656.47 | 3256.75 | 1299.99 |
| 152.0 | -1.437e+04 | -7685.49 | 2277.87 | 2.745e+04 | -1.111e+04 | -7478.52 | 3240.38 | 1294.04 |
| 172.0 | -1.413e+04 | -7075.35 | 2.148e+04 | 4.132e+04 | -1.111e+04 | -7275.38 | 3221.50 | 1287.29 |
| 196.0 | -1.388e+04 | -6888.75 | 3.907e+04 | 5.373e+04 | -1.111e+04 | -7098.94 | 3198.02 | 1278.94 |
| 220.0 | -1.360e+04 | -6643.73 | 7.052e+04 | 6.572e+04 | -1.111e+04 | -6864.61 | 3168.93 | 1268.63 |
| 244.0 | -1.332e+04 | -6415.53 | 1.020e+05 | 7.297e+04 | -1.111e+04 | -6633.52 | 3136.69 | 1257.25 |
| 267.0 | -1.304e+04 | -6202.99 | 1.325e+05 | 7.651e+04 | -1.111e+04 | -6423.24 | 3103.14 | 1245.86 |
| 289.0 | -1.115e+04 | -5188.76 | 1.000e+05 | 6.768e+04 | -1.111e+04 | -5397.49 | 1482.04 | 635.39 |
| 311.0 | -9984.26 | -4534.97 | 8.338e+04 | 5.624e+04 | -1.111e+04 | -4742.37 | 746.61 | 252.32 |
| 333.0 | -8937.57 | -3941.13 | 6.650e+04 | 4.411e+04 | -1.111e+04 | -4150.17 | 549.12 | 164.50 |
| 355.0 | -7995.51 | -3401.38 | 5.089e+04 | 3.114e+04 | -1.111e+04 | -3611.52 | 414.35 | 153.63 |
| 381.0 | -7054.01 | -2859.02 | 3.627e+04 | 1.670e+04 | -1.111e+04 | -3069.22 | 445.76 | 156.48 |
| 408.0 | -6332.47 | -2568.40 | 730.90 | 8424.18 | -1.111e+04 | -2620.35 | 837.28 | 265.62 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 3316.37 | 6.902e+04 | 1.00 | 1.958e+04 | 6.906e+04 |
| 23.0 | 1.00 | 3316.29 | 6.902e+04 | 1.00 | 1.958e+04 | 6.906e+04 |
| 46.0 | 1.00 | 3303.69 | 6.898e+04 | 1.00 | 1.958e+04 | 6.902e+04 |
| 69.0 | 1.00 | 3294.06 | 6.894e+04 | 1.00 | 1.958e+04 | 6.898e+04 |
| 92.0 | 1.00 | 3283.21 | 6.890e+04 | 1.00 | 1.958e+04 | 6.895e+04 |
| 112.0 | 1.00 | 3270.67 | 6.887e+04 | 1.00 | 1.958e+04 | 6.891e+04 |
| 132.0 | 1.00 | 3256.75 | 6.884e+04 | 1.00 | 1.958e+04 | 6.888e+04 |
| 152.0 | 1.00 | 3240.38 | 6.881e+04 | 1.00 | 1.958e+04 | 6.884e+04 |
| 172.0 | 1.00 | 3221.50 | 6.877e+04 | 1.00 | 1.958e+04 | 6.882e+04 |
| 196.0 | 1.00 | 3198.02 | 6.874e+04 | 1.00 | 1.958e+04 | 6.879e+04 |
| 220.0 | 1.00 | 3168.93 | 6.870e+04 | 1.00 | 1.958e+04 | 6.876e+04 |
| 244.0 | 1.00 | 3136.69 | 6.866e+04 | 1.00 | 1.958e+04 | 6.872e+04 |
| 267.0 | 1.00 | 3103.14 | 6.862e+04 | 1.00 | 1.958e+04 | 6.868e+04 |
| 289.0 | 1.00 | 1482.04 | 6.844e+04 | 1.00 | 1.958e+04 | 6.850e+04 |
| 311.0 | 1.00 | 746.61 | 6.832e+04 | 1.00 | 1.958e+04 | 6.838e+04 |
| 333.0 | 1.00 | 549.12 | 6.821e+04 | 1.00 | 1.958e+04 | 6.878e+04 |
| 355.0 | 1.00 | 414.35 | 6.812e+04 | 1.00 | 1.958e+04 | 6.889e+04 |
| 381.0 | 1.00 | 445.76 | 6.802e+04 | 1.00 | 1.958e+04 | 6.849e+04 |
| 408.0 | 1.00 | 837.28 | 6.794e+04 | 1.00 | 1.958e+04 | 6.800e+04 |

Macrosetti n. 6, 7, 8, 10, 11, 12 [fasce di piano]

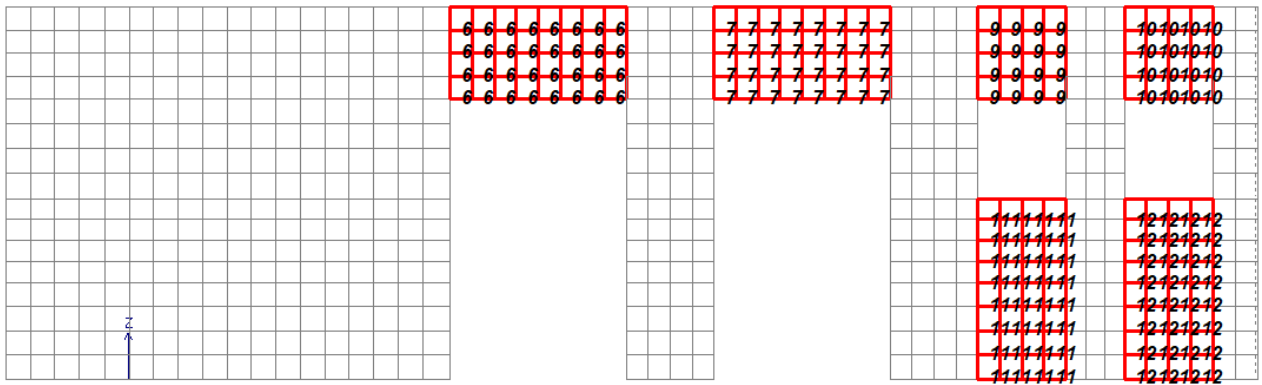


Fig 64. Elemento/i oggetto di verifica (Selezione in rosso).

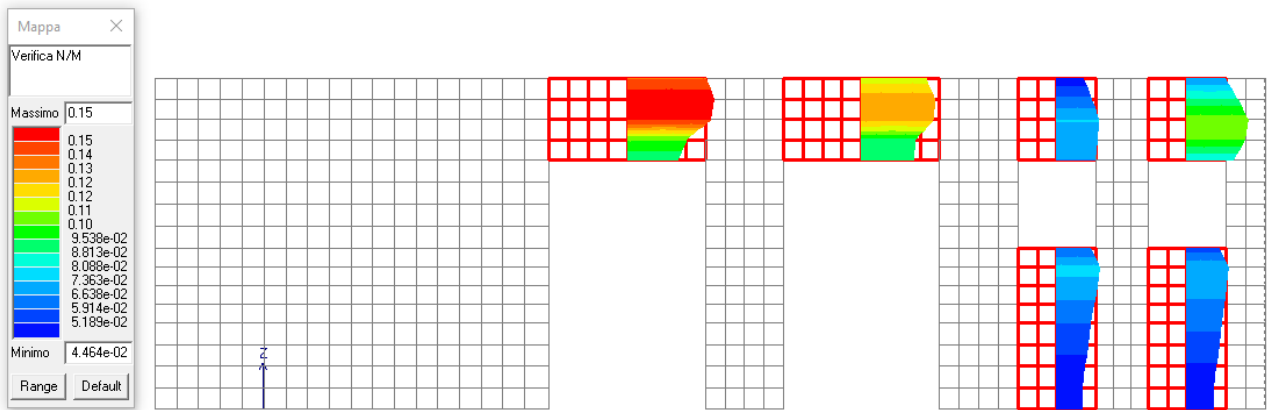


Fig 65. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

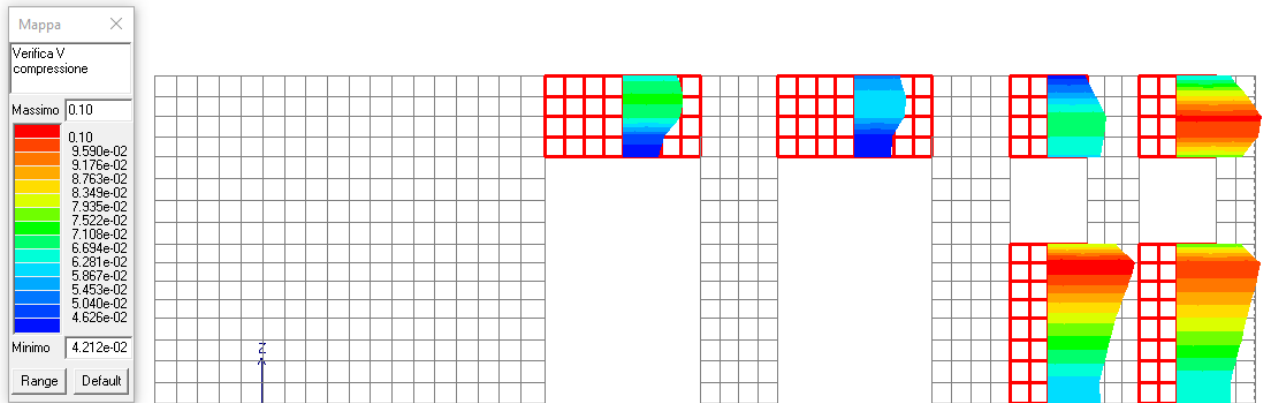


Fig 66. SLU: Mappa di Verifica V compressione – Verifica soddisfatta ($\rho \leq 1$).

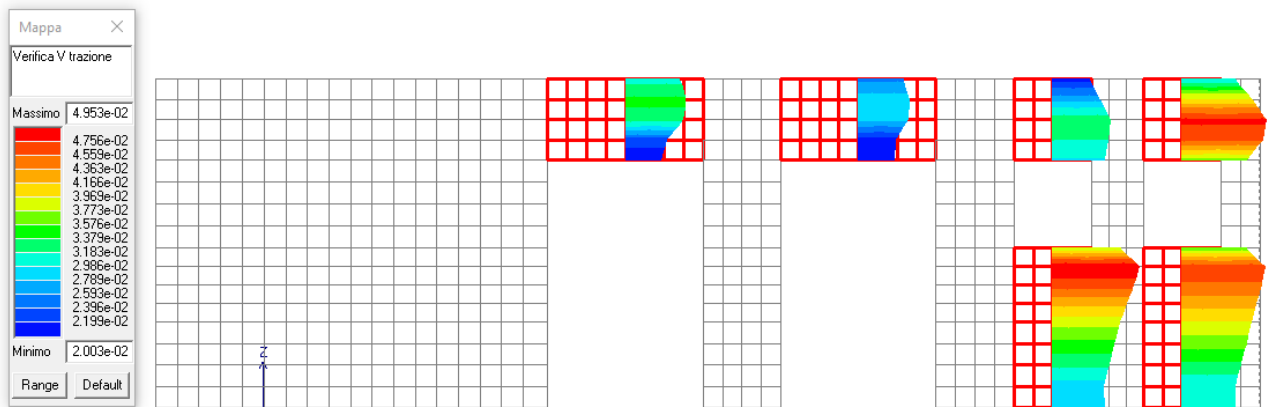


Fig 67. SLU: Mappa di verifica V trazione – Verifiche soddisfatte ($\rho \leq 1$).

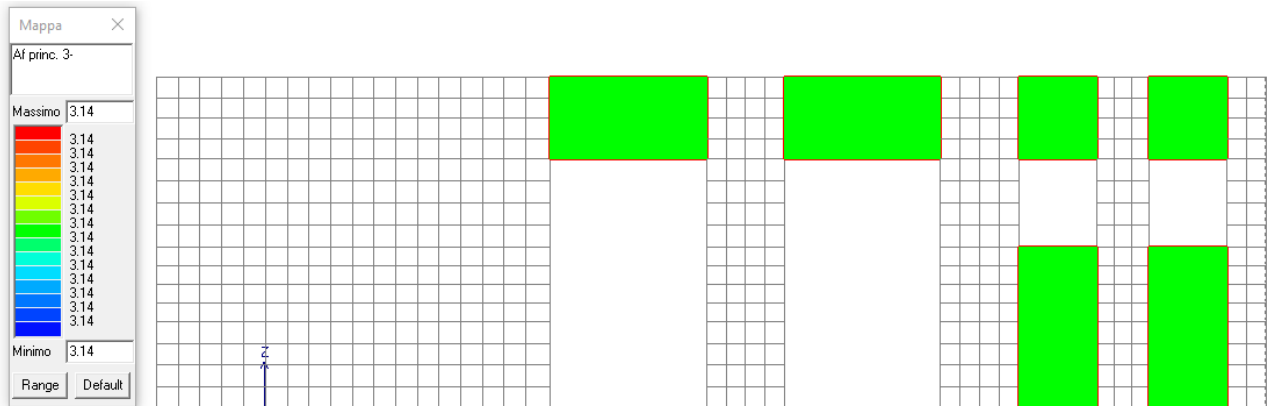


Fig 68. Mappa Armatura Verticale (singolo strato) da Calcolo [cm^2/m].

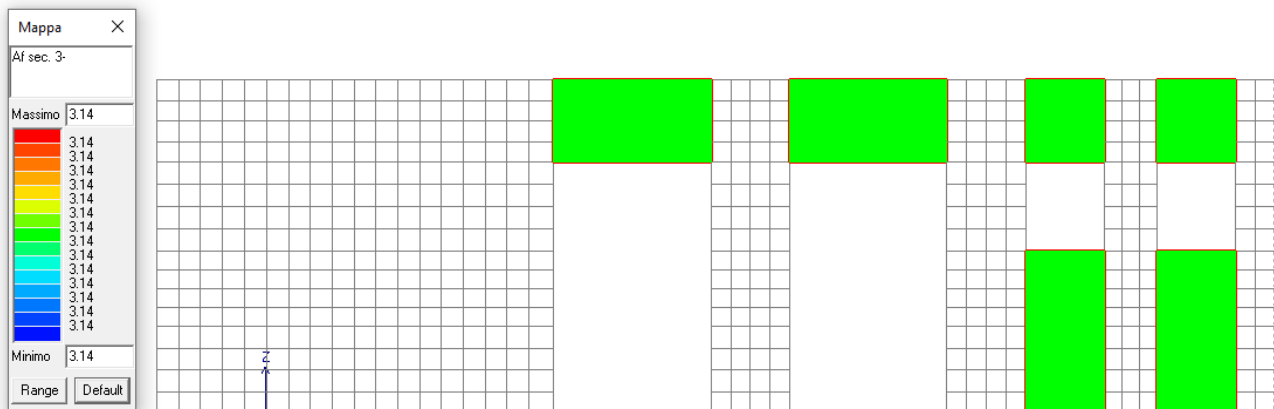


Fig 69. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm^2/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 6 | 88.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.04 | 0.02 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.05 | 0.02 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.15 | 0.0 | 0.07 | 0.03 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.15 | 0.0 | 0.07 | 0.03 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.14 | 0.0 | 0.07 | 0.03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.15 | 0.0 | 0.07 | 0.03 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 8.516e+04 | 0.0 | 0.0 | 0.0 | 946.26 | 946.26 |
| 289.0 | 0.0 | 0.0 | 9.869e+04 | 0.0 | 0.0 | 0.0 | 1096.57 | 1096.57 |
| 311.0 | 0.0 | 0.0 | 1.403e+05 | 0.0 | 0.0 | 0.0 | 1558.76 | 1558.76 |
| 333.0 | 0.0 | 0.0 | 1.461e+05 | 0.0 | 0.0 | 0.0 | 1623.67 | 1623.67 |
| 355.0 | 0.0 | 0.0 | 1.320e+05 | 0.0 | 0.0 | 0.0 | 1466.53 | 1466.53 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 946.26 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 289.0 | 2.50 | 1096.57 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 311.0 | 2.50 | 1558.76 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 333.0 | 2.50 | 1623.67 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 355.0 | 2.50 | 1466.53 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 7 | 88.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.04 | 0.02 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.04 | 0.02 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.06 | 0.03 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.06 | 0.03 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.05 | 0.03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.13 | 0.0 | 0.06 | 0.03 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 8.720e+04 | 0.0 | 0.0 | 0.0 | 968.86 | 968.86 |
| 289.0 | 0.0 | 0.0 | 8.973e+04 | 0.0 | 0.0 | 0.0 | 996.97 | 996.97 |
| 311.0 | 0.0 | 0.0 | 1.215e+05 | 0.0 | 0.0 | 0.0 | 1350.20 | 1350.20 |
| 333.0 | 0.0 | 0.0 | 1.228e+05 | 0.0 | 0.0 | 0.0 | 1364.83 | 1364.83 |
| 355.0 | 0.0 | 0.0 | 1.088e+05 | 0.0 | 0.0 | 0.0 | 1208.54 | 1208.54 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 968.86 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 289.0 | 2.50 | 996.97 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 311.0 | 2.50 | 1350.20 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 333.0 | 2.50 | 1364.83 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 355.0 | 2.50 | 1208.54 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 9 | 88.00 | 12.00 | 90.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.06 | 0.03 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.07 | 0.03 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.07 | 0.03 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.06 | 0.03 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.07 | 0.0 | 0.07 | 0.03 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 6.305e+04 | 0.0 | 0.0 | 0.0 | 1401.03 | 1401.03 |
| 289.0 | 0.0 | 0.0 | 6.785e+04 | 0.0 | 0.0 | 0.0 | 1507.76 | 1507.76 |
| 311.0 | 0.0 | 0.0 | 7.060e+04 | 0.0 | 0.0 | 0.0 | 1568.86 | 1568.86 |
| 333.0 | 0.0 | 0.0 | 5.797e+04 | 0.0 | 0.0 | 0.0 | 1288.14 | 1288.14 |
| 355.0 | 0.0 | 0.0 | 4.497e+04 | 0.0 | 0.0 | 0.0 | 999.27 | 999.27 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 1401.03 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 289.0 | 2.50 | 1507.76 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 311.0 | 2.50 | 1568.86 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 333.0 | 2.50 | 1288.14 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 355.0 | 2.50 | 999.27 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 10 | 88.00 | 12.00 | 90.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.08 | 0.04 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.10 | 0.05 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.10 | 0.05 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.08 | 0.04 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.06 | 0.03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.11 | 0.0 | 0.10 | 0.05 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 7.816e+04 | 0.0 | 0.0 | 0.0 | 1736.98 | 1736.98 |
| 289.0 | 0.0 | 0.0 | 9.773e+04 | 0.0 | 0.0 | 0.0 | 2171.78 | 2171.78 |
| 311.0 | 0.0 | 0.0 | 1.023e+05 | 0.0 | 0.0 | 0.0 | 2272.45 | 2272.45 |
| 333.0 | 0.0 | 0.0 | 8.530e+04 | 0.0 | 0.0 | 0.0 | 1895.58 | 1895.58 |
| 355.0 | 0.0 | 0.0 | 6.397e+04 | 0.0 | 0.0 | 0.0 | 1421.55 | 1421.55 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 1736.98 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 289.0 | 2.50 | 2171.78 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 311.0 | 2.50 | 2272.45 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 333.0 | 2.50 | 1895.58 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |
| 355.0 | 2.50 | 1421.55 | 2.246e+04 | 2.50 | 4.725e+04 | 2.246e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 11 | 172.00 | 12.00 | 90.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.06 | 0.03 | 0.0 |
| 23.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.06 | 0.03 | 0.0 |
| 46.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.07 | 0.03 | 0.0 |
| 69.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.07 | 0.04 | 0.0 |
| 92.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.08 | 0.04 | 0.0 |
| 112.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.09 | 0.04 | 0.0 |
| 132.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.10 | 0.05 | 0.0 |
| 152.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.10 | 0.05 | 0.0 |
| 172.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.08 | 0.04 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.08 | 0.0 | 0.10 | 0.05 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | 0.0 | 0.0 | 1.247e+05 | 0.0 | 0.0 | 0.0 | 2771.46 | 2771.46 |
| 23.0 | 0.0 | 0.0 | 1.224e+05 | 0.0 | 0.0 | 0.0 | 2720.26 | 2720.26 |
| 46.0 | 0.0 | 0.0 | 1.362e+05 | 0.0 | 0.0 | 0.0 | 3026.54 | 3026.54 |
| 69.0 | 0.0 | 0.0 | 1.486e+05 | 0.0 | 0.0 | 0.0 | 3301.80 | 3301.80 |
| 92.0 | 0.0 | 0.0 | 1.626e+05 | 0.0 | 0.0 | 0.0 | 3614.30 | 3614.30 |
| 112.0 | 0.0 | 0.0 | 1.785e+05 | 0.0 | 0.0 | 0.0 | 3966.66 | 3966.66 |
| 132.0 | 0.0 | 0.0 | 1.958e+05 | 0.0 | 0.0 | 0.0 | 4350.24 | 4350.24 |
| 152.0 | 0.0 | 0.0 | 2.088e+05 | 0.0 | 0.0 | 0.0 | 4639.29 | 4639.29 |
| 172.0 | 0.0 | 0.0 | 1.640e+05 | 0.0 | 0.0 | 0.0 | 3645.43 | 3645.43 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 2.50 | 2771.46 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 23.0 | 2.50 | 2720.26 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 46.0 | 2.50 | 3026.54 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 69.0 | 2.50 | 3301.80 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 92.0 | 2.50 | 3614.30 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 112.0 | 2.50 | 3966.66 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 132.0 | 2.50 | 4350.24 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 152.0 | 2.50 | 4639.29 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 172.0 | 2.50 | 3645.43 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 12 | 172.00 | 12.00 | 90.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.06 | 0.03 | 0.0 |
| 23.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.06 | 0.03 | 0.0 |
| 46.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.07 | 0.03 | 0.0 |
| 69.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.08 | 0.04 | 0.0 |
| 92.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.08 | 0.04 | 0.0 |
| 112.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.09 | 0.04 | 0.0 |
| 132.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.10 | 0.05 | 0.0 |
| 152.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.10 | 0.05 | 0.0 |
| 172.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.08 | 0.04 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.07 | 0.0 | 0.10 | 0.05 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | 0.0 | 0.0 | 1.282e+05 | 0.0 | 0.0 | 0.0 | 2848.31 | 2848.31 |
| 23.0 | 0.0 | 0.0 | 1.269e+05 | 0.0 | 0.0 | 0.0 | 2819.39 | 2819.39 |
| 46.0 | 0.0 | 0.0 | 1.405e+05 | 0.0 | 0.0 | 0.0 | 3122.82 | 3122.82 |
| 69.0 | 0.0 | 0.0 | 1.545e+05 | 0.0 | 0.0 | 0.0 | 3433.85 | 3433.85 |
| 92.0 | 0.0 | 0.0 | 1.673e+05 | 0.0 | 0.0 | 0.0 | 3717.17 | 3717.17 |
| 112.0 | 0.0 | 0.0 | 1.791e+05 | 0.0 | 0.0 | 0.0 | 3980.88 | 3980.88 |
| 132.0 | 0.0 | 0.0 | 1.910e+05 | 0.0 | 0.0 | 0.0 | 4244.11 | 4244.11 |
| 152.0 | 0.0 | 0.0 | 1.996e+05 | 0.0 | 0.0 | 0.0 | 4436.41 | 4436.41 |
| 172.0 | 0.0 | 0.0 | 1.560e+05 | 0.0 | 0.0 | 0.0 | 3467.02 | 3467.02 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 2.50 | 2848.31 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 23.0 | 2.50 | 2819.39 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 46.0 | 2.50 | 3122.82 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 69.0 | 2.50 | 3433.85 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 92.0 | 2.50 | 3717.17 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 112.0 | 2.50 | 3980.88 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 132.0 | 2.50 | 4244.11 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 152.0 | 2.50 | 4436.41 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |
| 172.0 | 2.50 | 3467.02 | 4.453e+04 | 2.50 | 9.367e+04 | 4.453e+04 |

Macrosetti n. 86, 87, 101, 103, 105 [fasce di piano]

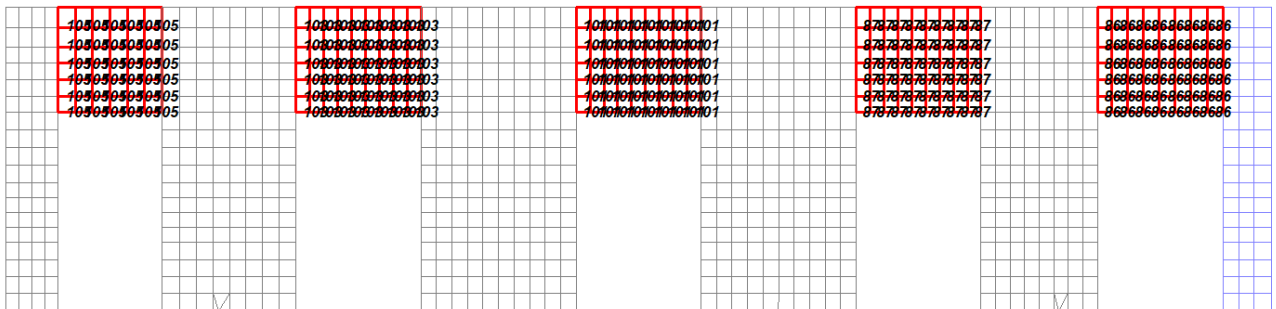


Fig 70. Elemento/i oggetto di verifica (Selezione in rosso).

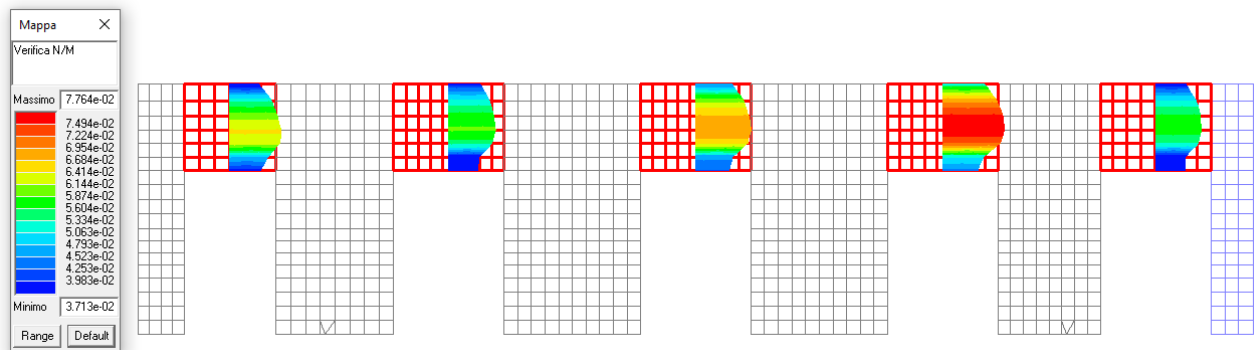


Fig 71. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

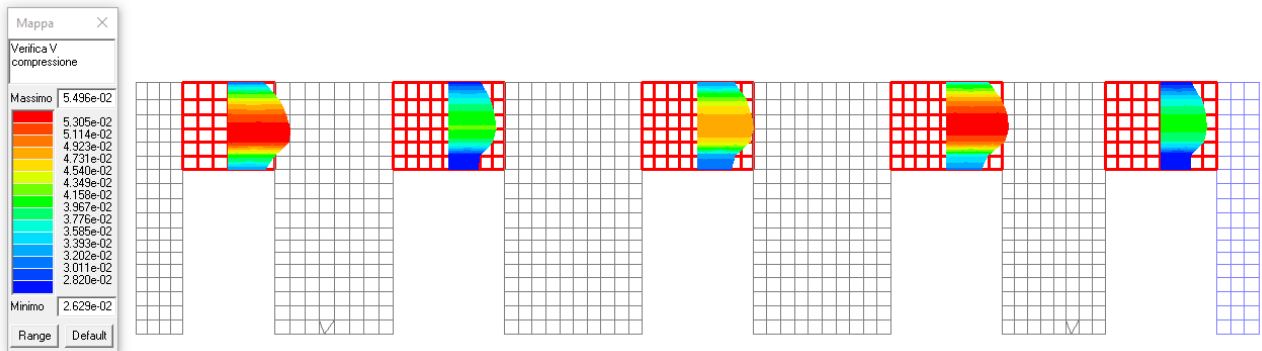


Fig 72. SLU: Mappa di Verifica V compressione – Verifica soddisfatta ($\rho \leq 1$).

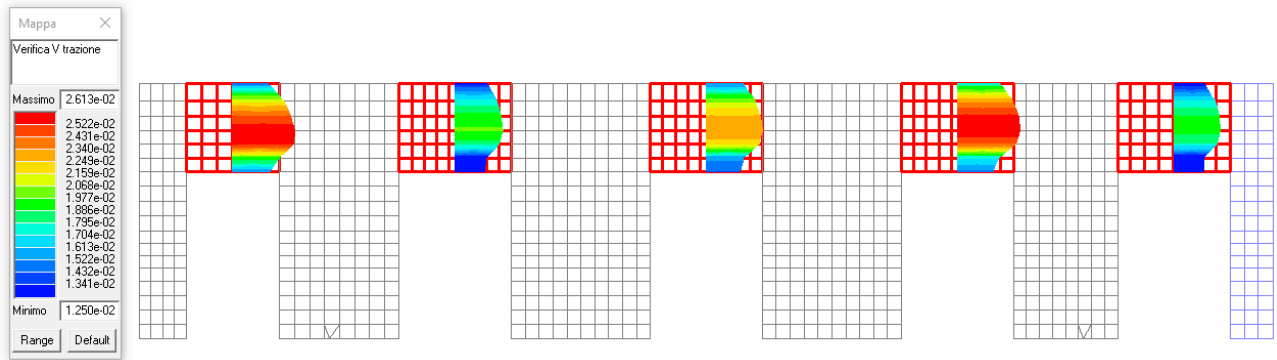


Fig 73. SLU: Mappa di verifica V trazione – Verifiche soddisfatte ($p \leq 1$).

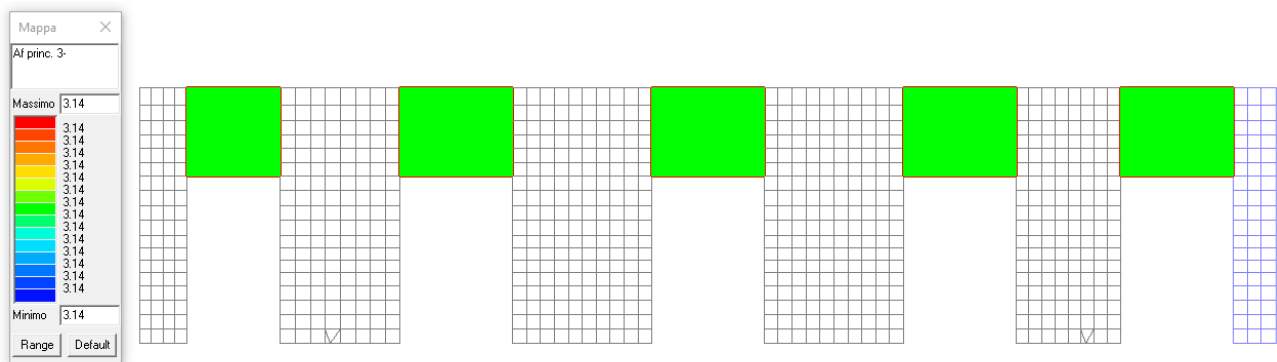


Fig 74. Mappa Armatura Verticale (singolo strato) da Calcolo [cm^2/m].

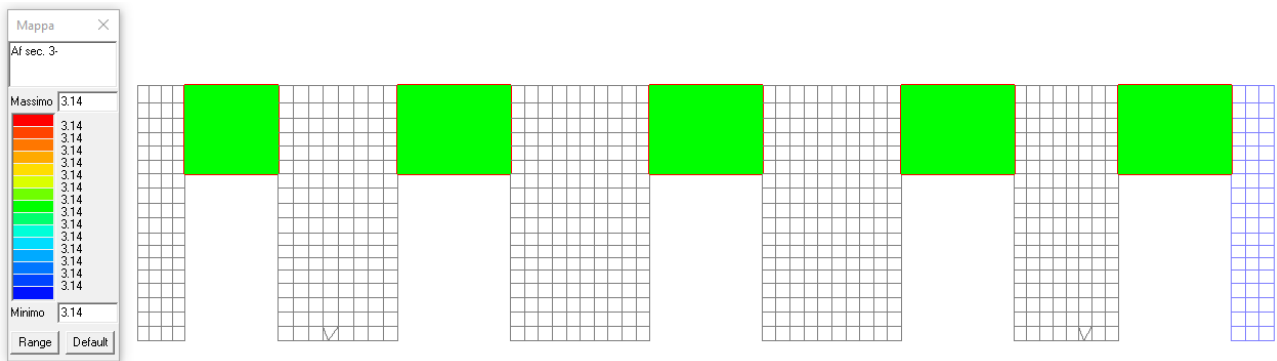


Fig 75. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm^2/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| 86 | 141.00 | 12.00 | 181.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|-----------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.04 | 0.02 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.04 | 0.02 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.06 | 0.0 | 0.04 | 0.02 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 8.678e+04 | 0.0 | 0.0 | 0.0 | 958.89 | 958.89 |
| 289.0 | 0.0 | 0.0 | 8.686e+04 | 0.0 | 0.0 | 0.0 | 959.73 | 959.73 |
| 311.0 | 0.0 | 0.0 | 1.239e+05 | 0.0 | 0.0 | 0.0 | 1369.41 | 1369.41 |
| 333.0 | 0.0 | 0.0 | 1.342e+05 | 0.0 | 0.0 | 0.0 | 1482.45 | 1482.45 |
| 355.0 | 0.0 | 0.0 | 1.319e+05 | 0.0 | 0.0 | 0.0 | 1457.44 | 1457.44 |
| 381.0 | 0.0 | 0.0 | 1.192e+05 | 0.0 | 0.0 | 0.0 | 1317.47 | 1317.47 |
| 408.0 | 0.0 | 0.0 | 8.859e+04 | 0.0 | 0.0 | 0.0 | 978.86 | 978.86 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 958.89 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 289.0 | 2.50 | 959.73 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 311.0 | 2.50 | 1369.41 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 333.0 | 2.50 | 1482.45 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 355.0 | 2.50 | 1457.44 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 381.0 | 2.50 | 1317.47 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 408.0 | 2.50 | 978.86 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 87 | 141.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.05 | 0.02 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.05 | 0.03 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.05 | 0.03 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.05 | 0.02 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.08 | 0.0 | 0.05 | 0.03 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 1.032e+05 | 0.0 | 0.0 | 0.0 | 1146.57 | 1146.57 |
| 289.0 | 0.0 | 0.0 | 1.190e+05 | 0.0 | 0.0 | 0.0 | 1321.97 | 1321.97 |
| 311.0 | 0.0 | 0.0 | 1.685e+05 | 0.0 | 0.0 | 0.0 | 1872.66 | 1872.66 |
| 333.0 | 0.0 | 0.0 | 1.800e+05 | 0.0 | 0.0 | 0.0 | 1999.92 | 1999.92 |
| 355.0 | 0.0 | 0.0 | 1.766e+05 | 0.0 | 0.0 | 0.0 | 1962.12 | 1962.12 |
| 381.0 | 0.0 | 0.0 | 1.601e+05 | 0.0 | 0.0 | 0.0 | 1778.54 | 1778.54 |
| 408.0 | 0.0 | 0.0 | 1.225e+05 | 0.0 | 0.0 | 0.0 | 1360.84 | 1360.84 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 1146.57 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 289.0 | 2.50 | 1321.97 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 311.0 | 2.50 | 1872.66 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 333.0 | 2.50 | 1999.92 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 355.0 | 2.50 | 1962.12 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 381.0 | 2.50 | 1778.54 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 408.0 | 2.50 | 1360.84 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 101 | 141.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.03 | 0.02 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.05 | 0.02 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.05 | 0.02 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.05 | 0.02 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.04 | 0.02 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.03 | 0.02 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.07 | 0.0 | 0.05 | 0.02 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 9.836e+04 | 0.0 | 0.0 | 0.0 | 1092.89 | 1092.89 |
| 289.0 | 0.0 | 0.0 | 1.071e+05 | 0.0 | 0.0 | 0.0 | 1189.93 | 1189.93 |
| 311.0 | 0.0 | 0.0 | 1.521e+05 | 0.0 | 0.0 | 0.0 | 1689.69 | 1689.69 |
| 333.0 | 0.0 | 0.0 | 1.610e+05 | 0.0 | 0.0 | 0.0 | 1789.24 | 1789.24 |
| 355.0 | 0.0 | 0.0 | 1.567e+05 | 0.0 | 0.0 | 0.0 | 1741.12 | 1741.12 |
| 381.0 | 0.0 | 0.0 | 1.409e+05 | 0.0 | 0.0 | 0.0 | 1566.10 | 1566.10 |
| 408.0 | 0.0 | 0.0 | 1.051e+05 | 0.0 | 0.0 | 0.0 | 1168.28 | 1168.28 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 1092.89 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 289.0 | 2.50 | 1189.93 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 311.0 | 2.50 | 1689.69 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 333.0 | 2.50 | 1789.24 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 355.0 | 2.50 | 1741.12 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 381.0 | 2.50 | 1566.10 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 408.0 | 2.50 | 1168.28 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 103 | 141.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.04 | 0.02 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.04 | 0.02 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.06 | 0.0 | 0.04 | 0.02 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 8.610e+04 | 0.0 | 0.0 | 0.0 | 956.65 | 956.65 |
| 289.0 | 0.0 | 0.0 | 8.810e+04 | 0.0 | 0.0 | 0.0 | 978.89 | 978.89 |
| 311.0 | 0.0 | 0.0 | 1.272e+05 | 0.0 | 0.0 | 0.0 | 1413.31 | 1413.31 |
| 333.0 | 0.0 | 0.0 | 1.373e+05 | 0.0 | 0.0 | 0.0 | 1525.59 | 1525.59 |
| 355.0 | 0.0 | 0.0 | 1.333e+05 | 0.0 | 0.0 | 0.0 | 1481.49 | 1481.49 |
| 381.0 | 0.0 | 0.0 | 1.203e+05 | 0.0 | 0.0 | 0.0 | 1336.58 | 1336.58 |
| 408.0 | 0.0 | 0.0 | 9.132e+04 | 0.0 | 0.0 | 0.0 | 1014.64 | 1014.64 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 956.65 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 289.0 | 2.50 | 978.89 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 311.0 | 2.50 | 1413.31 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 333.0 | 2.50 | 1525.59 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 355.0 | 2.50 | 1481.49 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 381.0 | 2.50 | 1336.58 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 408.0 | 2.50 | 1014.64 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 105 | 141.00 | 12.00 | 150.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.02 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.05 | 0.03 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.05 | 0.03 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.05 | 0.02 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.06 | 0.0 | 0.05 | 0.03 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|--------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 9.009e+04 | 0.0 | 0.0 | 0.0 | 1201.23 | 1201.23 |
| 289.0 | 0.0 | 0.0 | 1.126e+05 | 0.0 | 0.0 | 0.0 | 1501.00 | 1501.00 |
| 311.0 | 0.0 | 0.0 | 1.473e+05 | 0.0 | 0.0 | 0.0 | 1963.77 | 1963.77 |
| 333.0 | 0.0 | 0.0 | 1.494e+05 | 0.0 | 0.0 | 0.0 | 1991.93 | 1991.93 |
| 355.0 | 0.0 | 0.0 | 1.408e+05 | 0.0 | 0.0 | 0.0 | 1877.87 | 1877.87 |
| 381.0 | 0.0 | 0.0 | 1.226e+05 | 0.0 | 0.0 | 0.0 | 1635.27 | 1635.27 |
| 408.0 | 0.0 | 0.0 | 8.607e+04 | 0.0 | 0.0 | 0.0 | 1147.60 | 1147.60 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 1201.23 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 289.0 | 2.50 | 1501.00 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 311.0 | 2.50 | 1963.77 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 333.0 | 2.50 | 1991.93 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 355.0 | 2.50 | 1877.87 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 381.0 | 2.50 | 1635.27 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 408.0 | 2.50 | 1147.60 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |

1.1.1.1.3 Parete Fronte Sud-Est

Si riportano le verifiche analitiche dei macroelementi della parete oggetto di verifica identificata nella figura successiva.

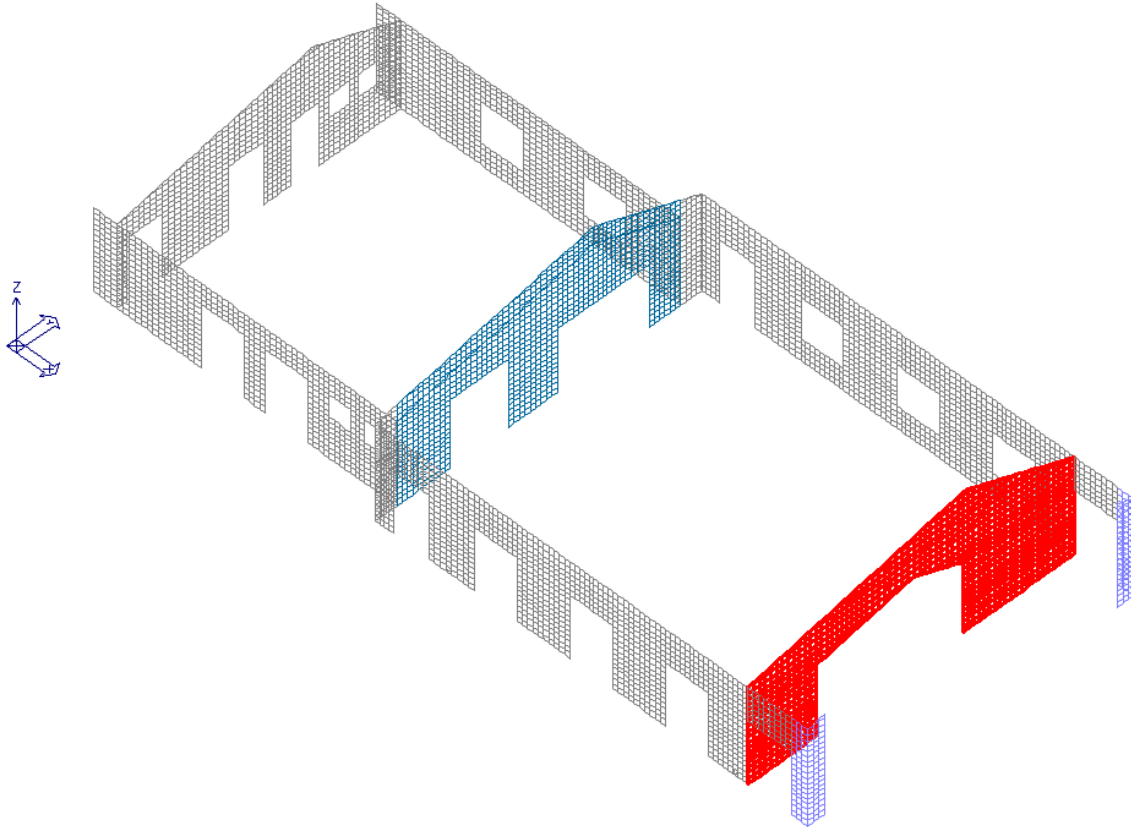


Fig 76. Parete oggetto di verifica (Selezione in rosso).

Macrosetti n. 63, 64 [maschi]

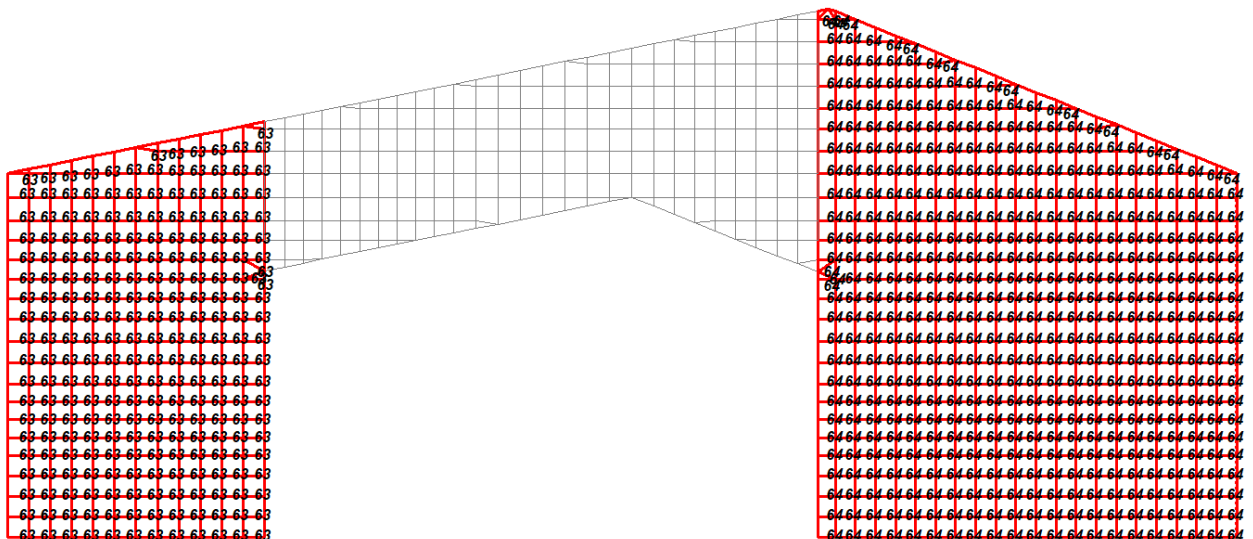


Fig 77. Elemento/i oggetto di verifica (Selezione in rosso).

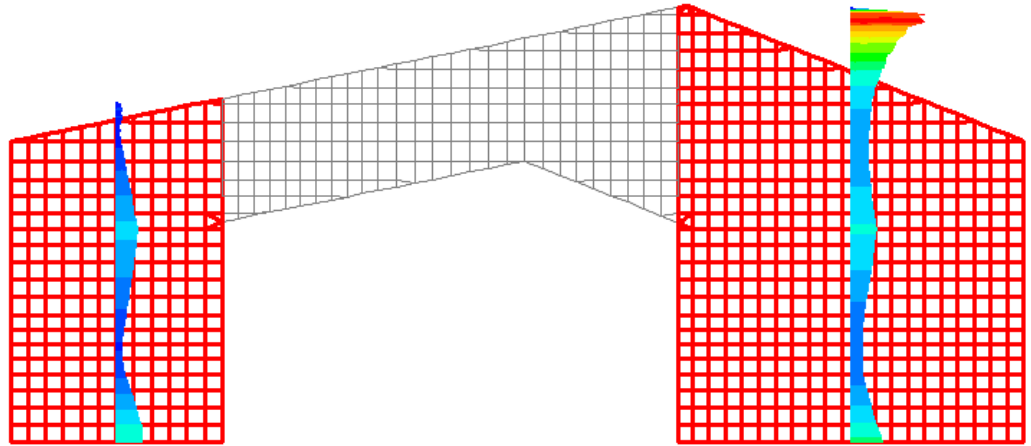
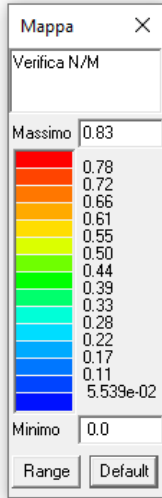


Fig 78. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

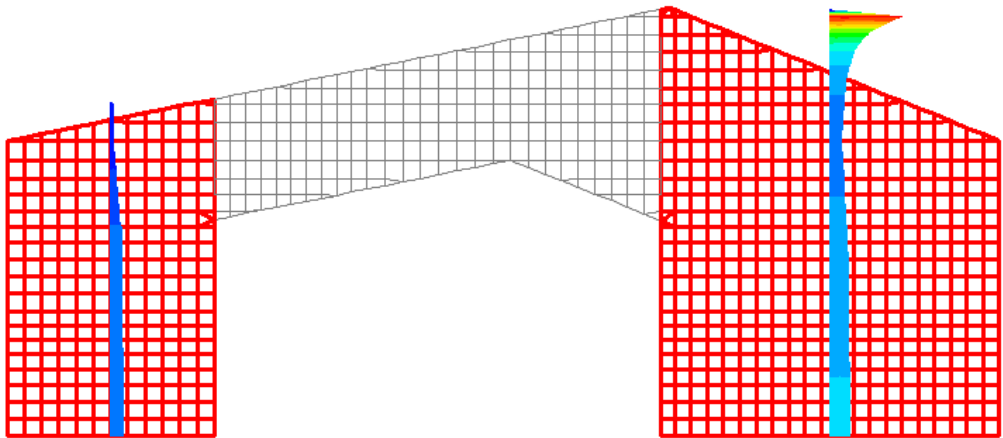
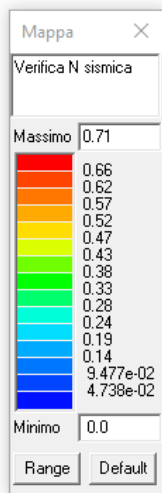


Fig 79. SLU: Mappa di verifica Nsismica – Verifiche soddisfatte ($\rho \leq 0.625$).

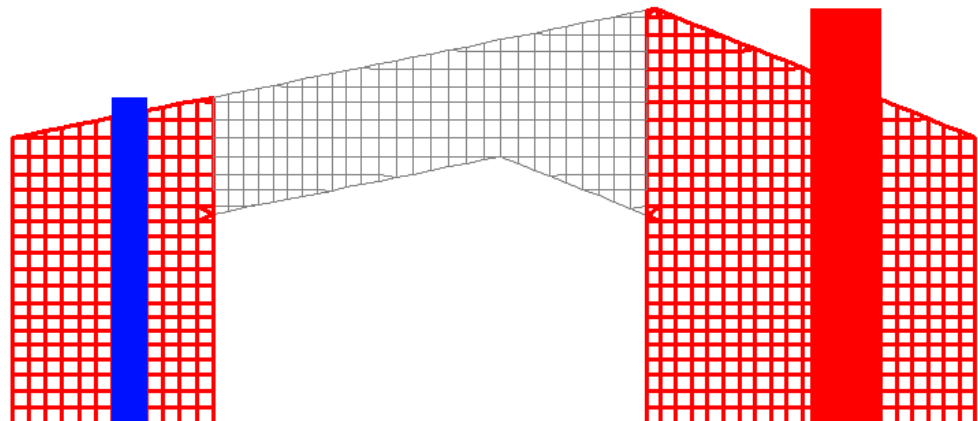
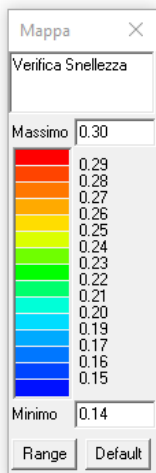


Fig 80. SLU: Mappa di Verifica Snellezza – Verifiche soddisfatte ($\rho \leq 1$).

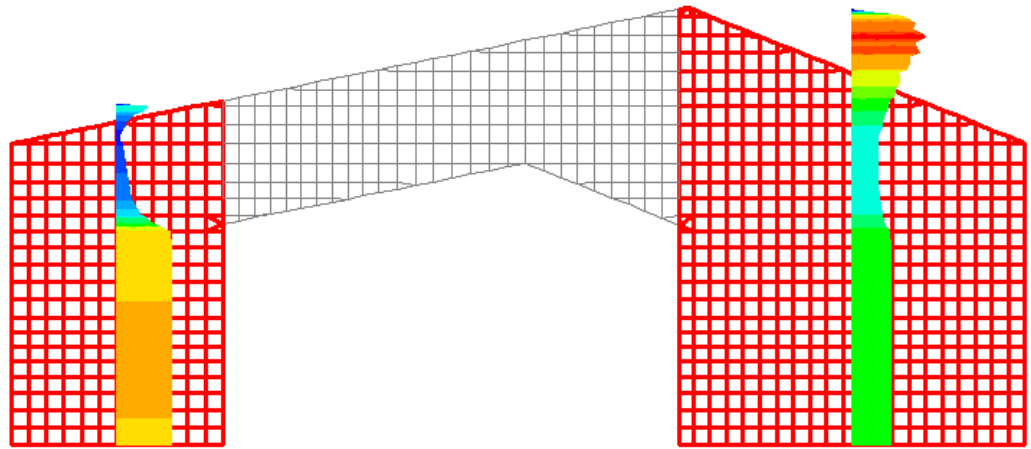
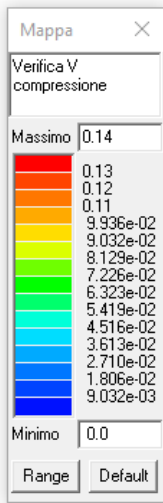


Fig 81. SLU: Mappa di Verifica V compressione – Verifica soddisfatta ($p \leq 1$).

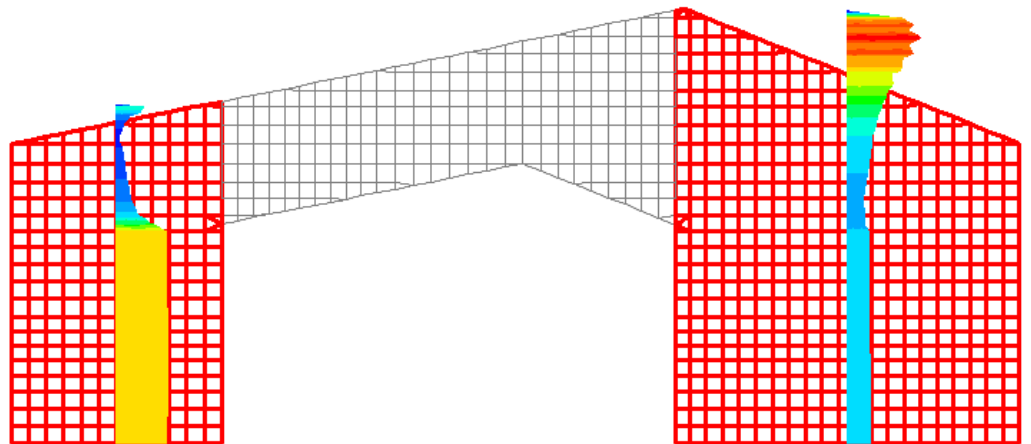
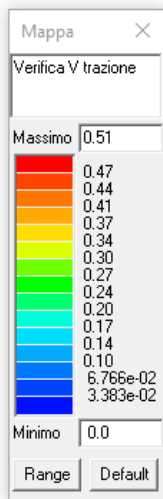


Fig 82. SLU: Mappa di verifica V trazione – Verifiche soddisfatte ($p \leq 1$).

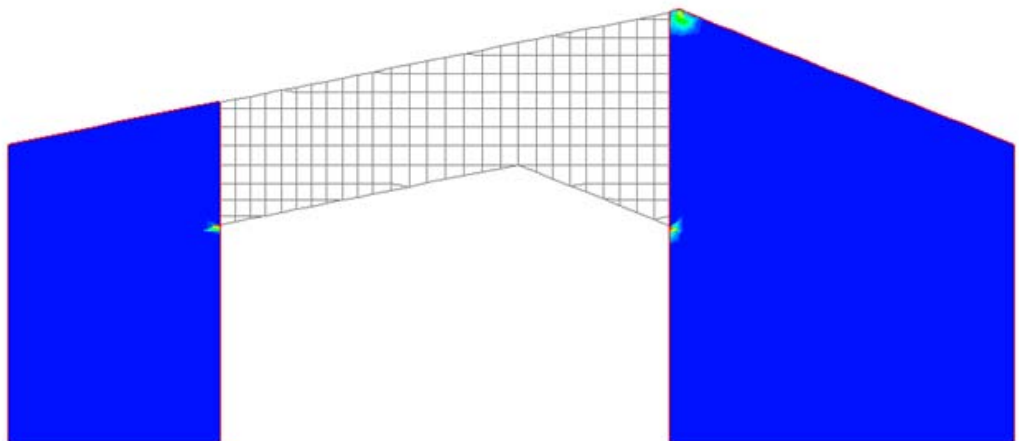
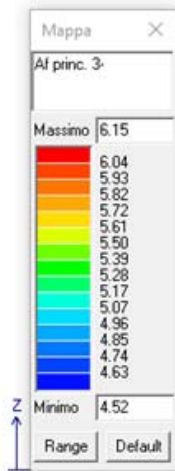


Fig 83. Mappa Armatura Verticale (singolo strato) da Calcolo [cm^2/m].

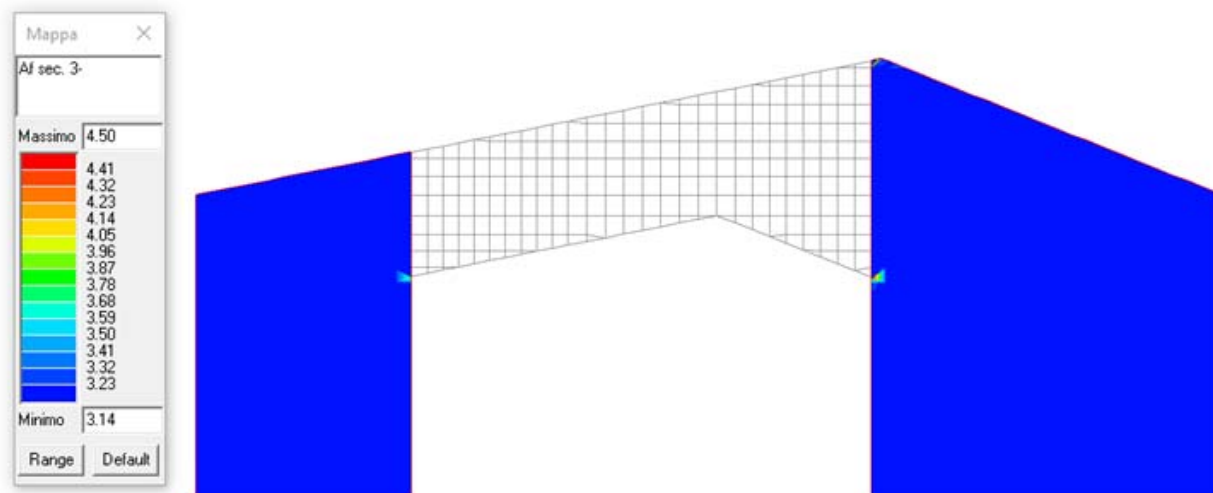


Fig 84. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm²/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 63 | 465.53 | 12.00 | 287.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.29 | 0.14 | 0.10 | 0.35 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.28 | 0.14 | 0.10 | 0.35 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.22 | 0.14 | 0.10 | 0.35 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.16 | 0.14 | 0.10 | 0.35 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.10 | 0.14 | 0.10 | 0.35 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.06 | 0.14 | 0.10 | 0.35 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.05 | 0.14 | 0.10 | 0.35 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.07 | 0.14 | 0.10 | 0.35 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.10 | 0.14 | 0.10 | 0.35 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.13 | 0.14 | 0.10 | 0.35 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.16 | 0.14 | 0.10 | 0.35 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.19 | 0.14 | 0.10 | 0.35 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.21 | 0.14 | 0.10 | 0.35 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.24 | 0.14 | 0.10 | 0.34 | 0.0 |
| 298.7 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.22 | 0.14 | 0.07 | 0.24 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.19 | 0.14 | 0.04 | 0.15 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.17 | 0.14 | 0.03 | 0.09 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.13 | 0.14 | 0.02 | 0.07 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.09 | 0.14 | 0.02 | 0.05 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.04 | 0.14 | 8.41e-03 | 0.03 | 0.0 |
| 412.7 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.04 | 0.14 | 4.24e-03 | 0.01 | 0.0 |
| 417.5 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.03 | 0.14 | 4.83e-03 | 0.02 | 0.0 |
| 422.3 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.04 | 0.14 | 7.37e-03 | 0.03 | 0.0 |
| 427.1 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.03 | 0.14 | 9.45e-03 | 0.03 | 0.0 |
| 431.9 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.04 | 0.14 | 0.01 | 0.05 | 0.0 |
| 433.0 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.04 | 0.14 | 0.01 | 0.05 | 0.0 |
| 436.7 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.05 | 0.14 | 0.02 | 0.06 | 0.0 |
| 441.5 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.06 | 0.14 | 0.02 | 0.08 | 0.0 |
| 446.3 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.05 | 0.14 | 0.03 | 0.10 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| 451.1 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.06 | 0.14 | 0.05 | 0.16 | 0.0 |
| 455.9 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.05 | 0.14 | 0.05 | 0.19 | 0.0 |
| 458.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.04 | 0.14 | 0.05 | 0.19 | 0.0 |
| 460.7 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.14 | 0.0 | 0.0 | 0.0 |
| 465.5 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.14 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.12 | 0.29 | 0.14 | 0.10 | 0.35 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|------------|------------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1.460e+04 | -9955.32 | 1.223e+05 | 9.413e+04 | -7300.60 | -7482.99 | 9541.99 | 9541.99 |
| 23.0 | -1.460e+04 | -7435.18 | 1.280e+05 | 8.829e+04 | -7300.60 | -7482.99 | 9541.99 | 9541.99 |
| 46.0 | -1.454e+04 | -7592.99 | 9.259e+04 | 6.860e+04 | -7300.60 | -7716.53 | 9684.29 | 9684.29 |
| 69.0 | -1.438e+04 | -7714.93 | 5.096e+04 | 4.955e+04 | -7300.60 | -7923.26 | 9737.37 | 9737.37 |
| 92.0 | -1.417e+04 | -7828.06 | 7842.38 | 3.179e+04 | -7300.60 | -8120.57 | 9760.42 | 9760.42 |
| 112.0 | -1.395e+04 | -8513.72 | 4.421e+05 | 6816.42 | -7300.60 | -8328.59 | 9729.74 | 9729.74 |
| 132.0 | -1.377e+04 | -8630.33 | 4.162e+05 | 3383.43 | -7300.60 | -8482.90 | 9697.62 | 9697.62 |
| 152.0 | -1.359e+04 | -9462.45 | 1.468e+05 | 2.285e+04 | -7300.60 | -8623.00 | 9680.84 | 9680.84 |
| 172.0 | -1.347e+04 | -9346.32 | 1.851e+05 | 3.239e+04 | -7300.60 | -8741.43 | 9655.76 | 9655.76 |
| 196.0 | -1.331e+04 | -9203.37 | 2.349e+05 | 4.257e+04 | -7300.60 | -8920.76 | 9635.53 | 9635.53 |
| 220.0 | -1.312e+04 | -1.183e+04 | 3.764e+05 | 5.279e+04 | -7300.60 | -9038.01 | 9617.99 | 9617.99 |
| 244.0 | -1.290e+04 | -1.157e+04 | 4.481e+05 | 6.088e+04 | -7300.60 | -9238.60 | 9601.70 | 9601.70 |
| 267.0 | -1.267e+04 | -8205.93 | 3.441e+05 | 6.715e+04 | -7300.60 | -9210.82 | 9594.45 | 9594.45 |
| 289.0 | -1.225e+04 | -7875.77 | 4.251e+05 | 7.612e+04 | -7300.60 | -9065.34 | 9511.93 | 9511.93 |
| 298.7 | -9850.40 | -6326.39 | 3.160e+05 | 6.887e+04 | -7300.60 | -6689.68 | 6512.61 | 6512.61 |
| 311.0 | -9388.61 | -6169.66 | 3.024e+05 | 5.832e+04 | -7300.60 | -6842.38 | 4140.13 | 4140.13 |
| 333.0 | -7977.13 | -5172.19 | 2.526e+05 | 5.049e+04 | -7300.60 | -3901.11 | 2571.70 | 2571.70 |
| 355.0 | -6580.89 | -4274.70 | 2.117e+05 | 3.899e+04 | -7300.60 | -3139.33 | 1998.36 | 1998.36 |
| 381.0 | -5008.39 | -3236.13 | 1.621e+05 | 2.683e+04 | -7300.60 | -2435.82 | 1517.77 | 1517.77 |
| 408.0 | -3386.48 | -2197.11 | 2.326e+05 | 7698.13 | -7300.60 | -1784.14 | 803.45 | 803.45 |
| 412.7 | -2537.00 | -1727.39 | 1.656e+05 | 7871.12 | -7300.60 | -2078.12 | 353.03 | 353.03 |
| 417.5 | -2011.31 | -1803.61 | 1.566e+05 | 3180.59 | -7300.60 | -1125.51 | 381.09 | 381.09 |
| 422.3 | -1781.35 | -1781.35 | 1.248e+05 | 2537.25 | -7300.60 | -1047.29 | 489.62 | 489.62 |
| 427.1 | -1627.51 | -1484.37 | 8.462e+04 | 3817.13 | -7300.60 | -1196.63 | 589.27 | 589.27 |
| 431.9 | -1470.55 | -1161.72 | 4.483e+04 | 4963.65 | -7300.60 | -1092.68 | 687.75 | 687.75 |
| 433.0 | -1435.04 | -1138.28 | 4.132e+04 | 5107.58 | -7300.60 | -1068.74 | 707.21 | 707.21 |
| 436.7 | -1177.83 | -751.13 | 2.607e+04 | 7430.03 | -7300.60 | -774.11 | 733.04 | 733.04 |
| 441.5 | -1048.31 | -680.89 | 1.612e+04 | 5826.68 | -7300.60 | -847.86 | 750.96 | 750.96 |
| 446.3 | -901.83 | -597.35 | 8614.96 | 4342.35 | -7300.60 | -788.54 | 798.37 | 798.37 |
| 451.1 | -730.08 | -645.74 | 4772.17 | 3288.91 | -7300.60 | -683.72 | 780.17 | 780.17 |
| 455.9 | -525.74 | -462.58 | 1207.77 | 2339.75 | -7300.60 | -514.71 | 671.91 | 671.91 |
| 458.0 | -419.98 | -369.25 | 533.94 | 1866.51 | -7300.60 | -417.30 | 570.00 | 570.00 |
| 460.7 | 0.0 | 0.0 | 0.0 | 0.0 | -7300.60 | 0.0 | 0.0 | 0.0 |
| 465.5 | 0.0 | 0.0 | 0.0 | 0.0 | -7300.60 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 9541.99 | 9.671e+04 | 1.00 | 2.763e+04 | 9.671e+04 |
| 23.0 | 1.00 | 9541.99 | 9.671e+04 | 1.00 | 2.763e+04 | 9.671e+04 |
| 46.0 | 1.00 | 9684.29 | 9.675e+04 | 1.00 | 2.763e+04 | 9.675e+04 |
| 69.0 | 1.00 | 9737.37 | 9.679e+04 | 1.00 | 2.763e+04 | 9.679e+04 |
| 92.0 | 1.00 | 9760.42 | 9.683e+04 | 1.00 | 2.763e+04 | 9.683e+04 |
| 112.0 | 1.00 | 9729.74 | 9.687e+04 | 1.00 | 2.763e+04 | 9.687e+04 |
| 132.0 | 1.00 | 9697.62 | 9.690e+04 | 1.00 | 2.763e+04 | 9.690e+04 |
| 152.0 | 1.00 | 9680.84 | 9.693e+04 | 1.00 | 2.763e+04 | 9.693e+04 |
| 172.0 | 1.00 | 9655.76 | 9.695e+04 | 1.00 | 2.763e+04 | 9.695e+04 |
| 196.0 | 1.00 | 9635.53 | 9.699e+04 | 1.00 | 2.763e+04 | 9.699e+04 |
| 220.0 | 1.00 | 9617.99 | 9.701e+04 | 1.00 | 2.763e+04 | 9.701e+04 |
| 244.0 | 1.00 | 9601.70 | 9.705e+04 | 1.00 | 2.763e+04 | 9.705e+04 |
| 267.0 | 1.00 | 9594.45 | 9.704e+04 | 1.00 | 2.763e+04 | 9.704e+04 |
| 289.0 | 1.00 | 9511.93 | 9.702e+04 | 1.00 | 2.763e+04 | 9.702e+04 |
| 298.7 | 1.00 | 6512.61 | 9.655e+04 | 1.00 | 2.763e+04 | 9.655e+04 |
| 311.0 | 1.00 | 4140.13 | 9.658e+04 | 1.00 | 2.763e+04 | 9.658e+04 |
| 333.0 | 1.00 | 2571.70 | 9.601e+04 | 1.00 | 2.763e+04 | 9.601e+04 |
| 355.0 | 1.00 | 1998.36 | 9.586e+04 | 1.00 | 2.763e+04 | 9.586e+04 |
| 381.0 | 1.00 | 1517.77 | 9.572e+04 | 1.00 | 2.763e+04 | 9.572e+04 |
| 408.0 | 1.00 | 803.45 | 9.559e+04 | 1.00 | 2.763e+04 | 9.559e+04 |
| 412.7 | 1.00 | 353.03 | 8.318e+04 | 1.00 | 2.402e+04 | 8.318e+04 |
| 417.5 | 1.00 | 381.09 | 7.895e+04 | 1.00 | 2.284e+04 | 7.895e+04 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| 422.3 | 1.00 | 489.62 | 6.639e+04 | 1.00 | 1.921e+04 | 6.639e+04 |
| 427.1 | 1.00 | 589.27 | 6.237e+04 | 1.00 | 1.803e+04 | 6.237e+04 |
| 431.9 | 1.00 | 687.75 | 4.980e+04 | 1.00 | 1.439e+04 | 4.980e+04 |
| 433.0 | 1.00 | 707.21 | 4.888e+04 | 1.00 | 1.413e+04 | 4.888e+04 |
| 436.7 | 1.00 | 733.04 | 4.569e+04 | 1.00 | 1.321e+04 | 4.569e+04 |
| 441.5 | 1.00 | 750.96 | 3.316e+04 | 1.00 | 9579.11 | 3.316e+04 |
| 446.3 | 1.00 | 798.37 | 2.909e+04 | 1.00 | 8400.14 | 2.909e+04 |
| 451.1 | 1.00 | 780.17 | 1.652e+04 | 1.00 | 4764.99 | 1.652e+04 |
| 455.9 | 1.00 | 671.91 | 1.244e+04 | 1.00 | 3586.03 | 1.244e+04 |
| 458.0 | 1.00 | 570.00 | 1.067e+04 | 1.00 | 3076.90 | 1.067e+04 |
| 460.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 465.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 64 | 592.00 | 12.00 | 469.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.35 | 0.30 | 0.07 | 0.15 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.29 | 0.30 | 0.07 | 0.15 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.23 | 0.30 | 0.07 | 0.15 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.18 | 0.30 | 0.07 | 0.15 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.13 | 0.30 | 0.07 | 0.15 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.12 | 0.30 | 0.07 | 0.15 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.12 | 0.30 | 0.07 | 0.15 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.13 | 0.30 | 0.07 | 0.15 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.14 | 0.30 | 0.07 | 0.15 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.18 | 0.30 | 0.07 | 0.15 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.21 | 0.30 | 0.07 | 0.15 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.24 | 0.30 | 0.07 | 0.15 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.26 | 0.30 | 0.07 | 0.15 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.29 | 0.30 | 0.07 | 0.14 | 0.0 |
| 297.1 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.28 | 0.30 | 0.06 | 0.12 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.26 | 0.30 | 0.05 | 0.12 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.23 | 0.30 | 0.05 | 0.11 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.22 | 0.30 | 0.05 | 0.13 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.20 | 0.30 | 0.05 | 0.15 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.19 | 0.30 | 0.05 | 0.17 | 0.0 |
| 417.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.19 | 0.30 | 0.05 | 0.17 | 0.0 |
| 426.1 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.20 | 0.30 | 0.05 | 0.19 | 0.0 |
| 433.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.21 | 0.30 | 0.05 | 0.19 | 0.0 |
| 435.1 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.21 | 0.30 | 0.06 | 0.20 | 0.0 |
| 444.2 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.24 | 0.30 | 0.06 | 0.20 | 0.0 |
| 453.2 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.22 | 0.30 | 0.06 | 0.23 | 0.0 |
| 458.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.22 | 0.30 | 0.07 | 0.24 | 0.0 |
| 462.3 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.23 | 0.30 | 0.07 | 0.24 | 0.0 |
| 471.3 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.25 | 0.30 | 0.08 | 0.27 | 0.0 |
| 480.4 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.27 | 0.30 | 0.08 | 0.28 | 0.0 |
| 489.4 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.31 | 0.30 | 0.09 | 0.32 | 0.0 |
| 498.5 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.32 | 0.30 | 0.09 | 0.31 | 0.0 |
| 505.4 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.33 | 0.30 | 0.09 | 0.31 | 0.0 |
| 507.5 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.37 | 0.30 | 0.10 | 0.36 | 0.0 |
| 516.6 | 1d12 | 1d12/25 | 1d10/25 | 0.20 | 0.39 | 0.30 | 0.11 | 0.38 | 0.0 |
| 525.6 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.41 | 0.30 | 0.11 | 0.38 | 0.0 |
| 530.4 | 1d12 | 1d12/25 | 1d10/25 | 0.24 | 0.47 | 0.30 | 0.12 | 0.45 | 0.0 |
| 534.7 | 1d12 | 1d12/25 | 1d10/25 | 0.25 | 0.49 | 0.30 | 0.12 | 0.45 | 0.0 |
| 543.7 | 1d12 | 1d12/25 | 1d10/25 | 0.29 | 0.51 | 0.30 | 0.12 | 0.43 | 0.0 |
| 552.8 | 1d12 | 1d12/25 | 1d10/25 | 0.35 | 0.61 | 0.30 | 0.14 | 0.51 | 0.0 |
| 555.4 | 1d12 | 1d12/25 | 1d10/25 | 0.37 | 0.61 | 0.30 | 0.13 | 0.50 | 0.0 |
| 561.8 | 1d12 | 1d12/25 | 1d10/25 | 0.43 | 0.63 | 0.30 | 0.11 | 0.42 | 0.0 |
| 570.9 | 1d12 | 1d12/25 | 1d10/25 | 0.55 | 0.83 | 0.30 | 0.12 | 0.46 | 0.0 |
| 579.9 | 1d12 | 1d12/25 | 1d10/25 | 0.71 | 0.74 | 0.30 | 0.09 | 0.37 | 0.0 |
| 580.4 | 1d12 | 1d12/25 | 1d10/25 | 0.64 | 0.82 | 0.30 | 0.09 | 0.32 | 0.0 |
| 589.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.30 | 0.0 | 0.0 | 0.0 |
| 589.6 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.30 | 0.0 | 0.0 | 0.0 |
| 592.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.30 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.71 | 0.83 | 0.30 | 0.14 | 0.51 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|------------|------------|-----------|-----------|------------|------------|-----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -3.862e+04 | -3.315e+04 | 2.051e+06 | 1.958e+05 | -1.931e+04 | -1.961e+04 | 1.107e+04 | 6744.73 |
| 23.0 | -3.862e+04 | -1.930e+04 | 9.362e+05 | 1.477e+05 | -1.931e+04 | -1.961e+04 | 1.107e+04 | 6744.73 |
| 46.0 | -3.830e+04 | -1.973e+04 | 1.650e+06 | 1.137e+05 | -1.931e+04 | -1.938e+04 | 1.115e+04 | 6789.65 |
| 69.0 | -3.790e+04 | -1.940e+04 | 1.624e+06 | 8.811e+04 | -1.931e+04 | -1.925e+04 | 1.117e+04 | 6788.44 |
| 92.0 | -3.745e+04 | -1.906e+04 | 1.602e+06 | 5.893e+04 | -1.931e+04 | -1.910e+04 | 1.116e+04 | 6778.28 |
| 112.0 | -3.706e+04 | -3.667e+04 | 2.821e+06 | 1.344e+04 | -1.931e+04 | -1.896e+04 | 1.115e+04 | 6761.66 |
| 132.0 | -3.668e+04 | -3.622e+04 | 2.850e+06 | 5736.69 | -1.931e+04 | -1.883e+04 | 1.108e+04 | 6695.29 |
| 152.0 | -3.630e+04 | -3.590e+04 | 2.805e+06 | 2.335e+04 | -1.931e+04 | -1.869e+04 | 1.104e+04 | 6648.88 |
| 172.0 | -3.590e+04 | -3.028e+04 | 2.347e+06 | 5.764e+04 | -1.931e+04 | -1.854e+04 | 1.101e+04 | 6615.34 |
| 196.0 | -3.545e+04 | -2.980e+04 | 2.401e+06 | 8.012e+04 | -1.931e+04 | -1.836e+04 | 1.095e+04 | 6550.96 |
| 220.0 | -3.494e+04 | -2.926e+04 | 2.457e+06 | 1.001e+05 | -1.931e+04 | -1.815e+04 | 1.091e+04 | 6515.55 |
| 244.0 | -3.442e+04 | -2.871e+04 | 2.517e+06 | 1.178e+05 | -1.931e+04 | -1.864e+04 | 1.088e+04 | 6475.39 |
| 267.0 | -3.390e+04 | -2.816e+04 | 2.576e+06 | 1.329e+05 | -1.931e+04 | -1.817e+04 | 1.087e+04 | 6441.18 |
| 289.0 | -3.324e+04 | -2.746e+04 | 2.674e+06 | 1.447e+05 | -1.931e+04 | -1.786e+04 | 1.082e+04 | 6363.37 |
| 297.1 | -3.115e+04 | -2.559e+04 | 2.481e+06 | 1.388e+05 | -1.931e+04 | -1.613e+04 | 9201.75 | 5175.76 |
| 311.0 | -3.039e+04 | -2.497e+04 | 2.365e+06 | 1.291e+05 | -1.931e+04 | -1.569e+04 | 8375.88 | 5239.77 |
| 333.0 | -2.817e+04 | -2.299e+04 | 2.192e+06 | 1.124e+05 | -1.931e+04 | -1.472e+04 | 7588.27 | 4790.81 |
| 355.0 | -2.653e+04 | -2.149e+04 | 2.138e+06 | 1.037e+05 | -1.931e+04 | -1.418e+04 | 7264.86 | 5568.35 |
| 381.0 | -2.475e+04 | -1.985e+04 | 2.101e+06 | 9.218e+04 | -1.931e+04 | -1.321e+04 | 7118.65 | 6465.01 |
| 408.0 | -2.297e+04 | -2.225e+04 | 2.631e+06 | 7.868e+04 | -1.931e+04 | -2.297e+04 | 7264.39 | 7264.39 |
| 417.0 | -2.189e+04 | -2.113e+04 | 2.440e+06 | 7.520e+04 | -1.931e+04 | -2.189e+04 | 7192.20 | 7192.20 |
| 426.1 | -2.140e+04 | -2.081e+04 | 2.218e+06 | 7.767e+04 | -1.931e+04 | -2.140e+04 | 7333.86 | 7333.86 |
| 433.0 | -2.111e+04 | -2.058e+04 | 2.049e+06 | 7.888e+04 | -1.931e+04 | -2.111e+04 | 7457.25 | 7457.25 |
| 435.1 | -2.051e+04 | -2.000e+04 | 1.998e+06 | 7.922e+04 | -1.931e+04 | -2.051e+04 | 7457.30 | 7457.30 |
| 444.2 | -2.018e+04 | -1.970e+04 | 1.809e+06 | 7.875e+04 | -1.931e+04 | -2.018e+04 | 7582.97 | 7582.97 |
| 453.2 | -1.983e+04 | -1.937e+04 | 1.633e+06 | 7.834e+04 | -1.931e+04 | -1.983e+04 | 7704.47 | 7704.47 |
| 458.0 | -1.964e+04 | -1.918e+04 | 1.545e+06 | 7.795e+04 | -1.931e+04 | -1.964e+04 | 7748.56 | 7748.56 |
| 462.3 | -1.909e+04 | -1.863e+04 | 1.470e+06 | 7.724e+04 | -1.931e+04 | -1.909e+04 | 7739.71 | 7739.71 |
| 471.3 | -1.876e+04 | -1.839e+04 | 1.339e+06 | 7.891e+04 | -1.931e+04 | -1.876e+04 | 7753.38 | 7753.38 |
| 480.4 | -1.841e+04 | -1.804e+04 | 1.201e+06 | 8.276e+04 | -1.931e+04 | -1.841e+04 | 7742.03 | 7742.03 |
| 489.4 | -1.770e+04 | -1.735e+04 | 1.089e+06 | 8.591e+04 | -1.931e+04 | -1.770e+04 | 7660.36 | 7660.36 |
| 498.5 | -1.735e+04 | -1.701e+04 | 9.783e+05 | 8.889e+04 | -1.931e+04 | -1.735e+04 | 7181.49 | 7181.49 |
| 505.4 | -1.740e+04 | -1.706e+04 | 8.581e+05 | 9.077e+04 | -1.931e+04 | -1.740e+04 | 6837.31 | 6837.31 |
| 507.5 | -1.715e+04 | -1.681e+04 | 8.197e+05 | 9.144e+04 | -1.931e+04 | -1.715e+04 | 7105.36 | 7105.36 |
| 516.6 | -1.696e+04 | -1.663e+04 | 7.164e+05 | 9.241e+04 | -1.931e+04 | -1.696e+04 | 6995.71 | 6995.71 |
| 525.6 | -1.667e+04 | -1.636e+04 | 6.193e+05 | 9.359e+04 | -1.931e+04 | -1.667e+04 | 6649.25 | 6649.25 |
| 530.4 | -1.653e+04 | -1.623e+04 | 5.663e+05 | 9.387e+04 | -1.931e+04 | -1.653e+04 | 6424.95 | 6424.95 |
| 534.7 | -1.629e+04 | -1.599e+04 | 5.218e+05 | 9.384e+04 | -1.931e+04 | -1.629e+04 | 6111.72 | 6111.72 |
| 543.7 | -1.620e+04 | -1.591e+04 | 4.245e+05 | 9.273e+04 | -1.931e+04 | -1.620e+04 | 5397.44 | 5397.44 |
| 552.8 | -1.607e+04 | -1.580e+04 | 3.199e+05 | 9.065e+04 | -1.931e+04 | -1.607e+04 | 4599.29 | 4599.29 |
| 555.4 | -1.602e+04 | -1.575e+04 | 2.885e+05 | 8.890e+04 | -1.931e+04 | -1.602e+04 | 4330.96 | 4330.96 |
| 561.8 | -1.581e+04 | -5812.69 | 7.657e+04 | 7.301e+04 | -1.931e+04 | -1.581e+04 | 3366.93 | 3366.93 |
| 570.9 | -1.514e+04 | -5069.95 | 4.009e+04 | 5.982e+04 | -1.931e+04 | -1.514e+04 | 2010.75 | 2010.75 |
| 579.9 | -1.264e+04 | -1.249e+04 | 3.026e+04 | 6.020e+04 | -1.931e+04 | -5441.86 | 1131.85 | 1224.54 |
| 580.4 | -1.109e+04 | -3602.05 | 3522.44 | 4.996e+04 | -1.931e+04 | -4911.43 | 1090.95 | 1040.23 |
| 589.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1.931e+04 | 0.0 | 0.0 | 0.0 |
| 589.6 | 0.0 | 0.0 | 0.0 | 0.0 | -1.931e+04 | 0.0 | 0.0 | 0.0 |
| 592.0 | 0.0 | 0.0 | 0.0 | 0.0 | -1.931e+04 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 1.107e+04 | 1.552e+05 | 1.00 | 4.394e+04 | 1.558e+05 |
| 23.0 | 1.00 | 1.107e+04 | 1.552e+05 | 1.00 | 4.394e+04 | 1.558e+05 |
| 46.0 | 1.00 | 1.115e+04 | 1.551e+05 | 1.00 | 4.394e+04 | 1.557e+05 |
| 69.0 | 1.00 | 1.117e+04 | 1.551e+05 | 1.00 | 4.394e+04 | 1.556e+05 |
| 92.0 | 1.00 | 1.116e+04 | 1.551e+05 | 1.00 | 4.394e+04 | 1.555e+05 |
| 112.0 | 1.00 | 1.115e+04 | 1.551e+05 | 1.00 | 4.394e+04 | 1.554e+05 |
| 132.0 | 1.00 | 1.108e+04 | 1.550e+05 | 1.00 | 4.394e+04 | 1.553e+05 |
| 152.0 | 1.00 | 1.104e+04 | 1.550e+05 | 1.00 | 4.394e+04 | 1.552e+05 |
| 172.0 | 1.00 | 1.101e+04 | 1.550e+05 | 1.00 | 4.394e+04 | 1.551e+05 |
| 196.0 | 1.00 | 1.095e+04 | 1.550e+05 | 1.00 | 4.394e+04 | 1.550e+05 |
| 220.0 | 1.00 | 1.091e+04 | 1.549e+05 | 1.00 | 4.394e+04 | 1.549e+05 |
| 244.0 | 1.00 | 1.088e+04 | 1.550e+05 | 1.00 | 4.394e+04 | 1.546e+05 |
| 267.0 | 1.00 | 1.087e+04 | 1.549e+05 | 1.00 | 4.394e+04 | 1.545e+05 |
| 289.0 | 1.00 | 1.082e+04 | 1.549e+05 | 1.00 | 4.394e+04 | 1.544e+05 |
| 297.1 | 1.00 | 9201.75 | 1.545e+05 | 1.00 | 4.394e+04 | 1.542e+05 |
| 311.0 | 1.00 | 8375.88 | 1.544e+05 | 1.00 | 4.394e+04 | 1.542e+05 |
| 333.0 | 1.00 | 7588.27 | 1.543e+05 | 1.00 | 4.394e+04 | 1.568e+05 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| 355.0 | 1.00 | 7264.86 | 1.542e+05 | 1.00 | 4.394e+04 | 1.565e+05 |
| 381.0 | 1.00 | 7118.65 | 1.540e+05 | 1.00 | 4.394e+04 | 1.562e+05 |
| 408.0 | 1.00 | 7264.39 | 1.558e+05 | 1.00 | 4.394e+04 | 1.558e+05 |
| 417.0 | 1.00 | 7192.20 | 1.519e+05 | 1.00 | 4.284e+04 | 1.519e+05 |
| 426.1 | 1.00 | 7333.86 | 1.394e+05 | 1.00 | 3.927e+04 | 1.394e+05 |
| 433.0 | 1.00 | 7457.25 | 1.365e+05 | 1.00 | 3.843e+04 | 1.365e+05 |
| 435.1 | 1.00 | 7457.30 | 1.355e+05 | 1.00 | 3.817e+04 | 1.355e+05 |
| 444.2 | 1.00 | 7582.97 | 1.318e+05 | 1.00 | 3.706e+04 | 1.318e+05 |
| 453.2 | 1.00 | 7704.47 | 1.193e+05 | 1.00 | 3.350e+04 | 1.193e+05 |
| 458.0 | 1.00 | 7748.56 | 1.173e+05 | 1.00 | 3.292e+04 | 1.173e+05 |
| 462.3 | 1.00 | 7739.71 | 1.154e+05 | 1.00 | 3.240e+04 | 1.154e+05 |
| 471.3 | 1.00 | 7753.38 | 1.029e+05 | 1.00 | 2.884e+04 | 1.029e+05 |
| 480.4 | 1.00 | 7742.03 | 9.917e+04 | 1.00 | 2.773e+04 | 9.917e+04 |
| 489.4 | 1.00 | 7660.36 | 8.657e+04 | 1.00 | 2.417e+04 | 8.657e+04 |
| 498.5 | 1.00 | 7181.49 | 8.283e+04 | 1.00 | 2.306e+04 | 8.283e+04 |
| 505.4 | 1.00 | 6837.31 | 8.005e+04 | 1.00 | 2.222e+04 | 8.005e+04 |
| 507.5 | 1.00 | 7105.36 | 7.029e+04 | 1.00 | 1.950e+04 | 7.029e+04 |
| 516.6 | 1.00 | 6995.71 | 6.659e+04 | 1.00 | 1.840e+04 | 6.659e+04 |
| 525.6 | 1.00 | 6649.25 | 6.292e+04 | 1.00 | 1.729e+04 | 6.292e+04 |
| 530.4 | 1.00 | 6424.95 | 5.204e+04 | 1.00 | 1.425e+04 | 5.204e+04 |
| 534.7 | 1.00 | 6111.72 | 5.027e+04 | 1.00 | 1.373e+04 | 5.027e+04 |
| 543.7 | 1.00 | 5397.44 | 4.667e+04 | 1.00 | 1.262e+04 | 4.667e+04 |
| 552.8 | 1.00 | 4599.29 | 3.395e+04 | 1.00 | 9063.31 | 3.395e+04 |
| 555.4 | 1.00 | 4330.96 | 3.291e+04 | 1.00 | 8745.00 | 3.291e+04 |
| 561.8 | 1.00 | 3366.93 | 3.037e+04 | 1.00 | 7958.03 | 3.037e+04 |
| 570.9 | 1.00 | 2010.75 | 1.726e+04 | 1.00 | 4396.57 | 1.726e+04 |
| 579.9 | 1.00 | 1131.85 | 1.221e+04 | 1.00 | 3291.28 | 1.336e+04 |
| 580.4 | 1.00 | 1090.95 | 1.194e+04 | 1.00 | 3235.15 | 1.294e+04 |
| 589.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 589.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 592.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Macrosetti n. 33 [fasce di piano]

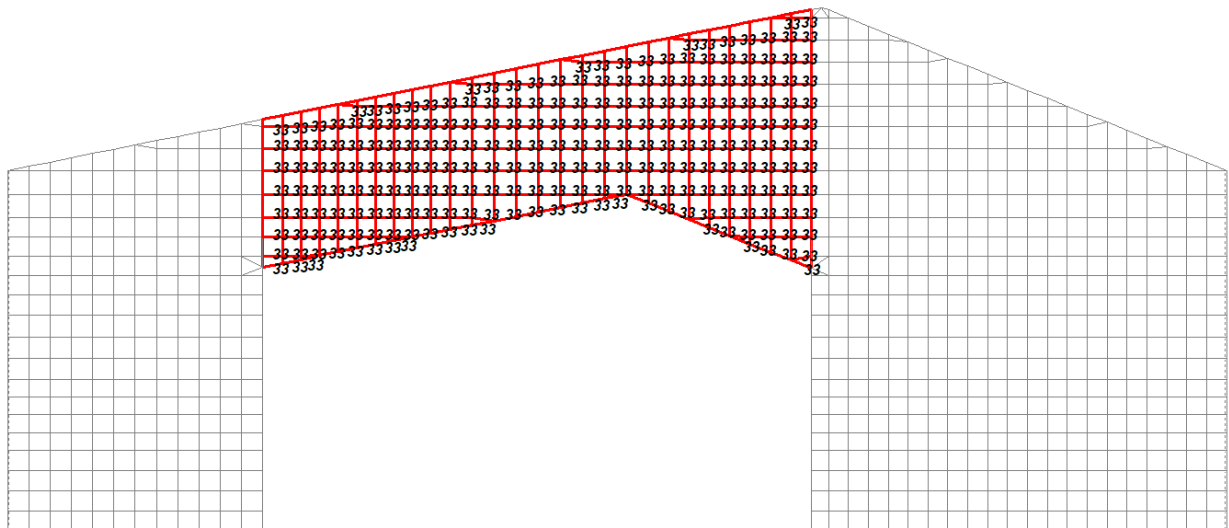


Fig 85. Elemento/i oggetto di verifica (Selezione in rosso).

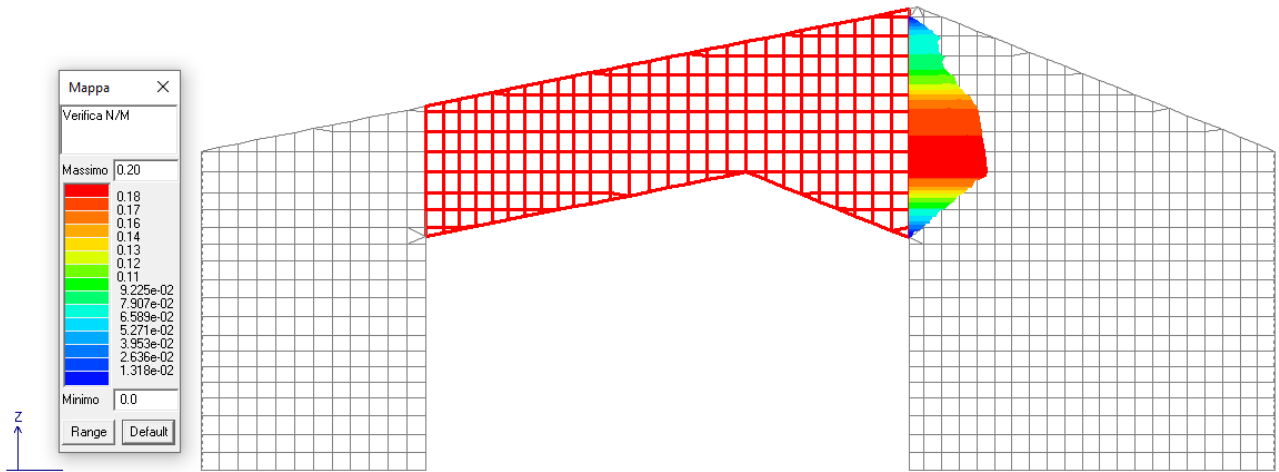


Fig 86. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

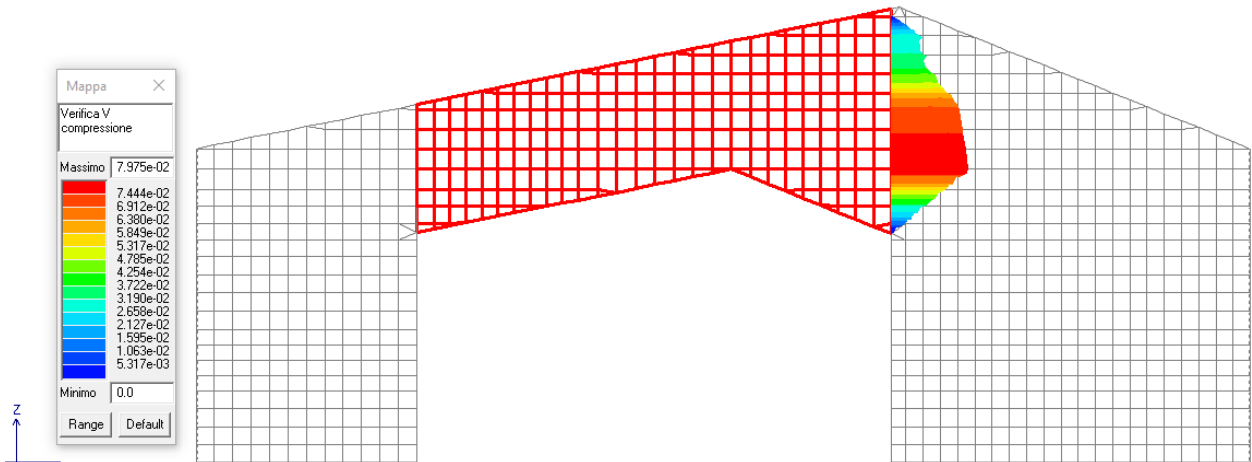


Fig 87. SLU: Mappa di Verifica V compressione – Verifica soddisfatta ($\rho \leq 1$).

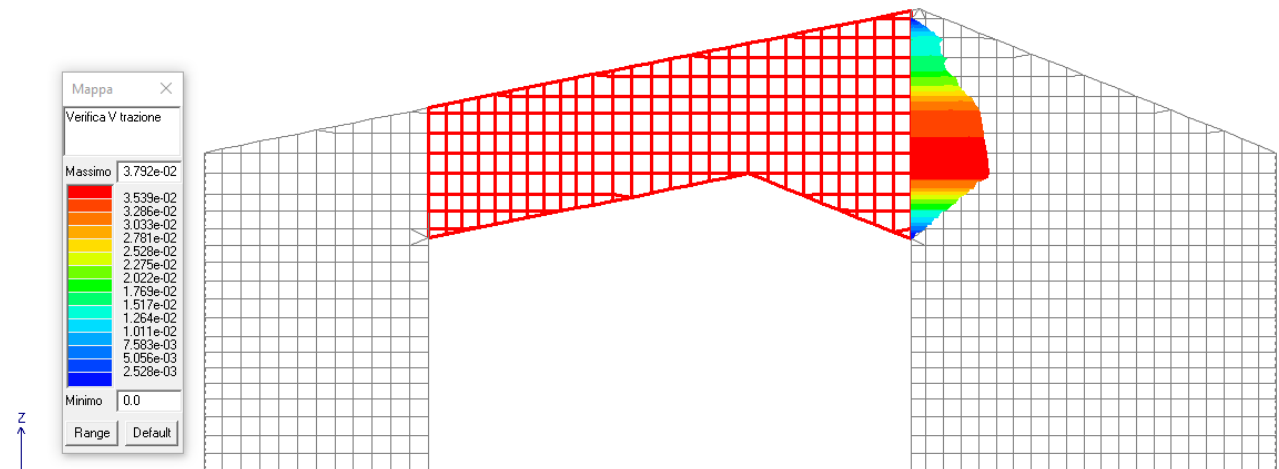


Fig 88. SLU: Mappa di verifica V trazione – Verifiche soddisfatte ($\rho \leq 1$).

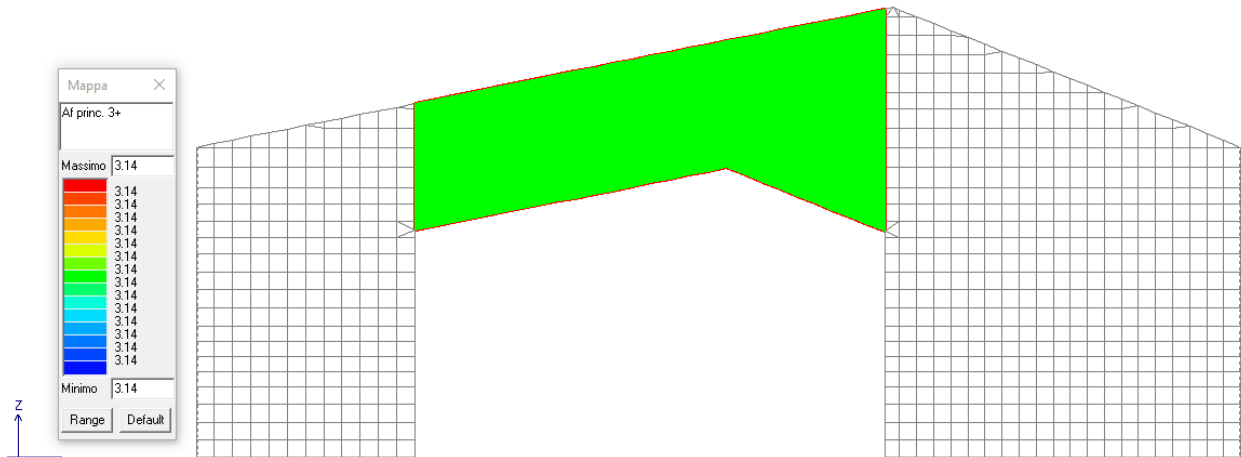


Fig 89. Mappa Armatura Verticale (singolo strato) da Calcolo [cm²/m].

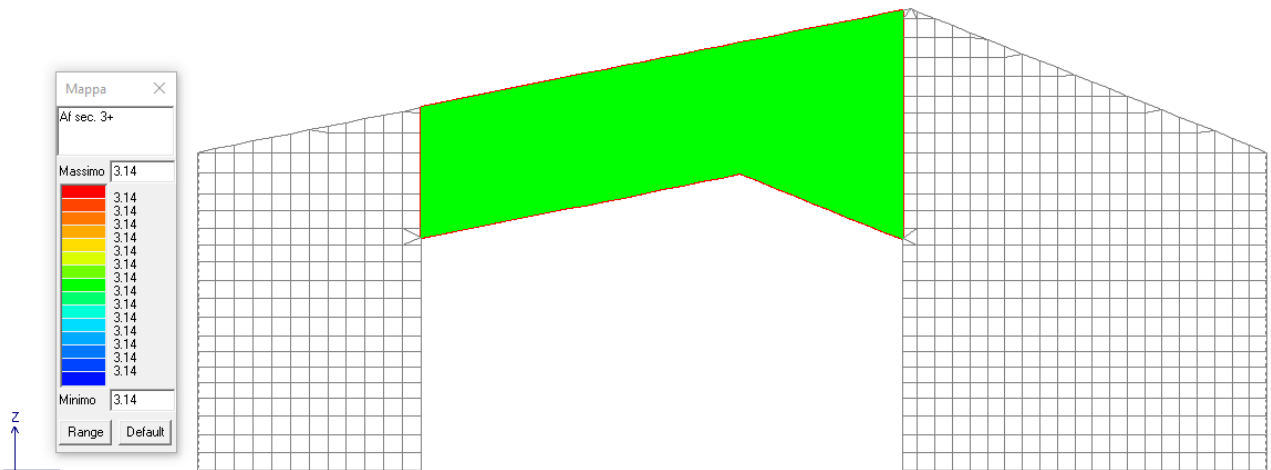


Fig 90. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm²/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 33 | 292.45 | 12.00 | 620.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|-----------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 297.1 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 298.7 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 6.91e-03 | 0.0 | 2.79e-03 | 1.33e-03 | 0.0 |
| 303.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 9.10e-03 | 0.0 | 3.67e-03 | 1.75e-03 | 0.0 |
| 306.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 7.37e-03 | 3.50e-03 | 0.0 |
| 307.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.01 | 5.06e-03 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.01 | 6.67e-03 | 0.0 |
| 311.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.01 | 6.72e-03 | 0.0 |
| 315.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.02 | 8.39e-03 | 0.0 |
| 315.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.02 | 0.01 | 0.0 |
| 320.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.02 | 0.01 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| 324.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.02 | 0.01 | 0.0 |
| 324.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.03 | 0.01 | 0.0 |
| 328.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.03 | 0.01 | 0.0 |
| 332.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.03 | 0.02 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.03 | 0.02 | 0.0 |
| 334.1 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.04 | 0.02 | 0.0 |
| 336.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.04 | 0.02 | 0.0 |
| 341.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.04 | 0.02 | 0.0 |
| 343.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.05 | 0.02 | 0.0 |
| 346.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.12 | 0.0 | 0.05 | 0.02 | 0.0 |
| 351.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.12 | 0.0 | 0.05 | 0.02 | 0.0 |
| 352.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.05 | 0.02 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.14 | 0.0 | 0.06 | 0.03 | 0.0 |
| 356.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.14 | 0.0 | 0.06 | 0.03 | 0.0 |
| 361.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.15 | 0.0 | 0.06 | 0.03 | 0.0 |
| 361.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.16 | 0.0 | 0.06 | 0.03 | 0.0 |
| 366.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.16 | 0.0 | 0.06 | 0.03 | 0.0 |
| 371.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.17 | 0.0 | 0.07 | 0.03 | 0.0 |
| 371.1 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.18 | 0.0 | 0.07 | 0.03 | 0.0 |
| 376.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.20 | 0.0 | 0.08 | 0.04 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.20 | 0.0 | 0.08 | 0.04 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.19 | 0.0 | 0.08 | 0.04 | 0.0 |
| 433.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.18 | 0.0 | 0.07 | 0.04 | 0.0 |
| 458.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.18 | 0.0 | 0.07 | 0.03 | 0.0 |
| 465.5 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.17 | 0.0 | 0.07 | 0.03 | 0.0 |
| 470.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.16 | 0.0 | 0.07 | 0.03 | 0.0 |
| 474.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.16 | 0.0 | 0.06 | 0.03 | 0.0 |
| 478.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.15 | 0.0 | 0.06 | 0.03 | 0.0 |
| 480.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.15 | 0.0 | 0.06 | 0.03 | 0.0 |
| 482.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.14 | 0.0 | 0.06 | 0.03 | 0.0 |
| 486.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.05 | 0.03 | 0.0 |
| 491.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.12 | 0.0 | 0.05 | 0.02 | 0.0 |
| 495.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.12 | 0.0 | 0.05 | 0.02 | 0.0 |
| 499.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.05 | 0.02 | 0.0 |
| 503.7 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.05 | 0.02 | 0.0 |
| 505.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.04 | 0.02 | 0.0 |
| 507.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.04 | 0.02 | 0.0 |
| 512.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.04 | 0.02 | 0.0 |
| 517.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.03 | 0.02 | 0.0 |
| 522.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.03 | 0.02 | 0.0 |
| 527.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.04 | 0.02 | 0.0 |
| 530.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.03 | 0.02 | 0.0 |
| 532.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.03 | 0.01 | 0.0 |
| 537.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.03 | 0.01 | 0.0 |
| 542.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.03 | 0.01 | 0.0 |
| 547.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.03 | 0.01 | 0.0 |
| 552.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.03 | 0.02 | 0.0 |
| 555.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.03 | 0.01 | 0.0 |
| 557.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.03 | 0.01 | 0.0 |
| 562.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.02 | 0.01 | 0.0 |
| 566.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.02 | 8.31e-03 | 0.0 |
| 571.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.01 | 5.61e-03 | 0.0 |
| 575.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 8.04e-03 | 3.82e-03 | 0.0 |
| 580.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 585.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 589.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | | | |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.20 | 0.0 | 0.08 | 0.04 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|--------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 297.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 298.7 | 0.0 | 0.0 | 6.587e+04 | 0.0 | 0.0 | 0.0 | 212.50 | 212.50 |
| 303.2 | 0.0 | 0.0 | 8.675e+04 | 0.0 | 0.0 | 0.0 | 279.83 | 279.83 |
| 306.4 | 0.0 | 0.0 | 1.740e+05 | 0.0 | 0.0 | 0.0 | 561.31 | 561.31 |
| 307.4 | 0.0 | 0.0 | 2.514e+05 | 0.0 | 0.0 | 0.0 | 811.04 | 811.04 |
| 311.0 | 0.0 | 0.0 | 3.314e+05 | 0.0 | 0.0 | 0.0 | 1069.08 | 1069.08 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| 311.6 | 0.0 | 0.0 | 3.338e+05 | 0.0 | 0.0 | 0.0 | 1076.76 | 1076.76 |
| 315.6 | 0.0 | 0.0 | 4.166e+05 | 0.0 | 0.0 | 0.0 | 1343.90 | 1343.90 |
| 315.8 | 0.0 | 0.0 | 4.980e+05 | 0.0 | 0.0 | 0.0 | 1606.61 | 1606.61 |
| 320.0 | 0.0 | 0.0 | 5.118e+05 | 0.0 | 0.0 | 0.0 | 1650.87 | 1650.87 |
| 324.2 | 0.0 | 0.0 | 5.782e+05 | 0.0 | 0.0 | 0.0 | 1865.21 | 1865.21 |
| 324.9 | 0.0 | 0.0 | 6.550e+05 | 0.0 | 0.0 | 0.0 | 2112.78 | 2112.78 |
| 328.4 | 0.0 | 0.0 | 6.658e+05 | 0.0 | 0.0 | 0.0 | 2147.79 | 2147.79 |
| 332.6 | 0.0 | 0.0 | 7.551e+05 | 0.0 | 0.0 | 0.0 | 2435.67 | 2435.67 |
| 333.0 | 0.0 | 0.0 | 7.994e+05 | 0.0 | 0.0 | 0.0 | 2578.60 | 2578.60 |
| 334.1 | 0.0 | 0.0 | 8.645e+05 | 0.0 | 0.0 | 0.0 | 2788.59 | 2788.59 |
| 336.8 | 0.0 | 0.0 | 9.132e+05 | 0.0 | 0.0 | 0.0 | 2945.76 | 2945.76 |
| 341.0 | 0.0 | 0.0 | 9.670e+05 | 0.0 | 0.0 | 0.0 | 3119.42 | 3119.42 |
| 343.4 | 0.0 | 0.0 | 1.072e+06 | 0.0 | 0.0 | 0.0 | 3456.65 | 3456.65 |
| 346.0 | 0.0 | 0.0 | 1.110e+06 | 0.0 | 0.0 | 0.0 | 3580.02 | 3580.02 |
| 351.0 | 0.0 | 0.0 | 1.163e+06 | 0.0 | 0.0 | 0.0 | 3750.01 | 3750.01 |
| 352.6 | 0.0 | 0.0 | 1.232e+06 | 0.0 | 0.0 | 0.0 | 3972.98 | 3972.98 |
| 355.0 | 0.0 | 0.0 | 1.331e+06 | 0.0 | 0.0 | 0.0 | 4293.75 | 4293.75 |
| 356.0 | 0.0 | 0.0 | 1.349e+06 | 0.0 | 0.0 | 0.0 | 4350.57 | 4350.57 |
| 361.0 | 0.0 | 0.0 | 1.428e+06 | 0.0 | 0.0 | 0.0 | 4607.59 | 4607.59 |
| 361.9 | 0.0 | 0.0 | 1.521e+06 | 0.0 | 0.0 | 0.0 | 4908.05 | 4908.05 |
| 366.0 | 0.0 | 0.0 | 1.524e+06 | 0.0 | 0.0 | 0.0 | 4917.02 | 4917.02 |
| 371.0 | 0.0 | 0.0 | 1.616e+06 | 0.0 | 0.0 | 0.0 | 5213.29 | 5213.29 |
| 371.1 | 0.0 | 0.0 | 1.702e+06 | 0.0 | 0.0 | 0.0 | 5490.41 | 5490.41 |
| 376.0 | 0.0 | 0.0 | 1.872e+06 | 0.0 | 0.0 | 0.0 | 6037.70 | 6037.70 |
| 381.0 | 0.0 | 0.0 | 1.884e+06 | 0.0 | 0.0 | 0.0 | 6075.85 | 6075.85 |
| 408.0 | 0.0 | 0.0 | 1.829e+06 | 0.0 | 0.0 | 0.0 | 5901.25 | 5901.25 |
| 433.0 | 0.0 | 0.0 | 1.742e+06 | 0.0 | 0.0 | 0.0 | 5618.30 | 5618.30 |
| 458.0 | 0.0 | 0.0 | 1.676e+06 | 0.0 | 0.0 | 0.0 | 5406.33 | 5406.33 |
| 465.5 | 0.0 | 0.0 | 1.606e+06 | 0.0 | 0.0 | 0.0 | 5181.85 | 5181.85 |
| 470.0 | 0.0 | 0.0 | 1.536e+06 | 0.0 | 0.0 | 0.0 | 4953.92 | 4953.92 |
| 474.2 | 0.0 | 0.0 | 1.502e+06 | 0.0 | 0.0 | 0.0 | 4843.97 | 4843.97 |
| 478.4 | 0.0 | 0.0 | 1.444e+06 | 0.0 | 0.0 | 0.0 | 4658.07 | 4658.07 |
| 480.4 | 0.0 | 0.0 | 1.383e+06 | 0.0 | 0.0 | 0.0 | 4461.12 | 4461.12 |
| 482.6 | 0.0 | 0.0 | 1.318e+06 | 0.0 | 0.0 | 0.0 | 4253.13 | 4253.13 |
| 486.8 | 0.0 | 0.0 | 1.254e+06 | 0.0 | 0.0 | 0.0 | 4044.33 | 4044.33 |
| 491.0 | 0.0 | 0.0 | 1.191e+06 | 0.0 | 0.0 | 0.0 | 3840.42 | 3840.42 |
| 495.2 | 0.0 | 0.0 | 1.125e+06 | 0.0 | 0.0 | 0.0 | 3627.57 | 3627.57 |
| 499.4 | 0.0 | 0.0 | 1.095e+06 | 0.0 | 0.0 | 0.0 | 3530.90 | 3530.90 |
| 503.7 | 0.0 | 0.0 | 1.077e+06 | 0.0 | 0.0 | 0.0 | 3474.11 | 3474.11 |
| 505.4 | 0.0 | 0.0 | 9.992e+05 | 0.0 | 0.0 | 0.0 | 3223.08 | 3223.08 |
| 507.9 | 0.0 | 0.0 | 9.364e+05 | 0.0 | 0.0 | 0.0 | 3020.77 | 3020.77 |
| 512.9 | 0.0 | 0.0 | 8.777e+05 | 0.0 | 0.0 | 0.0 | 2831.18 | 2831.18 |
| 517.9 | 0.0 | 0.0 | 8.058e+05 | 0.0 | 0.0 | 0.0 | 2599.37 | 2599.37 |
| 522.9 | 0.0 | 0.0 | 7.750e+05 | 0.0 | 0.0 | 0.0 | 2499.98 | 2499.98 |
| 527.9 | 0.0 | 0.0 | 8.624e+05 | 0.0 | 0.0 | 0.0 | 2781.83 | 2781.83 |
| 530.4 | 0.0 | 0.0 | 7.944e+05 | 0.0 | 0.0 | 0.0 | 2562.47 | 2562.47 |
| 532.9 | 0.0 | 0.0 | 7.343e+05 | 0.0 | 0.0 | 0.0 | 2368.80 | 2368.80 |
| 537.9 | 0.0 | 0.0 | 7.135e+05 | 0.0 | 0.0 | 0.0 | 2301.60 | 2301.60 |
| 542.9 | 0.0 | 0.0 | 6.966e+05 | 0.0 | 0.0 | 0.0 | 2247.07 | 2247.07 |
| 547.9 | 0.0 | 0.0 | 6.889e+05 | 0.0 | 0.0 | 0.0 | 2222.27 | 2222.27 |
| 552.8 | 0.0 | 0.0 | 7.602e+05 | 0.0 | 0.0 | 0.0 | 2452.41 | 2452.41 |
| 555.4 | 0.0 | 0.0 | 6.884e+05 | 0.0 | 0.0 | 0.0 | 2220.71 | 2220.71 |
| 557.4 | 0.0 | 0.0 | 6.239e+05 | 0.0 | 0.0 | 0.0 | 2012.58 | 2012.58 |
| 562.0 | 0.0 | 0.0 | 5.306e+05 | 0.0 | 0.0 | 0.0 | 1711.52 | 1711.52 |
| 566.6 | 0.0 | 0.0 | 4.127e+05 | 0.0 | 0.0 | 0.0 | 1331.16 | 1331.16 |
| 571.2 | 0.0 | 0.0 | 2.787e+05 | 0.0 | 0.0 | 0.0 | 898.93 | 898.93 |
| 575.8 | 0.0 | 0.0 | 1.900e+05 | 0.0 | 0.0 | 0.0 | 612.83 | 612.83 |
| 580.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 585.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 589.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 297.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 298.7 | 2.50 | 212.50 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 303.2 | 2.50 | 279.83 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 306.4 | 2.50 | 561.31 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 307.4 | 2.50 | 811.04 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 311.0 | 2.50 | 1069.08 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 311.6 | 2.50 | 1076.76 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 315.6 | 2.50 | 1343.90 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| 315.8 | 2.50 | 1606.61 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 320.0 | 2.50 | 1650.87 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 324.2 | 2.50 | 1865.21 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 324.9 | 2.50 | 2112.78 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 328.4 | 2.50 | 2147.79 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 332.6 | 2.50 | 2435.67 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 333.0 | 2.50 | 2578.60 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 334.1 | 2.50 | 2788.59 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 336.8 | 2.50 | 2945.76 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 341.0 | 2.50 | 3119.42 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 343.4 | 2.50 | 3456.65 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 346.0 | 2.50 | 3580.02 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 351.0 | 2.50 | 3750.01 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 352.6 | 2.50 | 3972.98 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 355.0 | 2.50 | 4293.75 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 356.0 | 2.50 | 4350.57 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 361.0 | 2.50 | 4607.59 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 361.9 | 2.50 | 4908.05 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 366.0 | 2.50 | 4917.02 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 371.0 | 2.50 | 5213.29 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 371.1 | 2.50 | 5490.41 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 376.0 | 2.50 | 6037.70 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 381.0 | 2.50 | 6075.85 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 408.0 | 2.50 | 5901.25 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 433.0 | 2.50 | 5618.30 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 458.0 | 2.50 | 5406.33 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 465.5 | 2.50 | 5181.85 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 470.0 | 2.50 | 4953.92 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 474.2 | 2.50 | 4843.97 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 478.4 | 2.50 | 4658.07 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 480.4 | 2.50 | 4461.12 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 482.6 | 2.50 | 4253.13 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 486.8 | 2.50 | 4044.33 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 491.0 | 2.50 | 3840.42 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 495.2 | 2.50 | 3627.57 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 499.4 | 2.50 | 3530.90 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 503.7 | 2.50 | 3474.11 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 505.4 | 2.50 | 3223.08 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 507.9 | 2.50 | 3020.77 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 512.9 | 2.50 | 2831.18 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 517.9 | 2.50 | 2599.37 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 522.9 | 2.50 | 2499.98 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 527.9 | 2.50 | 2781.83 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 530.4 | 2.50 | 2562.47 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 532.9 | 2.50 | 2368.80 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 537.9 | 2.50 | 2301.60 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 542.9 | 2.50 | 2247.07 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 547.9 | 2.50 | 2222.27 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 552.8 | 2.50 | 2452.41 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 555.4 | 2.50 | 2220.71 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 557.4 | 2.50 | 2012.58 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 562.0 | 2.50 | 1711.52 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 566.6 | 2.50 | 1331.16 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 571.2 | 2.50 | 898.93 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 575.8 | 2.50 | 612.83 | 7.618e+04 | 2.50 | 1.602e+05 | 7.618e+04 |
| 580.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 585.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 589.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

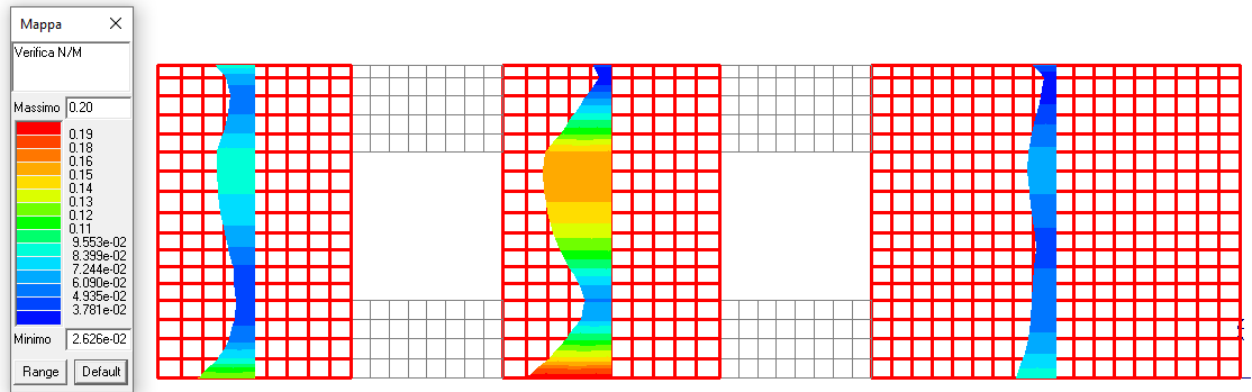


Fig 93. SLU: Mappa di verifica N/M – **Verifiche soddisfatte ($\rho \leq 1$).**

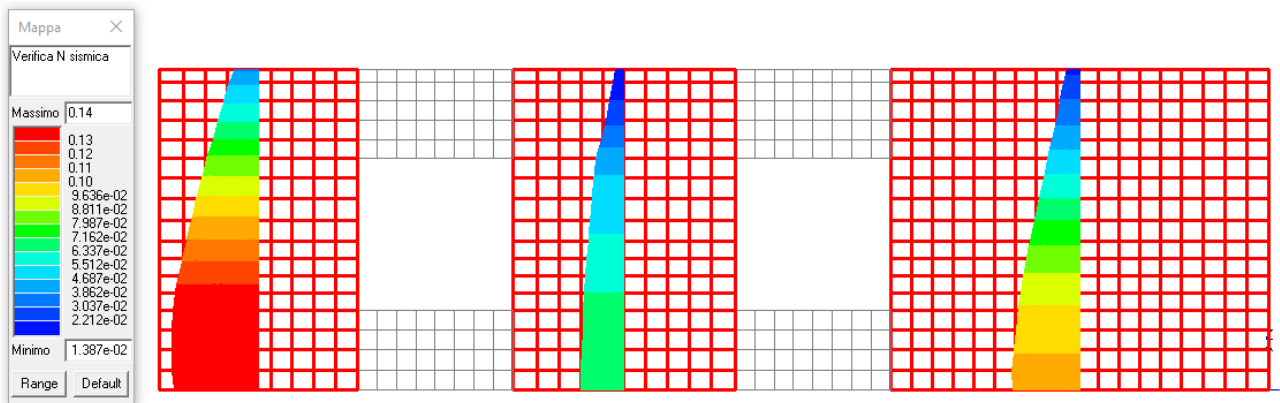


Fig 94. SLU: Mappa di verifica Nsismica – **Verifiche soddisfatte ($\rho \leq 0.625$).**

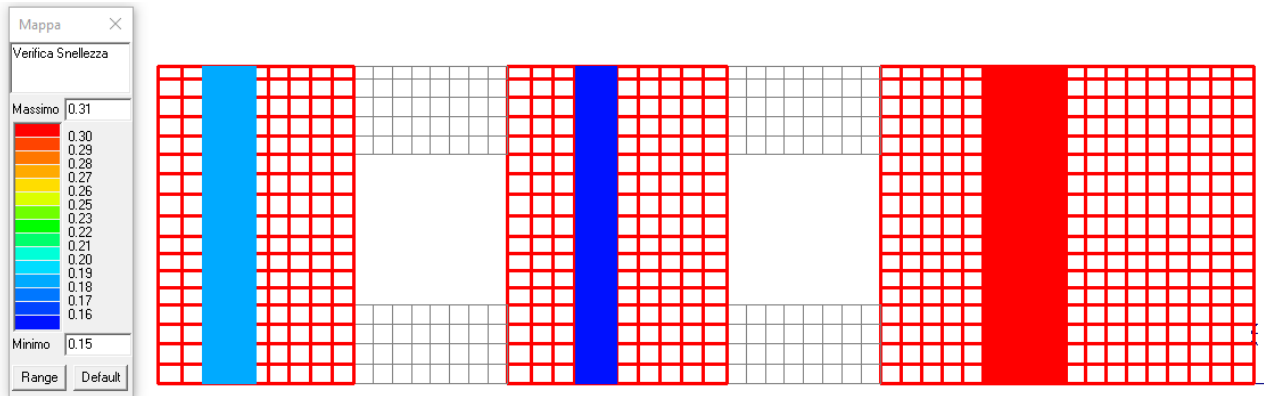


Fig 95. SLU: Mappa di Verifica Snellezza – **Verifiche soddisfatte ($\rho \leq 1$).**

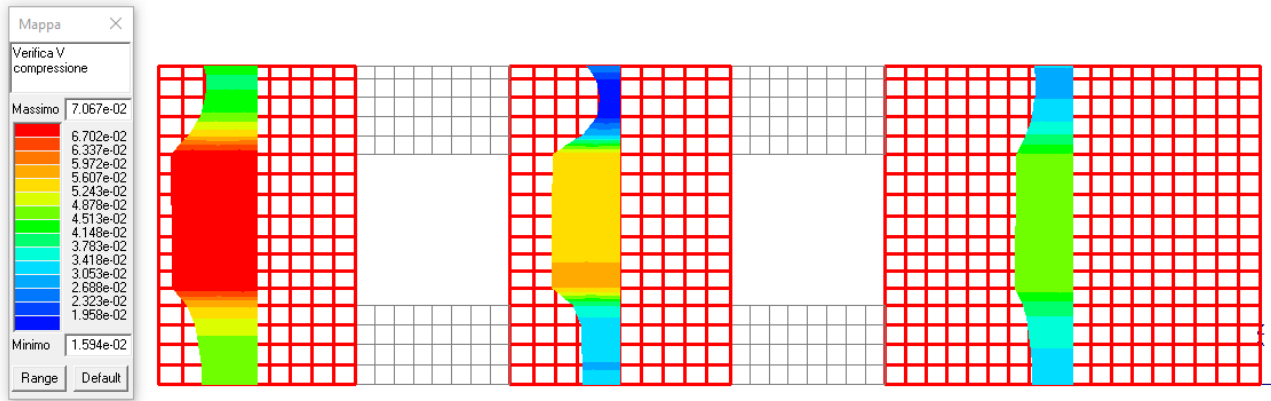


Fig 96. SLU: Mappa di Verifica V compressione – **Verifica soddisfatta ($\rho \leq 1$).**

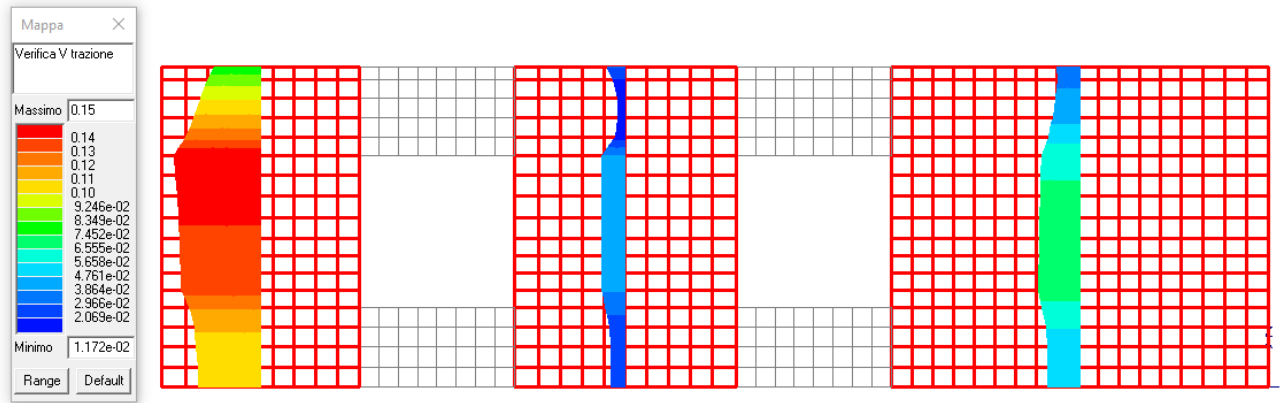


Fig 97. SLU: Mappa di verifica V trazione – **Verifiche soddisfatte ($\rho \leq 1$).**

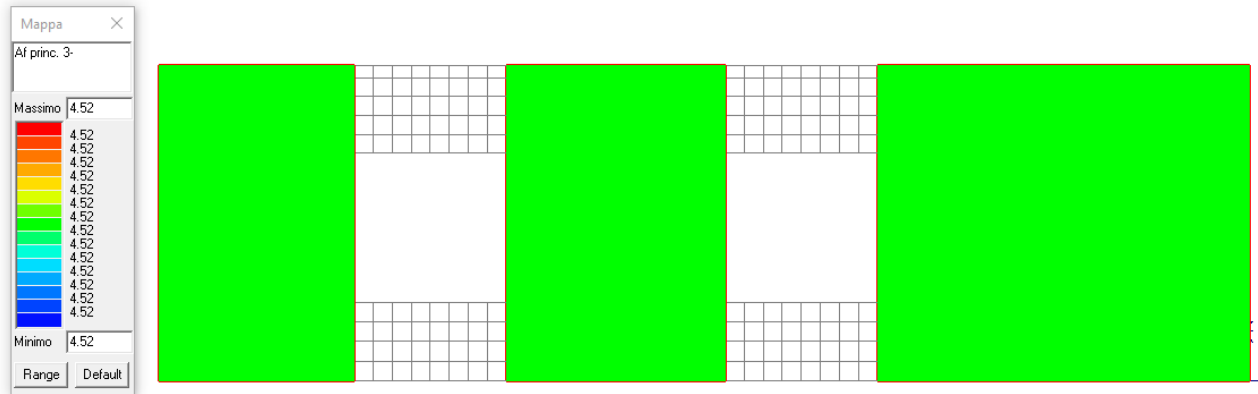


Fig 98. Mappa Armatura Verticale (singolo strato) da Calcolo [cm²/m].

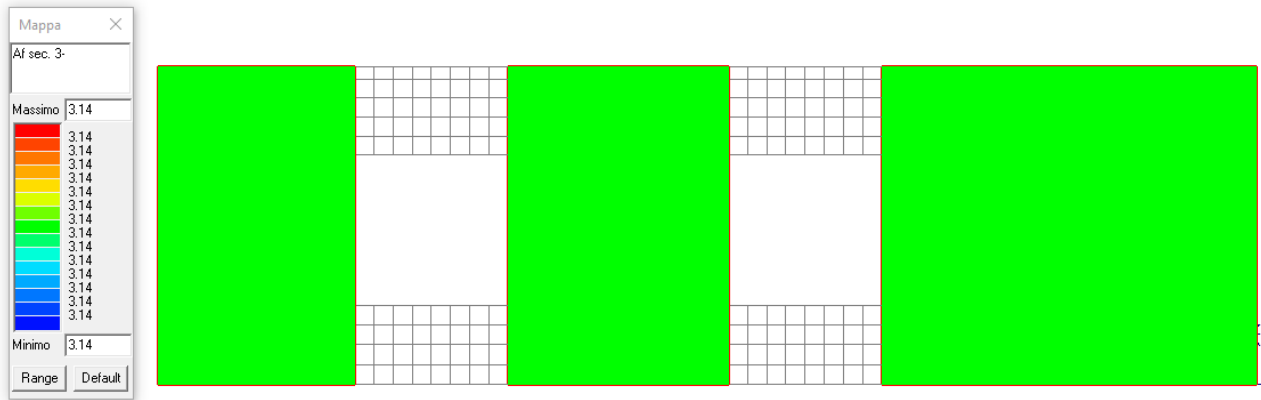


Fig 99. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm²/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 90 | 370.00 | 12.00 | 228.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.13 | 0.19 | 0.05 | 0.11 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.09 | 0.19 | 0.05 | 0.11 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.06 | 0.19 | 0.05 | 0.11 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.05 | 0.19 | 0.05 | 0.11 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.04 | 0.19 | 0.06 | 0.12 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.05 | 0.19 | 0.07 | 0.13 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.05 | 0.19 | 0.07 | 0.13 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.06 | 0.19 | 0.07 | 0.14 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.07 | 0.19 | 0.07 | 0.14 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.08 | 0.19 | 0.07 | 0.14 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.08 | 0.19 | 0.07 | 0.14 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.09 | 0.19 | 0.07 | 0.14 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.09 | 0.19 | 0.07 | 0.15 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.07 | 0.19 | 0.06 | 0.13 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.06 | 0.19 | 0.05 | 0.11 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.05 | 0.19 | 0.04 | 0.10 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.07 | 0.19 | 0.04 | 0.09 | 0.0 |
| 370.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.09 | 0.19 | 0.04 | 0.08 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.14 | 0.13 | 0.19 | 0.07 | 0.15 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|------------|------------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1.284e+04 | -1.206e+04 | 7.904e+04 | 3.738e+04 | -8135.15 | -8829.21 | 3552.69 | 2350.48 |
| 23.0 | -1.317e+04 | -1.238e+04 | 9.234e+04 | 2.406e+04 | -8135.15 | -9014.25 | 3551.94 | 2348.62 |
| 46.0 | -1.331e+04 | -9525.86 | 9.972e+04 | 1.506e+04 | -8135.15 | -9189.22 | 3750.25 | 2412.28 |
| 69.0 | -1.323e+04 | -8186.52 | 2.268e+05 | 5131.56 | -8135.15 | -9236.80 | 3956.73 | 2476.77 |
| 92.0 | -1.311e+04 | -7253.10 | 2.289e+05 | 329.59 | -8135.15 | -9262.20 | 4475.79 | 2684.34 |
| 112.0 | -1.278e+04 | -6722.85 | 2.485e+05 | 1405.50 | -8135.15 | -9393.67 | 5486.35 | 2964.83 |
| 132.0 | -1.222e+04 | -8143.53 | 6.737e+04 | 1.272e+04 | -8135.15 | -8842.47 | 5478.56 | 2986.64 |
| 152.0 | -1.162e+04 | -1.085e+04 | 1.265e+05 | 1.551e+04 | -8135.15 | -8258.70 | 5469.23 | 3010.03 |
| 172.0 | -1.099e+04 | -1.025e+04 | 1.393e+05 | 1.810e+04 | -8135.15 | -7764.74 | 5461.30 | 3038.27 |
| 196.0 | -1.028e+04 | -9566.60 | 1.576e+05 | 2.031e+04 | -8135.15 | -7070.39 | 5455.46 | 3075.53 |
| 220.0 | -9476.09 | -8803.41 | 1.703e+05 | 2.160e+04 | -8135.15 | -6329.76 | 5456.79 | 3126.33 |
| 244.0 | -8641.37 | -8010.40 | 1.810e+05 | 2.196e+04 | -8135.15 | -5573.16 | 5469.36 | 3188.25 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|-----------|----------|----------|----------|----------|
| 267.0 | -7869.69 | -7211.21 | 1.892e+05 | 2.142e+04 | -8135.15 | -4825.90 | 5494.21 | 3258.92 |
| 289.0 | -6959.60 | -6319.68 | 2.049e+05 | 1.635e+04 | -8135.15 | -4481.03 | 4334.72 | 2799.60 |
| 311.0 | -6102.26 | -5443.65 | 2.121e+05 | 1.193e+04 | -8135.15 | -3975.24 | 3581.99 | 2509.63 |
| 333.0 | -5258.84 | -5043.81 | 2.330e+05 | 8020.10 | -8135.15 | -3318.98 | 3248.43 | 2246.65 |
| 355.0 | -4419.20 | -4178.61 | 1.773e+05 | 1.420e+04 | -8135.15 | -2840.13 | 3159.58 | 1979.83 |
| 370.0 | -3654.28 | -3493.14 | 1.448e+05 | 2.171e+04 | -8135.15 | -2350.68 | 3330.98 | 1712.50 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 3552.69 | 7.854e+04 | 1.00 | 2.228e+04 | 7.931e+04 |
| 23.0 | 1.00 | 3551.94 | 7.858e+04 | 1.00 | 2.228e+04 | 7.938e+04 |
| 46.0 | 1.00 | 3750.25 | 7.861e+04 | 1.00 | 2.228e+04 | 7.941e+04 |
| 69.0 | 1.00 | 3956.73 | 7.862e+04 | 1.00 | 2.228e+04 | 7.940e+04 |
| 92.0 | 1.00 | 4475.79 | 7.862e+04 | 1.00 | 2.228e+04 | 7.938e+04 |
| 112.0 | 1.00 | 5486.35 | 7.865e+04 | 1.00 | 2.228e+04 | 7.932e+04 |
| 132.0 | 1.00 | 5478.56 | 7.854e+04 | 1.00 | 2.228e+04 | 7.921e+04 |
| 152.0 | 1.00 | 5469.23 | 7.843e+04 | 1.00 | 2.228e+04 | 7.909e+04 |
| 172.0 | 1.00 | 5461.30 | 7.833e+04 | 1.00 | 2.228e+04 | 7.897e+04 |
| 196.0 | 1.00 | 5455.46 | 7.819e+04 | 1.00 | 2.228e+04 | 7.882e+04 |
| 220.0 | 1.00 | 5456.79 | 7.804e+04 | 1.00 | 2.228e+04 | 7.867e+04 |
| 244.0 | 1.00 | 5469.36 | 7.789e+04 | 1.00 | 2.228e+04 | 7.850e+04 |
| 267.0 | 1.00 | 5494.21 | 7.774e+04 | 1.00 | 2.228e+04 | 7.834e+04 |
| 289.0 | 1.00 | 4334.72 | 7.768e+04 | 1.00 | 2.228e+04 | 7.816e+04 |
| 311.0 | 1.00 | 3581.99 | 7.758e+04 | 1.00 | 2.228e+04 | 7.799e+04 |
| 333.0 | 1.00 | 3248.43 | 7.745e+04 | 1.00 | 2.228e+04 | 7.782e+04 |
| 355.0 | 1.00 | 3159.58 | 7.735e+04 | 1.00 | 2.228e+04 | 7.765e+04 |
| 370.0 | 1.00 | 3330.98 | 7.725e+04 | 1.00 | 2.228e+04 | 7.749e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 93 | 370.00 | 12.00 | 256.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.20 | 0.15 | 0.03 | 0.02 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.15 | 0.15 | 0.03 | 0.02 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.11 | 0.15 | 0.03 | 0.02 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.07 | 0.15 | 0.03 | 0.03 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.06 | 0.15 | 0.04 | 0.03 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.07 | 0.15 | 0.06 | 0.04 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.10 | 0.15 | 0.06 | 0.04 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.12 | 0.15 | 0.06 | 0.04 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.14 | 0.15 | 0.06 | 0.04 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.15 | 0.15 | 0.06 | 0.04 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.16 | 0.15 | 0.06 | 0.04 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.16 | 0.15 | 0.06 | 0.04 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.16 | 0.15 | 0.06 | 0.04 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.12 | 0.15 | 0.03 | 0.02 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.09 | 0.15 | 0.02 | 0.01 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.06 | 0.15 | 0.02 | 0.01 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.03 | 0.15 | 0.02 | 0.02 | 0.0 |
| 370.0 | 1d12 | 1d12/25 | 1d10/25 | 0.01 | 0.04 | 0.15 | 0.03 | 0.03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.07 | 0.20 | 0.15 | 0.06 | 0.04 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|-----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -7411.67 | -5357.87 | 6719.09 | 5.238e+04 | -4425.50 | -5432.69 | 2524.51 | 585.39 |
| 23.0 | -7471.65 | -5536.80 | 1.388e+05 | 3.787e+04 | -4425.50 | -5495.45 | 2515.73 | 589.62 |
| 46.0 | -7249.65 | -5355.00 | 1.505e+05 | 2.699e+04 | -4425.50 | -5340.23 | 2551.41 | 576.04 |
| 69.0 | -7097.31 | -5224.30 | 1.651e+05 | 1.753e+04 | -4425.50 | -5235.95 | 2618.09 | 598.56 |
| 92.0 | -7029.14 | -5182.88 | 3.369e+05 | 906.94 | -4425.50 | -5182.88 | 3162.28 | 781.51 |
| 112.0 | -6883.37 | -6883.37 | 3.190e+04 | 2.011e+04 | -4425.50 | -5098.06 | 4634.27 | 935.94 |
| 132.0 | -6615.79 | -5136.38 | 2.393e+04 | 2.610e+04 | -4425.50 | -4902.83 | 4623.02 | 935.94 |
| 152.0 | -6348.22 | -4930.56 | 1.792e+04 | 3.140e+04 | -4425.50 | -4696.15 | 4612.03 | 935.94 |
| 172.0 | -6080.65 | -4724.74 | 1.191e+04 | 3.537e+04 | -4425.50 | -4489.87 | 4599.99 | 935.94 |
| 196.0 | -5786.32 | -3916.37 | 9638.18 | 3.817e+04 | -4425.50 | -4280.24 | 4584.97 | 935.94 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|-----------|----------|----------|----------|----------|
| 220.0 | -5465.24 | -3727.96 | 9691.24 | 4.031e+04 | -4425.50 | -3995.64 | 4565.88 | 935.94 |
| 244.0 | -5144.15 | -3480.98 | 8998.15 | 4.071e+04 | -4425.50 | -3730.82 | 4544.05 | 935.94 |
| 267.0 | -4829.76 | -3239.13 | 8334.63 | 3.944e+04 | -4425.50 | -3552.38 | 4520.49 | 935.94 |
| 289.0 | -3811.16 | -3298.09 | 1.651e+04 | 2.971e+04 | -4425.50 | -2784.77 | 2543.13 | 399.57 |
| 311.0 | -3112.81 | -1899.61 | 1.552e+04 | 2.160e+04 | -4425.50 | -2253.33 | 1514.52 | 276.98 |
| 333.0 | -2457.60 | -1439.63 | 4244.96 | 1.399e+04 | -4425.50 | -1607.89 | 1302.68 | 278.22 |
| 355.0 | -1871.43 | -944.70 | 1.785e+04 | 6343.24 | -4425.50 | -1156.17 | 1622.73 | 494.52 |
| 370.0 | -1502.92 | -1502.92 | 4485.48 | 1.009e+04 | -4425.50 | -871.03 | 2231.27 | 728.76 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 2524.51 | 8.246e+04 | 1.00 | 2.363e+04 | 8.279e+04 |
| 23.0 | 1.00 | 2515.73 | 8.248e+04 | 1.00 | 2.363e+04 | 8.281e+04 |
| 46.0 | 1.00 | 2551.41 | 8.245e+04 | 1.00 | 2.363e+04 | 8.276e+04 |
| 69.0 | 1.00 | 2618.09 | 8.243e+04 | 1.00 | 2.363e+04 | 8.273e+04 |
| 92.0 | 1.00 | 3162.28 | 8.242e+04 | 1.00 | 2.363e+04 | 8.272e+04 |
| 112.0 | 1.00 | 4634.27 | 8.240e+04 | 1.00 | 2.363e+04 | 8.268e+04 |
| 132.0 | 1.00 | 4623.02 | 8.236e+04 | 1.00 | 2.363e+04 | 8.263e+04 |
| 152.0 | 1.00 | 4612.03 | 8.233e+04 | 1.00 | 2.363e+04 | 8.258e+04 |
| 172.0 | 1.00 | 4599.99 | 8.229e+04 | 1.00 | 2.363e+04 | 8.253e+04 |
| 196.0 | 1.00 | 4584.97 | 8.225e+04 | 1.00 | 2.363e+04 | 8.248e+04 |
| 220.0 | 1.00 | 4565.88 | 8.219e+04 | 1.00 | 2.363e+04 | 8.242e+04 |
| 244.0 | 1.00 | 4544.05 | 8.214e+04 | 1.00 | 2.363e+04 | 8.236e+04 |
| 267.0 | 1.00 | 4520.49 | 8.211e+04 | 1.00 | 2.363e+04 | 8.230e+04 |
| 289.0 | 1.00 | 2543.13 | 8.197e+04 | 1.00 | 2.363e+04 | 8.211e+04 |
| 311.0 | 1.00 | 1514.52 | 8.187e+04 | 1.00 | 2.363e+04 | 8.198e+04 |
| 333.0 | 1.00 | 1302.68 | 8.175e+04 | 1.00 | 2.363e+04 | 8.186e+04 |
| 355.0 | 1.00 | 1622.73 | 8.166e+04 | 1.00 | 2.363e+04 | 8.175e+04 |
| 370.0 | 1.00 | 2231.27 | 8.161e+04 | 1.00 | 2.363e+04 | 8.168e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 96 | 370.00 | 12.00 | 436.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.09 | 0.31 | 0.03 | 0.05 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.08 | 0.31 | 0.03 | 0.05 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.06 | 0.31 | 0.03 | 0.05 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.06 | 0.31 | 0.04 | 0.06 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.05 | 0.31 | 0.04 | 0.06 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.05 | 0.31 | 0.05 | 0.07 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.05 | 0.31 | 0.05 | 0.07 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.05 | 0.31 | 0.05 | 0.07 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.05 | 0.31 | 0.05 | 0.07 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.06 | 0.31 | 0.05 | 0.07 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.06 | 0.31 | 0.05 | 0.07 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.07 | 0.31 | 0.05 | 0.07 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.06 | 0.31 | 0.05 | 0.06 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.05 | 0.31 | 0.04 | 0.05 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.04 | 0.31 | 0.03 | 0.05 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.03 | 0.31 | 0.03 | 0.04 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.03 | 0.31 | 0.03 | 0.04 | 0.0 |
| 370.0 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.05 | 0.31 | 0.03 | 0.04 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.11 | 0.09 | 0.31 | 0.05 | 0.07 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|------------|------------|-----------|-----------|------------|------------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1.961e+04 | -1.917e+04 | 7.210e+05 | 4.350e+04 | -1.142e+04 | -1.279e+04 | 4918.58 | 2264.14 |
| 23.0 | -1.991e+04 | -1.868e+04 | 1.016e+06 | 2.777e+04 | -1.142e+04 | -1.298e+04 | 4923.06 | 2275.62 |
| 46.0 | -1.917e+04 | -1.800e+04 | 9.461e+05 | 1.976e+04 | -1.142e+04 | -1.264e+04 | 5107.75 | 2304.49 |
| 69.0 | -1.855e+04 | -1.514e+04 | 1.054e+06 | 4050.23 | -1.142e+04 | -1.238e+04 | 5363.36 | 2406.49 |
| 92.0 | -1.799e+04 | -1.449e+04 | 9.811e+05 | 4459.87 | -1.142e+04 | -1.217e+04 | 5960.24 | 2699.35 |
| 112.0 | -1.731e+04 | -1.359e+04 | 9.658e+05 | 2688.75 | -1.142e+04 | -1.209e+04 | 6944.60 | 2941.67 |
| 132.0 | -1.646e+04 | -1.299e+04 | 8.852e+05 | 1228.08 | -1.142e+04 | -1.141e+04 | 6922.97 | 2921.42 |
| 152.0 | -1.552e+04 | -1.384e+04 | 2.414e+05 | 2.112e+04 | -1.142e+04 | -1.071e+04 | 6899.21 | 2896.34 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|------------|------------|-----------|-----------|------------|----------|----------|----------|
| 172.0 | -1.448e+04 | -1.301e+04 | 2.323e+05 | 2.245e+04 | -1.142e+04 | -9871.22 | 6872.97 | 2868.45 |
| 196.0 | -1.322e+04 | -1.273e+04 | 3.755e+05 | 2.499e+04 | -1.142e+04 | -8862.03 | 6840.71 | 2836.43 |
| 220.0 | -1.179e+04 | -1.130e+04 | 3.214e+05 | 2.840e+04 | -1.142e+04 | -7733.52 | 6800.43 | 2800.90 |
| 244.0 | -1.049e+04 | -9873.81 | 2.677e+05 | 2.999e+04 | -1.142e+04 | -6550.98 | 6753.97 | 2765.75 |
| 267.0 | -9278.62 | -8546.51 | 2.221e+05 | 2.921e+04 | -1.142e+04 | -5393.92 | 6702.69 | 2733.21 |
| 289.0 | -8002.57 | -5424.37 | 1.598e+05 | 2.414e+04 | -1.142e+04 | -4680.23 | 5601.64 | 2218.38 |
| 311.0 | -6875.91 | -4396.96 | 1.451e+05 | 1.939e+04 | -1.142e+04 | -3858.91 | 4830.58 | 1918.59 |
| 333.0 | -5747.21 | -3428.03 | 1.340e+05 | 1.428e+04 | -1.142e+04 | -3042.67 | 4455.25 | 1707.27 |
| 355.0 | -4605.92 | -4529.93 | 1.652e+05 | 1.107e+04 | -1.142e+04 | -2194.01 | 4336.11 | 1583.23 |
| 370.0 | -3701.72 | -3677.59 | 1.314e+05 | 2.355e+04 | -1.142e+04 | -1937.19 | 4490.11 | 1607.61 |

Macrosetti n. 51, 52, 53, 54, 58 [maschi]

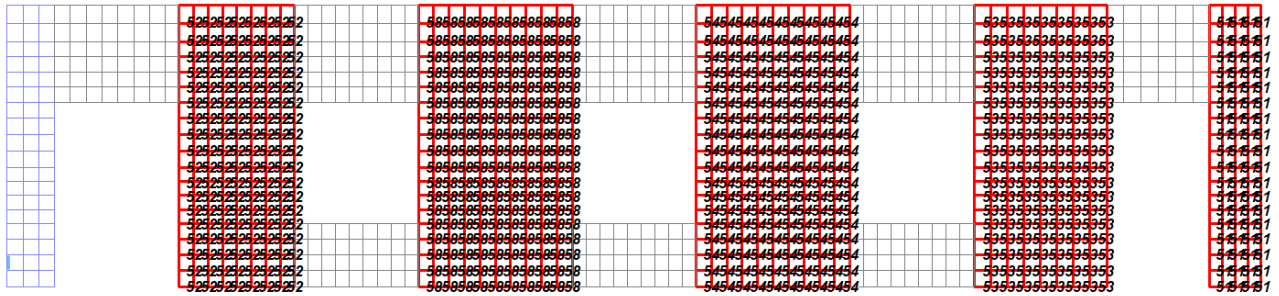


Fig 100. Elementi oggetto di verifica (in rosso).

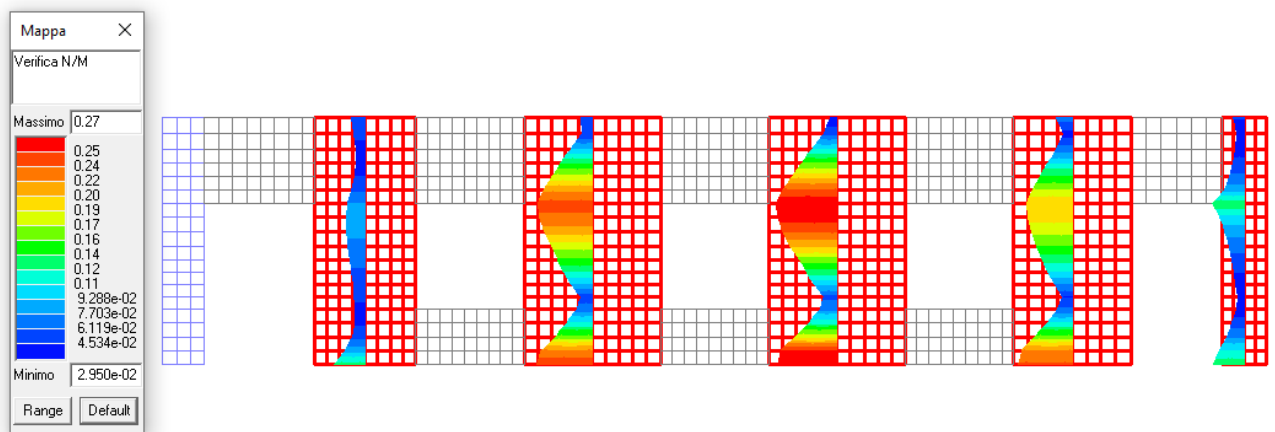


Fig 101. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

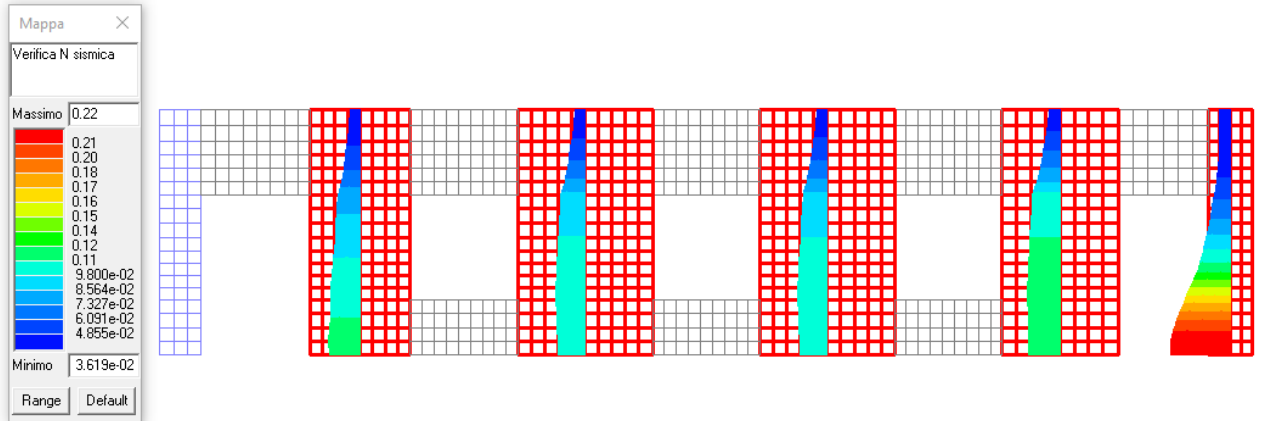


Fig 102. SLU: Mappa di verifica Nsismica – Verifiche soddisfatte ($\rho \leq 0.625$).

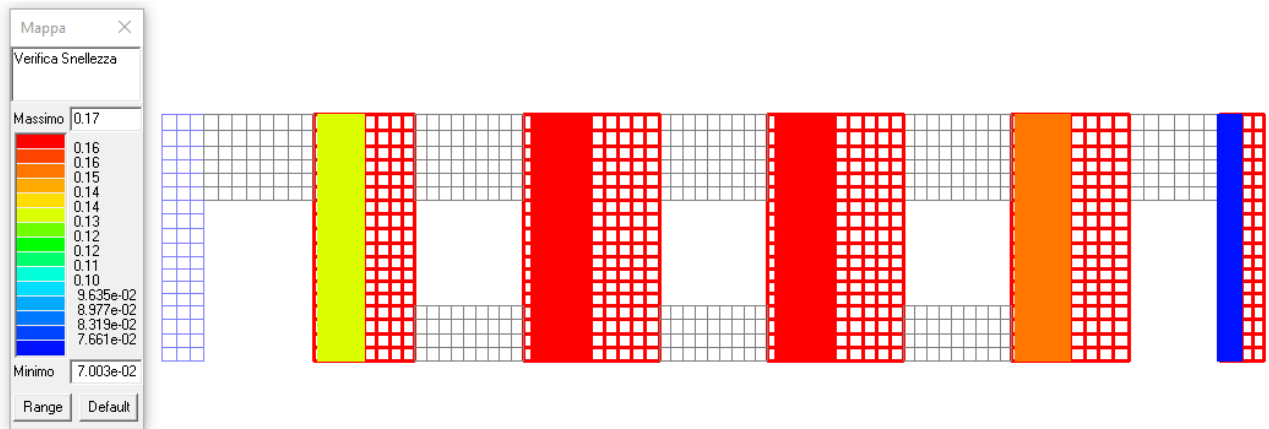


Fig 103. SLU: Mappa di Verifica Snellezza – **Verifiche soddisfatte ($\rho \leq 1$).**

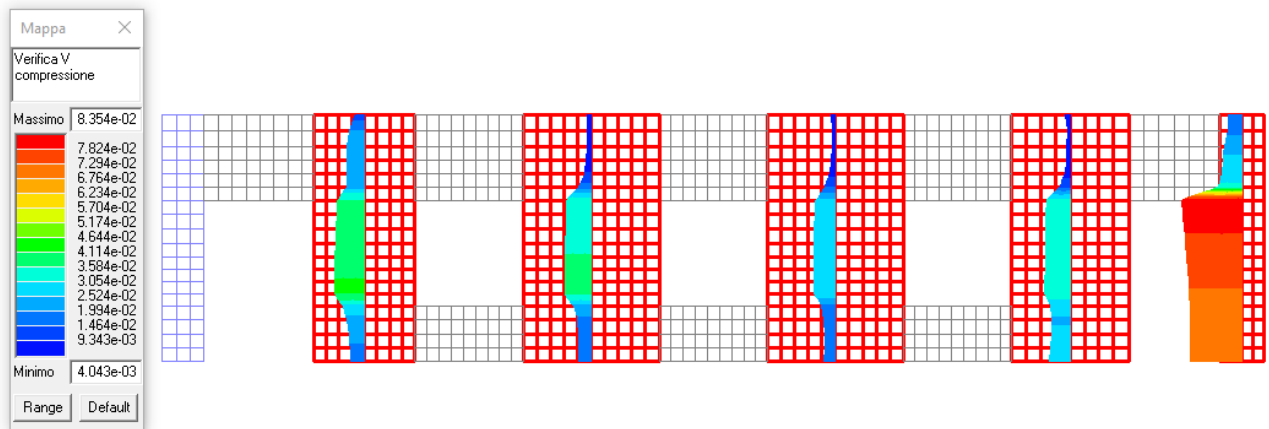


Fig 104. SLU: Mappa di Verifica V compressione – **Verifica soddisfatta ($\rho \leq 1$).**

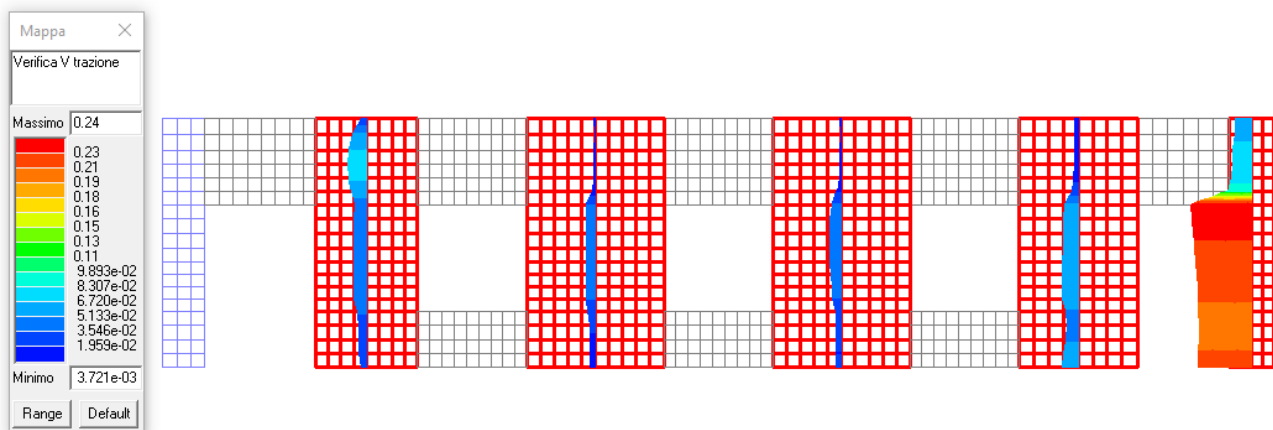


Fig 105. SLU: Mappa di verifica V trazione – **Verifiche soddisfatte ($\rho \leq 1$).**

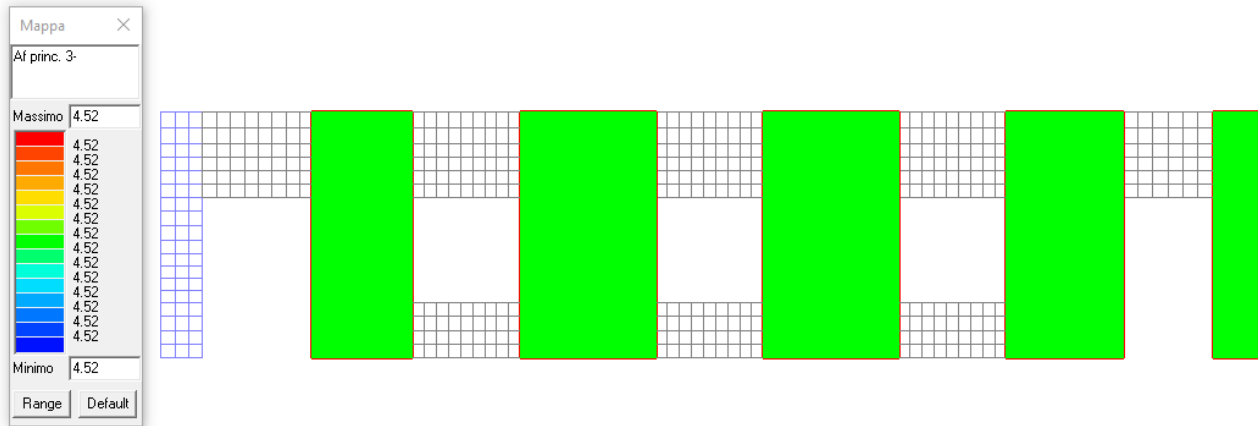


Fig 106. Mappa Armatura Verticale (singolo strato) da Calcolo [cm²/m].

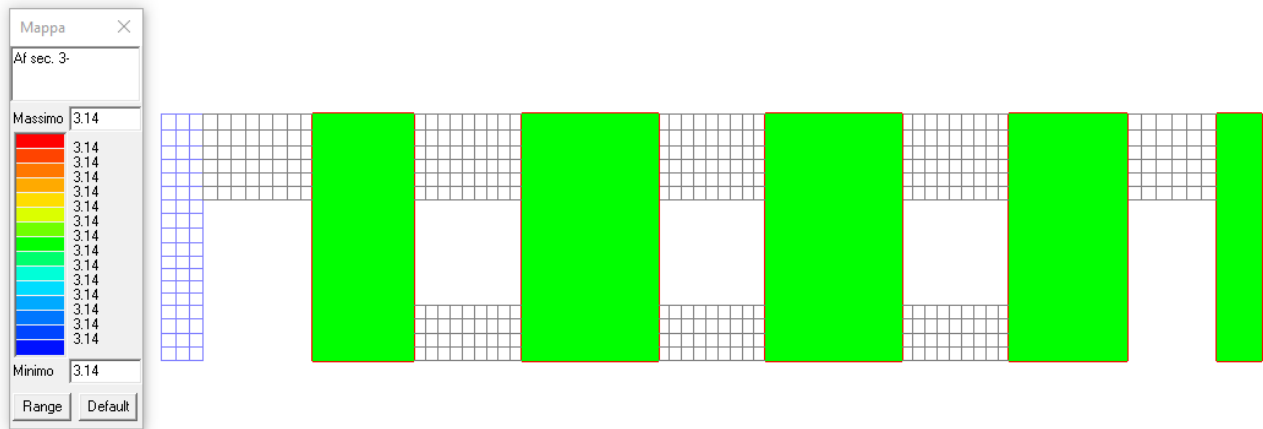


Fig 107. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm²/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 51 | 408.00 | 12.00 | 74.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.14 | 0.07 | 0.07 | 0.21 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.11 | 0.07 | 0.07 | 0.21 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.21 | 0.07 | 0.07 | 0.07 | 0.21 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.06 | 0.07 | 0.07 | 0.21 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.03 | 0.07 | 0.07 | 0.21 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.03 | 0.07 | 0.07 | 0.21 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.04 | 0.07 | 0.07 | 0.21 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.05 | 0.07 | 0.07 | 0.22 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.06 | 0.07 | 0.08 | 0.22 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.07 | 0.07 | 0.08 | 0.22 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.08 | 0.07 | 0.08 | 0.23 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.11 | 0.07 | 0.08 | 0.23 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.14 | 0.07 | 0.08 | 0.24 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.08 | 0.07 | 0.03 | 0.09 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.07 | 0.07 | 0.03 | 0.08 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.05 | 0.07 | 0.03 | 0.08 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.04 | 0.07 | 0.02 | 0.07 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.03 | 0.07 | 0.02 | 0.06 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.05 | 0.07 | 0.02 | 0.06 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.22 | 0.14 | 0.07 | 0.08 | 0.24 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -6988.86 | -4406.63 | 2.758e+04 | 9056.95 | -3343.42 | -6988.86 | 1265.81 | 1033.20 |
| 23.0 | -6988.86 | 14.54 | 2720.79 | 5426.80 | -3343.42 | -6988.86 | 1265.81 | 1033.20 |
| 46.0 | -6501.88 | -558.38 | 1.292e+04 | 3623.85 | -3343.42 | -6501.88 | 1249.48 | 1010.51 |
| 69.0 | -5965.92 | -2889.46 | 2.134e+04 | 950.15 | -3343.42 | -5886.16 | 1255.12 | 1014.18 |
| 92.0 | -5304.11 | -837.82 | 9052.97 | 1266.50 | -3343.42 | -5304.11 | 1260.90 | 1020.48 |
| 112.0 | -4660.12 | -3761.17 | 1.187e+04 | 747.04 | -3343.42 | -4658.59 | 1268.55 | 1029.68 |
| 132.0 | -4058.73 | -3562.27 | 9680.43 | 2167.95 | -3343.42 | -4053.93 | 1277.22 | 1040.22 |
| 152.0 | -3519.89 | -3103.30 | 9756.61 | 2730.06 | -3343.42 | -3460.97 | 1288.45 | 1053.46 |
| 172.0 | -3167.85 | -2646.80 | 9378.70 | 3264.61 | -3343.42 | -2817.29 | 1302.69 | 1069.67 |
| 196.0 | -2796.28 | -2167.77 | 6175.60 | 3980.12 | -3343.42 | -2146.49 | 1321.24 | 1090.23 |
| 220.0 | -2414.30 | -1676.26 | 2505.62 | 4839.41 | -3343.42 | -1452.27 | 1346.07 | 1117.14 |
| 244.0 | -2095.44 | -1216.34 | 2995.80 | 5934.20 | -3343.42 | -756.14 | 1374.40 | 1147.11 |
| 267.0 | -1851.84 | -813.78 | 1.044e+04 | 7281.12 | -3343.42 | -250.39 | 1410.27 | 1181.66 |
| 289.0 | -1599.69 | -105.55 | 8790.89 | 4094.24 | -3343.42 | -105.55 | 552.94 | 451.65 |
| 311.0 | -1395.97 | 81.97 | 4137.55 | 3169.87 | -3343.42 | -1355.07 | 455.67 | 377.11 |
| 333.0 | -1268.32 | 240.16 | 575.79 | 2397.53 | -3343.42 | -1250.18 | 445.61 | 366.97 |
| 355.0 | -1206.01 | 315.73 | 4338.69 | 1869.48 | -3343.42 | -1160.41 | 409.55 | 354.72 |
| 381.0 | -1218.62 | 262.66 | 7224.30 | 1469.88 | -3343.42 | -586.99 | 322.40 | 311.71 |
| 408.0 | -1344.30 | -1344.30 | 9569.00 | 2421.67 | -3343.42 | -191.31 | 303.51 | 302.98 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 1265.81 | 1.778e+04 | 1.00 | 4887.80 | 1.772e+04 |
| 23.0 | 1.00 | 1265.81 | 1.778e+04 | 1.00 | 4887.80 | 1.772e+04 |
| 46.0 | 1.00 | 1249.48 | 1.772e+04 | 1.00 | 4887.80 | 1.766e+04 |
| 69.0 | 1.00 | 1255.12 | 1.763e+04 | 1.00 | 4887.80 | 1.758e+04 |
| 92.0 | 1.00 | 1260.90 | 1.756e+04 | 1.00 | 4887.80 | 1.750e+04 |
| 112.0 | 1.00 | 1268.55 | 1.747e+04 | 1.00 | 4887.80 | 1.742e+04 |
| 132.0 | 1.00 | 1277.22 | 1.739e+04 | 1.00 | 4887.80 | 1.735e+04 |
| 152.0 | 1.00 | 1288.45 | 1.731e+04 | 1.00 | 4887.80 | 1.727e+04 |
| 172.0 | 1.00 | 1302.69 | 1.722e+04 | 1.00 | 4887.80 | 1.721e+04 |
| 196.0 | 1.00 | 1321.24 | 1.713e+04 | 1.00 | 4887.80 | 1.714e+04 |
| 220.0 | 1.00 | 1346.07 | 1.704e+04 | 1.00 | 4887.80 | 1.705e+04 |
| 244.0 | 1.00 | 1374.40 | 1.695e+04 | 1.00 | 4887.80 | 1.697e+04 |
| 267.0 | 1.00 | 1410.27 | 1.688e+04 | 1.00 | 4887.80 | 1.691e+04 |
| 289.0 | 1.00 | 552.94 | 1.686e+04 | 1.00 | 4887.80 | 1.688e+04 |
| 311.0 | 1.00 | 455.67 | 1.703e+04 | 1.00 | 4887.80 | 1.701e+04 |
| 333.0 | 1.00 | 445.61 | 1.701e+04 | 1.00 | 4887.80 | 1.700e+04 |
| 355.0 | 1.00 | 409.55 | 1.700e+04 | 1.00 | 4887.80 | 1.694e+04 |
| 381.0 | 1.00 | 322.40 | 1.693e+04 | 1.00 | 4887.80 | 1.693e+04 |
| 408.0 | 1.00 | 303.51 | 1.687e+04 | 1.00 | 4887.80 | 1.688e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 52 | 408.00 | 12.00 | 167.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.14 | 0.13 | 0.02 | 0.02 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.09 | 0.13 | 0.02 | 0.03 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.06 | 0.13 | 0.02 | 0.03 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.04 | 0.13 | 0.02 | 0.03 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.04 | 0.13 | 0.03 | 0.04 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.05 | 0.13 | 0.04 | 0.05 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.05 | 0.13 | 0.04 | 0.05 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.06 | 0.13 | 0.04 | 0.05 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.07 | 0.13 | 0.04 | 0.05 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.07 | 0.13 | 0.04 | 0.05 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.08 | 0.13 | 0.04 | 0.05 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.08 | 0.13 | 0.04 | 0.05 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.08 | 0.13 | 0.04 | 0.05 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.06 | 0.13 | 0.02 | 0.06 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.05 | 0.13 | 0.02 | 0.07 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.04 | 0.13 | 0.02 | 0.07 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.04 | 0.13 | 0.02 | 0.07 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.05 | 0.13 | 0.02 | 0.06 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.06 | 0.13 | 0.01 | 0.02 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.12 | 0.14 | 0.13 | 0.04 | 0.07 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -7983.79 | -5352.89 | 3.831e+04 | 2.276e+04 | -5153.23 | -5656.51 | 916.43 | 290.26 |
| 23.0 | -8194.27 | -4867.26 | 1.066e+04 | 1.455e+04 | -5153.23 | -5768.87 | 985.56 | 394.65 |
| 46.0 | -7927.28 | -2260.00 | 3.378e+04 | 8454.26 | -5153.23 | -5640.88 | 1074.39 | 424.60 |
| 69.0 | -7784.90 | -2306.72 | 6.832e+04 | 5354.72 | -5153.23 | -5578.95 | 1191.35 | 438.66 |
| 92.0 | -7773.98 | -4201.91 | 9.754e+04 | 749.64 | -5153.23 | -5598.38 | 1483.85 | 532.80 |
| 112.0 | -7654.13 | -4305.84 | 1.087e+05 | 227.28 | -5153.23 | -5669.40 | 2099.69 | 721.17 |
| 132.0 | -7363.62 | -6931.62 | 5.863e+04 | 8139.72 | -5153.23 | -5338.29 | 2082.60 | 705.30 |
| 152.0 | -7084.48 | -5136.93 | 4.080e+04 | 9582.44 | -5153.23 | -5045.34 | 2061.48 | 690.35 |
| 172.0 | -6815.71 | -4293.67 | 3.198e+04 | 1.078e+04 | -5153.23 | -4702.23 | 2036.35 | 689.90 |
| 196.0 | -6535.29 | -3555.15 | 3.796e+04 | 1.171e+04 | -5153.23 | -4472.40 | 2003.95 | 688.48 |
| 220.0 | -6245.34 | -4051.66 | 3.814e+04 | 1.279e+04 | -5153.23 | -4079.98 | 1962.78 | 686.38 |
| 244.0 | -5976.01 | -3956.62 | 3.235e+04 | 1.317e+04 | -5153.23 | -3696.06 | 1916.88 | 681.34 |
| 267.0 | -5768.03 | -5099.90 | 3.252e+04 | 1.305e+04 | -5153.23 | -3341.66 | 1846.50 | 664.49 |
| 289.0 | -4834.08 | -2201.42 | 3.427e+04 | 8698.98 | -5153.23 | -2201.42 | 1206.77 | 835.24 |
| 311.0 | -4273.60 | -2014.48 | 2.091e+04 | 6951.73 | -5153.23 | -2014.48 | 1221.33 | 1011.36 |
| 333.0 | -3770.15 | -1759.99 | 1.632e+04 | 5658.39 | -5153.23 | -1759.99 | 1226.25 | 1042.64 |
| 355.0 | -3335.20 | -3306.09 | 1.399e+04 | 6212.11 | -5153.23 | -1527.20 | 1170.47 | 988.39 |
| 381.0 | -2896.13 | -2844.28 | 1.267e+04 | 7811.75 | -5153.23 | -1293.29 | 992.28 | 808.38 |
| 408.0 | -2565.85 | -2502.12 | 7994.85 | 9106.67 | -5153.23 | -1376.41 | 614.74 | 304.29 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 916.43 | 5.051e+04 | 1.00 | 1.437e+04 | 5.086e+04 |
| 23.0 | 1.00 | 985.56 | 5.053e+04 | 1.00 | 1.437e+04 | 5.089e+04 |
| 46.0 | 1.00 | 1074.39 | 5.051e+04 | 1.00 | 1.437e+04 | 5.085e+04 |
| 69.0 | 1.00 | 1191.35 | 5.050e+04 | 1.00 | 1.437e+04 | 5.082e+04 |
| 92.0 | 1.00 | 1483.85 | 5.050e+04 | 1.00 | 1.437e+04 | 5.072e+04 |
| 112.0 | 1.00 | 2099.69 | 5.052e+04 | 1.00 | 1.437e+04 | 5.070e+04 |
| 132.0 | 1.00 | 2082.60 | 5.046e+04 | 1.00 | 1.437e+04 | 5.066e+04 |
| 152.0 | 1.00 | 2061.48 | 5.041e+04 | 1.00 | 1.437e+04 | 5.068e+04 |
| 172.0 | 1.00 | 2036.35 | 5.035e+04 | 1.00 | 1.437e+04 | 5.063e+04 |
| 196.0 | 1.00 | 2003.95 | 5.031e+04 | 1.00 | 1.437e+04 | 5.058e+04 |
| 220.0 | 1.00 | 1962.78 | 5.024e+04 | 1.00 | 1.437e+04 | 5.052e+04 |
| 244.0 | 1.00 | 1916.88 | 5.017e+04 | 1.00 | 1.437e+04 | 5.047e+04 |
| 267.0 | 1.00 | 1846.50 | 5.011e+04 | 1.00 | 1.437e+04 | 5.042e+04 |
| 289.0 | 1.00 | 1206.77 | 4.991e+04 | 1.00 | 1.437e+04 | 4.989e+04 |
| 311.0 | 1.00 | 1221.33 | 4.988e+04 | 1.00 | 1.437e+04 | 4.986e+04 |
| 333.0 | 1.00 | 1226.25 | 4.983e+04 | 1.00 | 1.437e+04 | 4.982e+04 |
| 355.0 | 1.00 | 1170.47 | 4.979e+04 | 1.00 | 1.437e+04 | 4.978e+04 |
| 381.0 | 1.00 | 992.28 | 4.975e+04 | 1.00 | 1.437e+04 | 4.975e+04 |
| 408.0 | 1.00 | 614.74 | 4.977e+04 | 1.00 | 1.437e+04 | 4.972e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 53 | 408.00 | 12.00 | 193.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.24 | 0.15 | 0.03 | 0.06 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.22 | 0.15 | 0.03 | 0.06 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.17 | 0.15 | 0.03 | 0.05 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.11 | 0.15 | 0.02 | 0.04 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.06 | 0.15 | 0.03 | 0.05 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.04 | 0.15 | 0.03 | 0.06 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.08 | 0.15 | 0.03 | 0.06 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.11 | 0.15 | 0.03 | 0.06 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.13 | 0.15 | 0.03 | 0.06 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.16 | 0.15 | 0.03 | 0.06 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.18 | 0.15 | 0.03 | 0.06 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.20 | 0.15 | 0.03 | 0.06 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.20 | 0.15 | 0.03 | 0.06 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.17 | 0.15 | 0.01 | 0.03 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.14 | 0.15 | 7.37e-03 | 0.02 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.11 | 0.15 | 4.99e-03 | 0.02 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.07 | 0.15 | 4.45e-03 | 0.02 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.04 | 0.15 | 4.24e-03 | 0.01 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.07 | 0.15 | 6.65e-03 | 0.01 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.12 | 0.24 | 0.15 | 0.03 | 0.06 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -9468.26 | -5717.11 | 2.385e+04 | 5.102e+04 | -6319.88 | -5330.72 | 1824.90 | 1165.66 |
| 23.0 | -9665.98 | -6013.21 | 6.778e+04 | 4.821e+04 | -6319.88 | -5448.98 | 1768.72 | 1041.37 |
| 46.0 | -9650.23 | -5984.66 | 6.290e+04 | 3.546e+04 | -6319.88 | -5517.62 | 1653.79 | 906.24 |
| 69.0 | -9698.00 | -6061.79 | 6.339e+04 | 2.362e+04 | -6319.88 | -5658.54 | 1572.19 | 783.33 |
| 92.0 | -9846.17 | -6164.66 | 7.872e+04 | 1.337e+04 | -6319.88 | -5876.64 | 1689.55 | 904.68 |
| 112.0 | -9845.50 | -6888.65 | 3.154e+04 | 9701.02 | -6319.88 | -6111.27 | 2221.19 | 1154.87 |
| 132.0 | -9643.78 | -5886.48 | 1.811e+04 | 1.672e+04 | -6319.88 | -5981.37 | 2209.87 | 1143.56 |
| 152.0 | -9442.05 | -5731.31 | 1.375e+04 | 2.291e+04 | -6319.88 | -5812.23 | 2196.86 | 1130.54 |
| 172.0 | -9240.33 | -5576.13 | 9379.80 | 2.809e+04 | -6319.88 | -5655.11 | 2181.42 | 1115.10 |
| 196.0 | -9018.43 | -5207.09 | 1.152e+04 | 3.317e+04 | -6319.88 | -5778.16 | 2161.73 | 1095.41 |
| 220.0 | -8776.36 | -5505.27 | 6.071e+04 | 3.812e+04 | -6319.88 | -5330.14 | 2137.04 | 1070.73 |
| 244.0 | -8534.30 | -5242.51 | 8.724e+04 | 4.117e+04 | -6319.88 | -5109.94 | 2110.48 | 1044.16 |
| 267.0 | -8297.27 | -5073.29 | 1.123e+05 | 4.210e+04 | -6319.88 | -4923.99 | 2085.58 | 1019.26 |
| 289.0 | -6905.80 | -4105.26 | 8.206e+04 | 3.578e+04 | -6319.88 | -4004.57 | 902.17 | 462.56 |
| 311.0 | -6028.00 | -3439.05 | 6.717e+04 | 2.873e+04 | -6319.88 | -3434.05 | 464.34 | 315.33 |
| 333.0 | -5225.21 | -2872.92 | 5.313e+04 | 2.150e+04 | -6319.88 | -2906.79 | 313.60 | 296.30 |
| 355.0 | -4492.45 | -2346.38 | 4.262e+04 | 1.404e+04 | -6319.88 | -4324.92 | 281.13 | 281.13 |
| 381.0 | -3752.73 | -1880.94 | 2.905e+04 | 7468.03 | -6319.88 | -1830.47 | 265.91 | 258.62 |
| 408.0 | -3171.50 | -2777.97 | 3847.35 | 1.451e+04 | -6319.88 | -1498.35 | 416.44 | 261.00 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 1824.90 | 6.333e+04 | 1.00 | 1.808e+04 | 6.407e+04 |
| 23.0 | 1.00 | 1768.72 | 6.335e+04 | 1.00 | 1.808e+04 | 6.412e+04 |
| 46.0 | 1.00 | 1653.79 | 6.336e+04 | 1.00 | 1.808e+04 | 6.412e+04 |
| 69.0 | 1.00 | 1572.19 | 6.339e+04 | 1.00 | 1.808e+04 | 6.413e+04 |
| 92.0 | 1.00 | 1689.55 | 6.343e+04 | 1.00 | 1.808e+04 | 6.353e+04 |
| 112.0 | 1.00 | 2221.19 | 6.348e+04 | 1.00 | 1.808e+04 | 6.347e+04 |
| 132.0 | 1.00 | 2209.87 | 6.345e+04 | 1.00 | 1.808e+04 | 6.344e+04 |
| 152.0 | 1.00 | 2196.86 | 6.342e+04 | 1.00 | 1.808e+04 | 6.341e+04 |
| 172.0 | 1.00 | 2181.42 | 6.339e+04 | 1.00 | 1.808e+04 | 6.338e+04 |
| 196.0 | 1.00 | 2161.73 | 6.341e+04 | 1.00 | 1.808e+04 | 6.329e+04 |
| 220.0 | 1.00 | 2137.04 | 6.333e+04 | 1.00 | 1.808e+04 | 6.331e+04 |
| 244.0 | 1.00 | 2110.48 | 6.328e+04 | 1.00 | 1.808e+04 | 6.328e+04 |
| 267.0 | 1.00 | 2085.58 | 6.325e+04 | 1.00 | 1.808e+04 | 6.324e+04 |
| 289.0 | 1.00 | 902.17 | 6.307e+04 | 1.00 | 1.808e+04 | 6.309e+04 |
| 311.0 | 1.00 | 464.34 | 6.296e+04 | 1.00 | 1.808e+04 | 6.343e+04 |
| 333.0 | 1.00 | 313.60 | 6.286e+04 | 1.00 | 1.808e+04 | 6.328e+04 |
| 355.0 | 1.00 | 281.13 | 6.313e+04 | 1.00 | 1.808e+04 | 6.313e+04 |
| 381.0 | 1.00 | 265.91 | 6.266e+04 | 1.00 | 1.808e+04 | 6.299e+04 |
| 408.0 | 1.00 | 416.44 | 6.260e+04 | 1.00 | 1.808e+04 | 6.290e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 54 | 408.00 | 12.00 | 223.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.26 | 0.17 | 0.02 | 0.02 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.25 | 0.17 | 0.02 | 0.02 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.18 | 0.17 | 0.02 | 0.02 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.12 | 0.17 | 0.02 | 0.02 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.07 | 0.17 | 0.02 | 0.02 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.06 | 0.17 | 0.03 | 0.04 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.10 | 0.17 | 0.03 | 0.04 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.13 | 0.17 | 0.03 | 0.04 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.16 | 0.17 | 0.03 | 0.05 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.21 | 0.17 | 0.03 | 0.05 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.24 | 0.17 | 0.03 | 0.05 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.26 | 0.17 | 0.03 | 0.05 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.27 | 0.17 | 0.03 | 0.04 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.24 | 0.17 | 0.01 | 0.02 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.20 | 0.17 | 8.14e-03 | 8.74e-03 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.16 | 0.17 | 5.64e-03 | 4.76e-03 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.11 | 0.17 | 4.49e-03 | 4.72e-03 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.06 | 0.17 | 4.04e-03 | 3.72e-03 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.03 | 0.17 | 5.12e-03 | 5.52e-03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.11 | 0.27 | 0.17 | 0.03 | 0.05 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|------------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -9424.48 | -5712.35 | 2.458e+04 | 5.600e+04 | -6471.47 | -6001.60 | 1070.76 | 416.68 |
| 23.0 | -9719.03 | -5894.86 | 2.437e+04 | 5.572e+04 | -6471.47 | -6184.11 | 1036.22 | 382.14 |
| 46.0 | -9761.12 | -5723.43 | 2.376e+04 | 4.045e+04 | -6471.47 | -6161.51 | 1032.43 | 399.21 |
| 69.0 | -9901.52 | -5739.65 | 2.605e+04 | 2.695e+04 | -6471.47 | -6200.30 | 1046.51 | 390.27 |
| 92.0 | -1.019e+04 | -5846.20 | 2.019e+04 | 1.622e+04 | -6471.47 | -6625.65 | 1292.80 | 463.12 |
| 112.0 | -1.025e+04 | -6462.90 | 7228.99 | 1.287e+04 | -6471.47 | -6660.14 | 2006.21 | 701.43 |
| 132.0 | -1.002e+04 | -6283.20 | 6370.24 | 2.166e+04 | -6471.47 | -6470.77 | 1995.56 | 702.49 |
| 152.0 | -9784.24 | -6103.51 | 5511.73 | 2.925e+04 | -6471.47 | -6281.20 | 2004.02 | 774.44 |
| 172.0 | -9550.64 | -5356.34 | 2.107e+04 | 3.554e+04 | -6471.47 | -6091.17 | 2030.43 | 915.06 |
| 196.0 | -9293.68 | -5166.23 | 1.048e+04 | 4.488e+04 | -6471.47 | -5881.73 | 2006.88 | 904.70 |
| 220.0 | -9013.35 | -4947.94 | 1628.55 | 5.166e+04 | -6471.47 | -5677.80 | 1977.27 | 893.91 |
| 244.0 | -8733.03 | -4712.11 | 1.314e+04 | 5.576e+04 | -6471.47 | -5471.57 | 1944.08 | 884.20 |
| 267.0 | -8458.55 | -4640.62 | 6794.70 | 5.720e+04 | -6471.47 | -5223.56 | 1872.41 | 755.06 |
| 289.0 | -7128.75 | -3690.74 | 1.886e+04 | 4.990e+04 | -6471.47 | -4086.70 | 1012.33 | 363.94 |
| 311.0 | -6277.66 | -3129.42 | 1.300e+04 | 4.106e+04 | -6471.47 | -3541.90 | 554.68 | 171.02 |
| 333.0 | -5504.59 | -2664.56 | 1.018e+04 | 3.201e+04 | -6471.47 | -3025.33 | 383.30 | 93.25 |
| 355.0 | -4801.51 | -2230.22 | 7307.06 | 2.237e+04 | -6471.47 | -2558.31 | 305.28 | 92.49 |
| 381.0 | -4095.35 | -1783.39 | 4405.34 | 1.145e+04 | -6471.47 | -2080.83 | 274.32 | 72.84 |
| 408.0 | -3518.46 | -1868.59 | 1114.40 | 6197.02 | -6471.47 | -1854.99 | 346.90 | 108.11 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 1070.76 | 6.854e+04 | 1.00 | 1.958e+04 | 6.860e+04 |
| 23.0 | 1.00 | 1036.22 | 6.858e+04 | 1.00 | 1.958e+04 | 6.863e+04 |
| 46.0 | 1.00 | 1032.43 | 6.857e+04 | 1.00 | 1.958e+04 | 6.865e+04 |
| 69.0 | 1.00 | 1046.51 | 6.858e+04 | 1.00 | 1.958e+04 | 6.867e+04 |
| 92.0 | 1.00 | 1292.80 | 6.866e+04 | 1.00 | 1.958e+04 | 6.870e+04 |
| 112.0 | 1.00 | 2006.21 | 6.866e+04 | 1.00 | 1.958e+04 | 6.872e+04 |
| 132.0 | 1.00 | 1995.56 | 6.863e+04 | 1.00 | 1.958e+04 | 6.868e+04 |
| 152.0 | 1.00 | 2004.02 | 6.859e+04 | 1.00 | 1.958e+04 | 6.864e+04 |
| 172.0 | 1.00 | 2030.43 | 6.856e+04 | 1.00 | 1.958e+04 | 6.861e+04 |
| 196.0 | 1.00 | 2006.88 | 6.852e+04 | 1.00 | 1.958e+04 | 6.857e+04 |
| 220.0 | 1.00 | 1977.27 | 6.849e+04 | 1.00 | 1.958e+04 | 6.853e+04 |
| 244.0 | 1.00 | 1944.08 | 6.845e+04 | 1.00 | 1.958e+04 | 6.850e+04 |
| 267.0 | 1.00 | 1872.41 | 6.841e+04 | 1.00 | 1.958e+04 | 6.844e+04 |
| 289.0 | 1.00 | 1012.33 | 6.820e+04 | 1.00 | 1.958e+04 | 6.830e+04 |
| 311.0 | 1.00 | 554.68 | 6.811e+04 | 1.00 | 1.958e+04 | 6.820e+04 |
| 333.0 | 1.00 | 383.30 | 6.801e+04 | 1.00 | 1.958e+04 | 6.795e+04 |
| 355.0 | 1.00 | 305.28 | 6.793e+04 | 1.00 | 1.958e+04 | 6.787e+04 |
| 381.0 | 1.00 | 274.32 | 6.785e+04 | 1.00 | 1.958e+04 | 6.779e+04 |
| 408.0 | 1.00 | 346.90 | 6.780e+04 | 1.00 | 1.958e+04 | 6.799e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 58 | 408.00 | 12.00 | 223.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.25 | 0.17 | 0.02 | 0.02 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.23 | 0.17 | 0.02 | 0.02 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.17 | 0.17 | 0.02 | 0.02 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.11 | 0.17 | 0.02 | 0.02 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.07 | 0.17 | 0.02 | 0.03 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.05 | 0.17 | 0.04 | 0.04 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.09 | 0.17 | 0.04 | 0.04 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.12 | 0.17 | 0.04 | 0.04 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.15 | 0.17 | 0.04 | 0.04 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.18 | 0.17 | 0.04 | 0.04 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.21 | 0.17 | 0.04 | 0.04 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.23 | 0.17 | 0.03 | 0.04 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.24 | 0.17 | 0.03 | 0.04 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.22 | 0.17 | 0.02 | 0.01 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.18 | 0.17 | 9.83e-03 | 9.02e-03 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.14 | 0.17 | 6.77e-03 | 6.45e-03 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.10 | 0.17 | 5.57e-03 | 4.86e-03 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.05 | 0.17 | 5.26e-03 | 4.02e-03 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.05 | 0.17 | 6.54e-03 | 6.09e-03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.11 | 0.25 | 0.17 | 0.04 | 0.04 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|------------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -9402.91 | -5990.53 | 5288.93 | 5.434e+04 | -6448.30 | -5935.39 | 1194.10 | 380.03 |
| 23.0 | -9699.94 | -6175.04 | 3.006e+04 | 5.018e+04 | -6448.30 | -6120.27 | 1203.61 | 382.75 |
| 46.0 | -9746.78 | -6178.17 | 3.289e+04 | 3.665e+04 | -6448.30 | -6101.69 | 1233.28 | 373.31 |
| 69.0 | -9892.85 | -6185.20 | 7.106e+04 | 2.463e+04 | -6448.30 | -6130.62 | 1300.64 | 401.32 |
| 92.0 | -1.019e+04 | -6268.67 | 8.738e+04 | 1.483e+04 | -6448.30 | -6277.32 | 1686.90 | 576.17 |
| 112.0 | -1.026e+04 | -6439.59 | 6920.10 | 1.179e+04 | -6448.30 | -6269.62 | 2512.93 | 705.11 |
| 132.0 | -1.003e+04 | -6259.89 | 4849.35 | 2.022e+04 | -6448.30 | -6078.66 | 2497.38 | 705.11 |
| 152.0 | -9793.92 | -6080.20 | 2779.24 | 2.746e+04 | -6448.30 | -5885.70 | 2481.03 | 705.11 |
| 172.0 | -9560.32 | -5900.50 | 709.20 | 3.353e+04 | -6448.30 | -5691.91 | 2462.08 | 705.11 |
| 196.0 | -9303.36 | -5959.37 | 243.66 | 3.960e+04 | -6448.30 | -5498.71 | 2437.83 | 705.11 |
| 220.0 | -9023.03 | -5699.93 | 1.098e+04 | 4.660e+04 | -6448.30 | -5300.58 | 2406.73 | 705.11 |
| 244.0 | -8742.71 | -5490.19 | 1.999e+04 | 5.086e+04 | -6448.30 | -5080.24 | 2371.12 | 705.11 |
| 267.0 | -8468.23 | -5275.86 | 3.018e+04 | 5.258e+04 | -6448.30 | -4874.15 | 2332.37 | 705.11 |
| 289.0 | -7138.24 | -4451.31 | 2.556e+04 | 4.586e+04 | -6448.30 | -4023.66 | 1206.95 | 263.80 |
| 311.0 | -6279.25 | -3901.48 | 2.215e+04 | 3.756e+04 | -6448.30 | -3469.94 | 669.15 | 176.67 |
| 333.0 | -5496.88 | -3390.07 | 1.871e+04 | 2.887e+04 | -6448.30 | -2984.53 | 460.52 | 126.18 |
| 355.0 | -4783.85 | -2923.40 | 1.838e+04 | 1.969e+04 | -6448.30 | -2522.72 | 378.29 | 95.18 |
| 381.0 | -4066.56 | -2484.39 | 1.241e+04 | 9666.28 | -6448.30 | -2053.82 | 356.52 | 78.74 |
| 408.0 | -3493.70 | -1392.20 | 5529.57 | 1.045e+04 | -6448.30 | -1644.95 | 443.27 | 119.22 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 1194.10 | 6.853e+04 | 1.00 | 1.958e+04 | 6.901e+04 |
| 23.0 | 1.00 | 1203.61 | 6.857e+04 | 1.00 | 1.958e+04 | 6.905e+04 |
| 46.0 | 1.00 | 1233.28 | 6.856e+04 | 1.00 | 1.958e+04 | 6.905e+04 |
| 69.0 | 1.00 | 1300.64 | 6.857e+04 | 1.00 | 1.958e+04 | 6.907e+04 |
| 92.0 | 1.00 | 1686.90 | 6.859e+04 | 1.00 | 1.958e+04 | 6.897e+04 |
| 112.0 | 1.00 | 2512.93 | 6.859e+04 | 1.00 | 1.958e+04 | 6.897e+04 |
| 132.0 | 1.00 | 2497.38 | 6.856e+04 | 1.00 | 1.958e+04 | 6.893e+04 |
| 152.0 | 1.00 | 2481.03 | 6.852e+04 | 1.00 | 1.958e+04 | 6.889e+04 |
| 172.0 | 1.00 | 2462.08 | 6.849e+04 | 1.00 | 1.958e+04 | 6.884e+04 |
| 196.0 | 1.00 | 2437.83 | 6.845e+04 | 1.00 | 1.958e+04 | 6.880e+04 |
| 220.0 | 1.00 | 2406.73 | 6.842e+04 | 1.00 | 1.958e+04 | 6.875e+04 |
| 244.0 | 1.00 | 2371.12 | 6.838e+04 | 1.00 | 1.958e+04 | 6.870e+04 |
| 267.0 | 1.00 | 2332.37 | 6.834e+04 | 1.00 | 1.958e+04 | 6.865e+04 |
| 289.0 | 1.00 | 1206.95 | 6.819e+04 | 1.00 | 1.958e+04 | 6.845e+04 |
| 311.0 | 1.00 | 669.15 | 6.809e+04 | 1.00 | 1.958e+04 | 6.832e+04 |
| 333.0 | 1.00 | 460.52 | 6.801e+04 | 1.00 | 1.958e+04 | 6.821e+04 |
| 355.0 | 1.00 | 378.29 | 6.792e+04 | 1.00 | 1.958e+04 | 6.810e+04 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| 381.0 | 1.00 | 356.52 | 6.784e+04 | 1.00 | 1.958e+04 | 6.784e+04 |
| 408.0 | 1.00 | 443.27 | 6.777e+04 | 1.00 | 1.958e+04 | 6.777e+04 |

Macrosetti n. 91, 92, 94, 95 [fasce di piano]

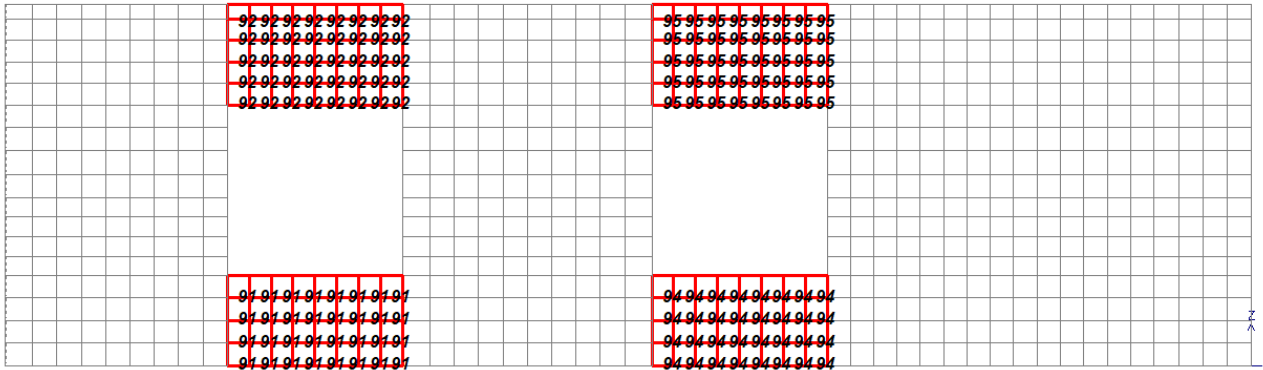


Fig 108. Elemento/i oggetto di verifica (Selezione in rosso).

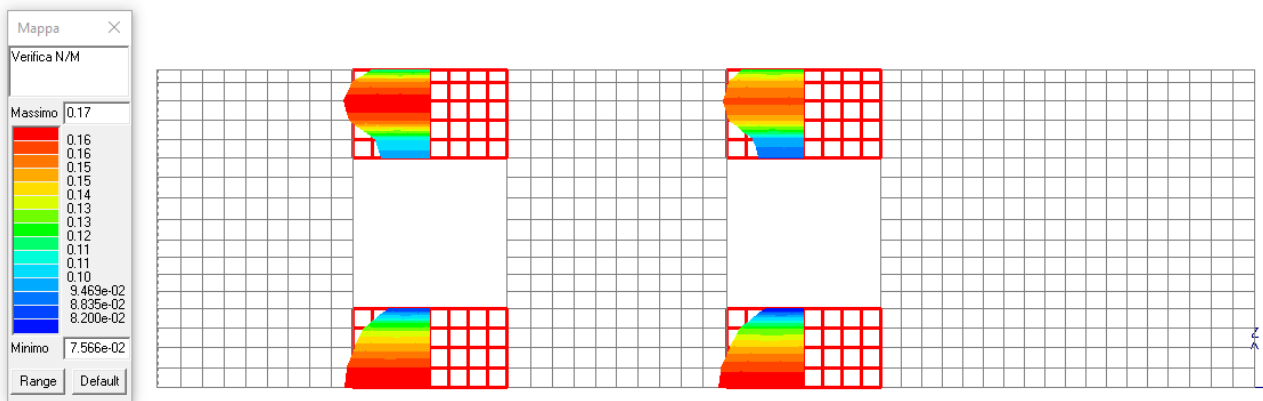


Fig 109. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

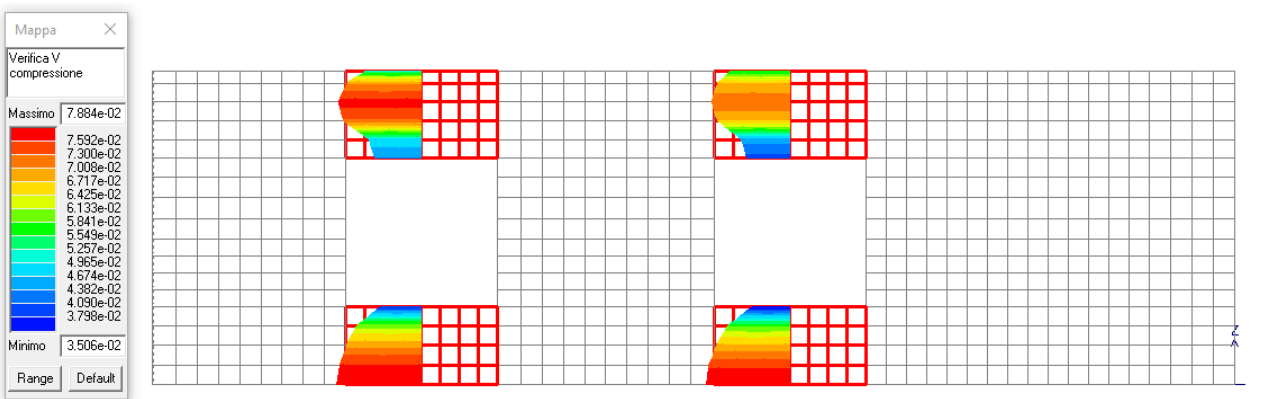


Fig 110. SLU: Mappa di Verifica V compressione – Verifica soddisfatta ($\rho \leq 1$).

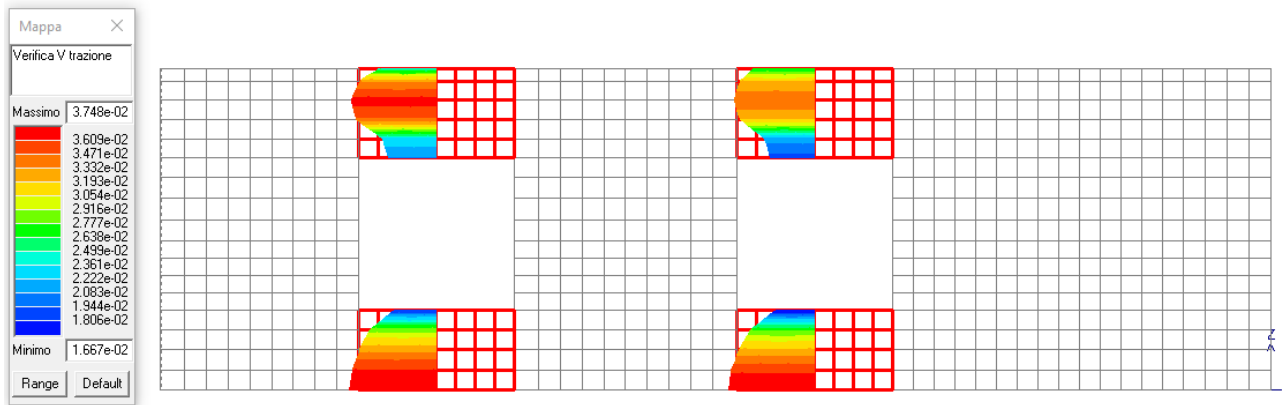


Fig 111. SLU: Mapa di verifica V trazione – Verifiche soddisfatte ($\rho \leq 1$).

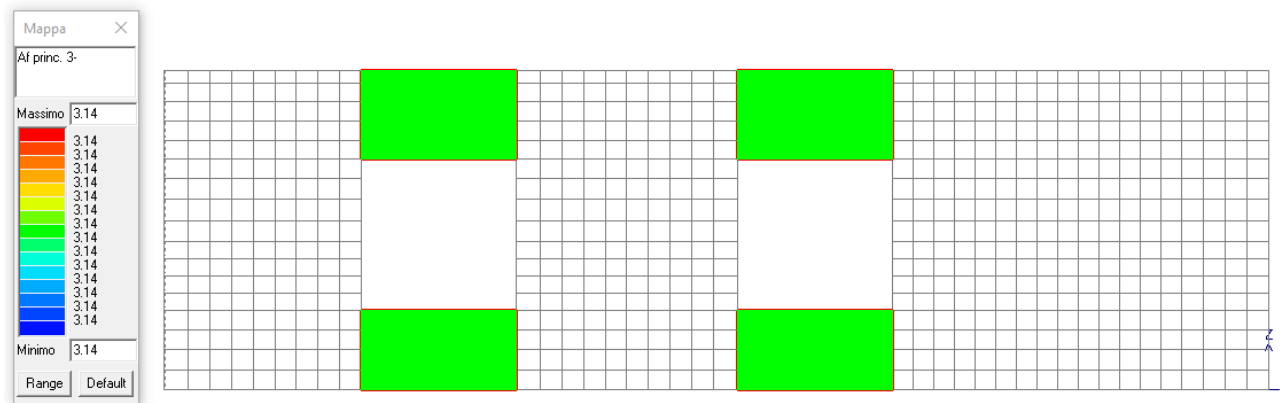


Fig 112. Mapa Armatura Verticale (singolo strato) da Calcolo [cm^2/m].

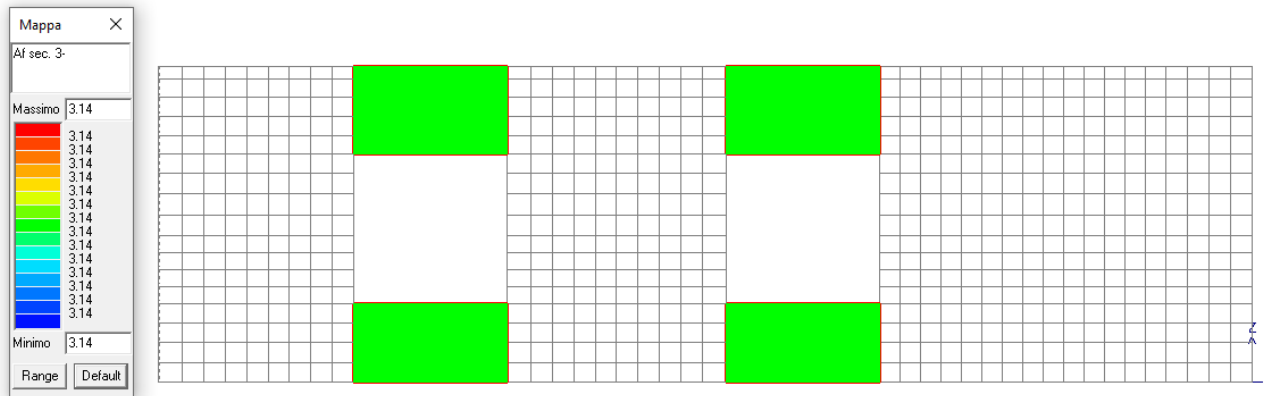


Fig 113. Mapa Armatura Orizzontale (singolo strato) da Calcolo [cm^2/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 91 | 92.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.17 | 0.0 | 0.08 | 0.04 | 0.0 |
| 23.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.16 | 0.0 | 0.08 | 0.04 | 0.0 |
| 46.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.15 | 0.0 | 0.07 | 0.03 | 0.0 |
| 69.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.06 | 0.03 | 0.0 |
| 92.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.04 | 0.02 | 0.0 |
| | | | | | | | | | |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.17 | 0.0 | 0.08 | 0.04 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|--------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | 0.0 | 0.0 | 1.669e+05 | 0.0 | 0.0 | 0.0 | 1853.93 | 1853.93 |
| 23.0 | 0.0 | 0.0 | 1.614e+05 | 0.0 | 0.0 | 0.0 | 1793.69 | 1793.69 |
| 46.0 | 0.0 | 0.0 | 1.467e+05 | 0.0 | 0.0 | 0.0 | 1630.47 | 1630.47 |
| 69.0 | 0.0 | 0.0 | 1.281e+05 | 0.0 | 0.0 | 0.0 | 1422.94 | 1422.94 |
| 92.0 | 0.0 | 0.0 | 8.079e+04 | 0.0 | 0.0 | 0.0 | 897.70 | 897.70 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 2.50 | 1853.93 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 23.0 | 2.50 | 1793.69 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 46.0 | 2.50 | 1630.47 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 69.0 | 2.50 | 1422.94 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 92.0 | 2.50 | 897.70 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 92 | 103.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.04 | 0.02 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.05 | 0.02 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.16 | 0.0 | 0.07 | 0.03 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.17 | 0.0 | 0.08 | 0.04 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.15 | 0.0 | 0.07 | 0.03 | 0.0 |
| 370.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.12 | 0.0 | 0.05 | 0.02 | 0.0 |
| | | | | | | | | | |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.17 | 0.0 | 0.08 | 0.04 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|--------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 1.040e+05 | 0.0 | 0.0 | 0.0 | 1155.69 | 1155.69 |
| 289.0 | 0.0 | 0.0 | 1.169e+05 | 0.0 | 0.0 | 0.0 | 1298.49 | 1298.49 |
| 311.0 | 0.0 | 0.0 | 1.729e+05 | 0.0 | 0.0 | 0.0 | 1920.91 | 1920.91 |
| 333.0 | 0.0 | 0.0 | 1.841e+05 | 0.0 | 0.0 | 0.0 | 2045.27 | 2045.27 |
| 355.0 | 0.0 | 0.0 | 1.664e+05 | 0.0 | 0.0 | 0.0 | 1849.21 | 1849.21 |
| 370.0 | 0.0 | 0.0 | 1.242e+05 | 0.0 | 0.0 | 0.0 | 1379.75 | 1379.75 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 1155.69 | 2.641e+04 | 2.50 | 5.554e+04 | 2.641e+04 |
| 289.0 | 2.50 | 1298.49 | 2.641e+04 | 2.50 | 5.554e+04 | 2.641e+04 |
| 311.0 | 2.50 | 1920.91 | 2.641e+04 | 2.50 | 5.554e+04 | 2.641e+04 |
| 333.0 | 2.50 | 2045.27 | 2.641e+04 | 2.50 | 5.554e+04 | 2.641e+04 |
| 355.0 | 2.50 | 1849.21 | 2.641e+04 | 2.50 | 5.554e+04 | 2.641e+04 |
| 370.0 | 2.50 | 1379.75 | 2.641e+04 | 2.50 | 5.554e+04 | 2.641e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 94 | 92.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.17 | 0.0 | 0.08 | 0.04 | 0.0 |
| 23.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.16 | 0.0 | 0.08 | 0.04 | 0.0 |
| 46.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.15 | 0.0 | 0.07 | 0.03 | 0.0 |
| 69.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.06 | 0.03 | 0.0 |
| 92.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.04 | 0.02 | 0.0 |
| | | | | | | | | | |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.17 | 0.0 | 0.08 | 0.04 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | 0.0 | 0.0 | 1.653e+05 | 0.0 | 0.0 | 0.0 | 1837.03 | 1837.03 |
| 23.0 | 0.0 | 0.0 | 1.601e+05 | 0.0 | 0.0 | 0.0 | 1778.61 | 1778.61 |
| 46.0 | 0.0 | 0.0 | 1.443e+05 | 0.0 | 0.0 | 0.0 | 1602.95 | 1602.95 |
| 69.0 | 0.0 | 0.0 | 1.234e+05 | 0.0 | 0.0 | 0.0 | 1371.29 | 1371.29 |
| 92.0 | 0.0 | 0.0 | 7.420e+04 | 0.0 | 0.0 | 0.0 | 824.45 | 824.45 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 2.50 | 1837.03 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 23.0 | 2.50 | 1778.61 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 46.0 | 2.50 | 1602.95 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 69.0 | 2.50 | 1371.29 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 92.0 | 2.50 | 824.45 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 95 | 103.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.04 | 0.02 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.05 | 0.02 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.15 | 0.0 | 0.07 | 0.03 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.16 | 0.0 | 0.07 | 0.03 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.15 | 0.0 | 0.07 | 0.03 | 0.0 |
| 370.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.12 | 0.0 | 0.06 | 0.03 | 0.0 |
| | | | | | | | | | |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.16 | 0.0 | 0.07 | 0.03 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 9.491e+04 | 0.0 | 0.0 | 0.0 | 1054.50 | 1054.50 |
| 289.0 | 0.0 | 0.0 | 1.079e+05 | 0.0 | 0.0 | 0.0 | 1198.48 | 1198.48 |
| 311.0 | 0.0 | 0.0 | 1.602e+05 | 0.0 | 0.0 | 0.0 | 1780.19 | 1780.19 |
| 333.0 | 0.0 | 0.0 | 1.730e+05 | 0.0 | 0.0 | 0.0 | 1921.76 | 1921.76 |
| 355.0 | 0.0 | 0.0 | 1.608e+05 | 0.0 | 0.0 | 0.0 | 1786.59 | 1786.59 |
| 370.0 | 0.0 | 0.0 | 1.324e+05 | 0.0 | 0.0 | 0.0 | 1471.02 | 1471.02 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 1054.50 | 2.641e+04 | 2.50 | 5.554e+04 | 2.641e+04 |
| 289.0 | 2.50 | 1198.48 | 2.641e+04 | 2.50 | 5.554e+04 | 2.641e+04 |
| 311.0 | 2.50 | 1780.19 | 2.641e+04 | 2.50 | 5.554e+04 | 2.641e+04 |
| 333.0 | 2.50 | 1921.76 | 2.641e+04 | 2.50 | 5.554e+04 | 2.641e+04 |
| 355.0 | 2.50 | 1786.59 | 2.641e+04 | 2.50 | 5.554e+04 | 2.641e+04 |
| 370.0 | 2.50 | 1471.02 | 2.641e+04 | 2.50 | 5.554e+04 | 2.641e+04 |

Macrosetti n. 55, 56, 57, 59, 60, 61 62, 85 [fasce di piano]

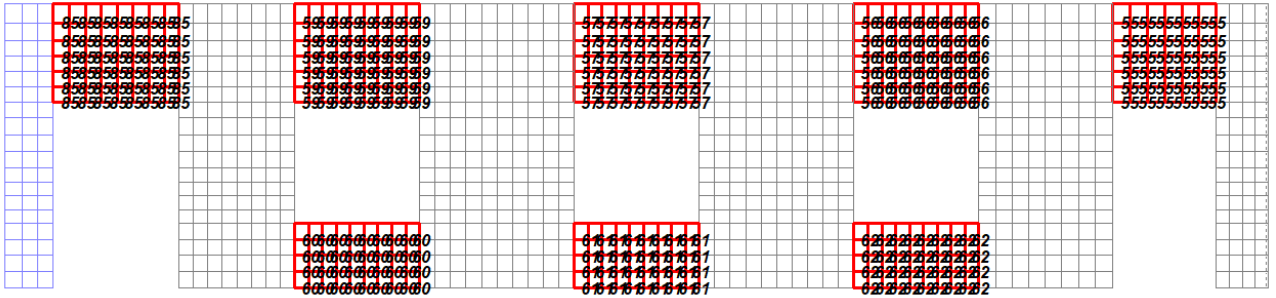


Fig 114. Elemento/i oggetto di verifica (Selezione in rosso).

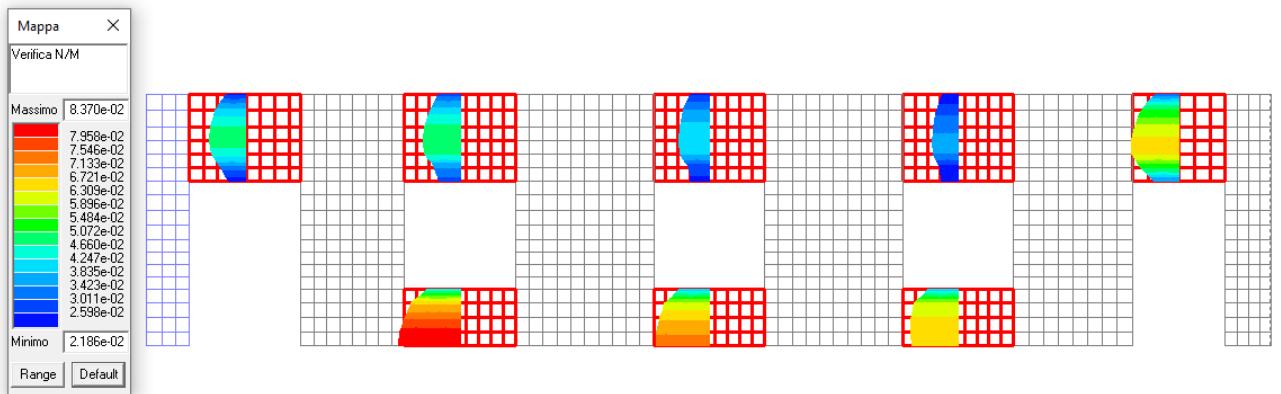


Fig 115. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($p \leq 1$).

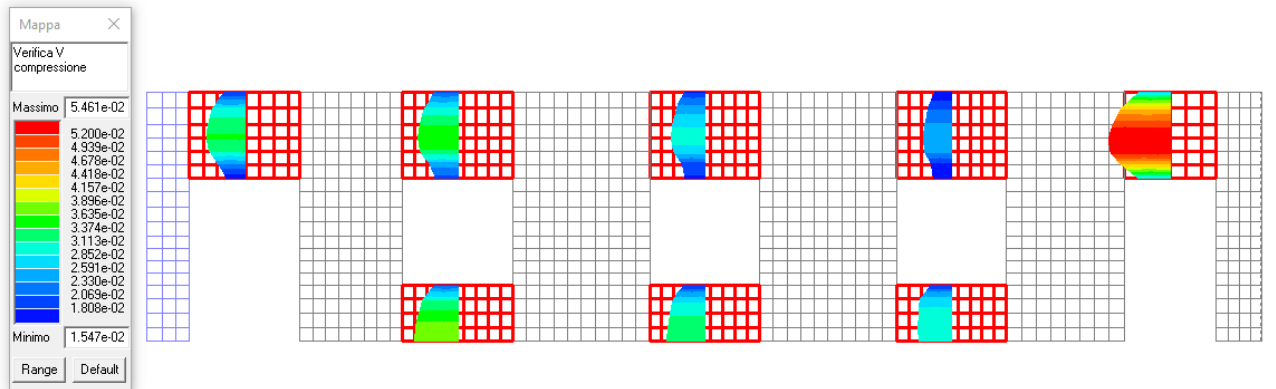


Fig 116. SLU: Mappa di Verifica V compressione – Verifica soddisfatta ($p \leq 1$).

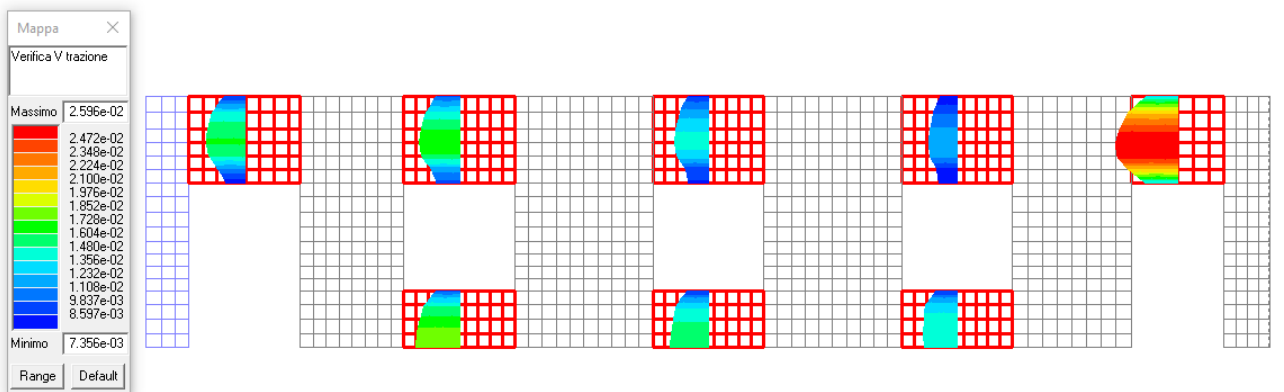


Fig 117. SLU: Mappa di verifica V trazione – Verifiche soddisfatte ($p \leq 1$).

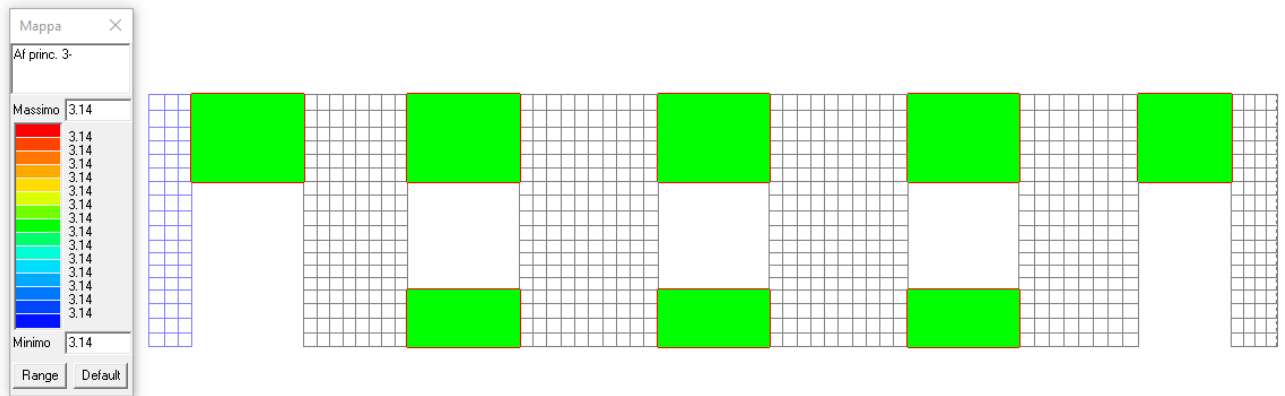


Fig 118. Mappa Armatura Verticale (singolo strato) da Calcolo [cm²/m].

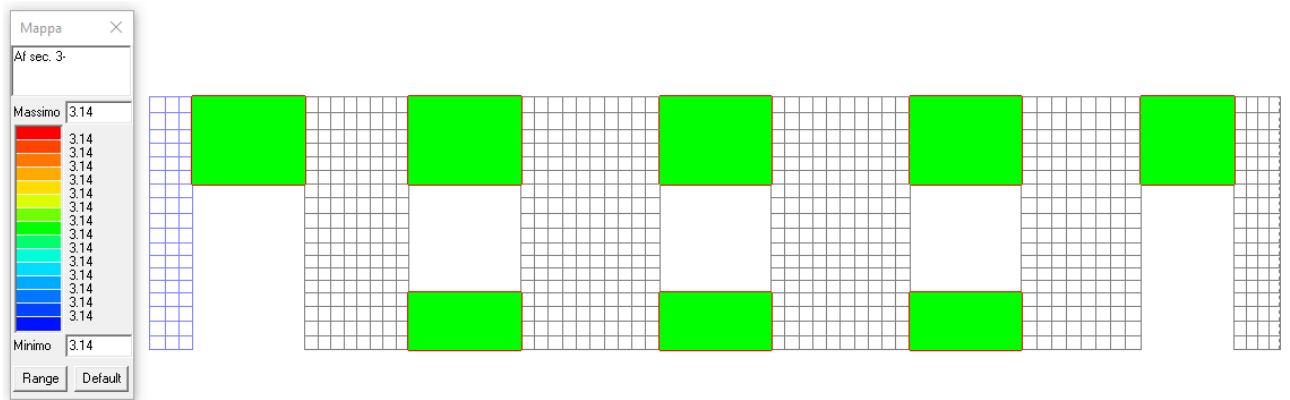


Fig 119. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm²/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 55 | 141.00 | 12.00 | 150.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.03 | 0.01 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.05 | 0.03 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.05 | 0.03 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.05 | 0.02 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.03 | 0.01 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.06 | 0.0 | 0.05 | 0.03 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 7.969e+04 | 0.0 | 0.0 | 0.0 | 1062.47 | 1062.47 |
| 289.0 | 0.0 | 0.0 | 1.208e+05 | 0.0 | 0.0 | 0.0 | 1610.99 | 1610.99 |
| 311.0 | 0.0 | 0.0 | 1.486e+05 | 0.0 | 0.0 | 0.0 | 1981.82 | 1981.82 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| 333.0 | 0.0 | 0.0 | 1.490e+05 | 0.0 | 0.0 | 0.0 | 1987.31 | 1987.31 |
| 355.0 | 0.0 | 0.0 | 1.402e+05 | 0.0 | 0.0 | 0.0 | 1869.85 | 1869.85 |
| 381.0 | 0.0 | 0.0 | 1.196e+05 | 0.0 | 0.0 | 0.0 | 1594.68 | 1594.68 |
| 408.0 | 0.0 | 0.0 | 7.614e+04 | 0.0 | 0.0 | 0.0 | 1015.18 | 1015.18 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 1062.47 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 289.0 | 2.50 | 1610.99 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 311.0 | 2.50 | 1981.82 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 333.0 | 2.50 | 1987.31 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 355.0 | 2.50 | 1869.85 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 381.0 | 2.50 | 1594.68 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 408.0 | 2.50 | 1015.18 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 56 | 141.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.02 | 7.69e-03 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.02 | 8.37e-03 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.02 | 0.01 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.02 | 0.01 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.02 | 9.82e-03 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.02 | 7.36e-03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 5.295e+04 | 0.0 | 0.0 | 0.0 | 588.32 | 588.32 |
| 289.0 | 0.0 | 0.0 | 5.764e+04 | 0.0 | 0.0 | 0.0 | 640.49 | 640.49 |
| 311.0 | 0.0 | 0.0 | 7.983e+04 | 0.0 | 0.0 | 0.0 | 887.05 | 887.05 |
| 333.0 | 0.0 | 0.0 | 8.199e+04 | 0.0 | 0.0 | 0.0 | 910.96 | 910.96 |
| 355.0 | 0.0 | 0.0 | 7.744e+04 | 0.0 | 0.0 | 0.0 | 860.46 | 860.46 |
| 381.0 | 0.0 | 0.0 | 6.762e+04 | 0.0 | 0.0 | 0.0 | 751.38 | 751.38 |
| 408.0 | 0.0 | 0.0 | 5.068e+04 | 0.0 | 0.0 | 0.0 | 563.06 | 563.06 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 588.32 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 289.0 | 2.50 | 640.49 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 311.0 | 2.50 | 887.05 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 333.0 | 2.50 | 910.96 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 355.0 | 2.50 | 860.46 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 381.0 | 2.50 | 751.38 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 408.0 | 2.50 | 563.06 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 57 | 141.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|-----------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.02 | 8.50e-03 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.02 | 9.23e-03 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.02 | 0.01 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.02 | 8.59e-03 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|--------|------------|--------|----------|-------------|------------|------------|-------|
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 5.855e+04 | 0.0 | 0.0 | 0.0 | 650.59 | 650.59 |
| 289.0 | 0.0 | 0.0 | 6.358e+04 | 0.0 | 0.0 | 0.0 | 706.44 | 706.44 |
| 311.0 | 0.0 | 0.0 | 9.145e+04 | 0.0 | 0.0 | 0.0 | 1016.07 | 1016.07 |
| 333.0 | 0.0 | 0.0 | 9.673e+04 | 0.0 | 0.0 | 0.0 | 1074.83 | 1074.83 |
| 355.0 | 0.0 | 0.0 | 9.259e+04 | 0.0 | 0.0 | 0.0 | 1028.77 | 1028.77 |
| 381.0 | 0.0 | 0.0 | 8.130e+04 | 0.0 | 0.0 | 0.0 | 903.37 | 903.37 |
| 408.0 | 0.0 | 0.0 | 5.918e+04 | 0.0 | 0.0 | 0.0 | 657.59 | 657.59 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 650.59 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 289.0 | 2.50 | 706.44 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 311.0 | 2.50 | 1016.07 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 333.0 | 2.50 | 1074.83 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 355.0 | 2.50 | 1028.77 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 381.0 | 2.50 | 903.37 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 408.0 | 2.50 | 657.59 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 59 | 141.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|-----------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.02 | 9.58e-03 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.02 | 0.01 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.03 | 0.02 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.03 | 0.02 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.02 | 9.76e-03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 6.603e+04 | 0.0 | 0.0 | 0.0 | 733.62 | 733.62 |
| 289.0 | 0.0 | 0.0 | 8.033e+04 | 0.0 | 0.0 | 0.0 | 892.56 | 892.56 |
| 311.0 | 0.0 | 0.0 | 1.103e+05 | 0.0 | 0.0 | 0.0 | 1225.16 | 1225.16 |
| 333.0 | 0.0 | 0.0 | 1.154e+05 | 0.0 | 0.0 | 0.0 | 1281.78 | 1281.78 |
| 355.0 | 0.0 | 0.0 | 1.104e+05 | 0.0 | 0.0 | 0.0 | 1226.80 | 1226.80 |
| 381.0 | 0.0 | 0.0 | 9.603e+04 | 0.0 | 0.0 | 0.0 | 1067.04 | 1067.04 |
| 408.0 | 0.0 | 0.0 | 6.724e+04 | 0.0 | 0.0 | 0.0 | 747.11 | 747.11 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 733.62 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 289.0 | 2.50 | 892.56 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 311.0 | 2.50 | 1225.16 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 333.0 | 2.50 | 1281.78 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 355.0 | 2.50 | 1226.80 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 381.0 | 2.50 | 1067.04 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 408.0 | 2.50 | 747.11 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 60 | 92.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.04 | 0.02 | 0.0 |
| 23.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.04 | 0.02 | 0.0 |
| 46.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.03 | 0.02 | 0.0 |
| 69.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.03 | 0.01 | 0.0 |
| 92.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.02 | 9.63e-03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.08 | 0.0 | 0.04 | 0.02 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|--------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | 0.0 | 0.0 | 8.208e+04 | 0.0 | 0.0 | 0.0 | 912.01 | 912.01 |
| 23.0 | 0.0 | 0.0 | 7.985e+04 | 0.0 | 0.0 | 0.0 | 887.17 | 887.17 |
| 46.0 | 0.0 | 0.0 | 7.324e+04 | 0.0 | 0.0 | 0.0 | 813.73 | 813.73 |
| 69.0 | 0.0 | 0.0 | 6.543e+04 | 0.0 | 0.0 | 0.0 | 727.05 | 727.05 |
| 92.0 | 0.0 | 0.0 | 4.285e+04 | 0.0 | 0.0 | 0.0 | 476.12 | 476.12 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 2.50 | 912.01 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 23.0 | 2.50 | 887.17 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 46.0 | 2.50 | 813.73 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 69.0 | 2.50 | 727.05 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 92.0 | 2.50 | 476.12 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 61 | 92.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.03 | 0.02 | 0.0 |
| 23.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.03 | 0.02 | 0.0 |
| 46.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.03 | 0.01 | 0.0 |
| 69.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.03 | 0.01 | 0.0 |
| 92.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.02 | 8.76e-03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.07 | 0.0 | 0.03 | 0.02 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|--------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | 0.0 | 0.0 | 7.075e+04 | 0.0 | 0.0 | 0.0 | 786.14 | 786.14 |
| 23.0 | 0.0 | 0.0 | 6.981e+04 | 0.0 | 0.0 | 0.0 | 775.67 | 775.67 |
| 46.0 | 0.0 | 0.0 | 6.526e+04 | 0.0 | 0.0 | 0.0 | 725.08 | 725.08 |
| 69.0 | 0.0 | 0.0 | 5.898e+04 | 0.0 | 0.0 | 0.0 | 655.36 | 655.36 |
| 92.0 | 0.0 | 0.0 | 3.900e+04 | 0.0 | 0.0 | 0.0 | 433.36 | 433.36 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 2.50 | 786.14 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 23.0 | 2.50 | 775.67 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 46.0 | 2.50 | 725.08 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 69.0 | 2.50 | 655.36 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 92.0 | 2.50 | 433.36 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 62 | 92.00 | 12.00 | 180.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.03 | 0.01 | 0.0 |
| 23.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.03 | 0.01 | 0.0 |
| 46.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.03 | 0.01 | 0.0 |
| 69.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.03 | 0.01 | 0.0 |
| 92.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.02 | 8.91e-03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.06 | 0.0 | 0.03 | 0.01 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | 0.0 | 0.0 | 6.206e+04 | 0.0 | 0.0 | 0.0 | 689.59 | 689.59 |
| 23.0 | 0.0 | 0.0 | 6.350e+04 | 0.0 | 0.0 | 0.0 | 705.53 | 705.53 |
| 46.0 | 0.0 | 0.0 | 6.227e+04 | 0.0 | 0.0 | 0.0 | 691.90 | 691.90 |
| 69.0 | 0.0 | 0.0 | 5.824e+04 | 0.0 | 0.0 | 0.0 | 647.06 | 647.06 |
| 92.0 | 0.0 | 0.0 | 3.968e+04 | 0.0 | 0.0 | 0.0 | 440.86 | 440.86 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 2.50 | 689.59 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 23.0 | 2.50 | 705.53 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 46.0 | 2.50 | 691.90 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 69.0 | 2.50 | 647.06 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |
| 92.0 | 2.50 | 440.86 | 2.352e+04 | 2.50 | 4.946e+04 | 2.352e+04 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 85 | 141.00 | 12.00 | 181.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|-----------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.02 | 7.83e-03 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.02 | 0.01 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.03 | 0.02 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.03 | 0.02 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.03 | 0.02 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.02 | 8.63e-03 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.05 | 0.0 | 0.03 | 0.02 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 5.426e+04 | 0.0 | 0.0 | 0.0 | 599.53 | 599.53 |
| 289.0 | 0.0 | 0.0 | 7.642e+04 | 0.0 | 0.0 | 0.0 | 844.37 | 844.37 |
| 311.0 | 0.0 | 0.0 | 1.053e+05 | 0.0 | 0.0 | 0.0 | 1163.39 | 1163.39 |
| 333.0 | 0.0 | 0.0 | 1.122e+05 | 0.0 | 0.0 | 0.0 | 1240.30 | 1240.30 |
| 355.0 | 0.0 | 0.0 | 1.088e+05 | 0.0 | 0.0 | 0.0 | 1202.58 | 1202.58 |
| 381.0 | 0.0 | 0.0 | 9.415e+04 | 0.0 | 0.0 | 0.0 | 1040.37 | 1040.37 |
| 408.0 | 0.0 | 0.0 | 5.979e+04 | 0.0 | 0.0 | 0.0 | 660.67 | 660.67 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 599.53 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 289.0 | 2.50 | 844.37 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 311.0 | 2.50 | 1163.39 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 333.0 | 2.50 | 1240.30 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 355.0 | 2.50 | 1202.58 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 381.0 | 2.50 | 1040.37 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |
| 408.0 | 2.50 | 660.67 | 3.639e+04 | 2.50 | 7.654e+04 | 3.639e+04 |

1.1.1.1.5 Parete Interna

Si riportano le verifiche analitiche dei macroelementi della parete oggetto di verifica identificata nella figura successiva.

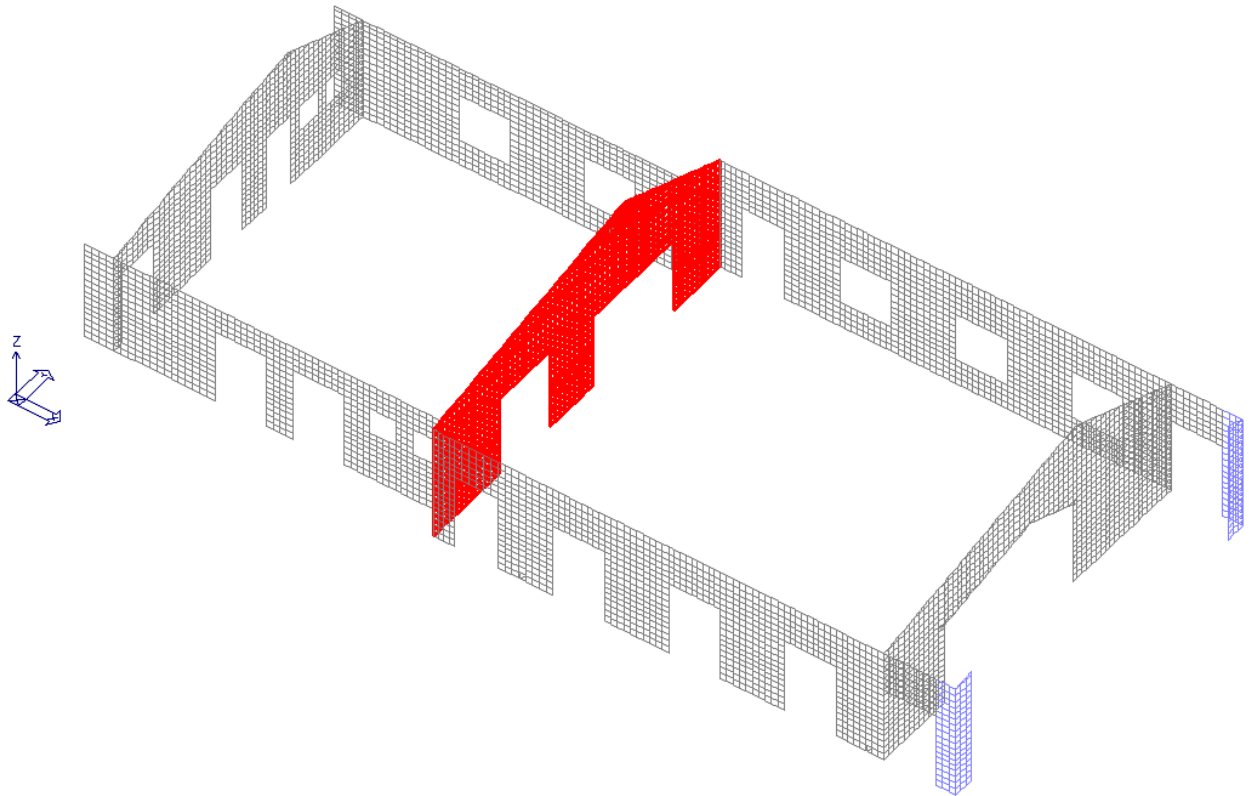


Fig 120. Parete oggetto di verifica (in rosso).

Macrosetti n. 14, 19, 34, 42, 43 [maschi]

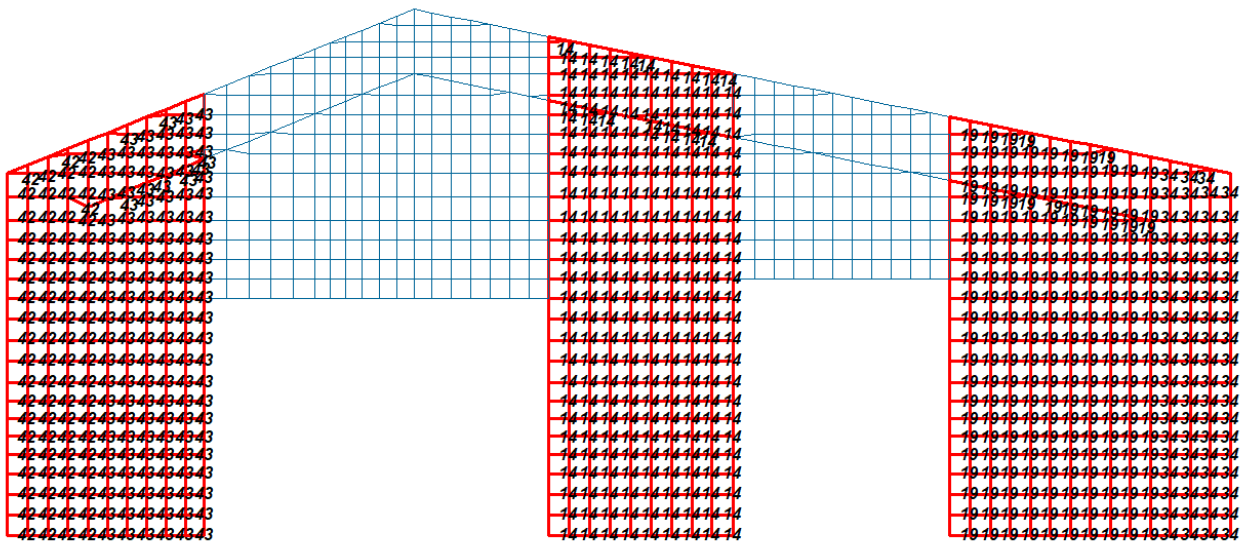


Fig 121. Elementi oggetto di verifica (Selezione in rosso).

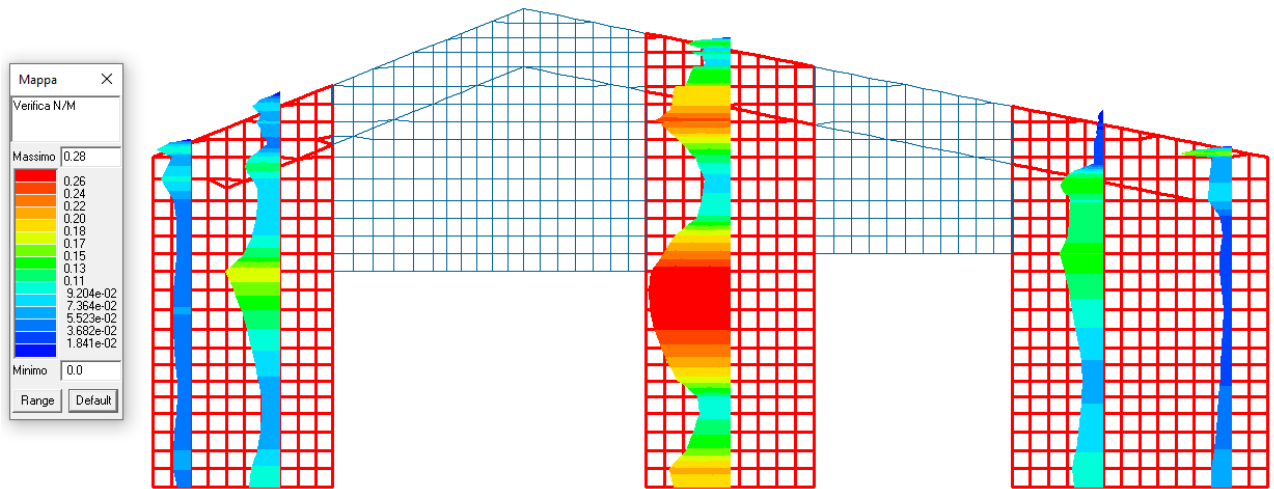


Fig 122. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

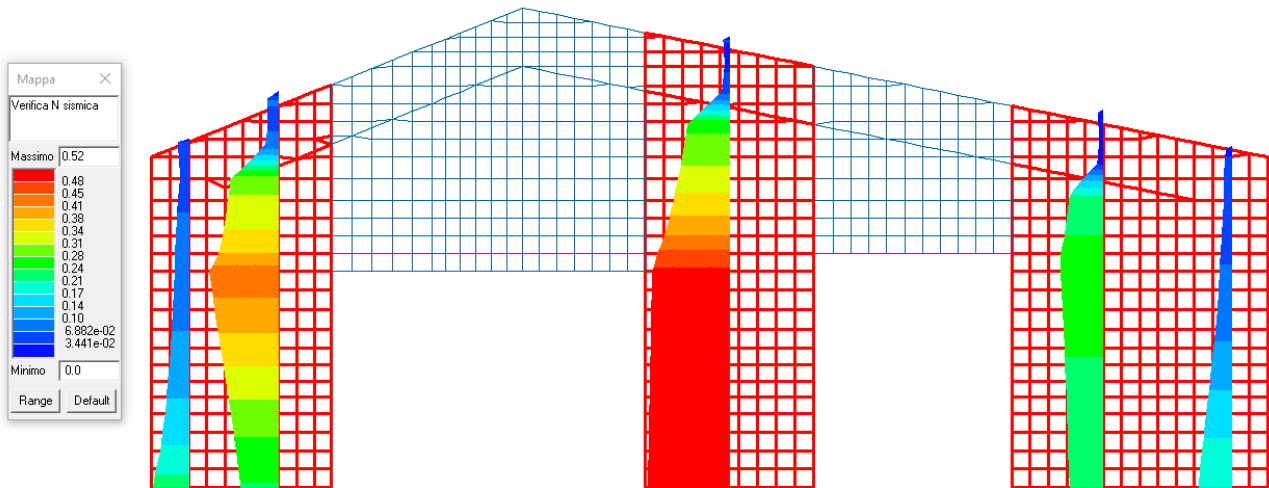


Fig 123. SLU: Mappa di verifica Nsismica – Verifiche soddisfatte ($\rho \leq 0.625$).

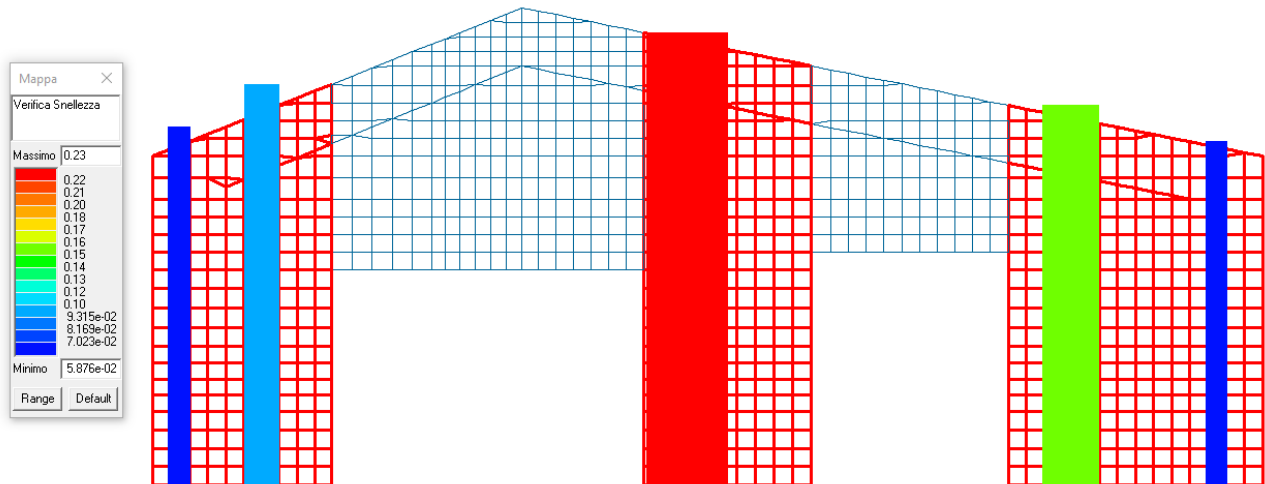


Fig 124. SLU: Mappa di Verifica Snellezza – Verifiche soddisfatte ($\rho \leq 1$).

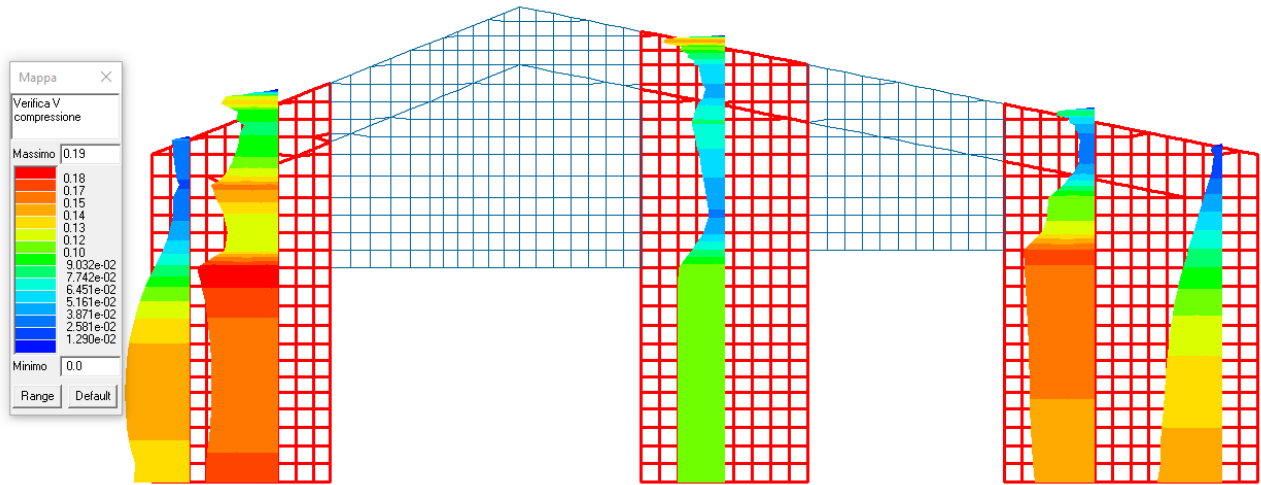


Fig 125. SLU: Mappa di Verifica V compressione – Verifica soddisfatta ($\rho \leq 1$).

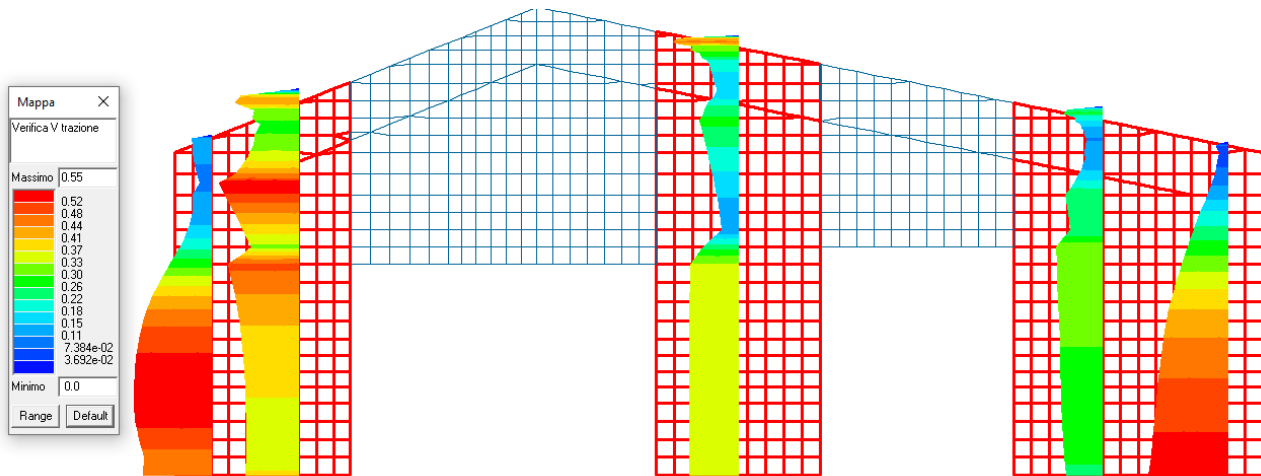


Fig 126. SLU: Mappa di verifica V trazione – Verifiche soddisfatte ($\rho \leq 1$).

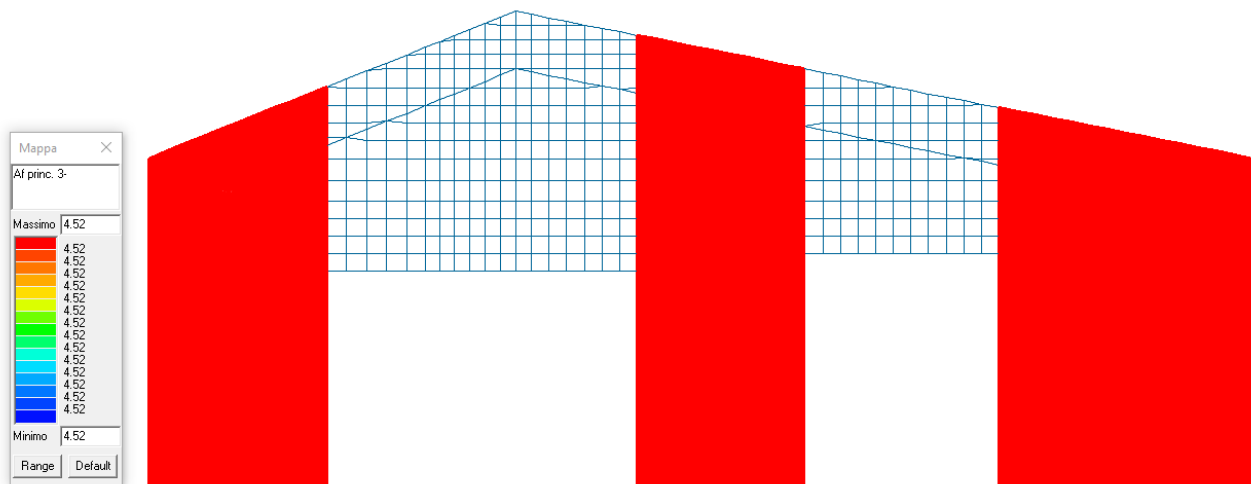


Fig 127. Mappa Armatura Verticale (singolo strato) da Calcolo [cm^2/m].

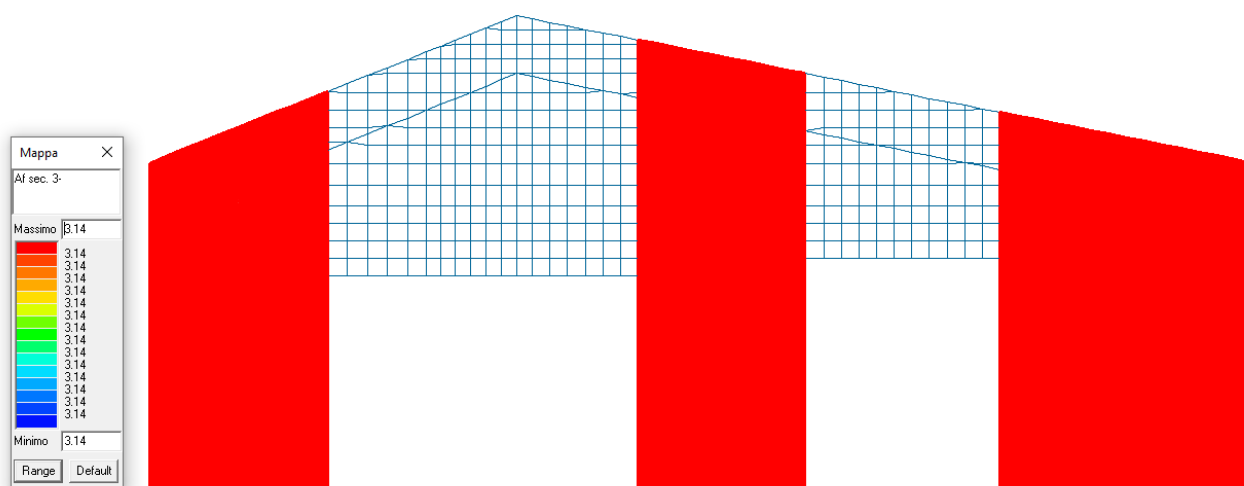


Fig 128. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm²/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 14 | 561.61 | 11.20 | 207.65 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.52 | 0.19 | 0.23 | 0.11 | 0.35 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.52 | 0.21 | 0.23 | 0.11 | 0.35 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.51 | 0.15 | 0.23 | 0.11 | 0.35 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.51 | 0.13 | 0.23 | 0.11 | 0.34 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.51 | 0.10 | 0.23 | 0.11 | 0.35 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.51 | 0.11 | 0.23 | 0.11 | 0.34 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.50 | 0.18 | 0.23 | 0.11 | 0.34 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.50 | 0.21 | 0.23 | 0.11 | 0.34 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.50 | 0.24 | 0.23 | 0.11 | 0.34 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.50 | 0.26 | 0.23 | 0.11 | 0.34 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.50 | 0.27 | 0.23 | 0.11 | 0.34 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.49 | 0.28 | 0.23 | 0.11 | 0.34 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.49 | 0.27 | 0.23 | 0.11 | 0.34 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.46 | 0.23 | 0.23 | 0.08 | 0.25 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.41 | 0.19 | 0.23 | 0.05 | 0.11 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.38 | 0.11 | 0.23 | 0.04 | 0.13 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.36 | 0.10 | 0.23 | 0.04 | 0.15 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.33 | 0.09 | 0.23 | 0.05 | 0.18 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.30 | 0.12 | 0.23 | 0.06 | 0.21 | 0.0 |
| 430.0 | 1d12 | 1d12/25 | 1d10/25 | 0.28 | 0.18 | 0.23 | 0.07 | 0.24 | 0.0 |
| 448.4 | 1d12 | 1d12/25 | 1d10/25 | 0.27 | 0.23 | 0.23 | 0.08 | 0.27 | 0.0 |
| 452.0 | 1d12 | 1d12/25 | 1d10/25 | 0.25 | 0.22 | 0.23 | 0.08 | 0.26 | 0.0 |
| 453.2 | 1d12 | 1d12/25 | 1d10/25 | 0.24 | 0.26 | 0.23 | 0.08 | 0.26 | 0.0 |
| 457.7 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.24 | 0.23 | 0.07 | 0.25 | 0.0 |
| 462.3 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.22 | 0.23 | 0.07 | 0.23 | 0.0 |
| 466.9 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.20 | 0.23 | 0.07 | 0.22 | 0.0 |
| 471.5 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.20 | 0.23 | 0.06 | 0.21 | 0.0 |
| 474.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.20 | 0.23 | 0.06 | 0.20 | 0.0 |
| 476.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.20 | 0.23 | 0.06 | 0.18 | 0.0 |
| 480.6 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.20 | 0.23 | 0.05 | 0.17 | 0.0 |
| 485.2 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.19 | 0.23 | 0.05 | 0.15 | 0.0 |
| 489.8 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.19 | 0.23 | 0.05 | 0.15 | 0.0 |
| 495.9 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.19 | 0.23 | 0.05 | 0.16 | 0.0 |
| 496.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.18 | 0.23 | 0.05 | 0.16 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| 496.1 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.15 | 0.23 | 0.05 | 0.16 | 0.0 |
| 520.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.13 | 0.23 | 0.06 | 0.20 | 0.0 |
| 520.1 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.09 | 0.23 | 0.07 | 0.20 | 0.0 |
| 524.8 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.08 | 0.23 | 0.07 | 0.21 | 0.0 |
| 529.4 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.09 | 0.23 | 0.09 | 0.26 | 0.0 |
| 534.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.09 | 0.23 | 0.09 | 0.27 | 0.0 |
| 538.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.13 | 0.23 | 0.11 | 0.33 | 0.0 |
| 538.6 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.09 | 0.23 | 0.10 | 0.33 | 0.0 |
| 543.2 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.09 | 0.23 | 0.10 | 0.32 | 0.0 |
| 547.8 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.15 | 0.23 | 0.15 | 0.45 | 0.0 |
| 552.4 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.12 | 0.23 | 0.14 | 0.43 | 0.0 |
| 556.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.23 | 0.0 | 0.0 | 0.0 |
| 557.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.23 | 0.0 | 0.0 | 0.0 |
| 561.6 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.23 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.52 | 0.28 | 0.23 | 0.15 | 0.45 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|------------|------------|-----------|-----------|------------|------------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -4.234e+04 | -2.323e+04 | 2.369e+05 | 4.992e+04 | -2.117e+04 | -2.587e+04 | 7369.22 | 6494.46 |
| 23.0 | -4.234e+04 | -2.323e+04 | 2.449e+05 | 5.324e+04 | -2.117e+04 | -2.587e+04 | 7369.22 | 6494.46 |
| 46.0 | -4.215e+04 | -2.399e+04 | 6.880e+05 | 1.758e+04 | -2.117e+04 | -2.571e+04 | 7378.85 | 6504.09 |
| 69.0 | -4.196e+04 | -2.380e+04 | 5.792e+05 | 1.342e+04 | -2.117e+04 | -2.553e+04 | 7351.33 | 6476.58 |
| 92.0 | -4.176e+04 | -2.368e+04 | 4.666e+05 | 1.211e+04 | -2.117e+04 | -2.535e+04 | 7364.57 | 6489.82 |
| 112.0 | -4.158e+04 | -2.585e+04 | 1.832e+05 | 2.790e+04 | -2.117e+04 | -2.519e+04 | 7352.78 | 6478.03 |
| 132.0 | -4.141e+04 | -2.549e+04 | 1.591e+05 | 4.807e+04 | -2.117e+04 | -2.502e+04 | 7340.10 | 6465.34 |
| 152.0 | -4.124e+04 | -2.552e+04 | 8.054e+04 | 5.757e+04 | -2.117e+04 | -2.475e+04 | 7330.87 | 6456.12 |
| 172.0 | -4.107e+04 | -2.542e+04 | 1.239e+05 | 6.447e+04 | -2.117e+04 | -2.487e+04 | 7315.40 | 6440.65 |
| 196.0 | -4.088e+04 | -2.526e+04 | 1.537e+05 | 7.054e+04 | -2.117e+04 | -2.461e+04 | 7296.99 | 6422.23 |
| 220.0 | -4.068e+04 | -2.520e+04 | 1.999e+05 | 7.401e+04 | -2.117e+04 | -2.454e+04 | 7272.44 | 6397.68 |
| 244.0 | -4.048e+04 | -2.500e+04 | 2.240e+05 | 7.443e+04 | -2.117e+04 | -2.422e+04 | 7250.27 | 6375.51 |
| 267.0 | -4.028e+04 | -2.496e+04 | 2.817e+05 | 7.214e+04 | -2.117e+04 | -2.409e+04 | 7227.43 | 6352.67 |
| 289.0 | -3.755e+04 | -2.300e+04 | 1.182e+05 | 6.030e+04 | -2.117e+04 | -2.138e+04 | 5033.63 | 4638.12 |
| 311.0 | -3.398e+04 | -2.114e+04 | 1.478e+05 | 4.880e+04 | -2.117e+04 | -2.004e+04 | 3231.14 | 2150.50 |
| 333.0 | -3.141e+04 | -1.956e+04 | 1.339e+05 | 2.797e+04 | -2.117e+04 | -3.131e+04 | 2454.25 | 2454.25 |
| 355.0 | -2.913e+04 | -1.666e+04 | 3.437e+05 | 1.430e+04 | -2.117e+04 | -2.913e+04 | 2861.54 | 2861.54 |
| 381.0 | -2.676e+04 | -1.543e+04 | 2.919e+05 | 1.319e+04 | -2.117e+04 | -2.669e+04 | 3406.46 | 3406.46 |
| 408.0 | -2.460e+04 | -1.334e+04 | 2.647e+04 | 2.765e+04 | -2.117e+04 | -2.459e+04 | 4003.98 | 4003.98 |
| 430.0 | -2.306e+04 | -1.248e+04 | 1.720e+04 | 4.037e+04 | -2.117e+04 | -2.306e+04 | 4561.42 | 4561.42 |
| 448.4 | -2.190e+04 | -1.183e+04 | 1.011e+04 | 5.257e+04 | -2.117e+04 | -2.190e+04 | 5095.98 | 5095.98 |
| 452.0 | -2.047e+04 | -1.097e+04 | 6.208e+04 | 4.879e+04 | -2.117e+04 | -2.047e+04 | 4957.84 | 4957.84 |
| 453.2 | -1.982e+04 | -1.075e+04 | 9.363e+04 | 5.654e+04 | -2.117e+04 | -1.982e+04 | 4873.68 | 4873.68 |
| 457.7 | -1.794e+04 | -9661.72 | 1.609e+05 | 5.103e+04 | -2.117e+04 | -1.794e+04 | 4631.89 | 4631.89 |
| 462.3 | -1.598e+04 | -8519.39 | 2.010e+05 | 4.580e+04 | -2.117e+04 | -1.598e+04 | 4405.88 | 4405.88 |
| 466.9 | -1.398e+04 | -7466.41 | 2.226e+05 | 4.088e+04 | -2.117e+04 | -1.398e+04 | 4200.99 | 4200.99 |
| 471.5 | -1.189e+04 | -7008.98 | 3.161e+05 | 3.905e+04 | -2.117e+04 | -1.189e+04 | 3999.48 | 3999.48 |
| 474.0 | -1.064e+04 | -6337.79 | 3.015e+05 | 3.748e+04 | -2.117e+04 | -1.064e+04 | 3820.09 | 3820.09 |
| 476.0 | -9543.51 | -5764.28 | 2.859e+05 | 3.772e+04 | -2.117e+04 | -9543.51 | 3453.26 | 3453.26 |
| 480.6 | -7582.47 | -4578.92 | 2.356e+05 | 3.680e+04 | -2.117e+04 | -7582.47 | 3107.15 | 3107.15 |
| 485.2 | -5692.71 | -3435.63 | 1.632e+05 | 3.616e+04 | -2.117e+04 | -5692.71 | 2909.52 | 2909.52 |
| 489.8 | -3982.76 | -2417.67 | 7.851e+04 | 3.609e+04 | -2.117e+04 | -3982.76 | 2833.22 | 2833.22 |
| 495.9 | -3693.18 | -2260.47 | 7.589e+04 | 3.434e+04 | -2.117e+04 | -3693.18 | 3061.49 | 3061.49 |
| 496.0 | -3654.23 | -2191.08 | 7.210e+04 | 3.250e+04 | -2.117e+04 | -3654.23 | 3064.46 | 3064.46 |
| 496.1 | -3491.67 | -2048.71 | 7.174e+04 | 2.814e+04 | -2.117e+04 | -2270.29 | 3245.73 | 3086.92 |
| 520.0 | -2584.34 | -1581.04 | 6.884e+04 | 2.280e+04 | -2.117e+04 | -2584.34 | 3783.42 | 3783.42 |
| 520.1 | -2433.00 | -1025.47 | 3.885e+04 | 1.673e+04 | -2.117e+04 | -2067.98 | 4422.66 | 3777.12 |
| 524.8 | -2219.90 | -938.48 | 2.777e+04 | 1.475e+04 | -2.117e+04 | -1918.25 | 4207.45 | 3750.29 |
| 529.4 | -2001.50 | -858.42 | 1.820e+04 | 1.278e+04 | -2.117e+04 | -1750.39 | 3946.79 | 3639.38 |
| 534.0 | -1756.68 | -696.33 | 3476.39 | 1.229e+04 | -2.117e+04 | -1575.28 | 3616.98 | 3435.06 |
| 538.0 | -1520.44 | -581.57 | 1573.01 | 1.191e+04 | -2.117e+04 | -1377.66 | 3269.82 | 3160.48 |
| 538.6 | -1423.04 | -831.03 | 1.036e+04 | 8591.48 | -2.117e+04 | -1135.27 | 3163.91 | 3059.19 |
| 543.2 | -1182.63 | -696.17 | 6367.09 | 7982.18 | -2.117e+04 | -1025.12 | 2741.69 | 2613.73 |
| 547.8 | -938.41 | -546.52 | 2815.66 | 6950.16 | -2.117e+04 | -931.50 | 2221.05 | 2097.40 |
| 552.4 | -721.25 | -402.69 | 856.33 | 5373.65 | -2.117e+04 | -721.25 | 1606.25 | 1486.68 |
| 556.0 | 0.0 | 0.0 | 0.0 | 0.0 | -2.117e+04 | 0.0 | 0.0 | 0.0 |
| 557.0 | 0.0 | 0.0 | 0.0 | 0.0 | -2.117e+04 | 0.0 | 0.0 | 0.0 |
| 561.6 | 0.0 | 0.0 | 0.0 | 0.0 | -2.117e+04 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 7369.22 | 6.524e+04 | 1.00 | 1.880e+04 | 6.491e+04 |
| 23.0 | 1.00 | 7369.22 | 6.524e+04 | 1.00 | 1.880e+04 | 6.491e+04 |
| 46.0 | 1.00 | 7378.85 | 6.521e+04 | 1.00 | 1.880e+04 | 6.488e+04 |
| 69.0 | 1.00 | 7351.33 | 6.518e+04 | 1.00 | 1.880e+04 | 6.486e+04 |
| 92.0 | 1.00 | 7364.57 | 6.514e+04 | 1.00 | 1.880e+04 | 6.484e+04 |
| 112.0 | 1.00 | 7352.78 | 6.511e+04 | 1.00 | 1.880e+04 | 6.481e+04 |
| 132.0 | 1.00 | 7340.10 | 6.508e+04 | 1.00 | 1.880e+04 | 6.480e+04 |
| 152.0 | 1.00 | 7330.87 | 6.503e+04 | 1.00 | 1.880e+04 | 6.480e+04 |
| 172.0 | 1.00 | 7315.40 | 6.505e+04 | 1.00 | 1.880e+04 | 6.473e+04 |
| 196.0 | 1.00 | 7296.99 | 6.501e+04 | 1.00 | 1.880e+04 | 6.472e+04 |
| 220.0 | 1.00 | 7272.44 | 6.499e+04 | 1.00 | 1.880e+04 | 6.468e+04 |
| 244.0 | 1.00 | 7250.27 | 6.493e+04 | 1.00 | 1.880e+04 | 6.468e+04 |
| 267.0 | 1.00 | 7227.43 | 6.491e+04 | 1.00 | 1.880e+04 | 6.465e+04 |
| 289.0 | 1.00 | 5033.63 | 6.441e+04 | 1.00 | 1.880e+04 | 6.457e+04 |
| 311.0 | 1.00 | 3231.14 | 6.416e+04 | 1.00 | 1.880e+04 | 6.671e+04 |
| 333.0 | 1.00 | 2454.25 | 6.624e+04 | 1.00 | 1.880e+04 | 6.624e+04 |
| 355.0 | 1.00 | 2861.54 | 6.584e+04 | 1.00 | 1.880e+04 | 6.584e+04 |
| 381.0 | 1.00 | 3406.46 | 6.539e+04 | 1.00 | 1.880e+04 | 6.539e+04 |
| 408.0 | 1.00 | 4003.98 | 6.500e+04 | 1.00 | 1.880e+04 | 6.500e+04 |
| 430.0 | 1.00 | 4561.42 | 6.472e+04 | 1.00 | 1.880e+04 | 6.472e+04 |
| 448.4 | 1.00 | 5095.98 | 6.451e+04 | 1.00 | 1.880e+04 | 6.451e+04 |
| 452.0 | 1.00 | 4957.84 | 6.424e+04 | 1.00 | 1.880e+04 | 6.424e+04 |
| 453.2 | 1.00 | 4873.68 | 6.412e+04 | 1.00 | 1.880e+04 | 6.412e+04 |
| 457.7 | 1.00 | 4631.89 | 6.378e+04 | 1.00 | 1.880e+04 | 6.378e+04 |
| 462.3 | 1.00 | 4405.88 | 6.342e+04 | 1.00 | 1.880e+04 | 6.342e+04 |
| 466.9 | 1.00 | 4200.99 | 6.305e+04 | 1.00 | 1.880e+04 | 6.305e+04 |
| 471.5 | 1.00 | 3999.48 | 6.266e+04 | 1.00 | 1.880e+04 | 6.266e+04 |
| 474.0 | 1.00 | 3820.09 | 6.243e+04 | 1.00 | 1.880e+04 | 6.243e+04 |
| 476.0 | 1.00 | 3453.26 | 6.223e+04 | 1.00 | 1.880e+04 | 6.223e+04 |
| 480.6 | 1.00 | 3107.15 | 6.187e+04 | 1.00 | 1.880e+04 | 6.187e+04 |
| 485.2 | 1.00 | 2909.52 | 6.152e+04 | 1.00 | 1.880e+04 | 6.152e+04 |
| 489.8 | 1.00 | 2833.22 | 6.120e+04 | 1.00 | 1.880e+04 | 6.120e+04 |
| 495.9 | 1.00 | 3061.49 | 6.115e+04 | 1.00 | 1.880e+04 | 6.115e+04 |
| 496.0 | 1.00 | 3064.46 | 6.114e+04 | 1.00 | 1.880e+04 | 6.114e+04 |
| 496.1 | 1.00 | 3245.73 | 6.089e+04 | 1.00 | 1.880e+04 | 6.111e+04 |
| 520.0 | 1.00 | 3783.42 | 6.095e+04 | 1.00 | 1.880e+04 | 6.095e+04 |
| 520.1 | 1.00 | 4422.66 | 6.085e+04 | 1.00 | 1.880e+04 | 6.092e+04 |
| 524.8 | 1.00 | 4207.45 | 5.711e+04 | 1.00 | 1.764e+04 | 5.717e+04 |
| 529.4 | 1.00 | 3946.79 | 4.551e+04 | 1.00 | 1.405e+04 | 4.555e+04 |
| 534.0 | 1.00 | 3616.98 | 4.186e+04 | 1.00 | 1.292e+04 | 4.190e+04 |
| 538.0 | 1.00 | 3269.82 | 3.073e+04 | 1.00 | 9481.02 | 3.075e+04 |
| 538.6 | 1.00 | 3163.91 | 3.021e+04 | 1.00 | 9333.49 | 3.026e+04 |
| 543.2 | 1.00 | 2741.69 | 2.658e+04 | 1.00 | 8203.65 | 2.661e+04 |
| 547.8 | 1.00 | 2221.05 | 1.498e+04 | 1.00 | 4617.62 | 1.498e+04 |
| 552.4 | 1.00 | 1606.25 | 1.133e+04 | 1.00 | 3487.78 | 1.132e+04 |
| 556.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 557.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 561.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 19 | 471.23 | 11.20 | 225.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.21 | 0.10 | 0.16 | 0.14 | 0.25 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.10 | 0.16 | 0.15 | 0.26 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.09 | 0.16 | 0.15 | 0.28 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.08 | 0.16 | 0.15 | 0.28 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.23 | 0.08 | 0.16 | 0.15 | 0.29 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.23 | 0.07 | 0.16 | 0.16 | 0.29 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.23 | 0.07 | 0.16 | 0.16 | 0.29 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.24 | 0.07 | 0.16 | 0.16 | 0.29 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.24 | 0.08 | 0.16 | 0.16 | 0.30 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.25 | 0.09 | 0.16 | 0.16 | 0.30 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.26 | 0.10 | 0.16 | 0.16 | 0.31 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.26 | 0.12 | 0.16 | 0.16 | 0.31 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.27 | 0.13 | 0.16 | 0.17 | 0.32 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.27 | 0.15 | 0.16 | 0.17 | 0.33 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.24 | 0.12 | 0.16 | 0.13 | 0.23 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.23 | 0.11 | 0.16 | 0.11 | 0.24 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.11 | 0.16 | 0.11 | 0.26 | 0.0 |
| 359.5 | 1d12 | 1d12/25 | 1d10/25 | 0.21 | 0.11 | 0.16 | 0.10 | 0.24 | 0.0 |
| 364.0 | 1d12 | 1d12/25 | 1d10/25 | 0.20 | 0.13 | 0.16 | 0.09 | 0.22 | 0.0 |
| 368.4 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.14 | 0.16 | 0.08 | 0.20 | 0.0 |
| 372.9 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.14 | 0.16 | 0.07 | 0.19 | 0.0 |
| 377.4 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.14 | 0.16 | 0.06 | 0.17 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.13 | 0.16 | 0.06 | 0.16 | 0.0 |
| 381.9 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.13 | 0.16 | 0.05 | 0.16 | 0.0 |
| 386.3 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.12 | 0.16 | 0.05 | 0.15 | 0.0 |
| 390.8 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.10 | 0.16 | 0.04 | 0.14 | 0.0 |
| 395.3 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.07 | 0.16 | 0.04 | 0.13 | 0.0 |
| 399.9 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.03 | 0.16 | 0.04 | 0.12 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.03 | 0.16 | 0.04 | 0.12 | 0.0 |
| 426.1 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.03 | 0.16 | 0.03 | 0.11 | 0.0 |
| 430.0 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.03 | 0.16 | 0.04 | 0.12 | 0.0 |
| 430.6 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.02 | 0.16 | 0.04 | 0.12 | 0.0 |
| 435.1 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.02 | 0.16 | 0.04 | 0.12 | 0.0 |
| 439.6 | 1d12 | 1d12/25 | 1d10/25 | 0.02 | 0.02 | 0.16 | 0.05 | 0.15 | 0.0 |
| 444.1 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.02 | 0.16 | 0.05 | 0.15 | 0.0 |
| 448.6 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.02 | 0.16 | 0.06 | 0.19 | 0.0 |
| 452.0 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.02 | 0.16 | 0.06 | 0.19 | 0.0 |
| 453.1 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.01 | 0.16 | 0.06 | 0.19 | 0.0 |
| 457.6 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.01 | 0.16 | 0.09 | 0.27 | 0.0 |
| 462.1 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.01 | 0.16 | 0.09 | 0.25 | 0.0 |
| 466.6 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.16 | 0.0 | 0.0 | 0.0 |
| 471.2 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.16 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.27 | 0.15 | 0.16 | 0.17 | 0.33 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|------------|------------|-----------|-----------|-----------|------------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1.882e+04 | -1.591e+04 | 5.332e+05 | 1.067e+04 | -9409.89 | -6703.44 | 1.034e+04 | 5536.79 |
| 23.0 | -1.932e+04 | -1.626e+04 | 5.509e+05 | 1.224e+04 | -9409.89 | -7051.76 | 1.062e+04 | 5853.65 |
| 46.0 | -1.959e+04 | -1.594e+04 | 5.061e+05 | 8186.28 | -9409.89 | -7800.43 | 1.090e+04 | 6112.22 |
| 69.0 | -1.991e+04 | -1.557e+04 | 4.704e+05 | 5953.28 | -9409.89 | -8685.58 | 1.114e+04 | 6266.62 |
| 92.0 | -2.023e+04 | -1.510e+04 | 4.383e+05 | 4720.46 | -9409.89 | -9612.34 | 1.128e+04 | 6363.87 |
| 112.0 | -2.053e+04 | -1.466e+04 | 4.117e+05 | 3044.40 | -9409.89 | -1.046e+04 | 1.138e+04 | 6422.08 |
| 132.0 | -2.088e+04 | -1.419e+04 | 3.922e+05 | 2425.93 | -9409.89 | -1.130e+04 | 1.147e+04 | 6467.62 |
| 152.0 | -2.128e+04 | -2.103e+04 | 4.315e+05 | 5941.00 | -9409.89 | -1.207e+04 | 1.157e+04 | 6510.32 |
| 172.0 | -2.170e+04 | -2.135e+04 | 4.857e+05 | 7101.28 | -9409.89 | -1.282e+04 | 1.169e+04 | 6560.75 |
| 196.0 | -2.223e+04 | -2.223e+04 | 5.605e+05 | 7859.74 | -9409.89 | -1.390e+04 | 1.184e+04 | 6644.41 |
| 220.0 | -2.277e+04 | -2.277e+04 | 6.353e+05 | 9174.46 | -9409.89 | -1.492e+04 | 1.201e+04 | 6767.02 |
| 244.0 | -2.330e+04 | -2.330e+04 | 7.150e+05 | 1.075e+04 | -9409.89 | -1.599e+04 | 1.222e+04 | 6908.71 |
| 267.0 | -2.375e+04 | -2.375e+04 | 8.002e+05 | 1.277e+04 | -9409.89 | -1.695e+04 | 1.247e+04 | 7058.28 |
| 289.0 | -2.408e+04 | -2.408e+04 | 8.974e+05 | 1.575e+04 | -9409.89 | -1.772e+04 | 1.274e+04 | 7208.15 |
| 311.0 | -2.152e+04 | -2.152e+04 | 6.654e+05 | 1.599e+04 | -9409.89 | -1.569e+04 | 9346.65 | 5008.03 |
| 333.0 | -2.025e+04 | -2.025e+04 | 5.847e+05 | 1.787e+04 | -9409.89 | -1.481e+04 | 8332.28 | 5278.67 |
| 355.0 | -1.920e+04 | -1.920e+04 | 5.290e+05 | 1.873e+04 | -9409.89 | -1.380e+04 | 8180.19 | 5726.51 |
| 359.5 | -1.879e+04 | -1.737e+04 | 4.917e+05 | 2.154e+04 | -9409.89 | -1.374e+04 | 7176.18 | 5248.49 |
| 364.0 | -1.750e+04 | -1.685e+04 | 5.854e+05 | 2.222e+04 | -9409.89 | -1.280e+04 | 6508.20 | 4846.47 |
| 368.4 | -1.599e+04 | -1.599e+04 | 6.704e+05 | 2.093e+04 | -9409.89 | -1.178e+04 | 5790.78 | 4473.51 |
| 372.9 | -1.445e+04 | -1.445e+04 | 7.072e+05 | 1.902e+04 | -9409.89 | -1.076e+04 | 5145.03 | 4142.96 |
| 377.4 | -1.285e+04 | -1.285e+04 | 7.120e+05 | 1.608e+04 | -9409.89 | -9862.76 | 4598.88 | 3839.80 |
| 381.0 | -1.148e+04 | -1.148e+04 | 6.910e+05 | 1.281e+04 | -9409.89 | -8970.23 | 4170.62 | 3607.37 |
| 381.9 | -1.092e+04 | -1.092e+04 | 6.864e+05 | 1.145e+04 | -9409.89 | -8203.55 | 3996.55 | 3535.85 |
| 386.3 | -9118.25 | -9118.25 | 6.205e+05 | 7901.16 | -9409.89 | -7008.72 | 3530.81 | 3266.84 |
| 390.8 | -7162.87 | -7162.87 | 5.084e+05 | 4887.60 | -9409.89 | -5687.58 | 3043.81 | 3029.98 |
| 395.3 | -5095.11 | -5095.11 | 3.462e+05 | 2256.56 | -9409.89 | -4905.60 | 2843.08 | 2843.08 |
| 399.9 | -3043.70 | -2491.51 | 1.475e+05 | 1168.56 | -9409.89 | -2936.18 | 2655.94 | 2655.94 |
| 408.0 | -2861.20 | -2395.28 | 1.400e+05 | 593.40 | -9409.89 | -2767.89 | 2696.17 | 2696.17 |
| 426.1 | -2167.46 | -1749.53 | 1.262e+05 | 3814.94 | -9409.89 | -2103.89 | 2404.18 | 2404.18 |
| 430.0 | -1947.41 | -1774.53 | 9.757e+04 | 2669.23 | -9409.89 | -1526.56 | 2329.30 | 2272.47 |
| 430.6 | -1793.49 | -1446.18 | 7.504e+04 | 2189.04 | -9409.89 | -1400.79 | 2308.67 | 2249.12 |
| 435.1 | -1673.09 | -1315.40 | 5.618e+04 | 1712.24 | -9409.89 | -1285.08 | 2188.43 | 2135.89 |
| 439.6 | -1538.55 | -1253.19 | 4.057e+04 | 1200.63 | -9409.89 | -1185.00 | 2062.40 | 2037.23 |
| 444.1 | -1376.77 | -1171.12 | 2.793e+04 | 871.26 | -9409.89 | -1376.77 | 1923.95 | 1923.95 |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|----------|----------|----------|----------|----------|
| 448.6 | -1187.86 | -1120.70 | 1.779e+04 | 855.99 | -9409.89 | -1187.86 | 1763.63 | 1763.63 |
| 452.0 | -1050.12 | -1039.50 | 1.101e+04 | 816.40 | -9409.89 | -1039.50 | 1649.00 | 1601.12 |
| 453.1 | -956.93 | -773.93 | 8195.53 | 446.81 | -9409.89 | -815.02 | 1521.88 | 1512.32 |
| 457.6 | -753.10 | -466.02 | 1073.97 | 680.46 | -9409.89 | -694.52 | 1320.84 | 1211.09 |
| 462.1 | -525.94 | -196.53 | 77.47 | 493.31 | -9409.89 | -512.32 | 965.43 | 856.53 |
| 466.6 | 0.0 | 0.0 | 0.0 | 0.0 | -9409.89 | 0.0 | 0.0 | 0.0 |
| 471.2 | 0.0 | 0.0 | 0.0 | 0.0 | -9409.89 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 1.034e+04 | 7.253e+04 | 1.00 | 2.213e+04 | 7.439e+04 |
| 23.0 | 1.00 | 1.062e+04 | 7.260e+04 | 1.00 | 2.213e+04 | 7.452e+04 |
| 46.0 | 1.00 | 1.090e+04 | 7.275e+04 | 1.00 | 2.213e+04 | 7.462e+04 |
| 69.0 | 1.00 | 1.114e+04 | 7.293e+04 | 1.00 | 2.213e+04 | 7.473e+04 |
| 92.0 | 1.00 | 1.128e+04 | 7.311e+04 | 1.00 | 2.213e+04 | 7.485e+04 |
| 112.0 | 1.00 | 1.138e+04 | 7.328e+04 | 1.00 | 2.213e+04 | 7.494e+04 |
| 132.0 | 1.00 | 1.147e+04 | 7.345e+04 | 1.00 | 2.213e+04 | 7.504e+04 |
| 152.0 | 1.00 | 1.157e+04 | 7.360e+04 | 1.00 | 2.213e+04 | 7.513e+04 |
| 172.0 | 1.00 | 1.169e+04 | 7.376e+04 | 1.00 | 2.213e+04 | 7.521e+04 |
| 196.0 | 1.00 | 1.184e+04 | 7.397e+04 | 1.00 | 2.213e+04 | 7.563e+04 |
| 220.0 | 1.00 | 1.201e+04 | 7.417e+04 | 1.00 | 2.213e+04 | 7.574e+04 |
| 244.0 | 1.00 | 1.222e+04 | 7.439e+04 | 1.00 | 2.213e+04 | 7.585e+04 |
| 267.0 | 1.00 | 1.247e+04 | 7.458e+04 | 1.00 | 2.213e+04 | 7.594e+04 |
| 289.0 | 1.00 | 1.274e+04 | 7.473e+04 | 1.00 | 2.213e+04 | 7.600e+04 |
| 311.0 | 1.00 | 9346.65 | 7.433e+04 | 1.00 | 2.213e+04 | 7.549e+04 |
| 333.0 | 1.00 | 8332.28 | 7.415e+04 | 1.00 | 2.213e+04 | 7.524e+04 |
| 355.0 | 1.00 | 8180.19 | 7.395e+04 | 1.00 | 2.213e+04 | 7.503e+04 |
| 359.5 | 1.00 | 7176.18 | 7.394e+04 | 1.00 | 2.213e+04 | 7.495e+04 |
| 364.0 | 1.00 | 6508.20 | 7.375e+04 | 1.00 | 2.213e+04 | 7.469e+04 |
| 368.4 | 1.00 | 5790.78 | 7.355e+04 | 1.00 | 2.213e+04 | 7.439e+04 |
| 372.9 | 1.00 | 5145.03 | 7.334e+04 | 1.00 | 2.213e+04 | 7.408e+04 |
| 377.4 | 1.00 | 4598.88 | 7.316e+04 | 1.00 | 2.213e+04 | 7.376e+04 |
| 381.0 | 1.00 | 4170.62 | 7.299e+04 | 1.00 | 2.213e+04 | 7.349e+04 |
| 381.9 | 1.00 | 3996.55 | 7.283e+04 | 1.00 | 2.213e+04 | 7.338e+04 |
| 386.3 | 1.00 | 3530.81 | 7.259e+04 | 1.00 | 2.213e+04 | 7.302e+04 |
| 390.8 | 1.00 | 3043.81 | 7.233e+04 | 1.00 | 2.213e+04 | 7.262e+04 |
| 395.3 | 1.00 | 2843.08 | 7.217e+04 | 1.00 | 2.213e+04 | 7.217e+04 |
| 399.9 | 1.00 | 2655.94 | 7.178e+04 | 1.00 | 2.213e+04 | 7.178e+04 |
| 408.0 | 1.00 | 2696.17 | 7.175e+04 | 1.00 | 2.213e+04 | 7.175e+04 |
| 426.1 | 1.00 | 2404.18 | 7.161e+04 | 1.00 | 2.213e+04 | 7.161e+04 |
| 430.0 | 1.00 | 2329.30 | 6.050e+04 | 1.00 | 1.872e+04 | 6.057e+04 |
| 430.6 | 1.00 | 2308.67 | 6.000e+04 | 1.00 | 1.857e+04 | 6.006e+04 |
| 435.1 | 1.00 | 2188.43 | 5.643e+04 | 1.00 | 1.746e+04 | 5.650e+04 |
| 439.6 | 1.00 | 2062.40 | 4.494e+04 | 1.00 | 1.390e+04 | 4.499e+04 |
| 444.1 | 1.00 | 1923.95 | 4.143e+04 | 1.00 | 1.280e+04 | 4.143e+04 |
| 448.6 | 1.00 | 1763.63 | 2.991e+04 | 1.00 | 9235.24 | 2.991e+04 |
| 452.0 | 1.00 | 1649.00 | 2.723e+04 | 1.00 | 8406.12 | 2.723e+04 |
| 453.1 | 1.00 | 1521.88 | 2.630e+04 | 1.00 | 8129.96 | 2.633e+04 |
| 457.6 | 1.00 | 1320.84 | 1.479e+04 | 1.00 | 4568.50 | 1.480e+04 |
| 462.1 | 1.00 | 965.43 | 1.122e+04 | 1.00 | 3463.22 | 1.122e+04 |
| 466.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 471.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 34 | 426.11 | 12.00 | 90.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|---------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.20 | 0.07 | 0.06 | 0.15 | 0.55 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.19 | 0.07 | 0.06 | 0.15 | 0.53 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.06 | 0.06 | 0.15 | 0.52 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.05 | 0.06 | 0.14 | 0.51 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.04 | 0.06 | 0.14 | 0.50 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.04 | 0.06 | 0.14 | 0.49 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.04 | 0.06 | 0.13 | 0.48 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.03 | 0.06 | 0.13 | 0.46 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.03 | 0.06 | 0.13 | 0.45 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.03 | 0.06 | 0.12 | 0.42 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.02 | 0.06 | 0.11 | 0.39 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.03 | 0.06 | 0.10 | 0.36 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.04 | 0.06 | 0.09 | 0.32 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.04 | 0.06 | 0.08 | 0.28 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.03 | 0.06 | 0.07 | 0.23 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.03 | 0.06 | 0.05 | 0.19 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.08 | 0.06 | 0.04 | 0.14 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.07 | 0.06 | 0.02 | 0.08 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.04 | 0.06 | 0.06 | 0.02 | 0.06 | 0.0 |
| 412.6 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.17 | 0.06 | 0.02 | 0.07 | 0.0 |
| 417.1 | 1d12 | 1d12/25 | 1d10/25 | 0.03 | 0.11 | 0.06 | 0.02 | 0.07 | 0.0 |
| 421.6 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.06 | 0.0 | 0.0 | 0.0 |
| 426.1 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.06 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.20 | 0.17 | 0.06 | 0.15 | 0.55 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|----------|----------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -7752.59 | -7567.66 | 6.314e+04 | 2092.49 | -3876.29 | -7532.55 | 4465.68 | 4465.68 |
| 23.0 | -7392.77 | -1067.41 | 4.962e+04 | 503.35 | -3876.29 | -7342.06 | 4292.65 | 4292.65 |
| 46.0 | -6880.26 | -872.82 | 4.108e+04 | 920.51 | -3876.29 | -6859.81 | 4247.99 | 4247.99 |
| 69.0 | -6463.94 | -793.41 | 3.612e+04 | 1061.67 | -3876.29 | -6356.58 | 4140.54 | 4140.54 |
| 92.0 | -5937.38 | -868.78 | 3.150e+04 | 1240.11 | -3876.29 | -5936.04 | 4040.14 | 4040.14 |
| 112.0 | -5459.95 | -889.25 | 2.899e+04 | 1283.07 | -3876.29 | -5459.57 | 3954.53 | 3954.53 |
| 132.0 | -5071.29 | -980.63 | 2.485e+04 | 1377.19 | -3876.29 | -5070.54 | 3864.17 | 3864.17 |
| 152.0 | -4609.50 | -1002.37 | 2.337e+04 | 1483.68 | -3876.29 | -4607.65 | 3758.84 | 3758.84 |
| 172.0 | -4155.81 | -1020.88 | 2.106e+04 | 1583.71 | -3876.29 | -4154.45 | 3629.34 | 3629.34 |
| 196.0 | -3665.58 | -999.58 | 1.680e+04 | 1668.02 | -3876.29 | -3665.58 | 3445.62 | 3445.62 |
| 220.0 | -3251.30 | -2851.63 | 8555.39 | 2207.62 | -3876.29 | -3210.25 | 3206.57 | 3206.57 |
| 244.0 | -2954.62 | -2628.43 | 8319.92 | 2859.47 | -3876.29 | -2811.58 | 2914.65 | 2914.65 |
| 267.0 | -2724.58 | -1223.08 | 1.823e+04 | 2773.90 | -3876.29 | -2483.58 | 2585.04 | 2585.04 |
| 289.0 | -2523.00 | -1208.90 | 1.882e+04 | 2672.95 | -3876.29 | -2178.95 | 2240.70 | 2240.70 |
| 311.0 | -2265.38 | -1375.37 | 1.891e+04 | 1464.97 | -3876.29 | -1841.50 | 1889.75 | 1889.75 |
| 333.0 | -1957.50 | -1388.65 | 2340.26 | 3324.69 | -3876.29 | -1459.12 | 1536.05 | 1536.05 |
| 355.0 | -1620.06 | -1002.34 | 537.38 | 7586.46 | -3876.29 | -949.67 | 1179.98 | 1103.51 |
| 381.0 | -1687.53 | -1440.86 | 1.970e+04 | 6934.27 | -3876.29 | -393.23 | 683.88 | 683.88 |
| 408.0 | -1341.52 | -536.34 | 1.221e+04 | 5762.74 | -3876.29 | -467.08 | 453.84 | 453.84 |
| 412.6 | -932.00 | -297.64 | 1.419e+04 | 8357.43 | -3876.29 | -370.21 | 370.27 | 314.86 |
| 417.1 | -609.77 | -406.17 | 6279.26 | 5250.54 | -3876.29 | -151.89 | 262.54 | 256.47 |
| 421.6 | 0.0 | 0.0 | 0.0 | 0.0 | -3876.29 | 0.0 | 0.0 | 0.0 |
| 426.1 | 0.0 | 0.0 | 0.0 | 0.0 | -3876.29 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 4465.68 | 2.940e+04 | 1.00 | 8129.96 | 2.940e+04 |
| 23.0 | 1.00 | 4292.65 | 2.937e+04 | 1.00 | 8129.96 | 2.937e+04 |
| 46.0 | 1.00 | 4247.99 | 2.928e+04 | 1.00 | 8129.96 | 2.928e+04 |
| 69.0 | 1.00 | 4140.54 | 2.918e+04 | 1.00 | 8129.96 | 2.918e+04 |
| 92.0 | 1.00 | 4040.14 | 2.911e+04 | 1.00 | 8129.96 | 2.911e+04 |
| 112.0 | 1.00 | 3954.53 | 2.902e+04 | 1.00 | 8129.96 | 2.902e+04 |
| 132.0 | 1.00 | 3864.17 | 2.895e+04 | 1.00 | 8129.96 | 2.895e+04 |
| 152.0 | 1.00 | 3758.84 | 2.887e+04 | 1.00 | 8129.96 | 2.887e+04 |
| 172.0 | 1.00 | 3629.34 | 2.878e+04 | 1.00 | 8129.96 | 2.878e+04 |
| 196.0 | 1.00 | 3445.62 | 2.869e+04 | 1.00 | 8129.96 | 2.869e+04 |
| 220.0 | 1.00 | 3206.57 | 2.861e+04 | 1.00 | 8129.96 | 2.861e+04 |
| 244.0 | 1.00 | 2914.65 | 2.854e+04 | 1.00 | 8129.96 | 2.854e+04 |
| 267.0 | 1.00 | 2585.04 | 2.848e+04 | 1.00 | 8129.96 | 2.848e+04 |
| 289.0 | 1.00 | 2240.70 | 2.842e+04 | 1.00 | 8129.96 | 2.842e+04 |
| 311.0 | 1.00 | 1889.75 | 2.836e+04 | 1.00 | 8129.96 | 2.836e+04 |
| 333.0 | 1.00 | 1536.05 | 2.829e+04 | 1.00 | 8129.96 | 2.829e+04 |
| 355.0 | 1.00 | 1179.98 | 2.820e+04 | 1.00 | 8129.96 | 2.821e+04 |
| 381.0 | 1.00 | 683.88 | 2.809e+04 | 1.00 | 8129.96 | 2.809e+04 |
| 408.0 | 1.00 | 453.84 | 2.811e+04 | 1.00 | 8129.96 | 2.811e+04 |
| 412.6 | 1.00 | 370.27 | 1.571e+04 | 1.00 | 4543.94 | 1.571e+04 |
| 417.1 | 1.00 | 262.54 | 1.188e+04 | 1.00 | 3438.65 | 1.188e+04 |
| 421.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 426.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 42 | 444.40 | 12.00 | 90.50 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.22 | 0.04 | 0.06 | 0.13 | 0.47 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.20 | 0.06 | 0.06 | 0.13 | 0.46 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.18 | 0.06 | 0.06 | 0.14 | 0.50 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.16 | 0.05 | 0.06 | 0.15 | 0.53 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.05 | 0.06 | 0.15 | 0.54 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.14 | 0.04 | 0.06 | 0.15 | 0.54 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.13 | 0.04 | 0.06 | 0.15 | 0.53 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.05 | 0.06 | 0.15 | 0.52 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.11 | 0.05 | 0.06 | 0.14 | 0.50 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.10 | 0.05 | 0.06 | 0.13 | 0.47 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.06 | 0.06 | 0.12 | 0.42 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.05 | 0.06 | 0.10 | 0.36 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.09 | 0.05 | 0.06 | 0.08 | 0.29 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.05 | 0.06 | 0.06 | 0.21 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.04 | 0.06 | 0.05 | 0.16 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.05 | 0.06 | 0.04 | 0.12 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.05 | 0.06 | 0.04 | 0.12 | 0.0 |
| 370.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.08 | 0.06 | 0.02 | 0.08 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.05 | 0.10 | 0.06 | 0.03 | 0.10 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.06 | 0.06 | 0.04 | 0.13 | 0.0 |
| 417.3 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.11 | 0.06 | 0.04 | 0.13 | 0.0 |
| 426.3 | 1d12 | 1d12/25 | 1d10/25 | 0.06 | 0.07 | 0.06 | 0.04 | 0.14 | 0.0 |
| 430.0 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.06 | 0.0 | 0.0 | 0.0 |
| 435.3 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.06 | 0.0 | 0.0 | 0.0 |
| 444.4 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.06 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.22 | 0.11 | 0.06 | 0.15 | 0.54 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -8543.05 | -3029.73 | 3.412e+04 | 974.49 | -4271.53 | -7333.86 | 3830.35 | 3830.35 |
| 23.0 | -7707.18 | -2613.30 | 4.584e+04 | 201.68 | -4271.53 | -6917.44 | 3779.22 | 3779.22 |
| 46.0 | -6798.26 | -2244.88 | 4.335e+04 | 1132.19 | -4271.53 | -6247.90 | 4076.97 | 4076.97 |
| 69.0 | -6146.52 | -2055.61 | 4.110e+04 | 1314.84 | -4271.53 | -5677.58 | 4293.54 | 4293.54 |
| 92.0 | -5617.10 | -2047.28 | 3.520e+04 | 1199.21 | -4271.53 | -5255.53 | 4383.11 | 4383.11 |
| 112.0 | -5259.49 | -2003.74 | 3.272e+04 | 1127.70 | -4271.53 | -4810.21 | 4388.18 | 4388.18 |
| 132.0 | -4915.72 | -4842.11 | 3.659e+04 | 1305.86 | -4271.53 | -4391.26 | 4335.26 | 4335.26 |
| 152.0 | -4597.65 | -4501.95 | 3.990e+04 | 1400.25 | -4271.53 | -3991.55 | 4234.15 | 4234.15 |
| 172.0 | -4308.61 | -4196.10 | 4.237e+04 | 1534.72 | -4271.53 | -3616.18 | 4082.37 | 4082.37 |
| 196.0 | -3933.93 | -3798.38 | 4.475e+04 | 1766.92 | -4271.53 | -3188.25 | 3830.82 | 3830.82 |
| 220.0 | -3638.11 | -3494.40 | 4.480e+04 | 1946.38 | -4271.53 | -2812.70 | 3453.48 | 3453.48 |
| 244.0 | -3404.82 | -3264.19 | 4.268e+04 | 1972.05 | -4271.53 | -2440.22 | 2934.71 | 2934.71 |
| 267.0 | -3258.16 | -3133.56 | 3.922e+04 | 1750.62 | -4271.53 | -2155.41 | 2320.13 | 2320.13 |
| 289.0 | -3143.57 | -3048.64 | 3.639e+04 | 1348.25 | -4271.53 | -2004.10 | 1734.06 | 1734.06 |
| 311.0 | -2982.34 | -2923.29 | 3.540e+04 | 660.29 | -4271.53 | -1845.43 | 1285.74 | 1285.74 |
| 333.0 | -2740.70 | -2726.93 | 3.642e+04 | 641.19 | -4271.53 | -1655.77 | 1015.96 | 1015.96 |
| 355.0 | -2431.09 | -2386.34 | 3.567e+04 | 3562.50 | -4271.53 | -1643.66 | 1021.61 | 1010.59 |
| 370.0 | -2160.23 | -1353.10 | 2.289e+04 | 7680.92 | -4271.53 | -1478.89 | 621.81 | 621.81 |
| 381.0 | -2006.53 | -1801.88 | 4.331e+04 | 8306.56 | -4271.53 | -796.00 | 794.68 | 794.68 |
| 408.0 | -2199.69 | -2199.69 | 3.559e+04 | 4405.49 | -4271.53 | -768.85 | 1020.70 | 1020.70 |
| 417.3 | -1766.26 | -931.22 | 1.371e+04 | 5633.61 | -4271.53 | -422.23 | 576.81 | 576.81 |
| 426.3 | -1198.26 | -671.74 | 7208.90 | 2918.35 | -4271.53 | -612.33 | 465.29 | 465.29 |
| 430.0 | 0.0 | 0.0 | 0.0 | 0.0 | -4271.53 | 0.0 | 0.0 | 0.0 |
| 435.3 | 0.0 | 0.0 | 0.0 | 0.0 | -4271.53 | 0.0 | 0.0 | 0.0 |
| 444.4 | 0.0 | 0.0 | 0.0 | 0.0 | -4271.53 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 3830.35 | 2.936e+04 | 1.00 | 8129.96 | 2.936e+04 |
| 23.0 | 1.00 | 3779.22 | 2.929e+04 | 1.00 | 8129.96 | 2.929e+04 |
| 46.0 | 1.00 | 4076.97 | 2.917e+04 | 1.00 | 8129.96 | 2.917e+04 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|----------|-----------|
| 69.0 | 1.00 | 4293.54 | 2.906e+04 | 1.00 | 8129.96 | 2.908e+04 |
| 92.0 | 1.00 | 4383.11 | 2.898e+04 | 1.00 | 8129.96 | 2.898e+04 |
| 112.0 | 1.00 | 4388.18 | 2.890e+04 | 1.00 | 8129.96 | 2.890e+04 |
| 132.0 | 1.00 | 4335.26 | 2.883e+04 | 1.00 | 8129.96 | 2.883e+04 |
| 152.0 | 1.00 | 4234.15 | 2.875e+04 | 1.00 | 8129.96 | 2.875e+04 |
| 172.0 | 1.00 | 4082.37 | 2.868e+04 | 1.00 | 8129.96 | 2.868e+04 |
| 196.0 | 1.00 | 3830.82 | 2.861e+04 | 1.00 | 8129.96 | 2.861e+04 |
| 220.0 | 1.00 | 3453.48 | 2.854e+04 | 1.00 | 8129.96 | 2.854e+04 |
| 244.0 | 1.00 | 2934.71 | 2.847e+04 | 1.00 | 8129.96 | 2.847e+04 |
| 267.0 | 1.00 | 2320.13 | 2.842e+04 | 1.00 | 8129.96 | 2.842e+04 |
| 289.0 | 1.00 | 1734.06 | 2.839e+04 | 1.00 | 8129.96 | 2.839e+04 |
| 311.0 | 1.00 | 1285.74 | 2.836e+04 | 1.00 | 8129.96 | 2.836e+04 |
| 333.0 | 1.00 | 1015.96 | 2.833e+04 | 1.00 | 8129.96 | 2.833e+04 |
| 355.0 | 1.00 | 1021.61 | 2.832e+04 | 1.00 | 8129.96 | 2.832e+04 |
| 370.0 | 1.00 | 621.81 | 2.829e+04 | 1.00 | 8129.96 | 2.829e+04 |
| 381.0 | 1.00 | 794.68 | 2.817e+04 | 1.00 | 8129.96 | 2.817e+04 |
| 408.0 | 1.00 | 1020.70 | 2.816e+04 | 1.00 | 8129.96 | 2.816e+04 |
| 417.3 | 1.00 | 576.81 | 1.572e+04 | 1.00 | 4543.94 | 1.572e+04 |
| 426.3 | 1.00 | 465.29 | 1.195e+04 | 1.00 | 3438.65 | 1.195e+04 |
| 430.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 435.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 444.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 43 | 497.14 | 11.20 | 131.15 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|--------------|------------|---------|------------|---------------|-----------------|--------------------|-------------------|-------------------|-------|
| cm | | | | | | | | | daN |
| 0.0 | 1d12 | 1d12/25 | 1d10/25 | 0.24 | 0.10 | 0.10 | 0.17 | 0.37 | 0.0 |
| 23.0 | 1d12 | 1d12/25 | 1d10/25 | 0.25 | 0.10 | 0.10 | 0.17 | 0.37 | 0.0 |
| 46.0 | 1d12 | 1d12/25 | 1d10/25 | 0.26 | 0.07 | 0.10 | 0.17 | 0.37 | 0.0 |
| 69.0 | 1d12 | 1d12/25 | 1d10/25 | 0.28 | 0.07 | 0.10 | 0.16 | 0.37 | 0.0 |
| 92.0 | 1d12 | 1d12/25 | 1d10/25 | 0.30 | 0.06 | 0.10 | 0.16 | 0.37 | 0.0 |
| 112.0 | 1d12 | 1d12/25 | 1d10/25 | 0.31 | 0.06 | 0.10 | 0.16 | 0.37 | 0.0 |
| 132.0 | 1d12 | 1d12/25 | 1d10/25 | 0.33 | 0.07 | 0.10 | 0.16 | 0.38 | 0.0 |
| 152.0 | 1d12 | 1d12/25 | 1d10/25 | 0.35 | 0.08 | 0.10 | 0.16 | 0.38 | 0.0 |
| 172.0 | 1d12 | 1d12/25 | 1d10/25 | 0.36 | 0.09 | 0.10 | 0.16 | 0.39 | 0.0 |
| 196.0 | 1d12 | 1d12/25 | 1d10/25 | 0.38 | 0.11 | 0.10 | 0.17 | 0.41 | 0.0 |
| 220.0 | 1d12 | 1d12/25 | 1d10/25 | 0.40 | 0.13 | 0.10 | 0.17 | 0.43 | 0.0 |
| 244.0 | 1d12 | 1d12/25 | 1d10/25 | 0.42 | 0.15 | 0.10 | 0.18 | 0.46 | 0.0 |
| 267.0 | 1d12 | 1d12/25 | 1d10/25 | 0.43 | 0.18 | 0.10 | 0.19 | 0.49 | 0.0 |
| 289.0 | 1d12 | 1d12/25 | 1d10/25 | 0.38 | 0.12 | 0.10 | 0.13 | 0.32 | 0.0 |
| 311.0 | 1d12 | 1d12/25 | 1d10/25 | 0.35 | 0.09 | 0.10 | 0.12 | 0.39 | 0.0 |
| 333.0 | 1d12 | 1d12/25 | 1d10/25 | 0.33 | 0.08 | 0.10 | 0.13 | 0.45 | 0.0 |
| 355.0 | 1d12 | 1d12/25 | 1d10/25 | 0.32 | 0.07 | 0.10 | 0.15 | 0.51 | 0.0 |
| 370.0 | 1d12 | 1d12/25 | 1d10/25 | 0.30 | 0.08 | 0.10 | 0.16 | 0.55 | 0.0 |
| 379.0 | 1d12 | 1d12/25 | 1d10/25 | 0.30 | 0.09 | 0.10 | 0.13 | 0.45 | 0.0 |
| 381.0 | 1d12 | 1d12/25 | 1d10/25 | 0.30 | 0.09 | 0.10 | 0.13 | 0.45 | 0.0 |
| 388.0 | 1d12 | 1d12/25 | 1d10/25 | 0.26 | 0.11 | 0.10 | 0.12 | 0.41 | 0.0 |
| 397.0 | 1d12 | 1d12/25 | 1d10/25 | 0.21 | 0.12 | 0.10 | 0.11 | 0.37 | 0.0 |
| 406.0 | 1d12 | 1d12/25 | 1d10/25 | 0.17 | 0.11 | 0.10 | 0.10 | 0.34 | 0.0 |
| 408.0 | 1d12 | 1d12/25 | 1d10/25 | 0.15 | 0.10 | 0.10 | 0.10 | 0.34 | 0.0 |
| 415.0 | 1d12 | 1d12/25 | 1d10/25 | 0.12 | 0.07 | 0.10 | 0.10 | 0.32 | 0.0 |
| 423.6 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.04 | 0.10 | 0.09 | 0.31 | 0.0 |
| 430.0 | 1d12 | 1d12/25 | 1d10/25 | 0.08 | 0.04 | 0.10 | 0.09 | 0.31 | 0.0 |
| 433.8 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.06 | 0.10 | 0.09 | 0.29 | 0.0 |
| 444.4 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.06 | 0.10 | 0.08 | 0.26 | 0.0 |
| 452.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.08 | 0.10 | 0.10 | 0.32 | 0.0 |
| 453.2 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.07 | 0.10 | 0.10 | 0.32 | 0.0 |
| 462.1 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.06 | 0.10 | 0.09 | 0.31 | 0.0 |
| 470.9 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.09 | 0.10 | 0.13 | 0.44 | 0.0 |
| 474.0 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.08 | 0.10 | 0.13 | 0.43 | 0.0 |
| 479.8 | 1d12 | 1d12/25 | 1d10/25 | 0.07 | 0.06 | 0.10 | 0.12 | 0.40 | 0.0 |
| 488.6 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.10 | 0.0 | 0.0 | 0.0 |
| 497.1 | 1d12 | 1d12/25 | 1d10/25 | 0.0 | 0.0 | 0.10 | 0.0 | 0.0 | 0.0 |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.43 | 0.18 | 0.10 | 0.19 | 0.55 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|------------|------------|-----------|-----------|----------|------------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 0.0 | -1.232e+04 | -3680.68 | 1.532e+05 | 7778.28 | -6159.66 | -3680.68 | 7016.55 | 4663.21 |
| 23.0 | -1.302e+04 | -1.065e+04 | 1.636e+05 | 9158.32 | -6159.66 | -4097.10 | 7067.67 | 4604.33 |
| 46.0 | -1.370e+04 | -1.049e+04 | 1.454e+05 | 4684.92 | -6159.66 | -5009.95 | 6863.11 | 4597.11 |
| 69.0 | -1.449e+04 | -1.026e+04 | 1.326e+05 | 2674.09 | -6159.66 | -6060.69 | 6713.67 | 4603.59 |
| 92.0 | -1.533e+04 | -9936.97 | 1.266e+05 | 778.25 | -6159.66 | -7246.28 | 6655.04 | 4632.71 |
| 112.0 | -1.619e+04 | -1.619e+04 | 1.418e+05 | 345.76 | -6159.66 | -8259.85 | 6656.67 | 4680.54 |
| 132.0 | -1.708e+04 | -1.708e+04 | 1.711e+05 | 649.54 | -6159.66 | -9286.85 | 6700.51 | 4748.11 |
| 152.0 | -1.796e+04 | -1.796e+04 | 2.018e+05 | 665.60 | -6159.66 | -1.050e+04 | 6780.53 | 4841.49 |
| 172.0 | -1.884e+04 | -1.884e+04 | 2.350e+05 | 388.40 | -6159.66 | -1.149e+04 | 6900.71 | 4965.43 |
| 196.0 | -1.987e+04 | -1.987e+04 | 2.811e+05 | 347.98 | -6159.66 | -1.264e+04 | 7105.91 | 5164.08 |
| 220.0 | -2.086e+04 | -2.086e+04 | 3.351e+05 | 1472.91 | -6159.66 | -1.383e+04 | 7423.94 | 5441.56 |
| 244.0 | -2.177e+04 | -2.177e+04 | 4.018e+05 | 2956.82 | -6159.66 | -1.494e+04 | 7879.82 | 5800.81 |
| 267.0 | -2.254e+04 | -2.254e+04 | 4.808e+05 | 4600.76 | -6159.66 | -1.589e+04 | 8435.08 | 6177.28 |
| 289.0 | -1.961e+04 | -1.961e+04 | 2.968e+05 | 3461.65 | -6159.66 | -1.374e+04 | 5457.91 | 4077.27 |
| 311.0 | -1.829e+04 | -1.829e+04 | 2.247e+05 | 3194.37 | -6159.66 | -1.289e+04 | 5118.99 | 4881.60 |
| 333.0 | -1.721e+04 | -1.721e+04 | 1.830e+05 | 3819.54 | -6159.66 | -1.721e+04 | 5639.32 | 5639.32 |
| 355.0 | -1.635e+04 | -1.635e+04 | 1.621e+05 | 5111.17 | -6159.66 | -1.635e+04 | 6459.02 | 6459.02 |
| 370.0 | -1.573e+04 | -1.573e+04 | 1.679e+05 | 4172.30 | -6159.66 | -1.573e+04 | 6968.67 | 6968.67 |
| 379.0 | -1.572e+04 | -1.426e+04 | 1.390e+05 | 1.084e+04 | -6159.66 | -1.572e+04 | 5725.00 | 5725.00 |
| 381.0 | -1.530e+04 | -1.380e+04 | 1.561e+05 | 9904.80 | -6159.66 | -1.530e+04 | 5601.45 | 5601.45 |
| 388.0 | -1.351e+04 | -1.220e+04 | 1.943e+05 | 9747.61 | -6159.66 | -1.351e+04 | 5177.41 | 5177.41 |
| 397.0 | -1.108e+04 | -1.006e+04 | 2.134e+05 | 9074.58 | -6159.66 | -1.108e+04 | 4709.55 | 4709.55 |
| 406.0 | -8642.15 | -8642.15 | 2.009e+05 | 5712.10 | -6159.66 | -8642.15 | 4337.29 | 4337.29 |
| 408.0 | -7998.38 | -7998.38 | 1.862e+05 | 4503.16 | -6159.66 | -7998.38 | 4296.58 | 4296.58 |
| 415.0 | -6118.49 | -6118.49 | 1.276e+05 | 4496.39 | -6159.66 | -6118.49 | 4069.51 | 4069.51 |
| 423.6 | -4075.93 | -2137.42 | 6757.89 | 5713.18 | -6159.66 | -4075.93 | 3843.95 | 3843.95 |
| 430.0 | -3945.36 | -2069.32 | 6263.42 | 5698.19 | -6159.66 | -3945.36 | 3839.39 | 3839.39 |
| 433.8 | -3788.38 | -2048.08 | 6016.20 | 8428.18 | -6159.66 | -3788.38 | 3681.80 | 3681.80 |
| 444.4 | -3453.01 | -2159.50 | 2.148e+04 | 8511.47 | -6159.66 | -3453.01 | 3282.70 | 3282.70 |
| 452.0 | -2984.69 | -1902.72 | 1.462e+04 | 7499.00 | -6159.66 | -2984.69 | 2969.11 | 2969.11 |
| 453.2 | -2805.98 | -1695.36 | 1.309e+04 | 6881.41 | -6159.66 | -2805.98 | 2870.34 | 2870.34 |
| 462.1 | -2299.88 | -1432.01 | 6707.16 | 5711.78 | -6159.66 | -2299.88 | 2438.25 | 2438.25 |
| 470.9 | -1780.16 | -1121.34 | 2562.17 | 4615.89 | -6159.66 | -1780.16 | 1941.20 | 1941.20 |
| 474.0 | -1583.94 | -998.02 | 1850.27 | 4058.47 | -6159.66 | -1583.94 | 1745.59 | 1745.59 |
| 479.8 | -1169.54 | -723.02 | 599.61 | 2827.20 | -6159.66 | -1169.54 | 1354.49 | 1354.49 |
| 488.6 | 0.0 | 0.0 | 0.0 | 0.0 | -6159.66 | 0.0 | 0.0 | 0.0 |
| 497.1 | 0.0 | 0.0 | 0.0 | 0.0 | -6159.66 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 0.0 | 1.00 | 7016.55 | 4.120e+04 | 1.00 | 1.258e+04 | 4.278e+04 |
| 23.0 | 1.00 | 7067.67 | 4.128e+04 | 1.00 | 1.258e+04 | 4.295e+04 |
| 46.0 | 1.00 | 6863.11 | 4.146e+04 | 1.00 | 1.258e+04 | 4.310e+04 |
| 69.0 | 1.00 | 6713.67 | 4.166e+04 | 1.00 | 1.258e+04 | 4.328e+04 |
| 92.0 | 1.00 | 6655.04 | 4.190e+04 | 1.00 | 1.258e+04 | 4.347e+04 |
| 112.0 | 1.00 | 6656.67 | 4.209e+04 | 1.00 | 1.258e+04 | 4.364e+04 |
| 132.0 | 1.00 | 6700.51 | 4.229e+04 | 1.00 | 1.258e+04 | 4.382e+04 |
| 152.0 | 1.00 | 6780.53 | 4.253e+04 | 1.00 | 1.258e+04 | 4.399e+04 |
| 172.0 | 1.00 | 6900.71 | 4.272e+04 | 1.00 | 1.258e+04 | 4.416e+04 |
| 196.0 | 1.00 | 7105.91 | 4.295e+04 | 1.00 | 1.258e+04 | 4.436e+04 |
| 220.0 | 1.00 | 7423.94 | 4.318e+04 | 1.00 | 1.258e+04 | 4.455e+04 |
| 244.0 | 1.00 | 7879.82 | 4.340e+04 | 1.00 | 1.258e+04 | 4.473e+04 |
| 267.0 | 1.00 | 8435.08 | 4.358e+04 | 1.00 | 1.258e+04 | 4.488e+04 |
| 289.0 | 1.00 | 5457.91 | 4.316e+04 | 1.00 | 1.258e+04 | 4.431e+04 |
| 311.0 | 1.00 | 5118.99 | 4.300e+04 | 1.00 | 1.258e+04 | 4.405e+04 |
| 333.0 | 1.00 | 5639.32 | 4.384e+04 | 1.00 | 1.258e+04 | 4.384e+04 |
| 355.0 | 1.00 | 6459.02 | 4.367e+04 | 1.00 | 1.258e+04 | 4.367e+04 |
| 370.0 | 1.00 | 6968.67 | 4.355e+04 | 1.00 | 1.258e+04 | 4.355e+04 |
| 379.0 | 1.00 | 5725.00 | 4.355e+04 | 1.00 | 1.258e+04 | 4.355e+04 |
| 381.0 | 1.00 | 5601.45 | 4.347e+04 | 1.00 | 1.258e+04 | 4.347e+04 |
| 388.0 | 1.00 | 5177.41 | 4.312e+04 | 1.00 | 1.258e+04 | 4.312e+04 |
| 397.0 | 1.00 | 4709.55 | 4.264e+04 | 1.00 | 1.258e+04 | 4.264e+04 |
| 406.0 | 1.00 | 4337.29 | 4.217e+04 | 1.00 | 1.258e+04 | 4.217e+04 |
| 408.0 | 1.00 | 4296.58 | 4.204e+04 | 1.00 | 1.258e+04 | 4.204e+04 |
| 415.0 | 1.00 | 4069.51 | 4.167e+04 | 1.00 | 1.258e+04 | 4.167e+04 |
| 423.6 | 1.00 | 3843.95 | 4.128e+04 | 1.00 | 1.258e+04 | 4.128e+04 |
| 430.0 | 1.00 | 3839.39 | 4.125e+04 | 1.00 | 1.258e+04 | 4.125e+04 |
| 433.8 | 1.00 | 3681.80 | 4.122e+04 | 1.00 | 1.258e+04 | 4.122e+04 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| 444.4 | 1.00 | 3282.70 | 4.115e+04 | 1.00 | 1.258e+04 | 4.115e+04 |
| 452.0 | 1.00 | 2969.11 | 3.009e+04 | 1.00 | 9198.30 | 3.009e+04 |
| 453.2 | 1.00 | 2870.34 | 2.957e+04 | 1.00 | 9046.12 | 2.957e+04 |
| 462.1 | 1.00 | 2438.25 | 2.605e+04 | 1.00 | 7965.40 | 2.605e+04 |
| 470.9 | 1.00 | 1941.20 | 1.449e+04 | 1.00 | 4428.50 | 1.449e+04 |
| 474.0 | 1.00 | 1745.59 | 1.327e+04 | 1.00 | 4055.00 | 1.327e+04 |
| 479.8 | 1.00 | 1354.49 | 1.095e+04 | 1.00 | 3347.78 | 1.095e+04 |
| 488.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 497.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Macrosetti n. 8, 13 [fasce di piano]

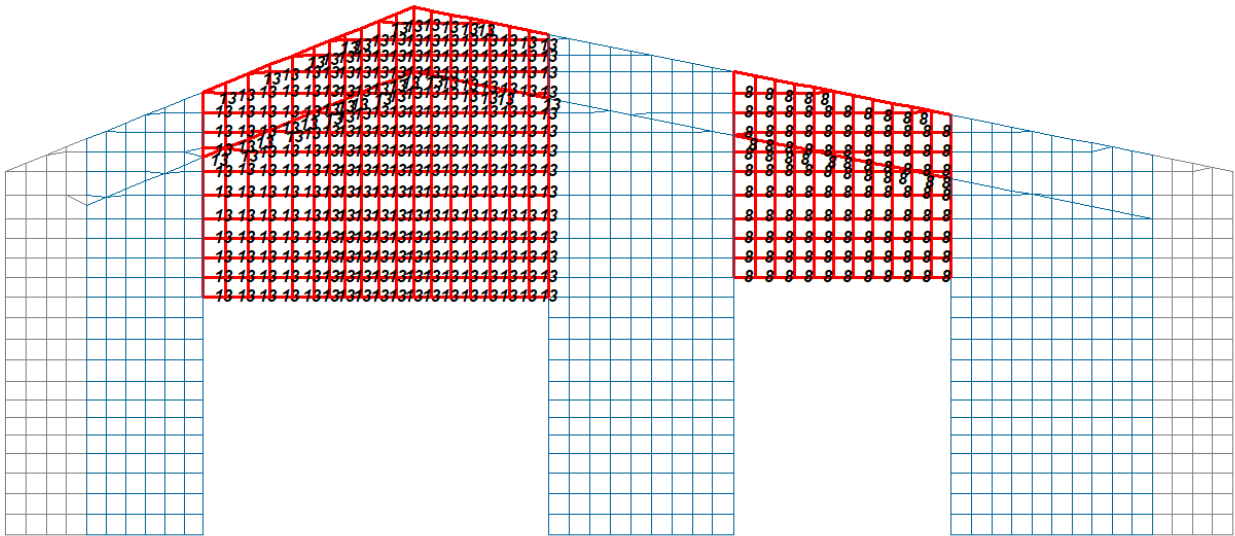


Fig 129. Elementi oggetto di verifica (Selezione in rosso).

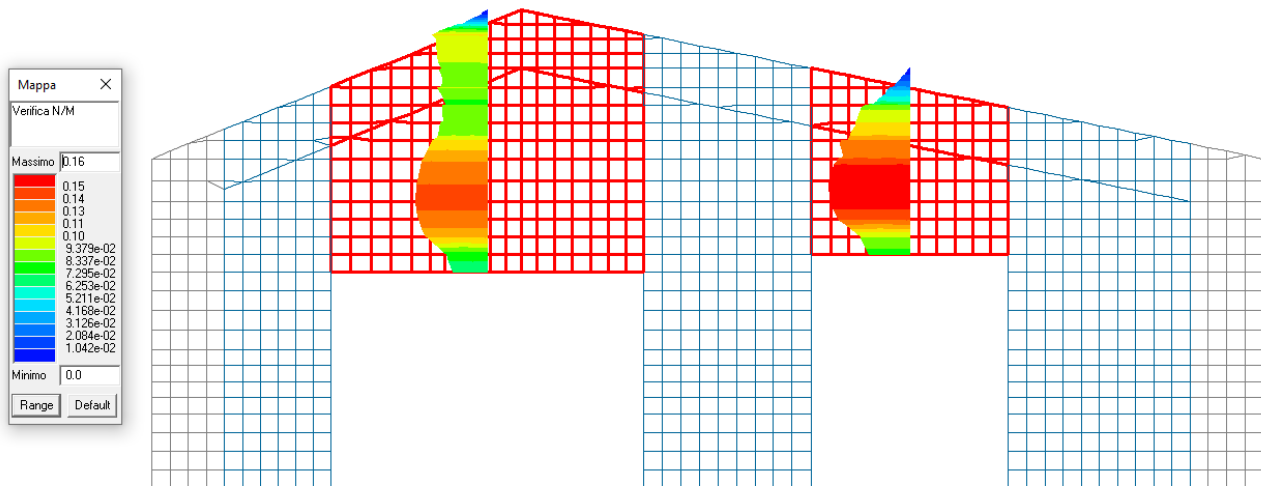


Fig 130. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

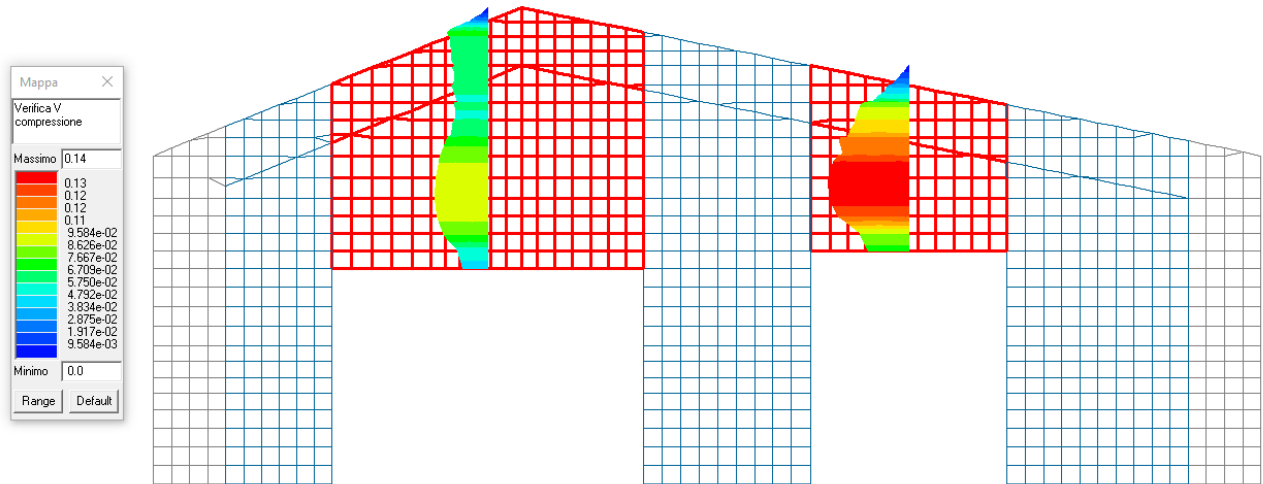


Fig 131. SLU: Mappa di Verifica V compressione – Verifica soddisfatta ($\rho \leq 1$).

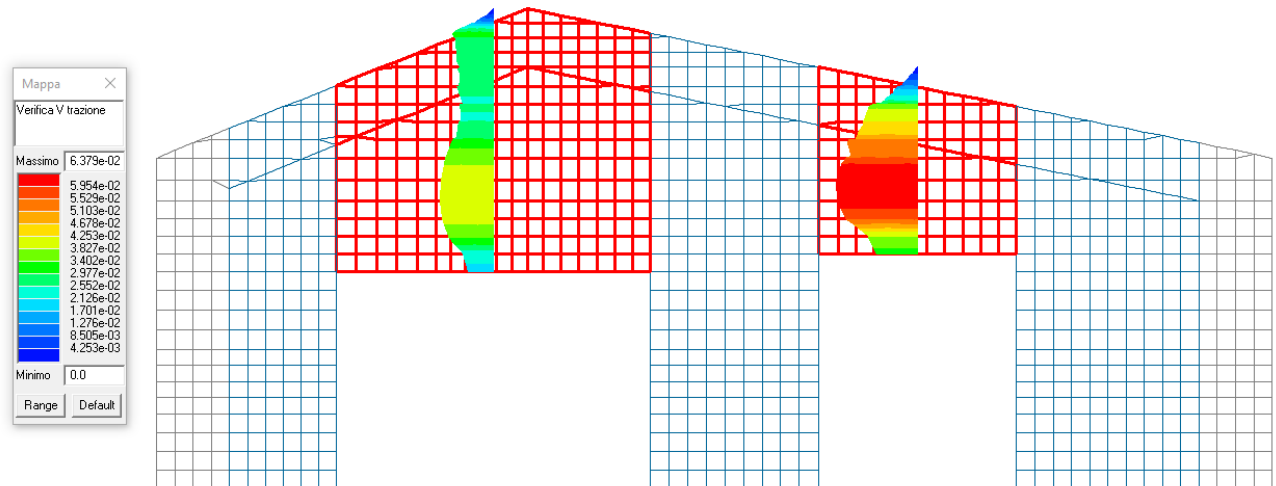


Fig 132. SLU: Mappa di verifica V trazione – Verifiche soddisfatte ($\rho \leq 1$).

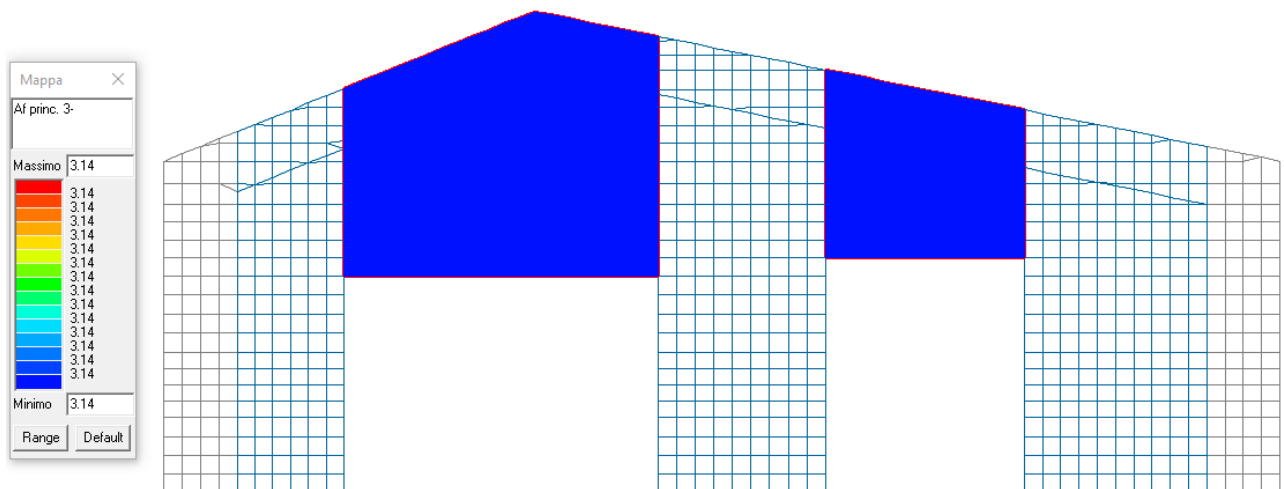


Fig 133. Mappa Armatura Verticale (singolo strato) da Calcolo [cm^2/m].

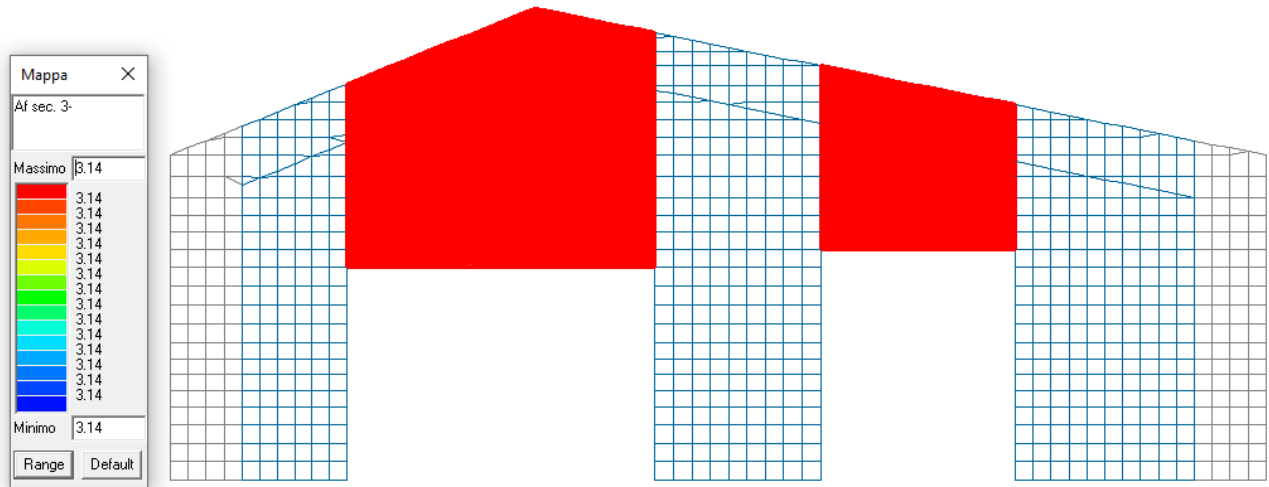


Fig 134. Mappa Armatura Orizzontale (singolo strato) da Calcolo [cm²/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

Si riporta il tabulato di verifica completo.

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 8 | 231.06 | 11.20 | 244.00 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|-----------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.07 | 0.03 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.09 | 0.04 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.14 | 0.0 | 0.13 | 0.06 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.15 | 0.0 | 0.14 | 0.06 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.16 | 0.0 | 0.14 | 0.06 | 0.0 |
| 399.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.15 | 0.0 | 0.14 | 0.06 | 0.0 |
| 404.3 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.14 | 0.0 | 0.13 | 0.06 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.14 | 0.0 | 0.13 | 0.06 | 0.0 |
| 408.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.12 | 0.05 | 0.0 |
| 413.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.12 | 0.05 | 0.0 |
| 417.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.12 | 0.05 | 0.0 |
| 421.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.12 | 0.05 | 0.0 |
| 426.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.14 | 0.0 | 0.12 | 0.06 | 0.0 |
| 430.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.12 | 0.05 | 0.0 |
| 430.5 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.12 | 0.0 | 0.11 | 0.05 | 0.0 |
| 434.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.12 | 0.0 | 0.11 | 0.05 | 0.0 |
| 439.3 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.10 | 0.05 | 0.0 |
| 443.7 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.10 | 0.04 | 0.0 |
| 448.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.10 | 0.04 | 0.0 |
| 452.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.10 | 0.04 | 0.0 |
| 471.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.08 | 0.04 | 0.0 |
| 474.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.08 | 0.03 | 0.0 |
| 475.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.06 | 0.03 | 0.0 |
| 480.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.06 | 0.03 | 0.0 |
| 484.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.05 | 0.02 | 0.0 |
| 488.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.04 | 0.02 | 0.0 |
| 493.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.04 | 0.02 | 0.0 |
| 496.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.02 | 0.0 |
| 496.1 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.03 | 0.01 | 0.0 |
| 497.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.03 | 0.01 | 0.0 |
| 502.1 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.02 | 9.86e-03 | 0.0 |
| 506.5 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.02 | 7.26e-03 | 0.0 |
| 510.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.01 | 0.0 | 0.01 | 4.70e-03 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|-----------|------------|--------|----------|-------------|------------|------------|-------|
| 515.3 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 5.65e-03 | 0.0 | 5.20e-03 | 2.31e-03 | 0.0 |
| 520.1 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | | | |
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.16 | 0.0 | 0.14 | 0.06 | |

| Quota | N v.N | N v.M/N | M v.M/N | Mo v.M/N | N v.Stab | N v.Vcls | V v.Vcls | V v.Vacc |
|-------|-------|---------|-----------|----------|----------|----------|----------|----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 289.0 | 0.0 | 0.0 | 4.944e+05 | 0.0 | 0.0 | 0.0 | 4052.71 | 4052.71 |
| 311.0 | 0.0 | 0.0 | 5.937e+05 | 0.0 | 0.0 | 0.0 | 4866.68 | 4866.68 |
| 333.0 | 0.0 | 0.0 | 8.688e+05 | 0.0 | 0.0 | 0.0 | 7121.45 | 7121.45 |
| 355.0 | 0.0 | 0.0 | 9.662e+05 | 0.0 | 0.0 | 0.0 | 7920.01 | 7920.01 |
| 381.0 | 0.0 | 0.0 | 9.830e+05 | 0.0 | 0.0 | 0.0 | 8057.55 | 8057.55 |
| 399.9 | 0.0 | 0.0 | 9.246e+05 | 0.0 | 0.0 | 0.0 | 7578.46 | 7578.46 |
| 404.3 | 0.0 | 0.0 | 8.856e+05 | 0.0 | 0.0 | 0.0 | 7259.00 | 7259.00 |
| 408.0 | 0.0 | 0.0 | 8.741e+05 | 0.0 | 0.0 | 0.0 | 7164.44 | 7164.44 |
| 408.6 | 0.0 | 0.0 | 8.204e+05 | 0.0 | 0.0 | 0.0 | 6724.49 | 6724.49 |
| 413.0 | 0.0 | 0.0 | 8.109e+05 | 0.0 | 0.0 | 0.0 | 6646.42 | 6646.42 |
| 417.4 | 0.0 | 0.0 | 8.138e+05 | 0.0 | 0.0 | 0.0 | 6670.57 | 6670.57 |
| 421.8 | 0.0 | 0.0 | 8.364e+05 | 0.0 | 0.0 | 0.0 | 6855.62 | 6855.62 |
| 426.2 | 0.0 | 0.0 | 8.504e+05 | 0.0 | 0.0 | 0.0 | 6970.37 | 6970.37 |
| 430.0 | 0.0 | 0.0 | 8.377e+05 | 0.0 | 0.0 | 0.0 | 6866.35 | 6866.35 |
| 430.5 | 0.0 | 0.0 | 7.529e+05 | 0.0 | 0.0 | 0.0 | 6171.66 | 6171.66 |
| 434.9 | 0.0 | 0.0 | 7.307e+05 | 0.0 | 0.0 | 0.0 | 5989.28 | 5989.28 |
| 439.3 | 0.0 | 0.0 | 7.130e+05 | 0.0 | 0.0 | 0.0 | 5843.95 | 5843.95 |
| 443.7 | 0.0 | 0.0 | 6.915e+05 | 0.0 | 0.0 | 0.0 | 5667.66 | 5667.66 |
| 448.4 | 0.0 | 0.0 | 6.611e+05 | 0.0 | 0.0 | 0.0 | 5418.75 | 5418.75 |
| 452.0 | 0.0 | 0.0 | 6.576e+05 | 0.0 | 0.0 | 0.0 | 5390.35 | 5390.35 |
| 471.2 | 0.0 | 0.0 | 5.785e+05 | 0.0 | 0.0 | 0.0 | 4742.17 | 4742.17 |
| 474.0 | 0.0 | 0.0 | 5.356e+05 | 0.0 | 0.0 | 0.0 | 4389.92 | 4389.92 |
| 475.6 | 0.0 | 0.0 | 4.403e+05 | 0.0 | 0.0 | 0.0 | 3608.98 | 3608.98 |
| 480.0 | 0.0 | 0.0 | 3.891e+05 | 0.0 | 0.0 | 0.0 | 3189.06 | 3189.06 |
| 484.4 | 0.0 | 0.0 | 3.351e+05 | 0.0 | 0.0 | 0.0 | 2747.06 | 2747.06 |
| 488.8 | 0.0 | 0.0 | 2.881e+05 | 0.0 | 0.0 | 0.0 | 2361.30 | 2361.30 |
| 493.2 | 0.0 | 0.0 | 2.591e+05 | 0.0 | 0.0 | 0.0 | 2123.77 | 2123.77 |
| 496.0 | 0.0 | 0.0 | 2.366e+05 | 0.0 | 0.0 | 0.0 | 1939.24 | 1939.24 |
| 496.1 | 0.0 | 0.0 | 2.146e+05 | 0.0 | 0.0 | 0.0 | 1758.94 | 1758.94 |
| 497.6 | 0.0 | 0.0 | 1.884e+05 | 0.0 | 0.0 | 0.0 | 1544.48 | 1544.48 |
| 502.1 | 0.0 | 0.0 | 1.520e+05 | 0.0 | 0.0 | 0.0 | 1245.87 | 1245.87 |
| 506.5 | 0.0 | 0.0 | 1.119e+05 | 0.0 | 0.0 | 0.0 | 917.43 | 917.43 |
| 510.9 | 0.0 | 0.0 | 7.240e+04 | 0.0 | 0.0 | 0.0 | 593.47 | 593.47 |
| 515.3 | 0.0 | 0.0 | 3.556e+04 | 0.0 | 0.0 | 0.0 | 291.47 | 291.47 |
| 520.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 289.0 | 2.50 | 4052.71 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 311.0 | 2.50 | 4866.68 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 333.0 | 2.50 | 7121.45 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 355.0 | 2.50 | 7920.01 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 381.0 | 2.50 | 8057.55 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 399.9 | 2.50 | 7578.46 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 404.3 | 2.50 | 7259.00 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 408.0 | 2.50 | 7164.44 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 408.6 | 2.50 | 6724.49 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 413.0 | 2.50 | 6646.42 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 417.4 | 2.50 | 6670.57 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 421.8 | 2.50 | 6855.62 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 426.2 | 2.50 | 6970.37 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 430.0 | 2.50 | 6866.35 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 430.5 | 2.50 | 6171.66 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 434.9 | 2.50 | 5989.28 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 439.3 | 2.50 | 5843.95 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 443.7 | 2.50 | 5667.66 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 448.4 | 2.50 | 5418.75 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 452.0 | 2.50 | 5390.35 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 471.2 | 2.50 | 4742.17 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 474.0 | 2.50 | 4389.92 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 475.6 | 2.50 | 3608.98 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 480.0 | 2.50 | 3189.06 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| 484.4 | 2.50 | 2747.06 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 488.8 | 2.50 | 2361.30 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 493.2 | 2.50 | 2123.77 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 496.0 | 2.50 | 1939.24 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 496.1 | 2.50 | 1758.94 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 497.6 | 2.50 | 1544.48 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 502.1 | 2.50 | 1245.87 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 506.5 | 2.50 | 917.43 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 510.9 | 2.50 | 593.47 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 515.3 | 2.50 | 291.47 | 5.605e+04 | 2.50 | 1.263e+05 | 5.605e+04 |
| 520.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Parete PDA | H totale | Spessore | L totale | Verif. N | Verif. N-M | Verif. Snellezza | Fattore V | Verif. V | Prog. composta |
|------------|----------|----------|----------|----------|------------|------------------|-----------|----------|----------------|
| | cm | cm | cm | | | | | | |
| 13 | 325.00 | 11.20 | 387.70 | ok | ok | ok | 1.25 | ok | SI |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|-----------|------------|--------|----------|-------------|------------|------------|-------|
| cm | | | | | | | | | daN |
| 267.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.04 | 0.02 | 0.0 |
| 289.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.05 | 0.02 | 0.0 |
| 311.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.12 | 0.0 | 0.08 | 0.04 | 0.0 |
| 333.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.09 | 0.04 | 0.0 |
| 355.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.14 | 0.0 | 0.09 | 0.04 | 0.0 |
| 381.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.13 | 0.0 | 0.09 | 0.04 | 0.0 |
| 408.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.12 | 0.0 | 0.08 | 0.04 | 0.0 |
| 423.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.07 | 0.03 | 0.0 |
| 430.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.07 | 0.03 | 0.0 |
| 433.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.06 | 0.03 | 0.0 |
| 444.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 452.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 454.3 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.06 | 0.03 | 0.0 |
| 464.5 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.06 | 0.03 | 0.0 |
| 474.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 474.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.05 | 0.02 | 0.0 |
| 481.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.06 | 0.03 | 0.0 |
| 488.5 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 489.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 494.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 496.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.07 | 0.03 | 0.0 |
| 496.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 497.1 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 498.5 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 502.9 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 504.3 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 507.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 507.3 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 511.7 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 512.1 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 516.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 517.3 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 520.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 527.3 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 537.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.06 | 0.03 | 0.0 |
| 538.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.07 | 0.03 | 0.0 |
| 547.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.07 | 0.03 | 0.0 |
| 554.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.07 | 0.03 | 0.0 |
| 556.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.10 | 0.0 | 0.07 | 0.03 | 0.0 |
| 561.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.07 | 0.03 | 0.0 |
| 561.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.11 | 0.0 | 0.07 | 0.03 | 0.0 |
| 566.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.09 | 0.0 | 0.06 | 0.03 | 0.0 |
| 568.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.08 | 0.0 | 0.05 | 0.02 | 0.0 |
| 570.4 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.07 | 0.0 | 0.05 | 0.02 | 0.0 |
| 574.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.06 | 0.0 | 0.04 | 0.02 | 0.0 |
| 574.8 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.05 | 0.0 | 0.03 | 0.01 | 0.0 |
| 576.5 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.04 | 0.0 | 0.03 | 0.01 | 0.0 |
| 579.2 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.03 | 0.0 | 0.02 | 0.01 | 0.0 |
| 583.6 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.01 | 5.73e-03 | 0.0 |
| 584.3 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.02 | 0.0 | 0.01 | 4.97e-03 | 0.0 |
| 588.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 9.10e-03 | 0.0 | 6.16e-03 | 2.73e-03 | 0.0 |
| 592.0 | 1+1d0 | 1+1d10/25 | 1+1d10/25 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | Af estremi | Af std | Af V (ori) | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | N add |
|-------|------------|--------|------------|--------|----------|-------------|------------|------------|-------|
| Quota | | | | Ver. N | Ver. N/M | Ver. Snell. | Ver. V cls | Ver. V acc | |
| | | | | 0.0 | 0.14 | 0.0 | 0.09 | 0.04 | |

| Quota | N v. N | N v. M/N | M v. M/N | Mo v. M/N | N v. Stab | N v. Vcls | V v. Vcls | V v. Vacc |
|-------|--------|----------|-----------|-----------|-----------|-----------|-----------|-----------|
| cm | daN | daN | daN cm | daN cm | daN | daN | daN | daN |
| 267.0 | 0.0 | 0.0 | 6.767e+05 | 0.0 | 0.0 | 0.0 | 3490.60 | 3490.60 |
| 289.0 | 0.0 | 0.0 | 8.113e+05 | 0.0 | 0.0 | 0.0 | 4185.30 | 4185.30 |
| 311.0 | 0.0 | 0.0 | 1.216e+06 | 0.0 | 0.0 | 0.0 | 6271.24 | 6271.24 |
| 333.0 | 0.0 | 0.0 | 1.380e+06 | 0.0 | 0.0 | 0.0 | 7116.38 | 7116.38 |
| 355.0 | 0.0 | 0.0 | 1.437e+06 | 0.0 | 0.0 | 0.0 | 7411.63 | 7411.63 |
| 381.0 | 0.0 | 0.0 | 1.400e+06 | 0.0 | 0.0 | 0.0 | 7222.38 | 7222.38 |
| 408.0 | 0.0 | 0.0 | 1.285e+06 | 0.0 | 0.0 | 0.0 | 6629.28 | 6629.28 |
| 423.6 | 0.0 | 0.0 | 1.149e+06 | 0.0 | 0.0 | 0.0 | 5926.08 | 5926.08 |
| 430.0 | 0.0 | 0.0 | 1.093e+06 | 0.0 | 0.0 | 0.0 | 5638.63 | 5638.63 |
| 433.8 | 0.0 | 0.0 | 9.867e+05 | 0.0 | 0.0 | 0.0 | 5090.23 | 5090.23 |
| 444.0 | 0.0 | 0.0 | 9.499e+05 | 0.0 | 0.0 | 0.0 | 4900.41 | 4900.41 |
| 452.0 | 0.0 | 0.0 | 9.289e+05 | 0.0 | 0.0 | 0.0 | 4791.83 | 4791.83 |
| 454.3 | 0.0 | 0.0 | 8.704e+05 | 0.0 | 0.0 | 0.0 | 4490.11 | 4490.11 |
| 464.5 | 0.0 | 0.0 | 8.817e+05 | 0.0 | 0.0 | 0.0 | 4548.45 | 4548.45 |
| 474.0 | 0.0 | 0.0 | 8.991e+05 | 0.0 | 0.0 | 0.0 | 4638.34 | 4638.34 |
| 474.2 | 0.0 | 0.0 | 8.116e+05 | 0.0 | 0.0 | 0.0 | 4186.68 | 4186.68 |
| 481.4 | 0.0 | 0.0 | 8.674e+05 | 0.0 | 0.0 | 0.0 | 4474.56 | 4474.56 |
| 488.5 | 0.0 | 0.0 | 9.204e+05 | 0.0 | 0.0 | 0.0 | 4747.77 | 4747.77 |
| 489.8 | 0.0 | 0.0 | 9.269e+05 | 0.0 | 0.0 | 0.0 | 4781.50 | 4781.50 |
| 494.2 | 0.0 | 0.0 | 9.661e+05 | 0.0 | 0.0 | 0.0 | 4983.68 | 4983.68 |
| 496.0 | 0.0 | 0.0 | 9.978e+05 | 0.0 | 0.0 | 0.0 | 5147.34 | 5147.34 |
| 496.4 | 0.0 | 0.0 | 9.230e+05 | 0.0 | 0.0 | 0.0 | 4761.51 | 4761.51 |
| 497.1 | 0.0 | 0.0 | 9.235e+05 | 0.0 | 0.0 | 0.0 | 4763.79 | 4763.79 |
| 498.5 | 0.0 | 0.0 | 9.156e+05 | 0.0 | 0.0 | 0.0 | 4723.23 | 4723.23 |
| 502.9 | 0.0 | 0.0 | 8.996e+05 | 0.0 | 0.0 | 0.0 | 4640.51 | 4640.51 |
| 504.3 | 0.0 | 0.0 | 9.004e+05 | 0.0 | 0.0 | 0.0 | 4644.65 | 4644.65 |
| 507.2 | 0.0 | 0.0 | 8.962e+05 | 0.0 | 0.0 | 0.0 | 4623.09 | 4623.09 |
| 507.3 | 0.0 | 0.0 | 8.959e+05 | 0.0 | 0.0 | 0.0 | 4621.87 | 4621.87 |
| 511.7 | 0.0 | 0.0 | 9.073e+05 | 0.0 | 0.0 | 0.0 | 4680.64 | 4680.64 |
| 512.1 | 0.0 | 0.0 | 9.116e+05 | 0.0 | 0.0 | 0.0 | 4702.45 | 4702.45 |
| 516.0 | 0.0 | 0.0 | 9.451e+05 | 0.0 | 0.0 | 0.0 | 4875.65 | 4875.65 |
| 517.3 | 0.0 | 0.0 | 9.467e+05 | 0.0 | 0.0 | 0.0 | 4883.55 | 4883.55 |
| 520.0 | 0.0 | 0.0 | 9.034e+05 | 0.0 | 0.0 | 0.0 | 4660.32 | 4660.32 |
| 527.3 | 0.0 | 0.0 | 9.850e+05 | 0.0 | 0.0 | 0.0 | 5081.49 | 5081.49 |
| 537.4 | 0.0 | 0.0 | 9.950e+05 | 0.0 | 0.0 | 0.0 | 5133.06 | 5133.06 |
| 538.0 | 0.0 | 0.0 | 9.992e+05 | 0.0 | 0.0 | 0.0 | 5154.45 | 5154.45 |
| 547.0 | 0.0 | 0.0 | 1.011e+06 | 0.0 | 0.0 | 0.0 | 5213.83 | 5213.83 |
| 554.0 | 0.0 | 0.0 | 1.021e+06 | 0.0 | 0.0 | 0.0 | 5267.97 | 5267.97 |
| 556.0 | 0.0 | 0.0 | 1.020e+06 | 0.0 | 0.0 | 0.0 | 5262.20 | 5262.20 |
| 561.0 | 0.0 | 0.0 | 1.093e+06 | 0.0 | 0.0 | 0.0 | 5635.99 | 5635.99 |
| 561.6 | 0.0 | 0.0 | 1.094e+06 | 0.0 | 0.0 | 0.0 | 5641.08 | 5641.08 |
| 566.0 | 0.0 | 0.0 | 9.409e+05 | 0.0 | 0.0 | 0.0 | 4853.60 | 4853.60 |
| 568.8 | 0.0 | 0.0 | 8.188e+05 | 0.0 | 0.0 | 0.0 | 4224.13 | 4224.13 |
| 570.4 | 0.0 | 0.0 | 7.387e+05 | 0.0 | 0.0 | 0.0 | 3810.63 | 3810.63 |
| 574.0 | 0.0 | 0.0 | 5.868e+05 | 0.0 | 0.0 | 0.0 | 3027.06 | 3027.06 |
| 574.8 | 0.0 | 0.0 | 5.015e+05 | 0.0 | 0.0 | 0.0 | 2587.05 | 2587.05 |
| 576.5 | 0.0 | 0.0 | 4.365e+05 | 0.0 | 0.0 | 0.0 | 2251.76 | 2251.76 |
| 579.2 | 0.0 | 0.0 | 3.542e+05 | 0.0 | 0.0 | 0.0 | 1827.44 | 1827.44 |
| 583.6 | 0.0 | 0.0 | 1.979e+05 | 0.0 | 0.0 | 0.0 | 1020.73 | 1020.73 |
| 584.3 | 0.0 | 0.0 | 1.716e+05 | 0.0 | 0.0 | 0.0 | 885.38 | 885.38 |
| 588.0 | 0.0 | 0.0 | 9.446e+04 | 0.0 | 0.0 | 0.0 | 487.28 | 487.28 |
| 592.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| cm | | daN | daN | | daN | daN |
| 267.0 | 2.50 | 3490.60 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 289.0 | 2.50 | 4185.30 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 311.0 | 2.50 | 6271.24 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 333.0 | 2.50 | 7116.38 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 355.0 | 2.50 | 7411.63 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 381.0 | 2.50 | 7222.38 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 408.0 | 2.50 | 6629.28 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 423.6 | 2.50 | 5926.08 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 430.0 | 2.50 | 5638.63 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |

| Quota | Ctg Vcls | Vrsd Vcls | Vrcd Vcls | Ctg Vac | Vrsd Vac | Vrcd Vac |
|-------|----------|-----------|-----------|---------|-----------|-----------|
| 433.8 | 2.50 | 5090.23 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 444.0 | 2.50 | 4900.41 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 452.0 | 2.50 | 4791.83 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 454.3 | 2.50 | 4490.11 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 464.5 | 2.50 | 4548.45 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 474.0 | 2.50 | 4638.34 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 474.2 | 2.50 | 4186.68 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 481.4 | 2.50 | 4474.56 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 488.5 | 2.50 | 4747.77 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 489.8 | 2.50 | 4781.50 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 494.2 | 2.50 | 4983.68 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 496.0 | 2.50 | 5147.34 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 496.4 | 2.50 | 4761.51 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 497.1 | 2.50 | 4763.79 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 498.5 | 2.50 | 4723.23 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 502.9 | 2.50 | 4640.51 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 504.3 | 2.50 | 4644.65 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 507.2 | 2.50 | 4623.09 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 507.3 | 2.50 | 4621.87 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 511.7 | 2.50 | 4680.64 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 512.1 | 2.50 | 4702.45 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 516.0 | 2.50 | 4875.65 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 517.3 | 2.50 | 4883.55 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 520.0 | 2.50 | 4660.32 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 527.3 | 2.50 | 5081.49 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 537.4 | 2.50 | 5133.06 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 538.0 | 2.50 | 5154.45 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 547.0 | 2.50 | 5213.83 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 554.0 | 2.50 | 5267.97 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 556.0 | 2.50 | 5262.20 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 561.0 | 2.50 | 5635.99 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 561.6 | 2.50 | 5641.08 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 566.0 | 2.50 | 4853.60 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 568.8 | 2.50 | 4224.13 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 570.4 | 2.50 | 3810.63 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 574.0 | 2.50 | 3027.06 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 574.8 | 2.50 | 2587.05 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 576.5 | 2.50 | 2251.76 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 579.2 | 2.50 | 1827.44 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 583.6 | 2.50 | 1020.73 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 584.3 | 2.50 | 885.38 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 588.0 | 2.50 | 487.28 | 7.908e+04 | 2.50 | 1.782e+05 | 7.908e+04 |
| 592.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

2.2.2 Verifica Cordoli Copertura

Il progetto e la verifica strutturale dei cordoli di copertura è stato svolto mediante l'ausilio di programma di calcolo Pro-Sap, implementando i risultati delle analisi ottenute dal solutore di calcolo sul modello strutturale per le fondazioni. I cordoli sono trattati come elementi *beam D2* (elementi trave).

Parametri sismici di riferimento e Criteri di Progetto:

- Terreno: Cat. “**B**” – **T1**
- Comportamento Strutturale: **NON DISSIPATIVO**;
- Fattore di Comportamento: **$q_x=q_y= 1.5$**
- Progettazione **Non Dissipativa in Campo Sostanzialmente Elastico**.

Materiali:

- Calcestruzzo **C25/30**;
- Acciaio **B450C**.

2.2.2.1 Legenda Tabella Verifica Cordoli agli SLU

La progettazione degli elementi trave viene eseguita a pressoflessione retta; la progettazione delle staffe è legata alle sollecitazioni di taglio e torsione.

In particolare vengono riportati: il rapporto x/d , le verifiche per sollecitazioni proporzionali e la verifica per compressione media, le quantità di armatura inferiore e superiore oltre che l'armatura trasversale.

| | |
|---------------|---|
| %Af | Percentuale di area di armatura rispetto a quella di calcestruzzo |
| Af inf. | Area di armatura longitudinale posta all'intradosso |
| Af sup | Area di armatura longitudinale posta all'estradosso |
| Af long. | Area complessiva armatura longitudinale |
| x/d | rapporto tra posizione dell'asse neutro e altezza utile |
| V N/M | Verifica a pressoflessione rapporto E_d/R_d : valore minore o uguale a 1 per verifica positiva |
| Staffe | Dati tratto di staffatura oggetto di verifica, nello specifico: numero delle braccia, diametro, passo, lunghezza L tratto |
| V V/T cls | Verifica a taglio/torsione lato cls con rapporto V_{ed}/V_{rd} : valore minore o uguale a 1 per verifica positiva |
| V V/T acciaio | Verifica a taglio/torsione lato acciaio con rapporto V_{ed}/V_{rd} : valore minore o uguale a 1 per verifica positiva |
| Rif. cmb. | Riferimento combinazioni da cui si generano le verifiche più gravose per la trave |

Avendo progettato a comportamento strutturale non dissipativo le verifiche geotecniche vengono effettuate senza nessun incremento.

2.2.2.2 Cordoli Sez. 23x45

Numerazione Travate: **6 – 8**

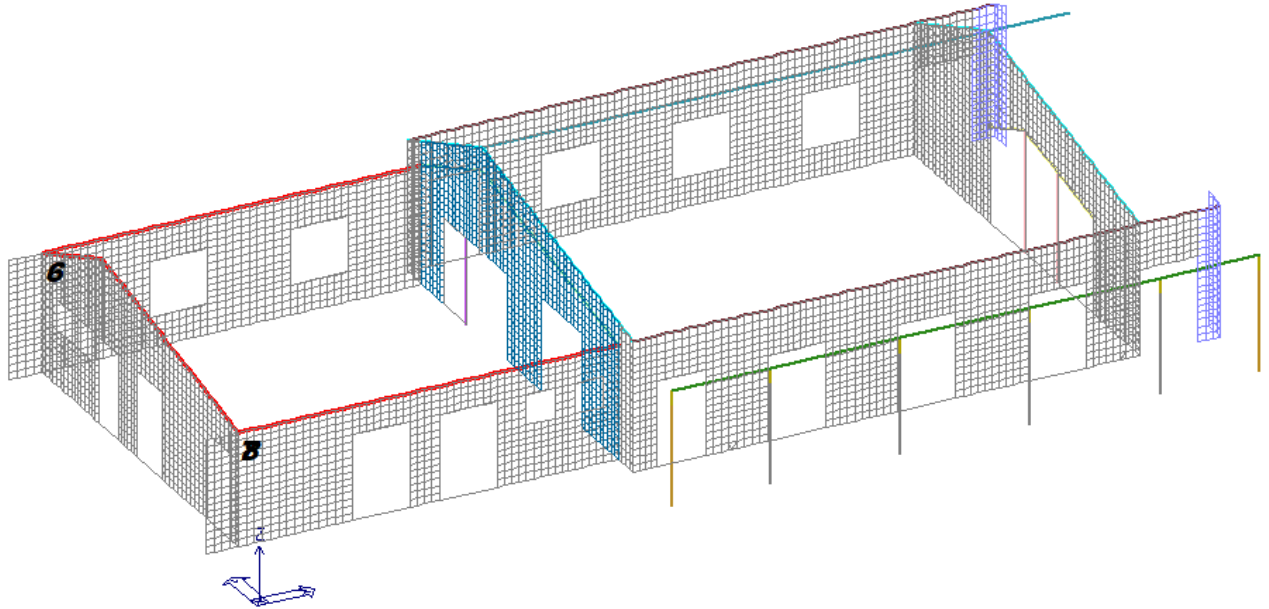


Fig 135. Numerazione Travate oggetto di verifica da modello di calcolo.

Mappe Cromatiche di Verifica

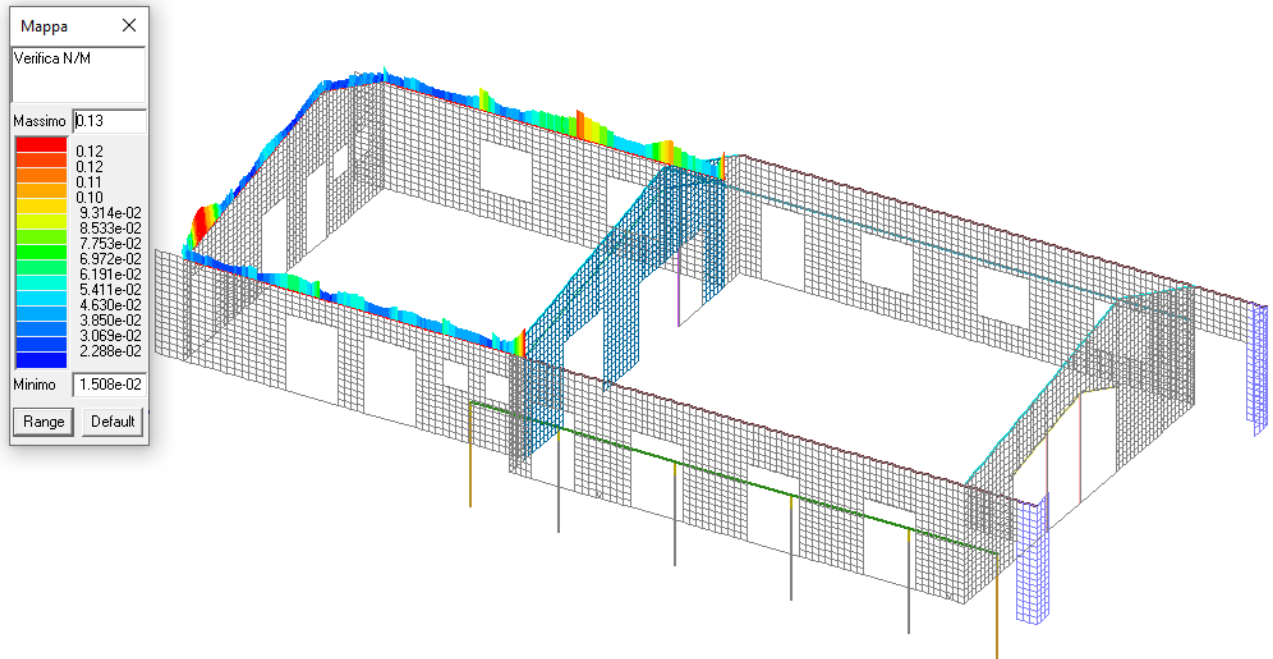


Fig 136. SLU: Mappa di Verifica a Pressoflessione N/M.

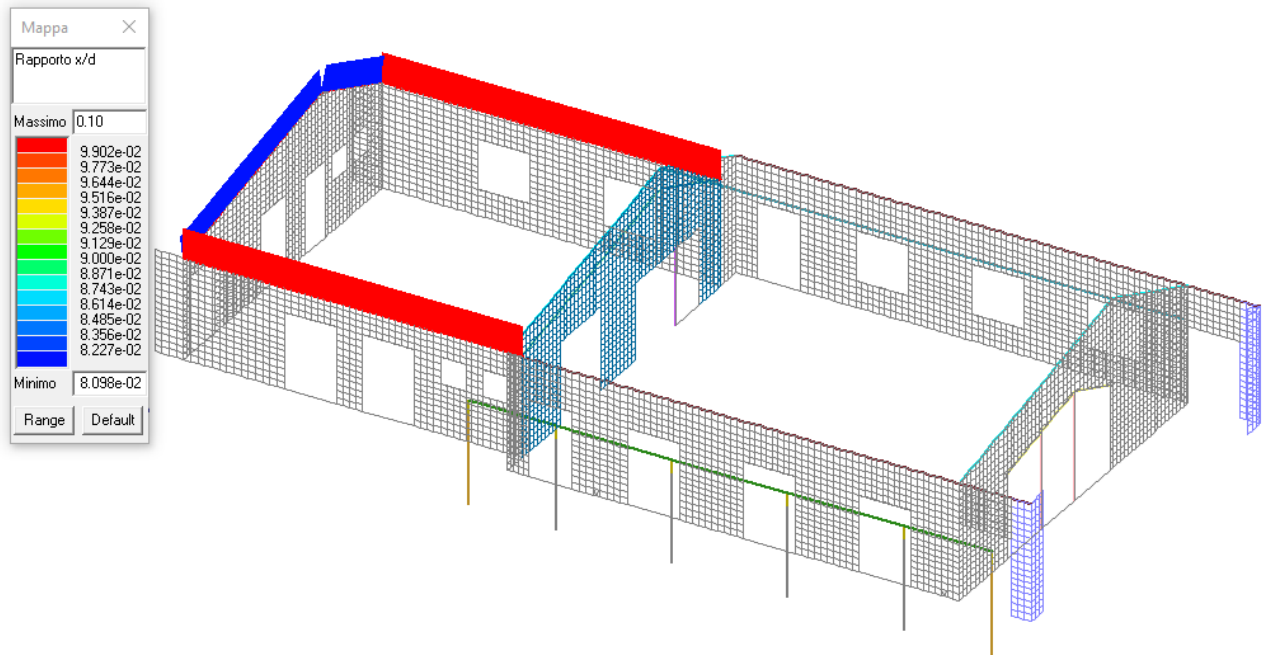


Fig 137. SLU: Mappa Rapporto x/d.

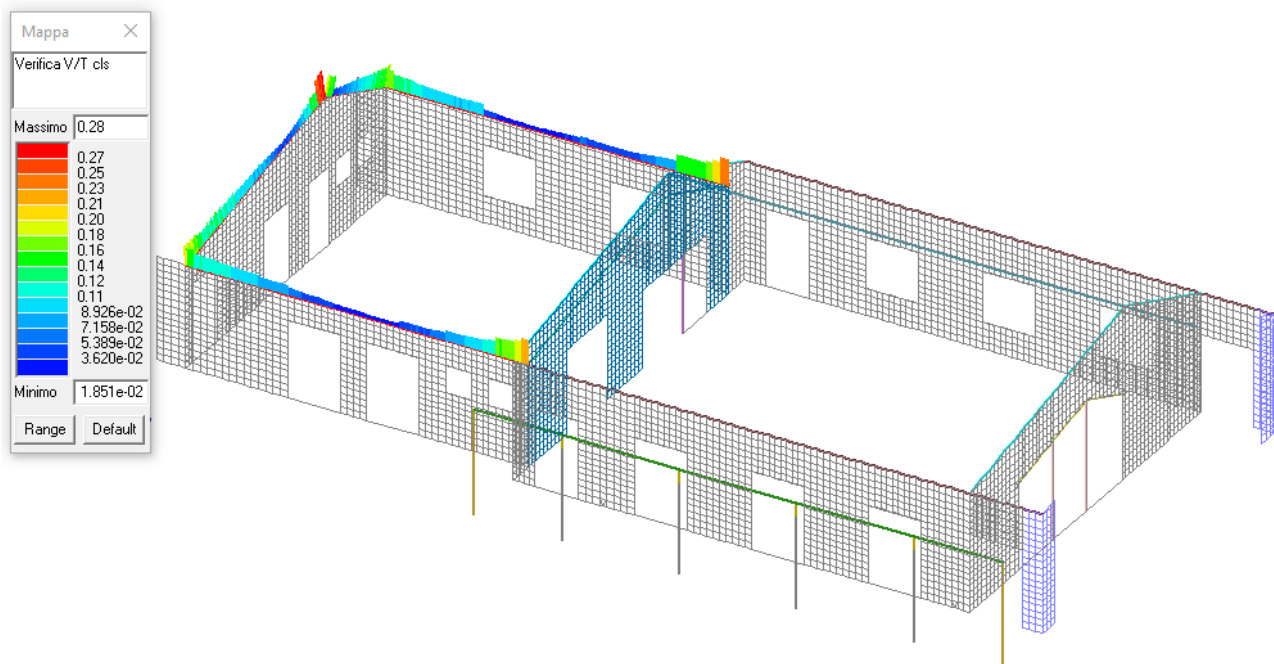


Fig 138. SLU: Mappa Verifica V/T cls.

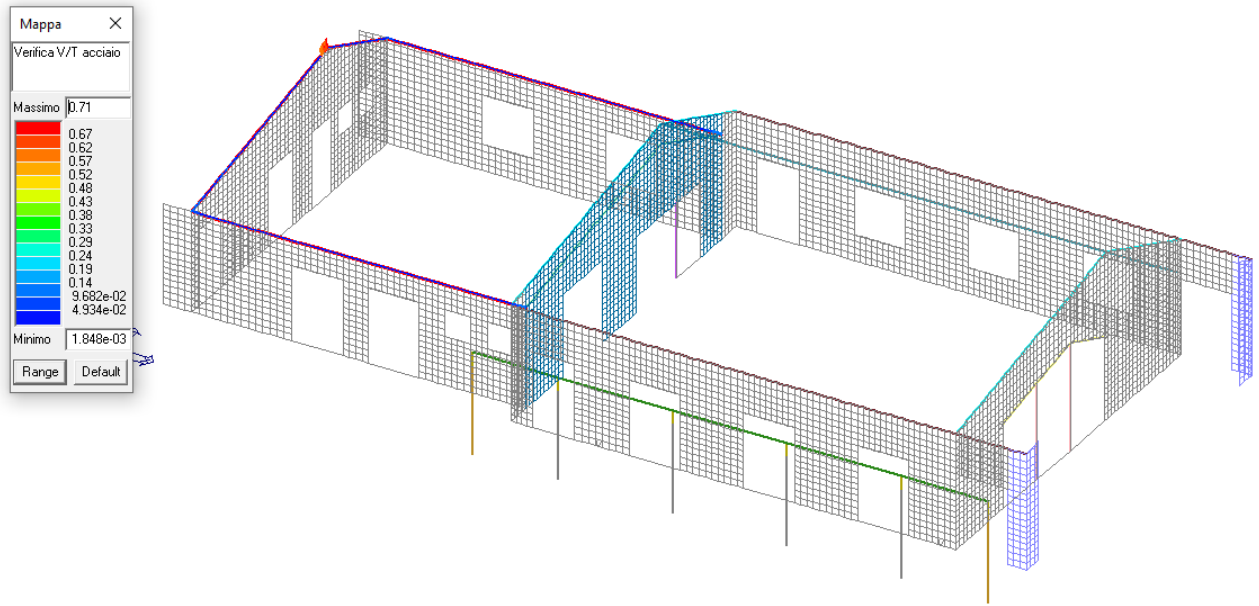


Fig 139. SLU: Mappa Verifica V/T acciaio.

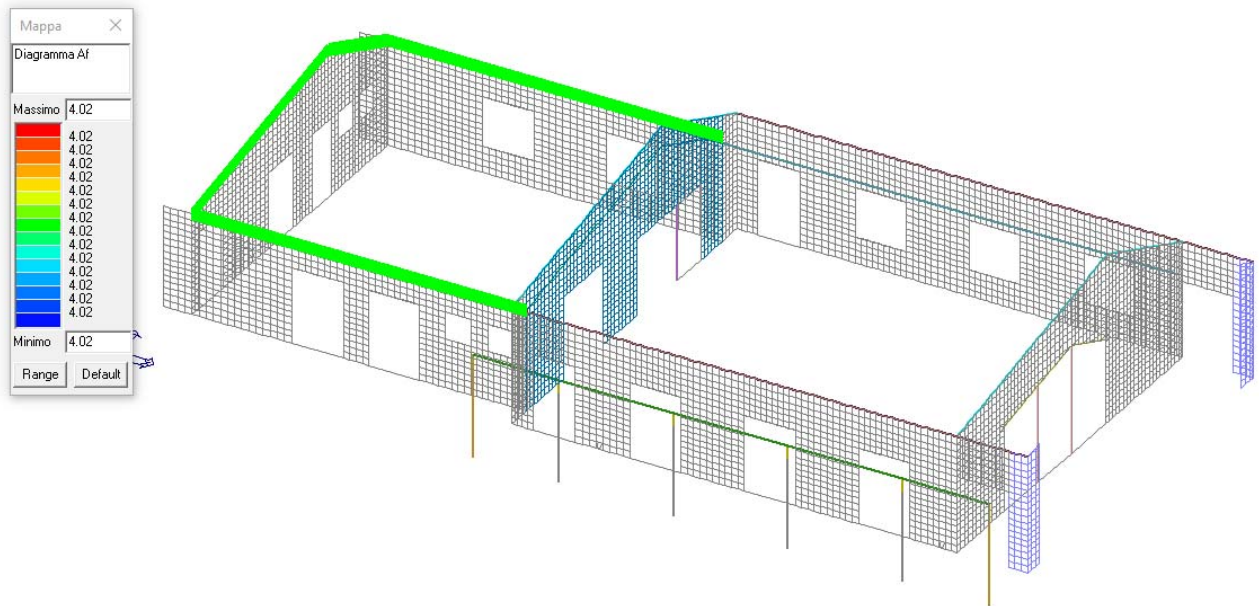


Fig 140. SLU: Mappa Armatura Longitudinale da calcolo [cm²].

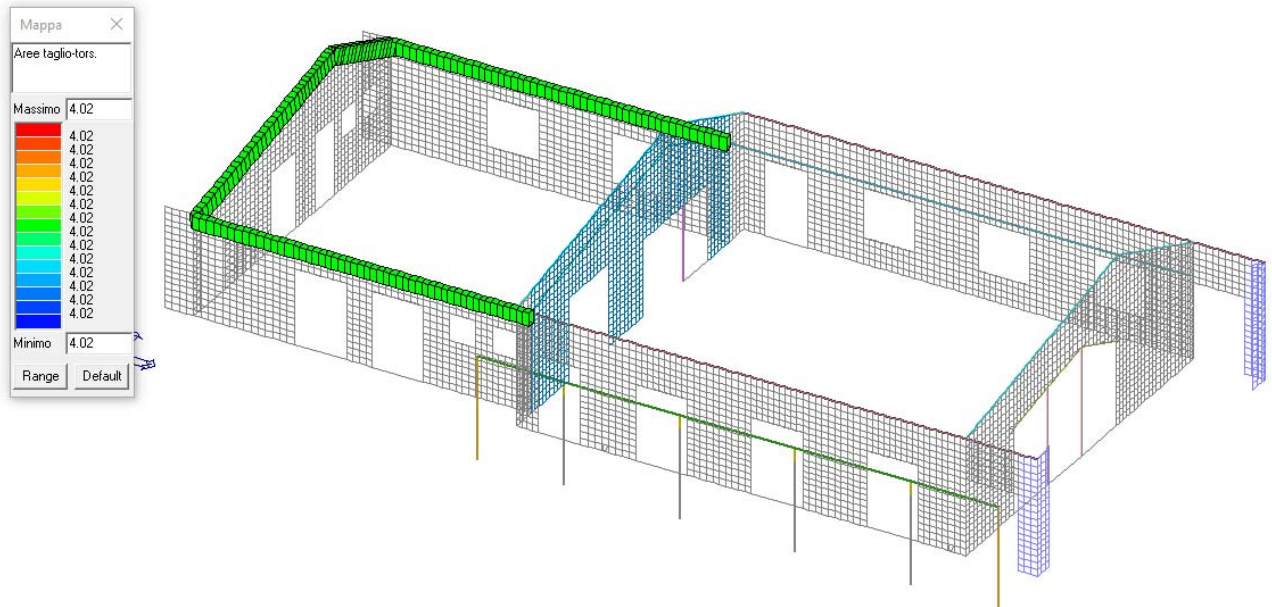


Fig 141. SLU: Mappa Armatura Trasversale da calcolo [cm²/m].

2.2.2.3 Cordoli sotto interno

Numerazione Travate: **4 – 9**

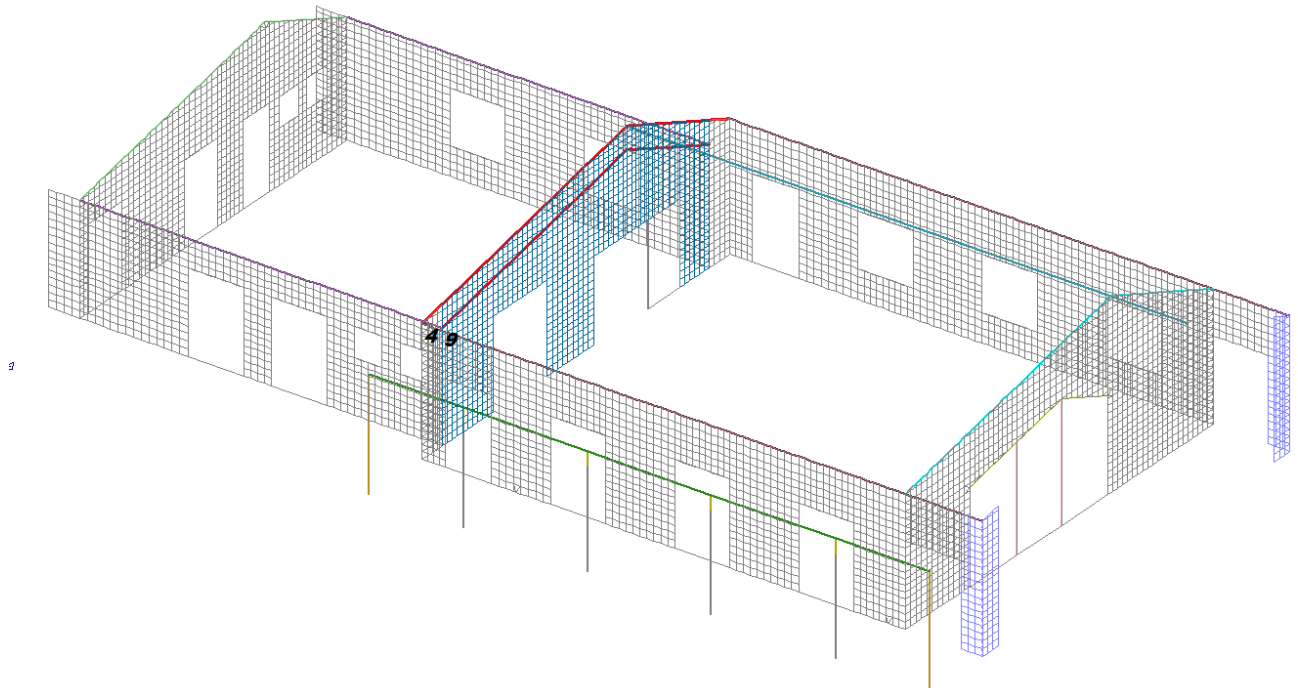


Fig 142. Numerazione Travate oggetto di verifica da modello di calcolo.

Mappe Cromatiche di Verifica

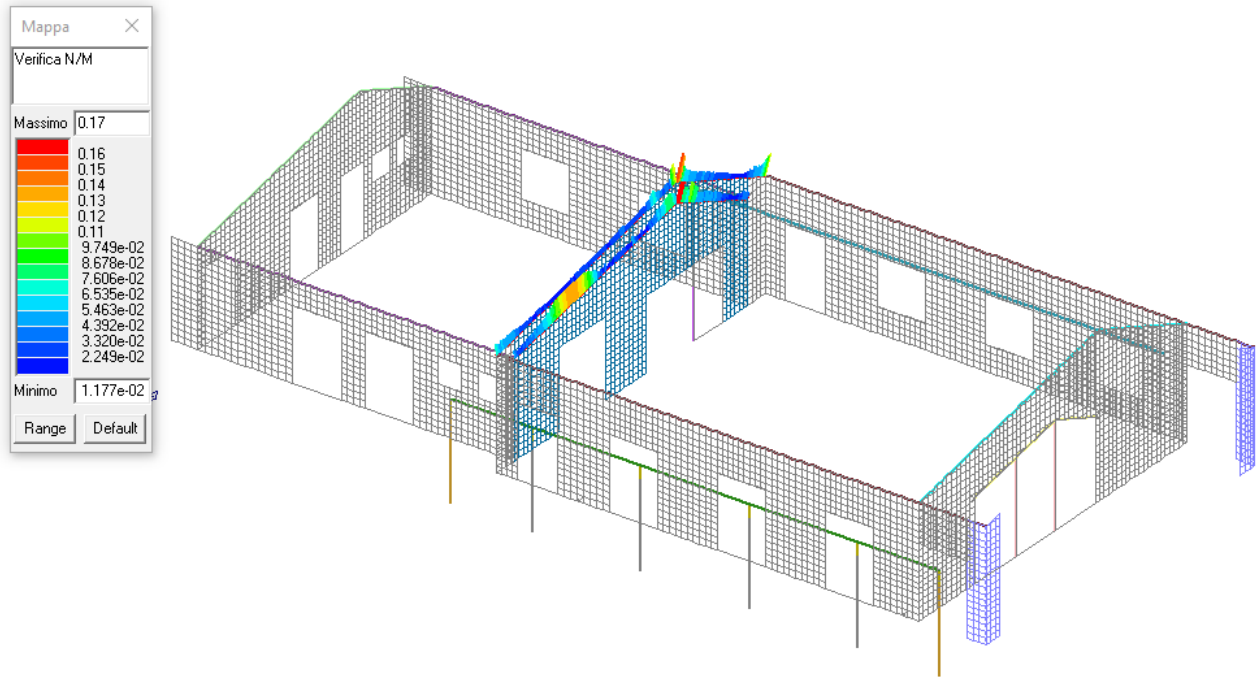


Fig 143. SLU: Mappa di Verifica a Pressoflessione N/M.

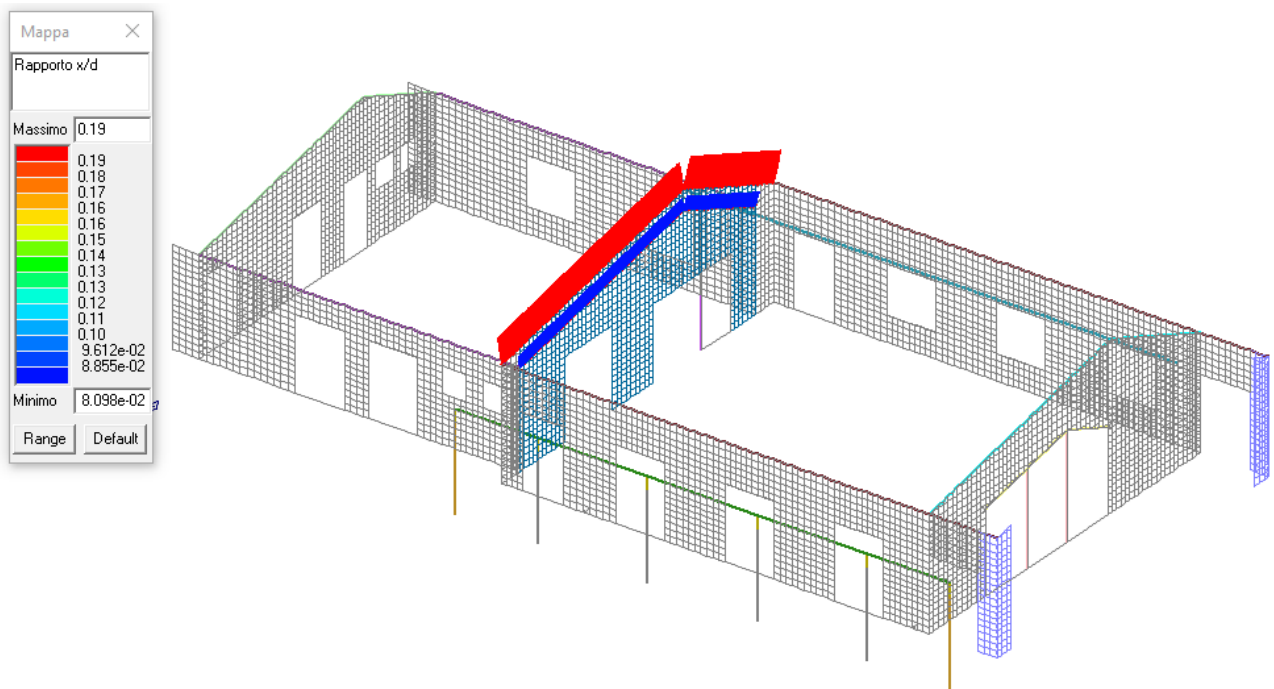


Fig 144. SLU: Mappa Rapporto x/d.

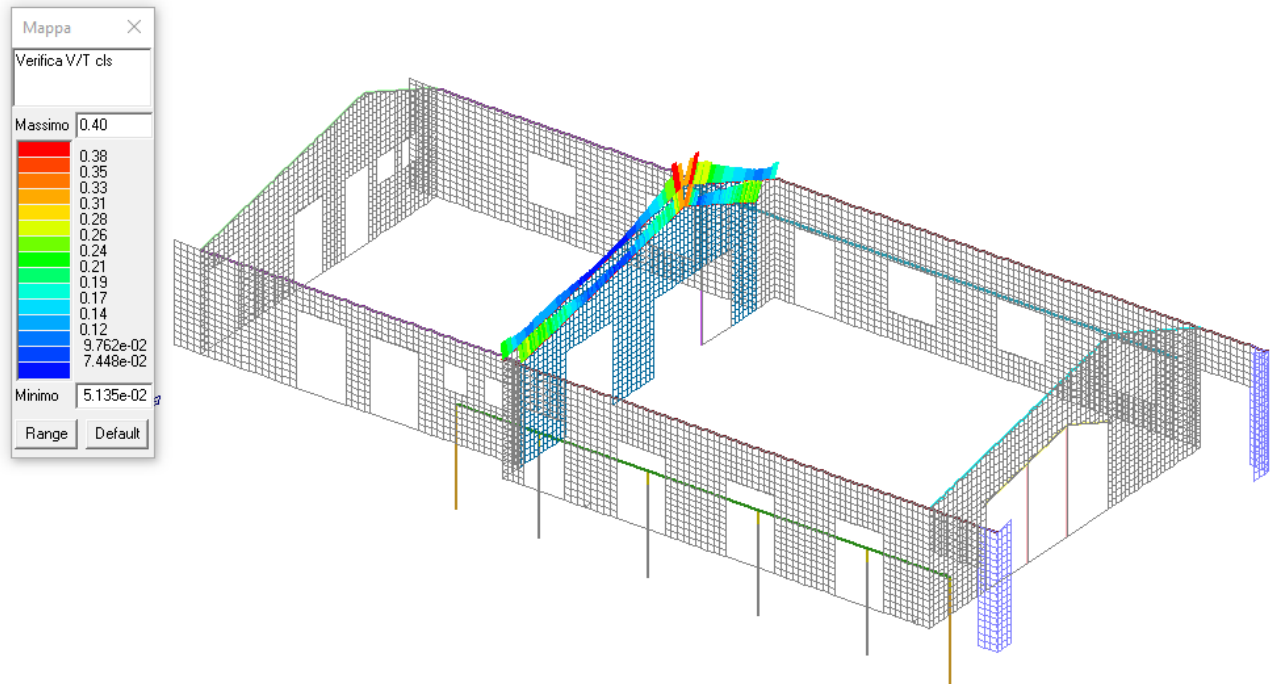


Fig 145. SLU: Mappa Verifica V/T cls.

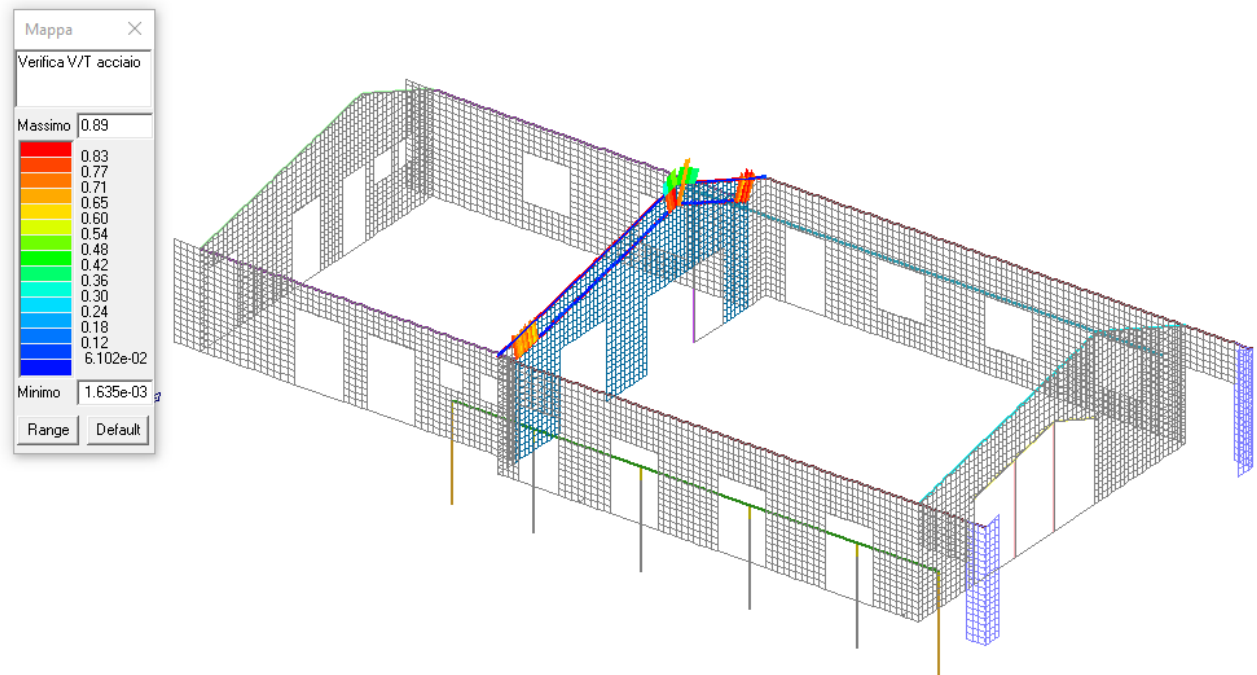


Fig 146. SLU: Mappa Verifica V/T acciaio.

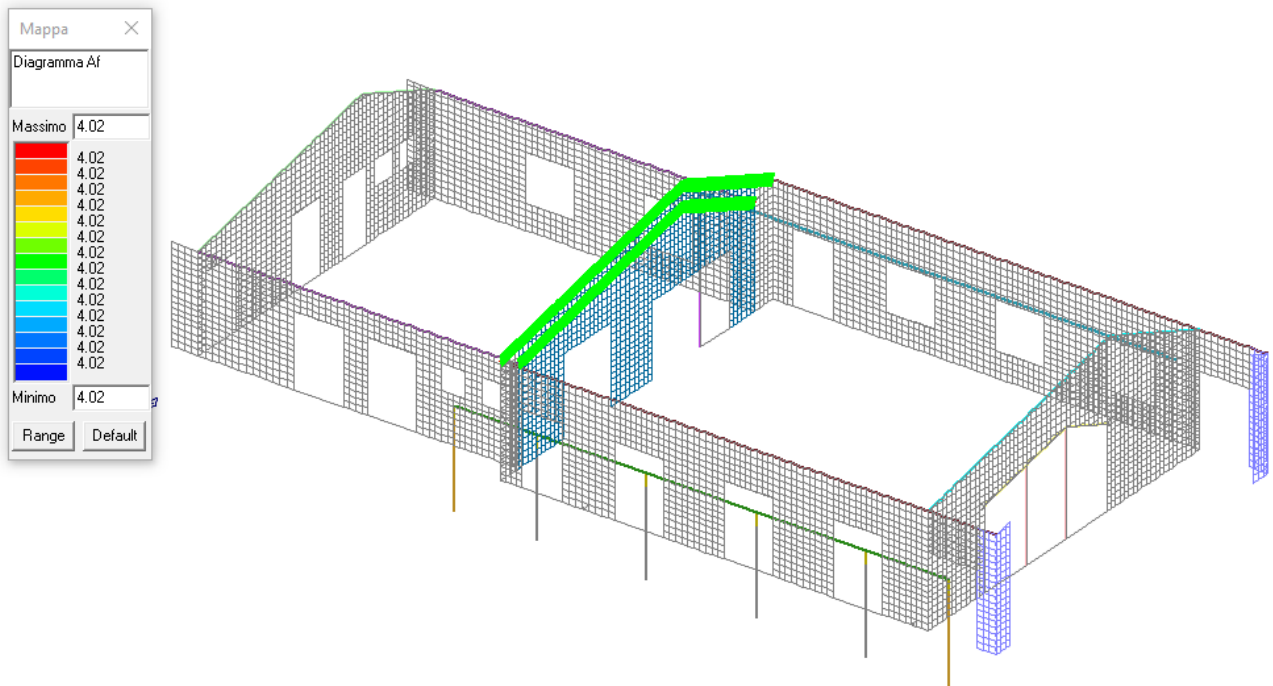


Fig 147. SLU: Mappa Armatura Longitudinale da calcolo [cm²].

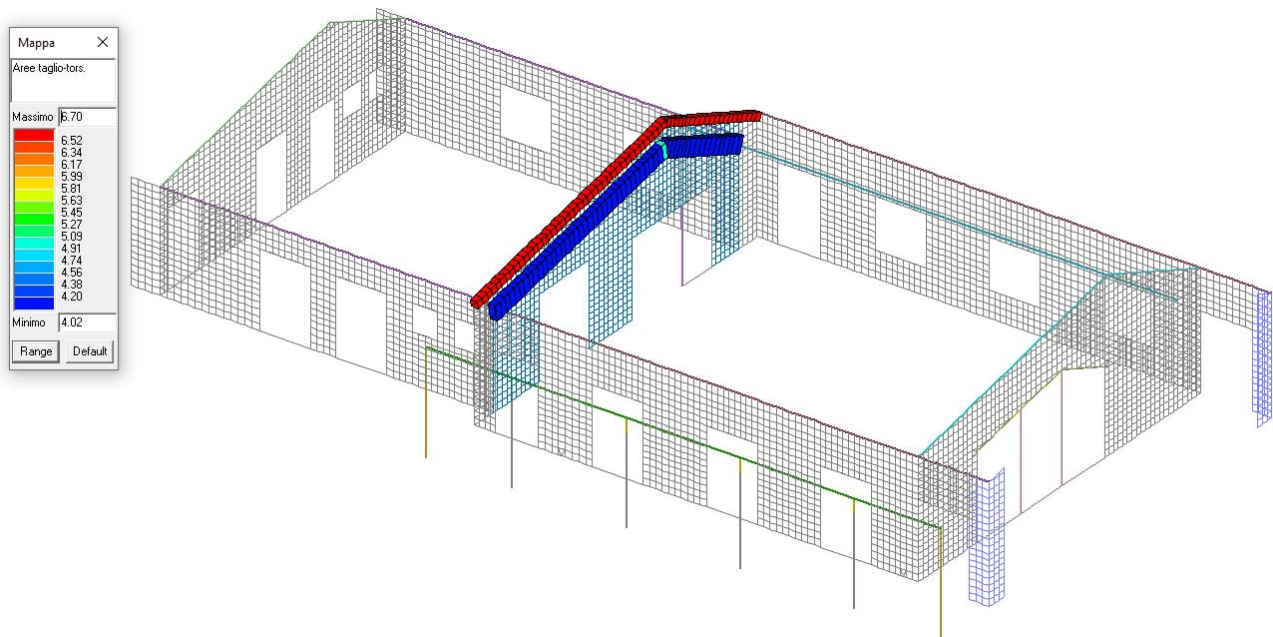


Fig 148. SLU: Mappa Armatura Trasversale da calcolo [cm²/m].

2.2.2.4 Cordolo facciata 23x25

Numerazione Travate: 10

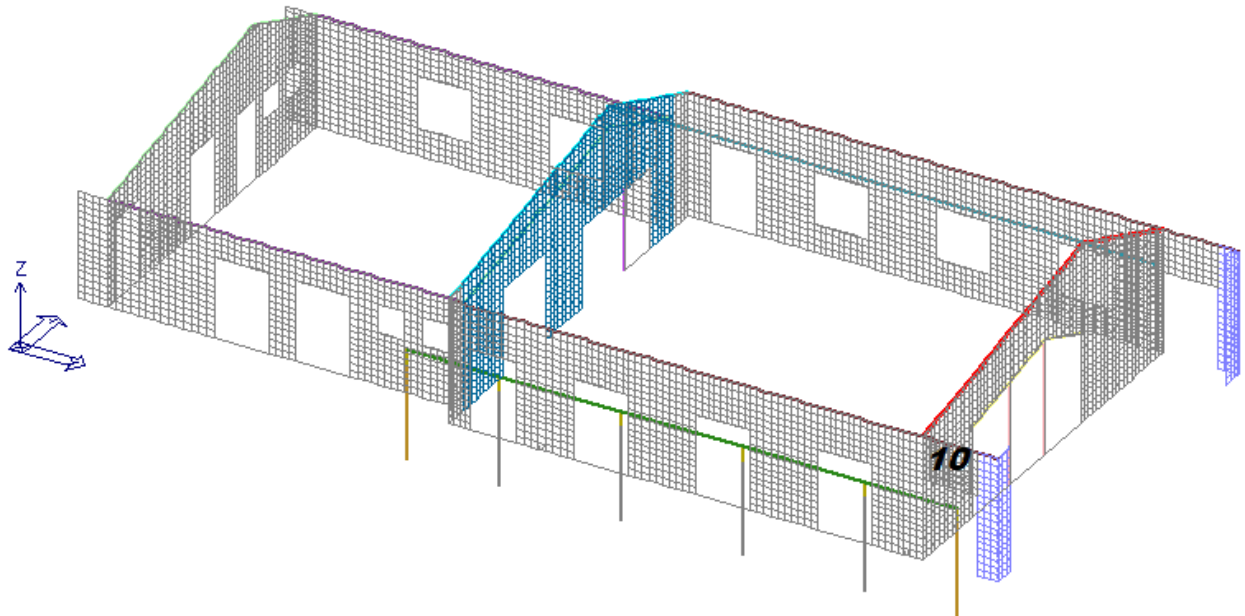


Fig 149. Numerazione Travate oggetto di verifica da modello di calcolo.

Mappe Cromatiche di Verifica

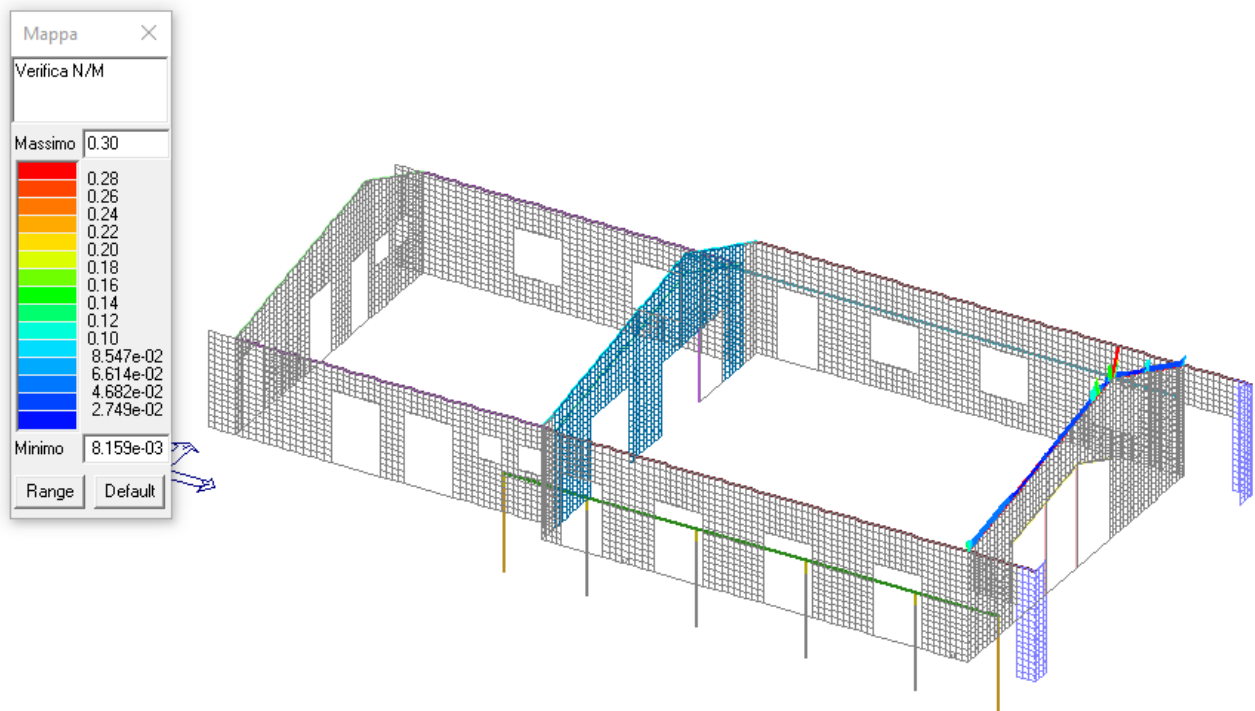


Fig 150. SLU: Mappa di Verifica a Pressoflessione N/M.

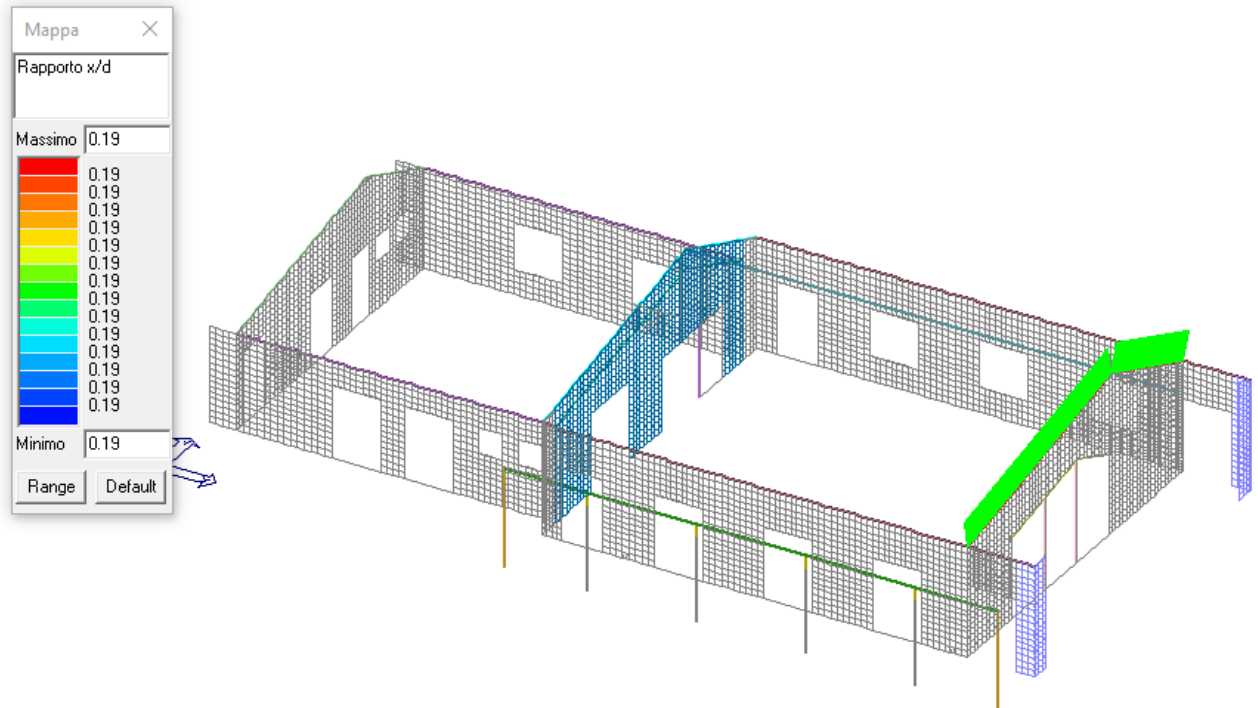


Fig 151. SLU: Mappa Rapporto x/d.

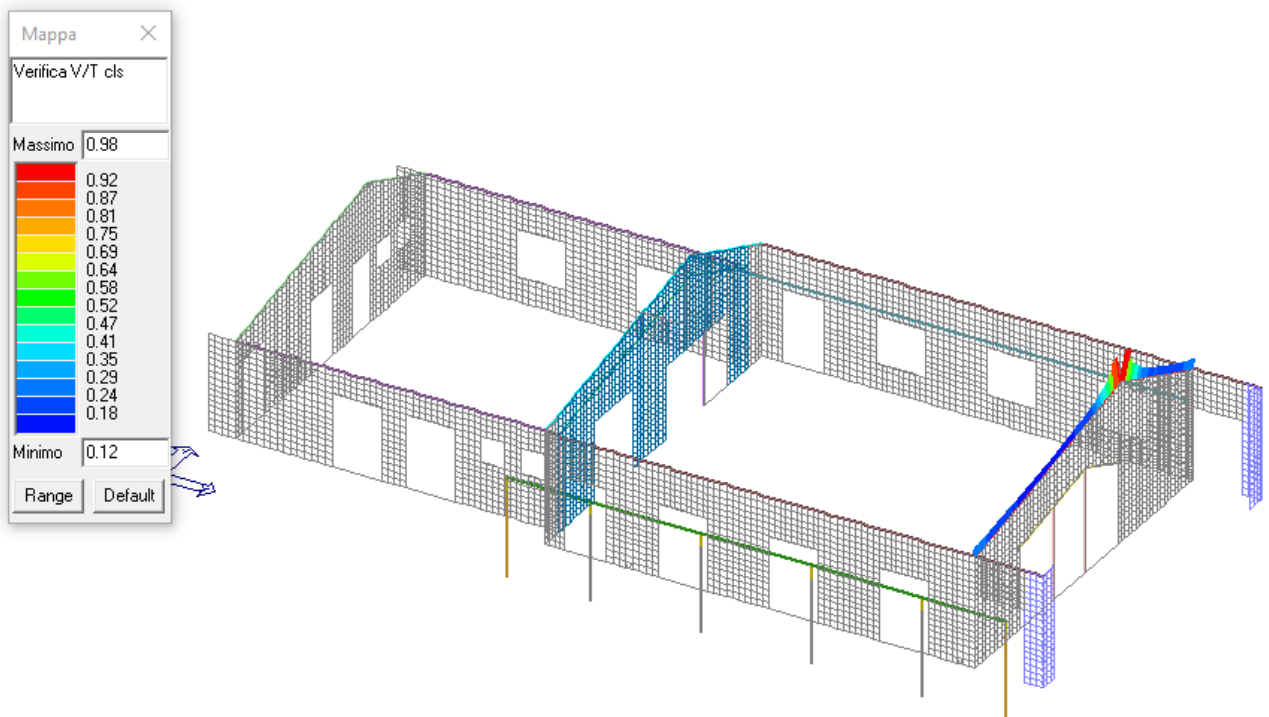


Fig 152. SLU: Mappa Verifica V/T cls.

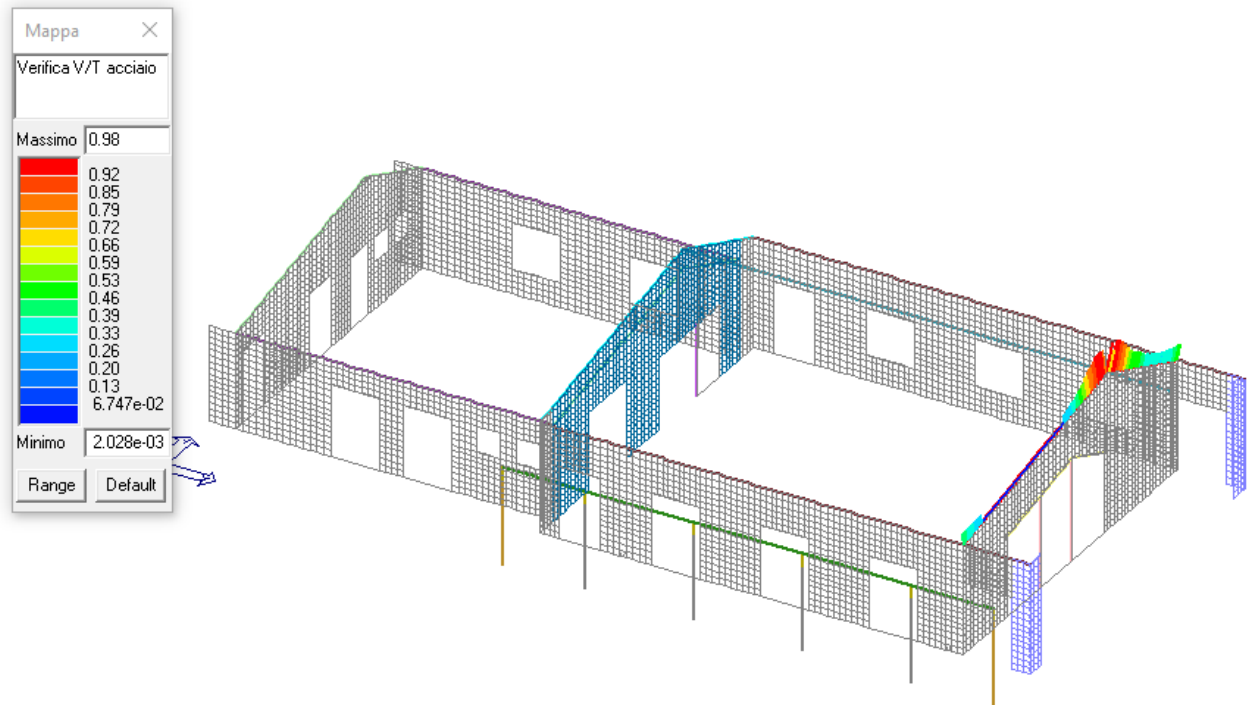


Fig 153. SLU: Mappa Verifica V/T acciaio.

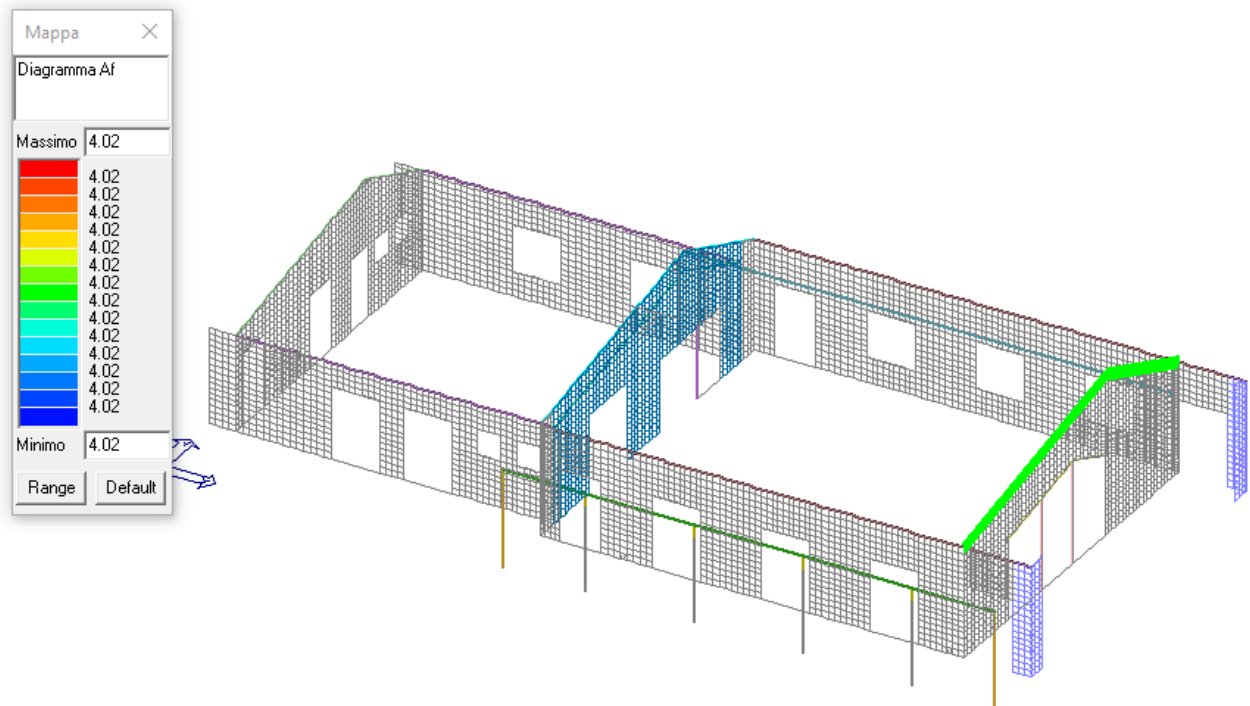


Fig 154. SLU: Mappa Armatura Longitudinale da calcolo [cm²].

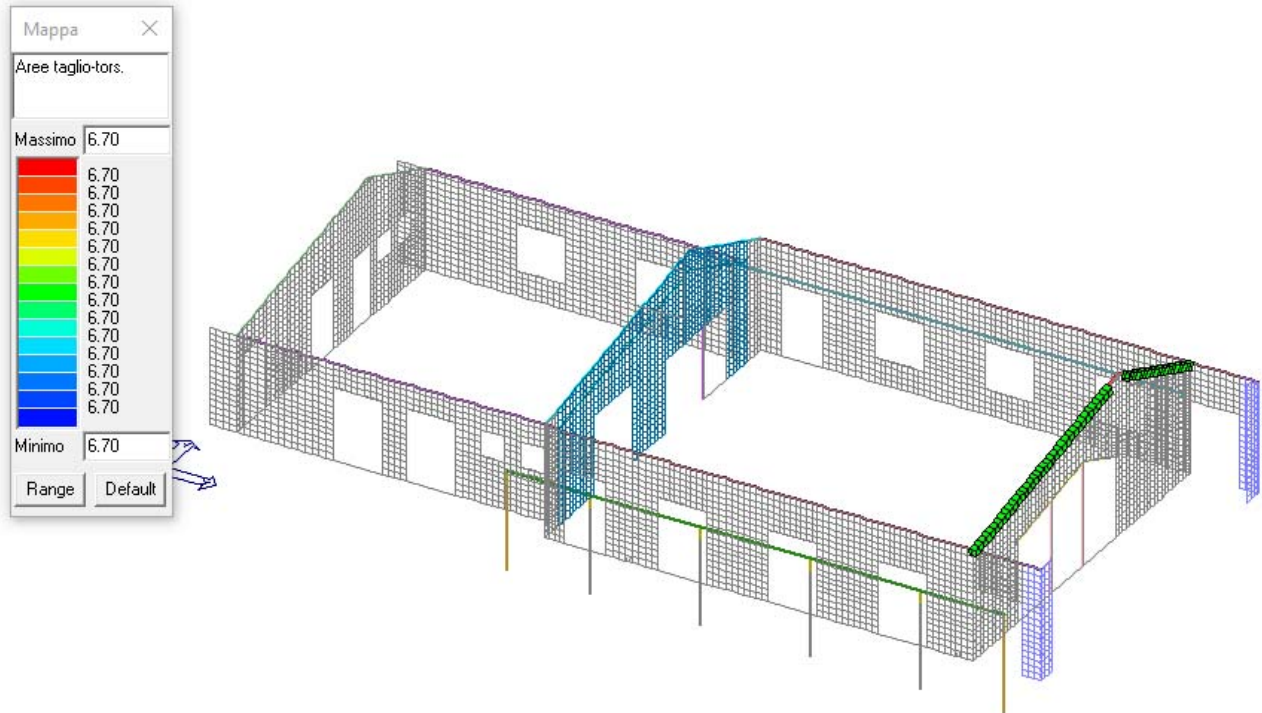


Fig 155. SLU: Mappa Armatura Trasversale da calcolo [cm²/m].

2.2.2.5 Cordoli laterali b23xh var

Numerazione Travate: **11 - 12**

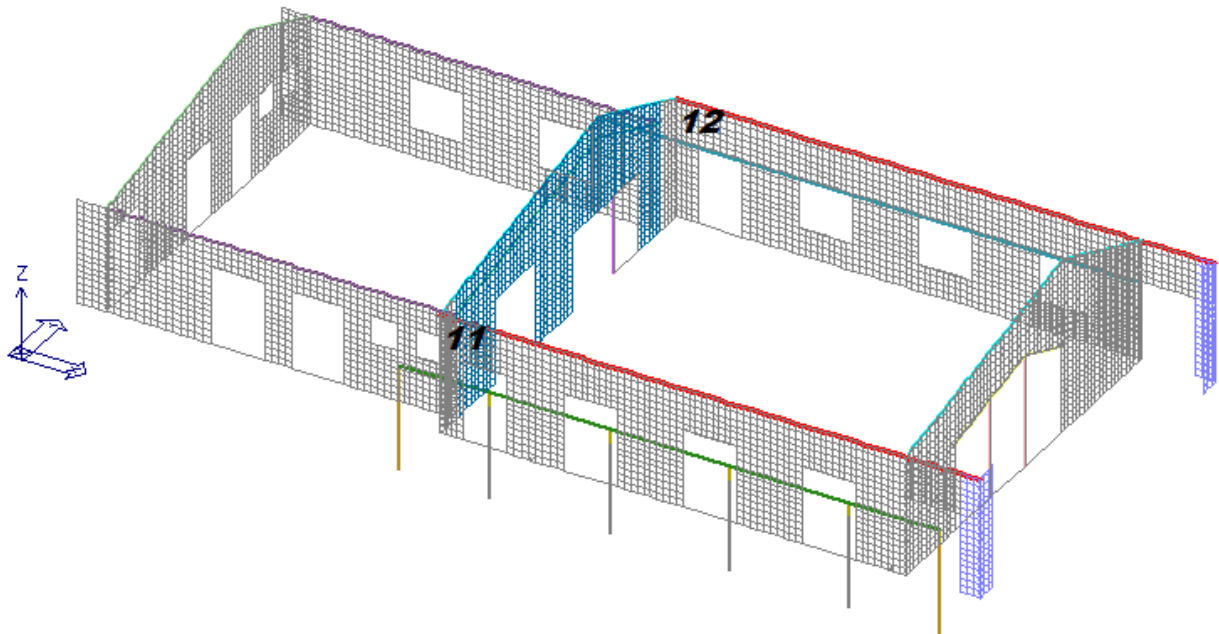


Fig 156. Numerazione Travate oggetto di verifica da modello di calcolo.

Mappe Cromatiche di Verifica

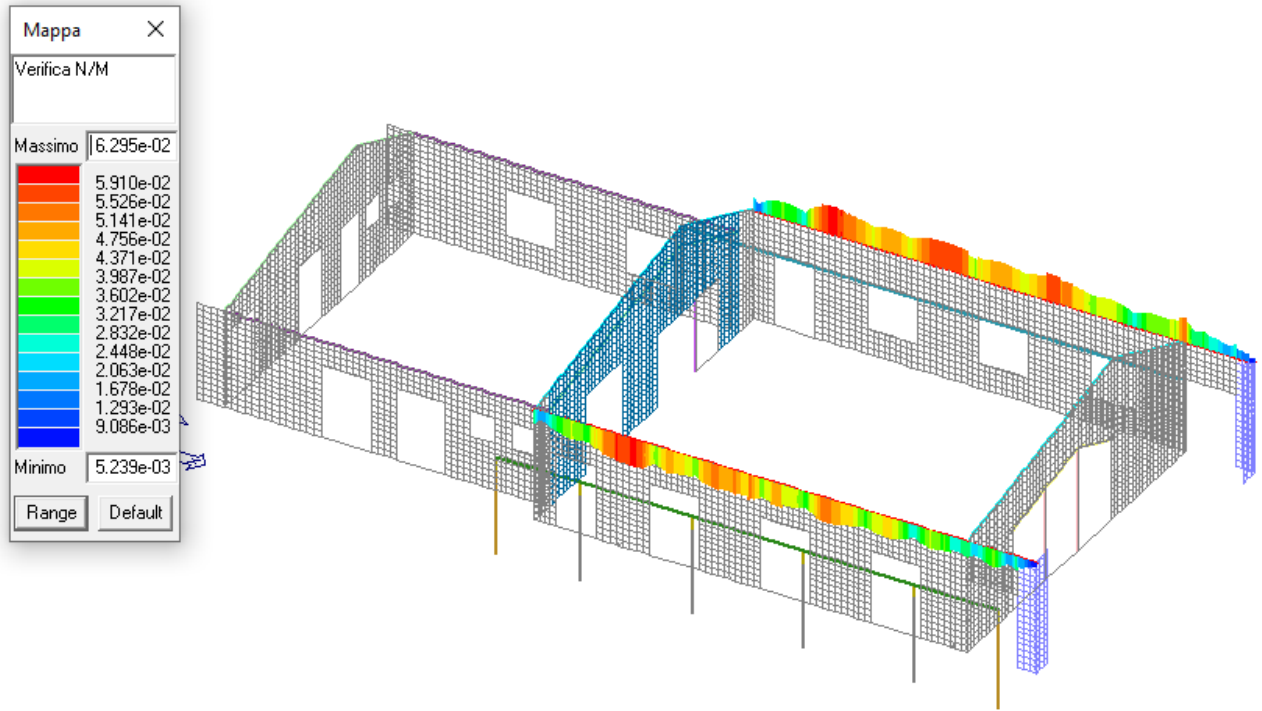


Fig 157. SLU: Mappa di Verifica a Pressoflessione N/M.

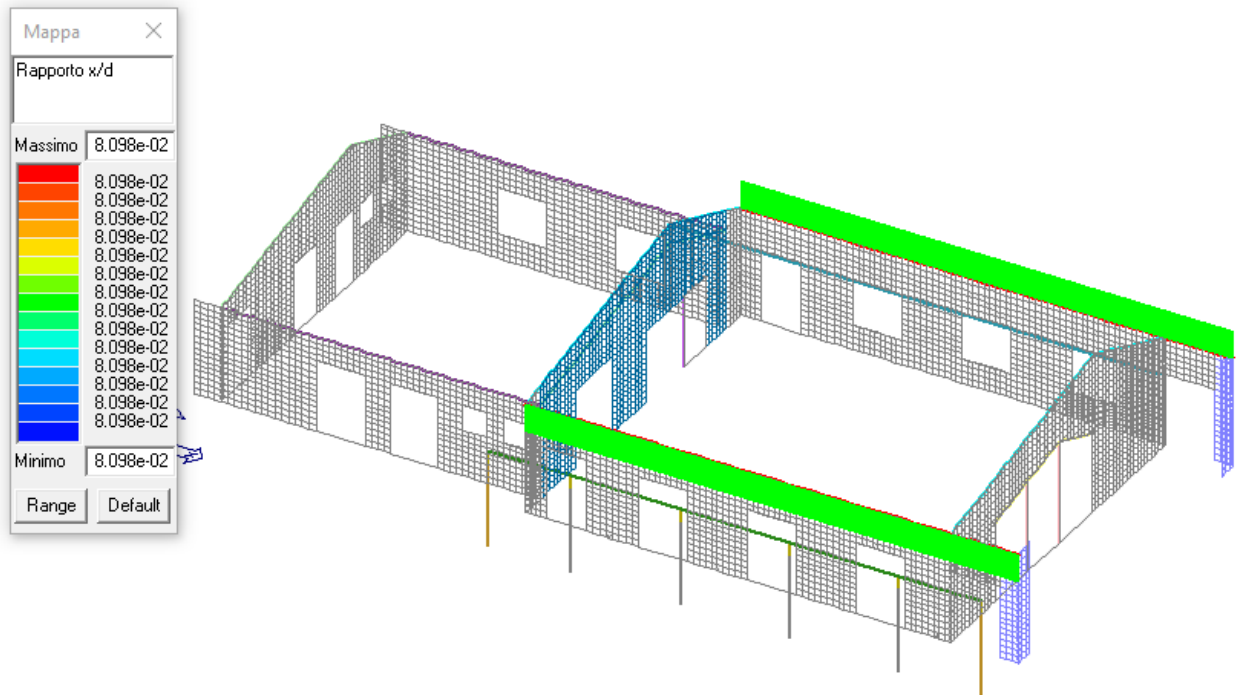


Fig 158. SLU: Mappa Rapporto x/d.

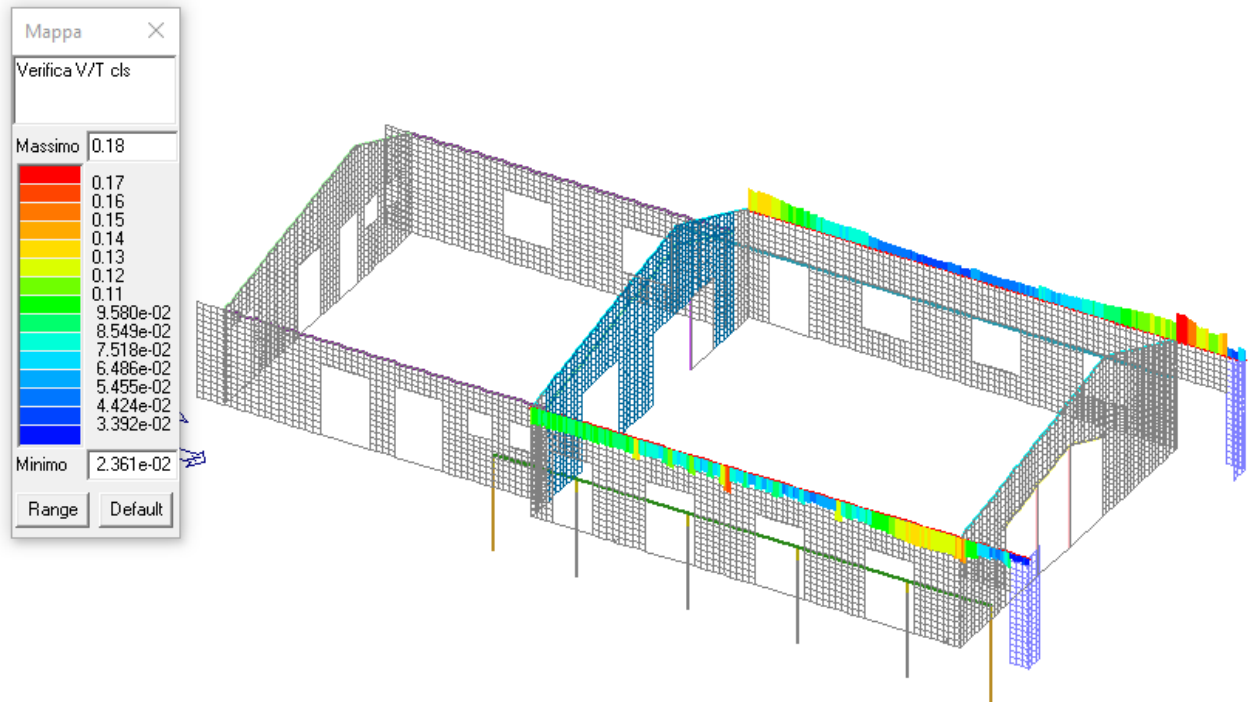


Fig 159. SLU: Mappa Verifica V/T cls.

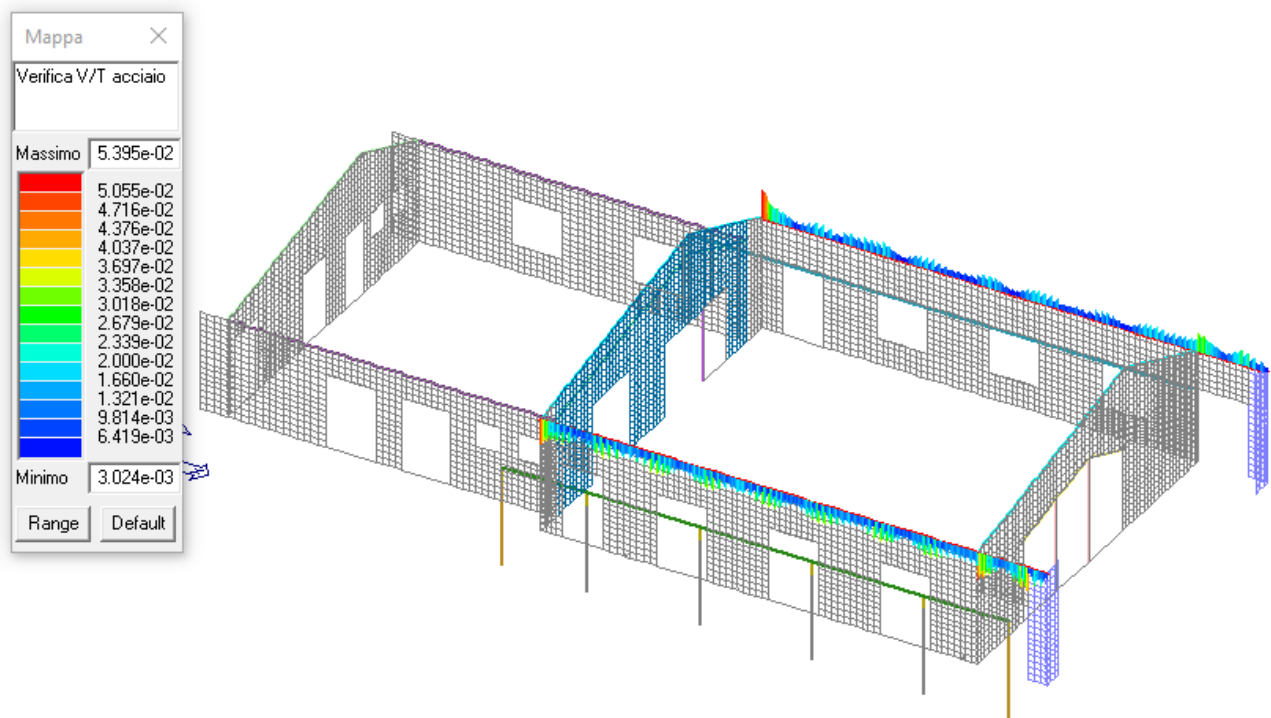


Fig 160. SLU: Mappa Verifica V/T acciaio.

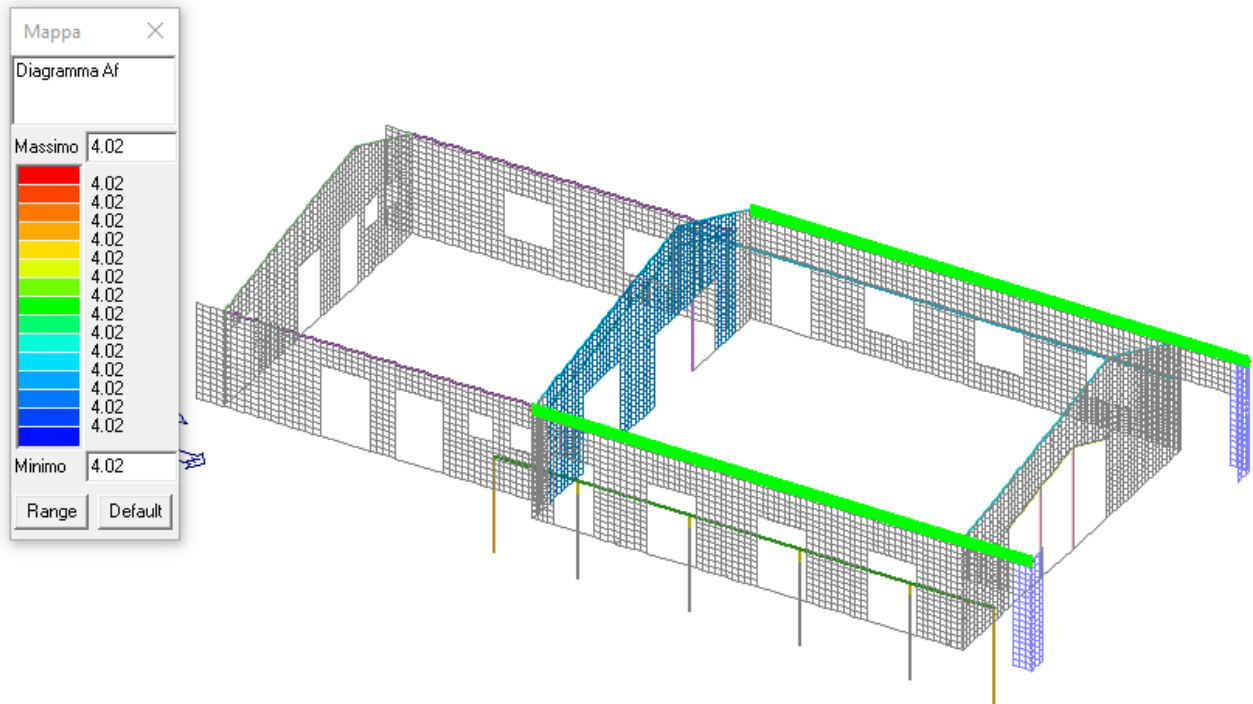


Fig 161. SLU: Mappa Armatura Longitudinale da calcolo [cm²].

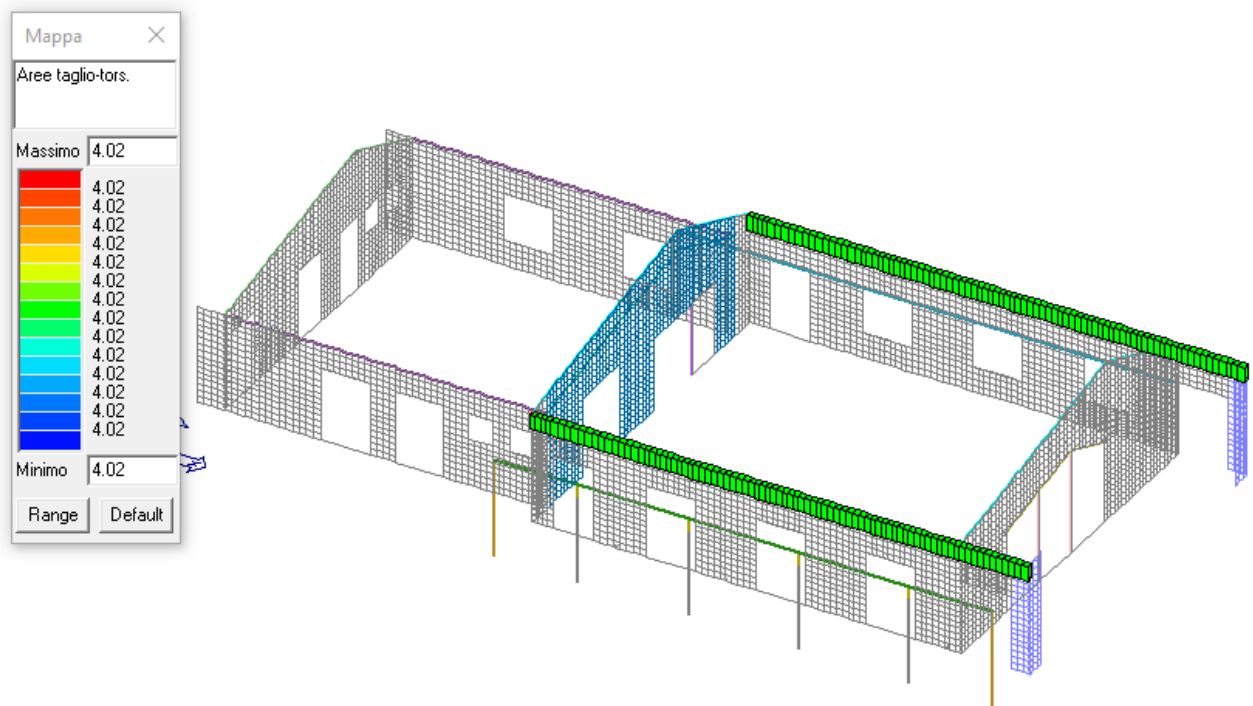


Fig 162. SLU: Mappa Armatura Trasversale da calcolo [cm²/m].

2.2.3 Verifica Setti di fondazione in c.a.

Il progetto e la verifica strutturale dei Setti in c.a. delle opere di fondazione è stato svolto mediante l'ausilio di programma di calcolo Pro-Sap, implementando i risultati delle analisi ottenute dal solutore di calcolo sul modello strutturale delle elevazioni.

Parametri sismici di riferimento e Criteri di Progetto:

- Terreno: Cat. “**B**” – **T1** –
- Comportamento Strutturale: **NON DISSIPATIVO**;
- Fattore di Comportamento: **$q_x=q_y= 1.5$**
- Progettazione **Non Dissipativa in Campo Sostanzialmente Elastico**.

Materiali:

- Calcestruzzo **C25/30**;
- Acciaio **B450C**.

2.2.3.1 Legenda Verifiche da Modello di Calcolo

La progettazione viene svolta in **campo sostanzialmente elastico** per **sistemi a comportamento NON DISSIPATIVO** come Pareti Estese Debolmente Armate costituite da elementi D3.

Tra le verifiche vengono riportati in mappe cromatiche sintetiche:

- V N/M Verifica delle sollecitazioni Normali (momento e sforzo normale) verificato se ≤ 1.0 ;
- Ver. Nsismica. Rapporto Nd/Nu : rapporto tra azione di calcolo e resistenza a compressione (normalizzato a 1 in quanto da confrontare con 40% in CDB e 35 % in CDA).
- Verifica Snellezza Verifica di snellezza in accordo con il §4.1.2.3.9.2 DM17.01.2018, verificato se ≤ 1.0 .
- Verifica V compressione Verifica a taglio compressione (lato cls).
- Verifica V trazione Verifica a taglio trazione (lato acciaio).
- Af pr+ quantità di armatura richiesta in direzione principale relativa alla faccia positiva (Verticale per setti) (valore derivante da calcolo o minimo normativo) espressa in cm^2/m ;
- Af pr- quantità di armatura richiesta in direzione principale relativa alla faccia negativa (verticale per setti) (valore derivante da calcolo o minimo normativo) espressa in cm^2/m ;
- Af sec+ quantità di armatura richiesta in direzione secondaria relativa alla faccia positiva (orizzontale per setti) (valore derivante da calcolo o minimo normativo) espressa in cm^2/m ;
- Af sec- quantità di armatura richiesta in direzione secondaria relativa alla faccia negativa orizzontale per setti) (valore derivante da calcolo o minimo normativo) espressa in cm^2/m .

2.2.3.2 Mappe cromatiche sintetiche di verifica da modello di calcolo

Si riportano le mappe cromatiche sintetiche di verifica, in accordo con quanto descritto in precedenza, dei setti in c.a. del sistema di fondazione. Nella figura successiva si riporta una vista di insieme del sistema di setti oggetto di verifica.

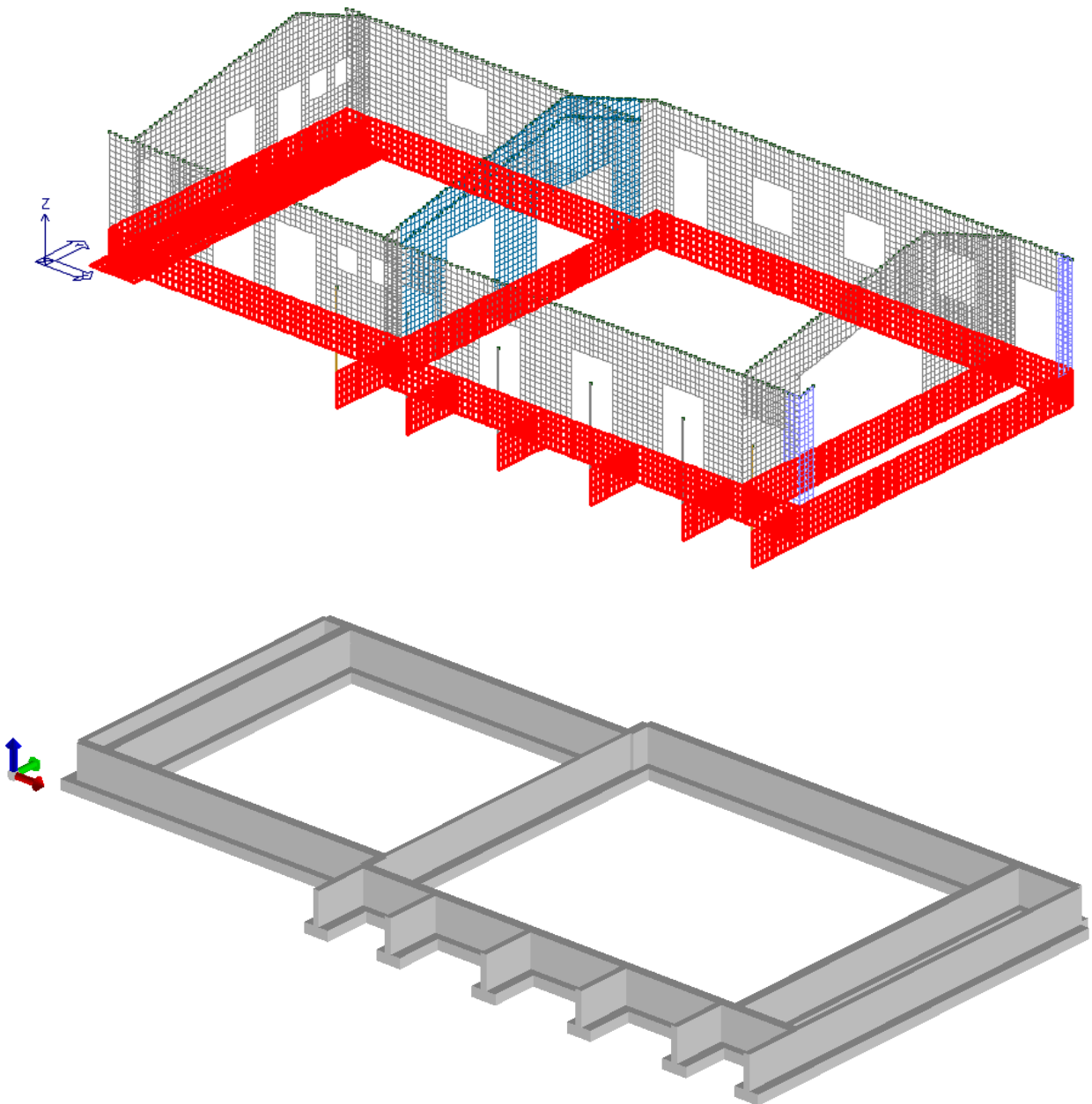


Fig 163. Setti di fondazione oggetto di verifica – Vista Unifilare (Completa) – Vista solida (fondazioni).

Verifiche SLU

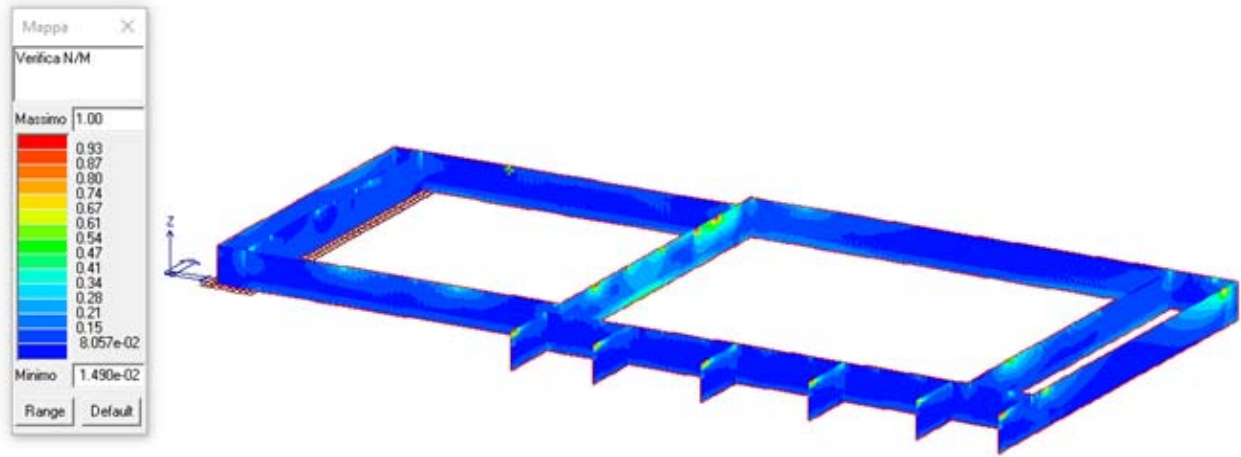


Fig 164. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

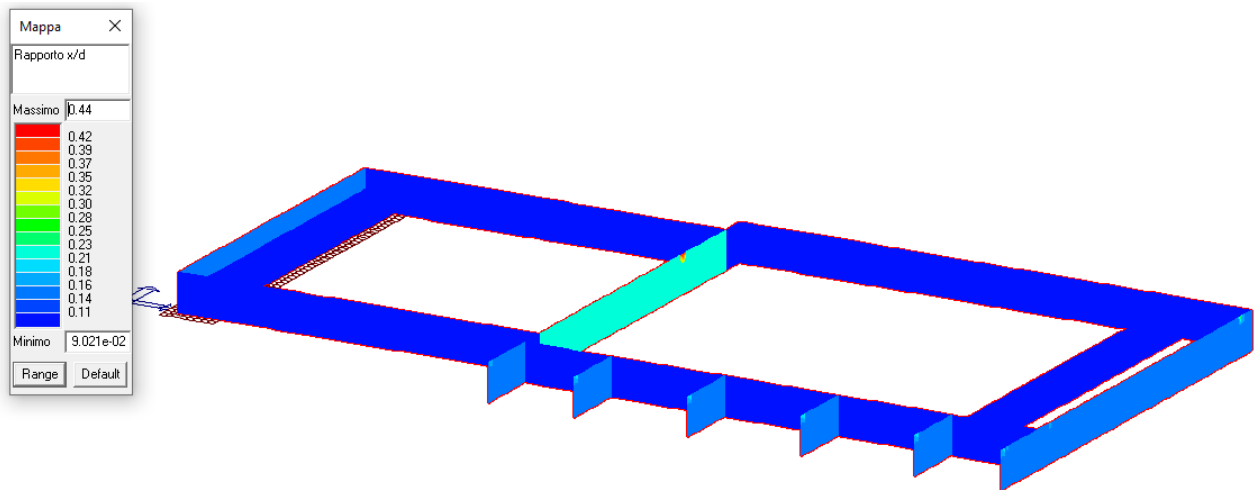


Fig 165. SLU: Mappa rapporto x/d.

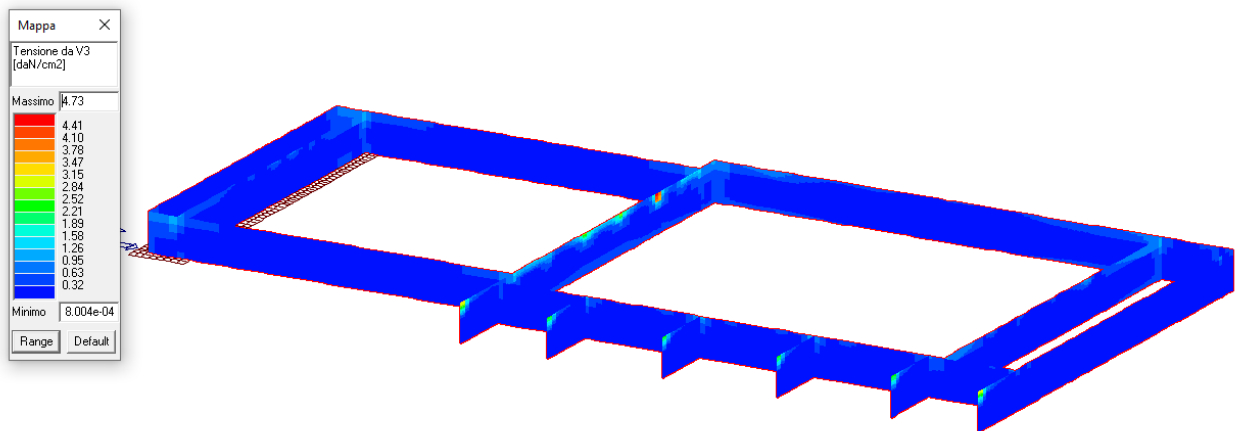


Fig 166. SLU: Mappa Tensione V3 – Massima tensione tangenziale [$\tau < V_{Rd}/H_u \cdot L$ – taglio resistente [4.1.23] per unità di lunghezza diviso per altezza utile = v_{min}]

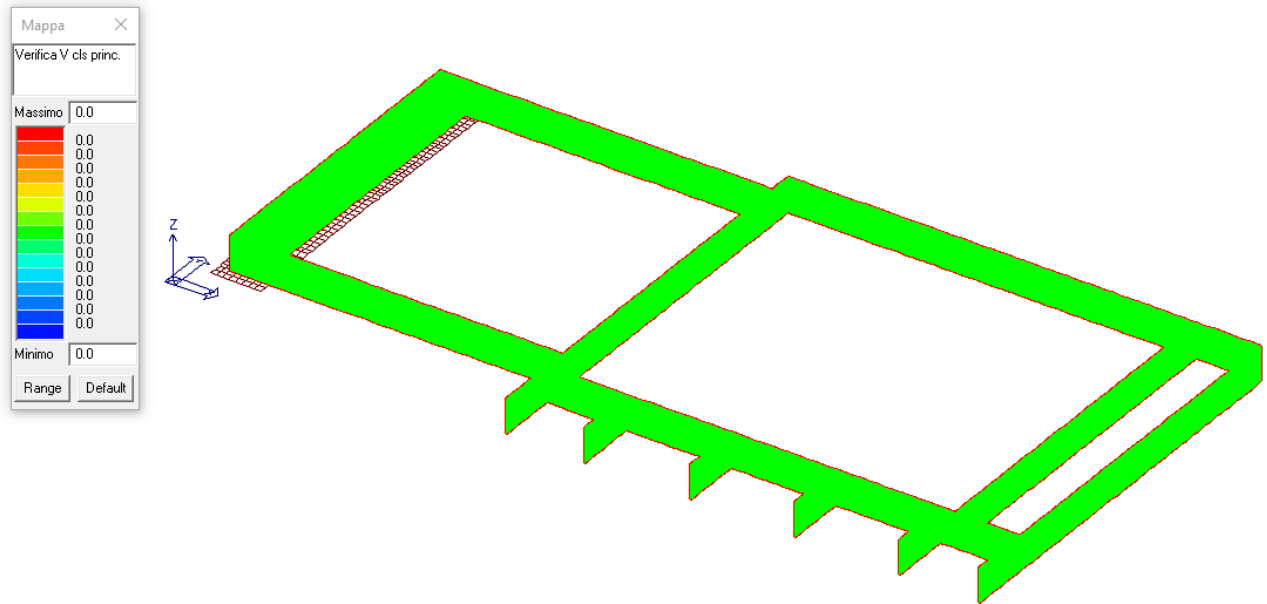


Fig 167. SLU: Mappa di Verifica Vcls direzione principale – Verifica non necessaria in quanto $\tau < \tau_{min}$ [$M \leq 1.0$ Verifica Soddisfatta].

Mappa Armatura Verticale da Calcolo

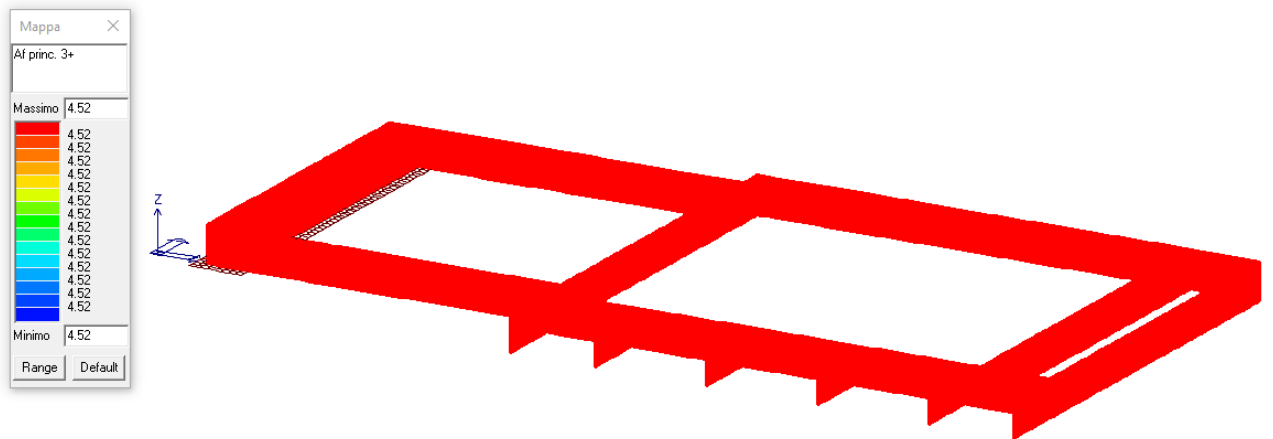


Fig 168. Mappa Armatura Verticale Faccia Positiva da Calcolo [cm²/m]. .

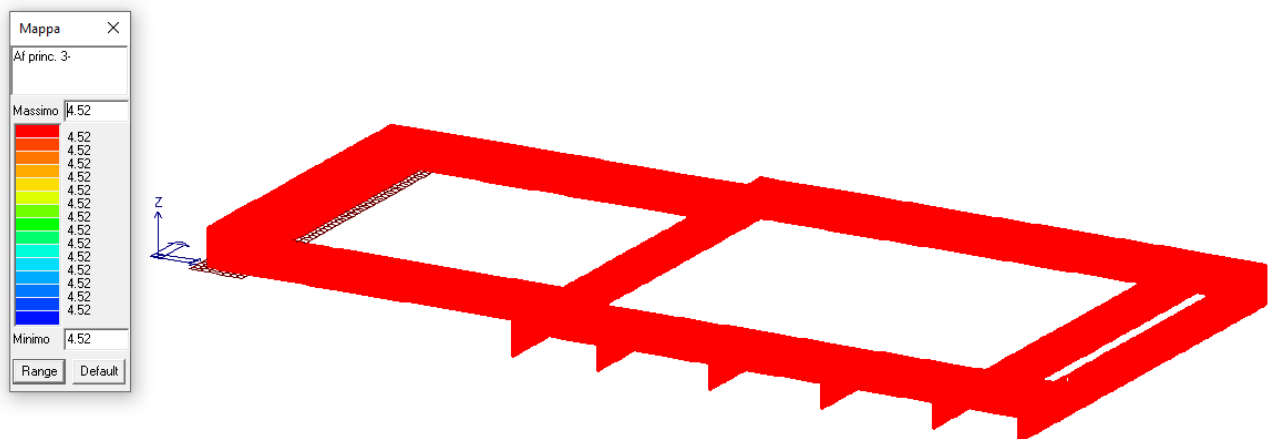


Fig 169. Mappa Armatura Verticale Faccia Negativa da Calcolo [cm²/m]. .

Mappa Armatura Orizzontale da Calcolo

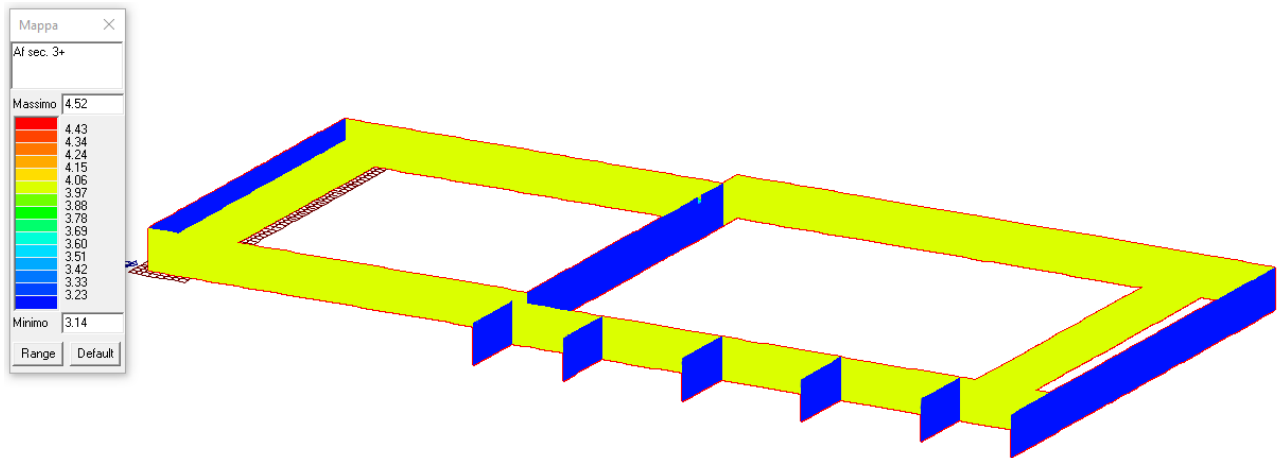


Fig 170. Mappa Armatura Orizzontale Faccia Positiva da Calcolo [cm^2/m]. .

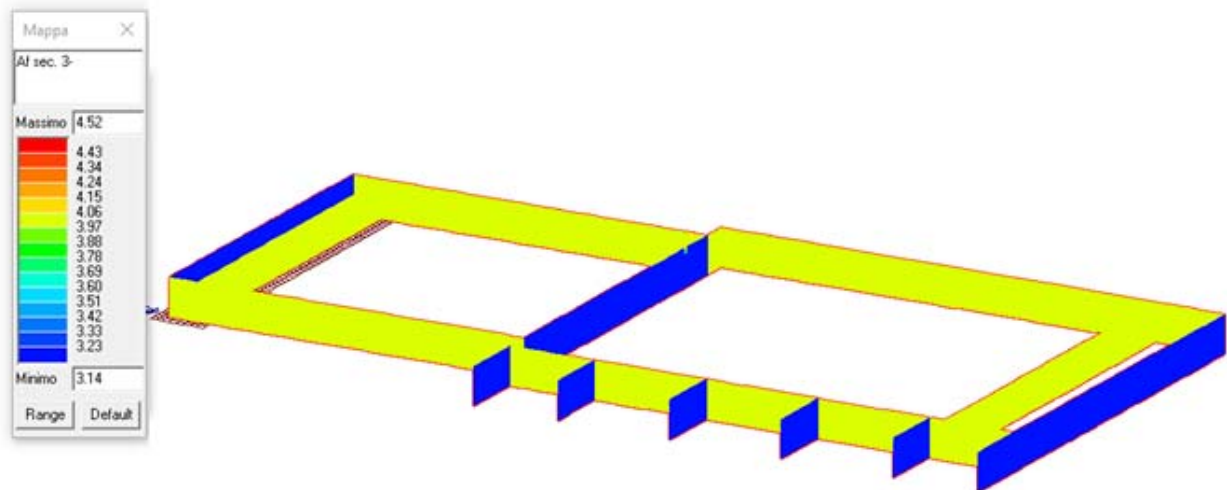


Fig 171. Mappa Armatura Orizzontale Faccia Negativa da Calcolo [cm^2/m]. .

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

2.2.3.3 Verifiche Analitiche da Modello di Calcolo

1.1.1.1.6 Verifica Macrosetti sp. 40 cm

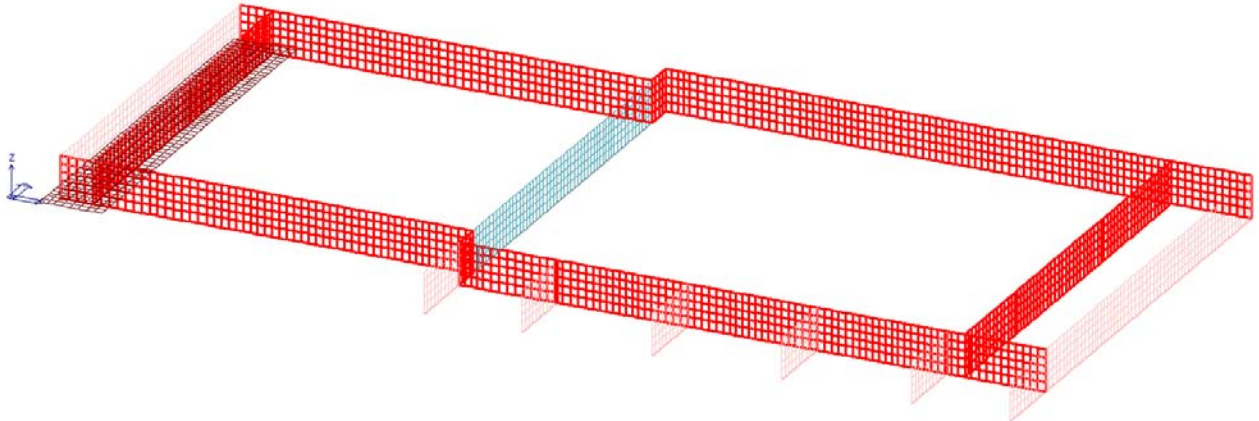


Fig 172. Individuazione del Macrosetto oggetto di Verifica (Selezione in rosso).

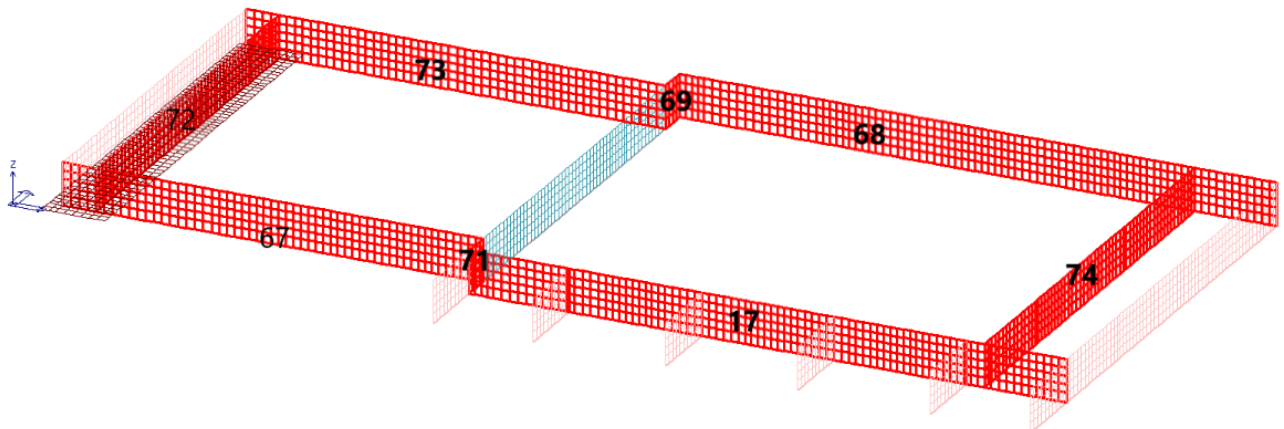


Fig 173. Numerazione Macrosetto oggetto di verifica.

Si riporta il tabulato di verifica completo.

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 17 | 40.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|-------|--------|-------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 31 | ok | 0.09 | 5.95e-02 | 2.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -123.2 | -24.2 | -11.8 | 162.8 | -172.9 | 37.7 |
| 32 | ok | 0.09 | 0.1 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.2 | -38.7 | 22.0 | 43.3 | -184.0 | -66.1 |
| 33 | ok | 0.09 | 0.2 | 1.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -1.1 | 53.4 | 1.4 | 58.9 | 8.0 | 51.1 |
| 34 | ok | 0.09 | 0.1 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.3 | -49.3 | 31.9 | -95.2 | 13.3 | 66.1 |
| 35 | ok | 0.09 | 0.1 | 2.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.0 | -65.6 | -38.0 | -90.4 | 2.2 | -67.2 |
| 36 | ok | 0.09 | 0.1 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -69.3 | -53.2 | 14.8 | -77.5 | 43.3 | 59.0 |
| 37 | ok | 0.09 | 9.79e-02 | 2.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.5 | -74.0 | -38.6 | -71.5 | 17.6 | -73.7 |
| 39 | ok | 0.09 | 0.1 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.2 | -95.1 | -41.4 | 53.4 | 11.1 | 23.3 |
| 40 | ok | 0.09 | 0.1 | 4.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -116.8 | -153.7 | 84.4 | 87.2 | 121.8 | -60.1 |
| 3720 | ok | 0.09 | 0.1 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.6 | -82.9 | -11.2 | 86.9 | -17.7 | 17.3 |
| 3899 | ok | 0.09 | 7.48e-02 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.9 | -67.3 | -7.8 | 79.6 | -3.3 | -15.5 |
| 3932 | ok | 0.09 | 4.57e-02 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -67.3 | -47.5 | -3.4 | 5.9 | 0.4 | -0.8 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|-------|-------|--------|--------|--------|
| 3960 | ok | 0.09 | 8.18e-02 | 2.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -101.3 | -39.1 | 5.8 | 171.5 | -470.5 | 49.8 |
| 3977 | ok | 0.09 | 7.70e-02 | 1.75e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -97.0 | -35.6 | 4.3 | 107.1 | -419.2 | -15.0 |
| 3994 | ok | 0.09 | 0.1 | 1.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -93.3 | -43.2 | 6.4 | 84.7 | -276.9 | -35.3 |
| 4036 | ok | 0.09 | 0.1 | 1.89e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -76.6 | -40.5 | -5.7 | -115.2 | -9.3 | -17.5 |
| 4053 | ok | 0.09 | 0.1 | 1.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.0 | -10.1 | -0.7 | -177.0 | -74.1 | -3.4 |
| 4070 | ok | 0.09 | 0.2 | 1.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -82.6 | 18.5 | 8.8 | 211.0 | 208.1 | -45.4 |
| 4087 | ok | 0.09 | 0.2 | 1.81e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.3 | 10.3 | -4.2 | 218.0 | 152.1 | 55.3 |
| 4104 | ok | 0.09 | 8.57e-02 | 1.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -74.1 | -2.4 | -3.4 | 208.5 | 27.2 | 38.3 |
| 4121 | ok | 0.09 | 9.06e-02 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.5 | -29.2 | 3.6 | -71.8 | 52.3 | -13.3 |
| 4138 | ok | 0.09 | 0.1 | 1.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -73.1 | -45.0 | 5.1 | -72.5 | 44.2 | 51.5 |
| 4195 | ok | 0.09 | 8.54e-02 | 1.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.0 | -57.9 | -8.1 | -103.1 | 19.9 | -66.0 |
| 4212 | ok | 0.09 | 7.73e-02 | 1.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.1 | -41.5 | -5.9 | -112.8 | 23.5 | -25.1 |
| 4229 | ok | 0.09 | 6.41e-02 | 1.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -70.3 | -21.9 | -0.4 | -216.8 | -77.6 | 17.6 |
| 4246 | ok | 0.09 | 0.1 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -69.3 | -16.0 | -1.5 | -225.2 | -213.6 | 14.7 |
| 4263 | ok | 0.09 | 0.2 | 1.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.5 | 29.1 | -20.4 | 415.2 | 660.0 | 57.0 |
| 4280 | ok | 0.09 | 0.1 | 1.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.9 | -0.7 | -2.3 | 373.8 | 131.0 | 69.8 |
| 4297 | ok | 0.09 | 6.42e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -67.4 | -19.5 | 2.2 | -219.7 | -79.7 | -13.4 |
| 4314 | ok | 0.09 | 8.85e-02 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.9 | -22.7 | 0.8 | -217.1 | 4.1 | -9.2 |
| 4331 | ok | 0.09 | 0.1 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -73.9 | -55.3 | 8.3 | -157.4 | 22.7 | 59.3 |
| 4391 | ok | 0.09 | 5.69e-02 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.2 | -46.9 | 2.0 | 13.8 | -20.3 | -5.0 |
| 4408 | ok | 0.09 | 0.1 | 1.74e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.9 | -33.8 | 9.5 | 113.2 | 240.9 | -66.4 |
| 4425 | ok | 0.09 | 8.48e-02 | 1.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -67.4 | -56.3 | -10.7 | 107.7 | 196.6 | 122.8 |
| 4442 | ok | 0.09 | 9.00e-02 | 1.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.2 | -86.3 | -7.2 | 124.4 | -80.1 | 99.9 |
| 4497 | ok | 0.09 | 7.16e-02 | 1.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -85.9 | -45.9 | -2.2 | 6.5 | 2.3 | -0.7 |
| 4514 | ok | 0.09 | 6.70e-02 | 1.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -74.2 | -31.4 | -6.6 | 5.2 | -8.4 | -2.4 |
| 4531 | ok | 0.09 | 6.34e-02 | 1.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -71.5 | -25.0 | -1.4 | 4.3 | -24.4 | -5.8 |
| 4548 | ok | 0.09 | 0.1 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.2 | -18.5 | -1.4 | 5.1 | -65.7 | -20.3 |
| 4565 | ok | 0.09 | 0.2 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.9 | 24.4 | 17.0 | 396.8 | 644.7 | -62.0 |
| 4582 | ok | 0.09 | 0.1 | 1.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.8 | -5.3 | -3.0 | 351.3 | 108.8 | 53.7 |
| 4599 | ok | 0.09 | 6.06e-02 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.1 | -23.8 | 2.5 | -204.7 | -69.5 | -12.0 |
| 4616 | ok | 0.09 | 7.54e-02 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.0 | -27.6 | 1.3 | -200.3 | 8.7 | -8.2 |
| 4633 | ok | 0.09 | 9.30e-02 | 1.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.1 | -54.4 | 9.1 | -118.2 | 14.5 | 28.3 |
| 4689 | ok | 0.09 | 0.1 | 1.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -70.4 | -52.7 | 15.4 | -55.5 | 29.9 | 27.9 |
| 6883 | ok | 0.09 | 0.3 | 3.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -136.8 | -44.6 | -26.4 | 761.3 | 354.6 | 241.0 |
| 6903 | ok | 0.09 | 0.1 | 3.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -133.5 | -30.5 | -2.0 | 676.3 | 45.6 | 306.5 |
| 6923 | ok | 0.09 | 0.1 | 3.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -144.0 | -37.1 | 3.4 | 961.7 | -225.3 | 281.0 |
| 6943 | ok | 0.09 | 0.1 | 7.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -331.0 | -10.6 | 48.7 | 1086.4 | -19.9 | 1.0 |
| 7333 | ok | 0.09 | 0.2 | 3.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -102.3 | -20.7 | -88.4 | 662.4 | 303.1 | 523.6 |
| 7334 | ok | 0.09 | 0.2 | 3.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.9 | 31.5 | -39.8 | 177.3 | 261.0 | 305.9 |
| 7335 | ok | 0.09 | 0.2 | 2.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.3 | -11.6 | 63.7 | 99.3 | -45.2 | -110.3 |
| 7336 | ok | 0.09 | 0.1 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.3 | 1.0 | -52.9 | -51.2 | -27.9 | -84.9 |
| 7337 | ok | 0.09 | 0.1 | 2.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.5 | 11.5 | 45.1 | -45.9 | -85.3 | 108.8 |
| 7338 | ok | 0.09 | 0.1 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.8 | 3.4 | -48.8 | -35.3 | -51.2 | -81.3 |
| 7339 | ok | 0.09 | 0.1 | 2.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.6 | 9.0 | 45.8 | 52.1 | 9.4 | -48.3 |
| 7340 | ok | 0.09 | 0.1 | 2.73e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.9 | 15.4 | 40.2 | 48.0 | 22.7 | -48.7 |
| 7341 | ok | 0.09 | 0.1 | 2.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -73.4 | -2.1 | -63.1 | 187.9 | 69.3 | 160.4 |
| 7494 | ok | 0.09 | 0.1 | 2.77e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.7 | 14.3 | 47.5 | 60.3 | 22.4 | -57.5 |
| 7495 | ok | 0.09 | 0.1 | 2.73e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.8 | 9.8 | 55.3 | 81.4 | 22.6 | -72.6 |
| 7496 | ok | 0.09 | 0.1 | 2.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.0 | 4.9 | 62.6 | 114.7 | 24.6 | -97.0 |
| 7497 | ok | 0.09 | 0.2 | 3.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -72.9 | -4.2 | -66.9 | 358.0 | 288.8 | 412.7 |
| 7498 | ok | 0.09 | 0.2 | 2.97e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.2 | 8.0 | -52.8 | 258.7 | 255.1 | 353.9 |
| 7499 | ok | 0.09 | 0.2 | 2.99e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.3 | 16.1 | -44.6 | 212.2 | 224.4 | 311.0 |
| 7500 | ok | 0.09 | 0.2 | 2.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.4 | -6.3 | 72.7 | 99.2 | -25.1 | -94.2 |
| 7501 | ok | 0.09 | 0.1 | 2.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.3 | -9.2 | 78.9 | 137.9 | -24.0 | -111.7 |
| 7502 | ok | 0.09 | 0.1 | 2.83e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.9 | -9.0 | 74.1 | 180.0 | -13.9 | -147.3 |
| 7503 | ok | 0.09 | 0.1 | 2.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.4 | -20.4 | -84.8 | 151.5 | 73.5 | 140.7 |
| 7504 | ok | 0.09 | 0.1 | 2.75e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.5 | -17.3 | -84.2 | 165.3 | 166.6 | 226.0 |
| 7505 | ok | 0.09 | 0.2 | 2.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.6 | -9.4 | -74.8 | 141.5 | 164.2 | 218.4 |
| 7506 | ok | 0.09 | 0.1 | 2.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.9 | 0.8 | -62.9 | -25.7 | -44.7 | -80.2 |
| 7507 | ok | 0.09 | 0.1 | 2.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.8 | 10.4 | 54.4 | -21.3 | -100.2 | 96.4 |
| 7508 | ok | 0.09 | 0.1 | 2.57e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.4 | 3.7 | 64.2 | 9.2 | -103.3 | 71.4 |
| 7509 | ok | 0.09 | 0.1 | 2.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.7 | -3.4 | -74.5 | 67.3 | 44.3 | 156.4 |
| 7510 | ok | 0.09 | 0.1 | 2.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.5 | -12.6 | 81.5 | 152.5 | -17.7 | -113.9 |
| 7512 | ok | 0.09 | 0.1 | 2.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.8 | -15.8 | -82.0 | 161.8 | 28.6 | 142.6 |
| 7513 | ok | 0.09 | 0.1 | 2.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.7 | -14.2 | -74.7 | 175.2 | 83.1 | 206.0 |
| 7514 | ok | 0.09 | 0.1 | 2.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.7 | -2.3 | -65.8 | 18.4 | -67.2 | -46.7 |
| 7515 | ok | 0.09 | 0.1 | 2.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.9 | 2.9 | -56.8 | -11.8 | -64.2 | -70.9 |
| 7516 | ok | 0.09 | 0.1 | 2.58e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.6 | -10.3 | -75.3 | 80.5 | -84.2 | 116.0 |
| 7517 | ok | 0.09 | 0.1 | 2.68e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.5 | 1.6 | 63.7 | 219.6 | 151.8 | -238.9 |
| 7518 | ok | 0.09 | 0.1 | 2.81e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -69.4 | 14.3 | 42.2 | 199.8 | 41.0 | -226.0 |
| 7519 | ok | 0.09 | 0.2 | 2.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.1 | -33.0 | -86.8 | 149.6 | 28.9 | 170.3 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|-----------|-----------|--------|--------|--------|
| 7520 | ok | 0.09 | 0.1 | 2.57e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.2 | 7.0 | 55.8 | -14.5 | -70.2 | 76.0 |
| 7521 | ok | 0.09 | 0.1 | 2.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.8 | -3.4 | 65.7 | 152.7 | 97.7 | -203.2 |
| 7522 | ok | 0.09 | 0.1 | 2.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.6 | -11.6 | 75.5 | 176.3 | 100.6 | -214.4 |
| 7523 | ok | 0.09 | 0.1 | 2.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.3 | -14.5 | 82.5 | 162.3 | 25.0 | -138.1 |
| 7525 | ok | 0.09 | 0.1 | 2.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.1 | -20.7 | -83.5 | 203.7 | 19.6 | 183.7 |
| 7526 | ok | 0.09 | 0.1 | 2.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.4 | -17.9 | -77.5 | 157.6 | 16.4 | 156.4 |
| 7527 | ok | 0.09 | 0.1 | 2.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.1 | -3.1 | -66.4 | 18.3 | -66.2 | -46.2 |
| 7528 | ok | 0.09 | 0.1 | 2.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.2 | 2.5 | -57.1 | -11.3 | -62.0 | -69.0 |
| 7529 | ok | 0.09 | 0.1 | 2.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.1 | 3.2 | -48.8 | -34.1 | -48.2 | -78.6 |
| 7640 | ok | 0.09 | 0.2 | 3.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.3 | 9.0 | -67.3 | 67.7 | 135.6 | 113.4 |
| 7641 | ok | 0.09 | 0.2 | 3.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.1 | 26.2 | -73.1 | 69.0 | 147.2 | 112.9 |
| 7642 | ok | 0.09 | 0.2 | 4.85e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.7 | 45.5 | -76.4 | 94.8 | 129.9 | 81.9 |
| 7643 | ok | 0.09 | 0.2 | 4.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -82.9 | -65.2 | 129.9 | -125.9 | -140.9 | 62.7 |
| 7650 | ok | 0.09 | 0.1 | 2.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -87.9 | -4.2 | 48.3 | 219.4 | 39.0 | -145.8 |
| 7651 | ok | 0.09 | 0.1 | 2.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.3 | -10.9 | -79.4 | 151.6 | 24.2 | 136.6 |
| 7652 | ok | 0.09 | 0.1 | 2.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.3 | -11.7 | -79.7 | 154.3 | 16.7 | 132.1 |
| 7653 | ok | 0.09 | 0.1 | 2.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.1 | -22.2 | -75.7 | 298.0 | 55.2 | 221.9 |
| 7907 | ok | 0.09 | 6.58e-02 | 2.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -96.1 | -18.9 | -6.2 | 17.9 | -442.6 | 58.1 |
| 7908 | ok | 0.09 | 5.73e-02 | 1.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -89.5 | -11.6 | -1.6 | -23.0 | -382.4 | 40.7 |
| 7909 | ok | 0.09 | 4.76e-02 | 1.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -85.4 | -8.0 | -7.35e-02 | -3.0 | -288.1 | 39.9 |
| 7910 | ok | 0.09 | 0.2 | 2.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -76.7 | -6.3 | 58.6 | -81.9 | -329.7 | -204.4 |
| 7911 | ok | 0.09 | 6.56e-02 | 1.97e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -100.0 | -19.8 | 8.2 | 142.5 | -364.2 | 130.6 |
| 7912 | ok | 0.09 | 5.40e-02 | 1.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -89.9 | -9.6 | -0.8 | 34.9 | -313.7 | 107.6 |
| 7913 | ok | 0.09 | 4.59e-02 | 1.81e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -85.1 | -7.9 | 2.0 | 8.7 | -236.4 | 91.6 |
| 7914 | ok | 0.09 | 9.07e-02 | 2.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -84.7 | -5.2 | -44.9 | 170.7 | 112.4 | 307.1 |
| 7915 | ok | 0.09 | 0.2 | 4.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -134.9 | 11.0 | 83.5 | 691.1 | 86.7 | -59.7 |
| 7916 | ok | 0.09 | 0.1 | 3.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -118.8 | -0.5 | 54.8 | 326.3 | -59.5 | -1.0 |
| 7917 | ok | 0.09 | 7.01e-02 | 2.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -93.6 | -0.3 | 45.7 | 150.9 | -64.0 | 7.5 |
| 7918 | ok | 0.09 | 6.94e-02 | 2.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -82.7 | 18.7 | 3.7 | 95.7 | 25.8 | -0.8 |
| 7919 | ok | 0.09 | 7.22e-02 | 2.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -70.6 | -4.71e-02 | -30.8 | 138.4 | 117.1 | 226.9 |
| 7920 | ok | 0.09 | 5.88e-02 | 1.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -95.0 | -16.0 | 8.3 | 104.6 | -338.4 | 101.9 |
| 7921 | ok | 0.09 | 4.92e-02 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -87.9 | -7.5 | 8.3 | 56.7 | -231.4 | 117.0 |
| 7922 | ok | 0.09 | 4.17e-02 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.0 | -6.9 | 10.1 | 40.9 | -157.7 | 104.7 |
| 7923 | ok | 0.09 | 7.94e-02 | 2.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.6 | 5.4 | -22.8 | 129.6 | 105.6 | 189.1 |
| 7924 | ok | 0.09 | 6.91e-02 | 1.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -90.0 | -11.8 | 12.4 | 75.6 | -256.4 | 17.2 |
| 7925 | ok | 0.09 | 5.38e-02 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.7 | -6.7 | 16.8 | 54.2 | -173.2 | 11.2 |
| 7926 | ok | 0.09 | 3.68e-02 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.5 | -10.8 | 26.8 | 60.8 | -88.3 | 125.2 |
| 7927 | ok | 0.09 | 0.1 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.4 | 10.0 | -23.2 | 127.2 | 93.3 | 163.3 |
| 7928 | ok | 0.09 | 8.39e-02 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.4 | -8.7 | 25.4 | 43.0 | -174.1 | -39.9 |
| 7929 | ok | 0.09 | 5.02e-02 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.0 | -6.9 | 23.2 | 49.0 | -121.4 | -19.0 |
| 7930 | ok | 0.09 | 3.86e-02 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.9 | -4.5 | 14.5 | 85.9 | -29.4 | 118.1 |
| 7931 | ok | 0.09 | 9.69e-02 | 1.93e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.5 | 12.6 | -9.5 | 129.2 | 114.6 | 161.8 |
| 7932 | ok | 0.09 | 0.2 | 2.85e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.9 | 27.5 | -38.9 | 171.5 | 215.1 | 277.1 |
| 7933 | ok | 0.09 | 0.2 | 2.95e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 30.5 | 53.0 | -24.1 | -7.5 | 26.5 | 64.5 |
| 7934 | ok | 0.09 | 9.14e-02 | 7.81e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -30.4 | -7.9 | 24.8 | 24.8 | -96.4 | -58.6 |
| 7935 | ok | 0.09 | 6.03e-02 | 8.97e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -37.6 | -8.5 | 25.2 | 49.4 | -72.1 | -43.7 |
| 7936 | ok | 0.09 | 4.43e-02 | 1.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.1 | -11.5 | 31.0 | 76.2 | -35.4 | -40.7 |
| 7937 | ok | 0.09 | 0.1 | 1.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.2 | 9.2 | -12.6 | 127.1 | 98.2 | 144.1 |
| 7938 | ok | 0.09 | 0.2 | 2.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.6 | 18.5 | -40.6 | 157.4 | 179.5 | 248.6 |
| 7939 | ok | 0.09 | 0.1 | 3.74e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -0.3 | 40.7 | -2.3 | -0.9 | -30.9 | 1.9 |
| 7940 | ok | 0.09 | 0.1 | 3.95e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -12.2 | -2.4 | 15.4 | 23.6 | -46.8 | -61.5 |
| 7941 | ok | 0.09 | 6.70e-02 | 6.18e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.5 | -7.2 | 21.2 | 48.8 | -35.6 | -54.3 |
| 7942 | ok | 0.09 | 5.05e-02 | 8.64e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.1 | -6.5 | 21.6 | 73.4 | -14.9 | -44.4 |
| 7943 | ok | 0.09 | 0.1 | 1.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.5 | 4.7 | -17.5 | 123.3 | 85.0 | 128.9 |
| 7944 | ok | 0.09 | 0.2 | 2.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.5 | 8.3 | -45.2 | 144.9 | 149.3 | 224.9 |
| 7945 | ok | 0.09 | 0.1 | 3.21e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.2 | 41.2 | 1.7 | -2.0 | -19.2 | 7.0 |
| 7946 | ok | 0.09 | 7.70e-02 | 1.76e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.4 | 17.2 | 3.8 | 12.7 | -15.6 | 42.6 |
| 7947 | ok | 0.09 | 6.41e-02 | 4.10e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -13.5 | -2.1 | 15.6 | 53.5 | -20.9 | -57.9 |
| 7948 | ok | 0.09 | 5.98e-02 | 6.75e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.3 | -5.5 | 17.4 | 73.2 | 12.6 | -49.4 |
| 7949 | ok | 0.09 | 0.1 | 1.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.0 | 0.7 | -23.4 | 123.4 | 73.9 | 116.9 |
| 7950 | ok | 0.09 | 0.1 | 2.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.4 | -22.1 | 62.5 | 88.3 | -84.4 | -94.5 |
| 7951 | ok | 0.09 | 0.1 | 4.04e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.6 | 42.9 | -1.2 | -2.0 | -8.8 | 9.1 |
| 7952 | ok | 0.09 | 0.1 | 3.21e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.8 | 16.5 | -2.5 | 17.4 | -3.2 | 50.8 |
| 7953 | ok | 0.09 | 6.67e-02 | 4.63e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.4 | -3.7 | -13.6 | -20.7 | -1.6 | 24.1 |
| 7954 | ok | 0.09 | 6.20e-02 | 7.10e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -19.0 | -3.5 | 12.0 | 77.7 | 21.5 | -50.6 |
| 7955 | ok | 0.09 | 0.1 | 1.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.0 | -7.6 | 31.6 | 107.0 | -28.7 | -25.8 |
| 7956 | ok | 0.09 | 0.2 | 2.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.7 | -15.0 | 60.9 | 92.6 | -61.5 | -103.5 |
| 7957 | ok | 0.09 | 0.3 | 2.75e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 27.3 | 71.2 | 22.3 | 2.2 | 3.1 | 48.5 |
| 7958 | ok | 0.09 | 8.65e-02 | 6.42e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.1 | -4.2 | -18.3 | -29.3 | -2.6 | 22.2 |
| 7959 | ok | 0.09 | 5.79e-02 | 7.89e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -29.8 | -2.4 | -16.1 | -32.8 | 0.5 | 23.1 |
| 7960 | ok | 0.09 | 6.50e-02 | 9.62e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.1 | -2.9 | -14.1 | -49.0 | 8.3 | -2.8 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-------|-------|-------|--------|-----------|-------|
| 7961 | ok | 0.09 | 9.82e-02 | 1.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.1 | -1.8 | 31.3 | 82.8 | -6.2 | -25.6 |
| 7962 | ok | 0.09 | 0.1 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.8 | 0.6 | -18.1 | -54.8 | 2.0 | 42.7 |
| 7963 | ok | 0.09 | 6.55e-02 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.8 | 5.1 | -19.3 | -4.9 | 6.7 | 9.6 |
| 7964 | ok | 0.09 | 5.28e-02 | 1.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.8 | -1.6 | -19.3 | -68.3 | 0.8 | 5.5 |
| 7965 | ok | 0.09 | 9.39e-02 | 1.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.7 | -0.9 | 36.6 | 90.4 | 5.3 | -32.4 |
| 7966 | ok | 0.09 | 0.1 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -70.8 | -0.8 | -10.4 | -124.5 | -11.2 | 36.1 |
| 7967 | ok | 0.09 | 8.03e-02 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.1 | 8.6 | -10.9 | -18.7 | 2.8 | 6.8 |
| 7968 | ok | 0.09 | 5.04e-02 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.2 | 3.0 | -3.9 | -88.0 | -18.8 | 11.2 |
| 7969 | ok | 0.09 | 9.08e-02 | 1.89e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.7 | -2.2 | 37.1 | 89.5 | 16.7 | -36.5 |
| 7970 | ok | 0.09 | 0.1 | 1.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -69.9 | 13.0 | 7.0 | 162.5 | 51.7 | -32.9 |
| 7971 | ok | 0.09 | 8.66e-02 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.9 | 11.1 | 4.5 | 85.5 | 64.6 | 5.9 |
| 7972 | ok | 0.09 | 5.48e-02 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.1 | 1.5 | -8.8 | -108.1 | -60.1 | 14.9 |
| 7973 | ok | 0.09 | 0.1 | 1.93e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.9 | -1.5 | -18.7 | 89.4 | 20.8 | 87.0 |
| 7974 | ok | 0.09 | 0.1 | 1.58e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.0 | 14.9 | 17.8 | 254.0 | 333.4 | 19.1 |
| 7975 | ok | 0.09 | 8.38e-02 | 1.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.8 | 7.8 | 8.4 | 59.1 | 64.0 | 35.5 |
| 7976 | ok | 0.09 | 6.03e-02 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.2 | 3.9 | 1.4 | 48.4 | 27.8 | 50.3 |
| 7977 | ok | 0.09 | 7.77e-02 | 2.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.9 | 1.8 | 25.6 | -53.6 | -25.6 | -68.7 |
| 7978 | ok | 0.09 | 0.1 | 1.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.2 | 11.5 | -19.2 | 150.5 | 185.0 | 164.4 |
| 7979 | ok | 0.09 | 8.79e-02 | 1.57e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.6 | 6.6 | -12.4 | 83.8 | 94.2 | 97.4 |
| 7980 | ok | 0.09 | 5.53e-02 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.6 | 3.8 | -20.9 | 75.1 | 69.9 | 73.5 |
| 7981 | ok | 0.09 | 6.91e-02 | 1.93e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.1 | 2.2 | 1.4 | 94.2 | 21.6 | 50.7 |
| 7982 | ok | 0.09 | 9.37e-02 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -69.2 | 7.5 | -8.7 | 191.5 | 33.7 | 146.3 |
| 7983 | ok | 0.09 | 7.87e-02 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.2 | 8.0 | -9.7 | 123.5 | 58.1 | 111.6 |
| 7984 | ok | 0.09 | 5.56e-02 | 1.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.4 | 3.5 | -13.2 | 101.7 | 64.3 | 82.6 |
| 7985 | ok | 0.09 | 6.72e-02 | 1.83e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.1 | 2.0 | 7.5 | 102.4 | 4.5 | 56.9 |
| 7986 | ok | 0.09 | 8.38e-02 | 1.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -72.5 | 4.5 | -0.6 | 193.1 | -15.4 | 93.0 |
| 7987 | ok | 0.09 | 6.83e-02 | 1.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.9 | 8.8 | -2.3 | 145.8 | 11.5 | 91.8 |
| 7988 | ok | 0.09 | 5.06e-02 | 1.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.6 | 3.8 | -6.3 | 119.3 | 39.4 | 80.6 |
| 7989 | ok | 0.09 | 6.38e-02 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.4 | -1.5 | -31.1 | -66.6 | -18.5 | -50.9 |
| 7990 | ok | 0.09 | 9.11e-02 | 1.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -71.4 | 9.2 | 9.0 | 189.4 | -51.7 | 45.5 |
| 7991 | ok | 0.09 | 6.57e-02 | 1.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.3 | 9.3 | 6.8 | 143.4 | -15.0 | 62.5 |
| 7992 | ok | 0.09 | 4.61e-02 | 1.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.7 | 4.7 | 5.8 | 119.6 | 3.8 | 65.3 |
| 7993 | ok | 0.09 | 7.12e-02 | 1.73e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.5 | -1.7 | -22.9 | -70.5 | -6.9 | -45.2 |
| 7994 | ok | 0.09 | 0.1 | 1.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.9 | 7.8 | 18.5 | 132.5 | -51.9 | -4.2 |
| 7995 | ok | 0.09 | 5.67e-02 | 1.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.6 | 6.8 | 13.8 | 121.4 | -23.6 | 36.1 |
| 7996 | ok | 0.09 | 4.30e-02 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.3 | -3.4 | 18.6 | -95.1 | 31.3 | -12.0 |
| 7997 | ok | 0.09 | 7.15e-02 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.3 | -1.5 | -24.5 | -71.5 | 4.0 | -42.0 |
| 7998 | ok | 0.09 | 0.1 | 2.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.5 | 0.6 | -46.7 | -57.2 | -14.4 | -80.5 |
| 7999 | ok | 0.09 | 0.2 | 3.66e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -7.2 | -17.4 | 7.9 | -6.4 | 38.2 | 64.4 |
| 8000 | ok | 0.09 | 7.80e-02 | 8.02e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -26.0 | -7.7 | 18.1 | -21.6 | 35.6 | 50.4 |
| 8001 | ok | 0.09 | 5.63e-02 | 8.45e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.6 | -4.5 | 17.9 | -18.1 | 30.3 | 36.7 |
| 8002 | ok | 0.09 | 4.81e-02 | 9.94e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -36.6 | -4.4 | 5.9 | -81.3 | 28.2 | -4.3 |
| 8003 | ok | 0.09 | 7.42e-02 | 1.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.4 | -13.1 | 35.9 | -68.4 | 12.6 | 35.2 |
| 8004 | ok | 0.09 | 0.1 | 1.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.6 | -0.2 | -42.7 | 33.7 | 55.4 | 58.1 |
| 8005 | ok | 0.09 | 0.1 | 6.96e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.0 | 39.1 | -1.1 | 26.9 | -0.6 | -23.8 |
| 8006 | ok | 0.09 | 9.30e-02 | 3.98e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -7.0 | 14.5 | 7.8 | 82.9 | 30.0 | 48.1 |
| 8007 | ok | 0.09 | 5.48e-02 | 5.56e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -9.3 | 11.9 | 1.0 | 79.6 | -0.5 | 41.9 |
| 8008 | ok | 0.09 | 4.54e-02 | 7.88e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.6 | -7.5 | 13.9 | -69.2 | 26.2 | 11.1 |
| 8009 | ok | 0.09 | 7.49e-02 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.6 | -7.0 | -25.8 | -63.1 | 18.1 | -27.3 |
| 8010 | ok | 0.09 | 9.73e-02 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.3 | -8.8 | -46.0 | 32.1 | 55.6 | 57.9 |
| 8011 | ok | 0.09 | 0.1 | 3.58e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -0.9 | 39.0 | -2.9 | 16.6 | -7.03e-04 | -23.8 |
| 8012 | ok | 0.09 | 8.17e-02 | 2.30e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.6 | 22.1 | -2.3 | 64.2 | 31.3 | 42.3 |
| 8013 | ok | 0.09 | 5.41e-02 | 3.82e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -6.1 | 11.6 | -1.3 | 63.9 | 4.0 | 43.6 |
| 8014 | ok | 0.09 | 4.46e-02 | 6.14e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -23.8 | -7.4 | -1.7 | -60.3 | 23.8 | 10.4 |
| 8015 | ok | 0.09 | 7.76e-02 | 1.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.8 | -8.2 | -27.1 | 23.6 | 39.0 | 39.1 |
| 8016 | ok | 0.09 | 9.96e-02 | 1.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.5 | -14.8 | -49.7 | 32.1 | 57.1 | 60.1 |
| 8017 | ok | 0.09 | 0.1 | 3.42e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.0 | 36.3 | -2.4 | 15.3 | 25.7 | 20.0 |
| 8018 | ok | 0.09 | 8.07e-02 | 1.45e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.6 | 20.2 | 3.8 | 61.7 | 36.0 | 67.0 |
| 8019 | ok | 0.09 | 5.47e-02 | 2.88e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -5.5 | 10.3 | -3.4 | 57.1 | 5.6 | 50.1 |
| 8020 | ok | 0.09 | 4.78e-02 | 5.33e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.4 | -7.6 | 4.0 | -56.5 | 17.6 | 20.2 |
| 8021 | ok | 0.09 | 7.59e-02 | 1.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.1 | -14.8 | -33.9 | -57.9 | 31.6 | -13.8 |
| 8022 | ok | 0.09 | 0.1 | 1.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.7 | -21.0 | -54.9 | 33.1 | 58.7 | 63.2 |
| 8023 | ok | 0.09 | 0.1 | 3.42e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.0 | 34.8 | 1.2 | 15.8 | 27.3 | 38.3 |
| 8024 | ok | 0.09 | 8.40e-02 | 1.94e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.7 | 19.4 | -6.1 | 57.9 | 33.0 | 54.3 |
| 8025 | ok | 0.09 | 5.41e-02 | 3.68e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -5.6 | 9.9 | -7.4 | 57.7 | 4.7 | 55.8 |
| 8026 | ok | 0.09 | 4.47e-02 | 6.29e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.4 | -8.5 | -5.8 | -56.0 | 20.6 | 19.1 |
| 8027 | ok | 0.09 | 7.23e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.4 | -18.5 | -39.0 | -57.8 | 38.9 | -6.4 |
| 8028 | ok | 0.09 | 0.1 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.3 | 4.6 | 37.9 | -64.7 | -49.7 | 102.3 |
| 8029 | ok | 0.09 | 0.1 | 4.15e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -0.9 | 33.7 | -0.6 | 20.2 | 27.1 | 39.4 |
| 8030 | ok | 0.09 | 8.52e-02 | 3.10e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.1 | 16.5 | 4.3 | 27.0 | 15.4 | 47.4 |
| 8031 | ok | 0.09 | 5.53e-02 | 4.91e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.2 | -8.8 | -16.6 | -33.1 | 13.7 | -4.3 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-------|-------|-----------|--------|--------|--------|
| 8032 | ok | 0.09 | 3.93e-02 | 7.76e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.6 | -10.4 | -16.3 | -59.5 | 24.4 | 19.6 |
| 8033 | ok | 0.09 | 6.66e-02 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.4 | 2.0 | 16.3 | -70.2 | -26.9 | 63.6 |
| 8034 | ok | 0.09 | 0.1 | 2.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.6 | 9.3 | 37.1 | -62.0 | -62.2 | 107.5 |
| 8035 | ok | 0.09 | 0.1 | 1.12e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -0.6 | 32.9 | 1.0 | 29.3 | -4.3 | 52.8 |
| 8036 | ok | 0.09 | 9.73e-02 | 5.36e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.2 | 17.6 | -3.9 | 31.0 | -3.5 | 66.2 |
| 8037 | ok | 0.09 | 4.48e-02 | 7.14e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.5 | -10.9 | -22.2 | -41.6 | 14.4 | -3.7 |
| 8038 | ok | 0.09 | 3.33e-02 | 9.60e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -30.2 | -10.8 | -21.1 | -68.2 | 26.8 | 24.5 |
| 8039 | ok | 0.09 | 6.22e-02 | 1.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.0 | -11.4 | -25.3 | -66.0 | 22.5 | 39.4 |
| 8040 | ok | 0.09 | 0.1 | 2.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.3 | 11.7 | 39.4 | -55.8 | -74.5 | 110.3 |
| 8041 | ok | 0.09 | 0.2 | 5.19e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 32.1 | 61.5 | 24.1 | 8.4 | -11.5 | 73.9 |
| 8042 | ok | 0.09 | 7.15e-02 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.1 | -14.2 | -23.3 | -26.9 | 21.6 | -26.7 |
| 8043 | ok | 0.09 | 4.83e-02 | 1.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.6 | -9.0 | -23.9 | -23.2 | 21.0 | -9.1 |
| 8044 | ok | 0.09 | 3.56e-02 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.1 | -7.6 | -18.5 | -82.7 | 23.6 | 35.0 |
| 8045 | ok | 0.09 | 5.94e-02 | 1.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.3 | -19.6 | -51.0 | -62.1 | 54.5 | 27.2 |
| 8046 | ok | 0.09 | 0.1 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.4 | -13.4 | -32.2 | -89.2 | 13.6 | -14.2 |
| 8047 | ok | 0.09 | 5.29e-02 | 1.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.9 | -4.1 | -19.4 | -119.5 | 32.6 | 23.4 |
| 8048 | ok | 0.09 | 3.88e-02 | 1.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.7 | -7.7 | -24.5 | -96.0 | 24.6 | 43.7 |
| 8049 | ok | 0.09 | 5.46e-02 | 1.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.2 | -17.9 | -48.1 | -64.5 | 50.5 | 48.4 |
| 8050 | ok | 0.09 | 6.97e-02 | 1.74e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.0 | -17.0 | -5.5 | -103.8 | 30.7 | -3.9 |
| 8051 | ok | 0.09 | 4.90e-02 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.1 | -3.1 | -16.2 | -154.3 | 18.5 | 42.9 |
| 8052 | ok | 0.09 | 4.25e-02 | 1.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.2 | -5.6 | -19.9 | -112.7 | 10.6 | 59.0 |
| 8053 | ok | 0.09 | 5.72e-02 | 1.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.0 | -3.1 | 1.7 | -65.5 | -31.8 | 70.8 |
| 8054 | ok | 0.09 | 6.54e-02 | 1.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -71.7 | -11.9 | -1.4 | -181.0 | -5.0 | 46.0 |
| 8055 | ok | 0.09 | 5.67e-02 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.4 | -4.0 | -4.3 | -181.9 | -18.8 | 62.0 |
| 8056 | ok | 0.09 | 4.78e-02 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.3 | -3.5 | -0.9 | -126.6 | -29.6 | 70.5 |
| 8057 | ok | 0.09 | 6.18e-02 | 1.89e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.4 | -4.4 | 7.5 | -57.6 | -52.4 | 64.7 |
| 8058 | ok | 0.09 | 7.14e-02 | 1.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.7 | -11.9 | 2.4 | -240.0 | -83.9 | 65.1 |
| 8059 | ok | 0.09 | 6.31e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.4 | -6.2 | -1.0 | -206.0 | -83.2 | 70.4 |
| 8060 | ok | 0.09 | 5.13e-02 | 1.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.6 | -4.3 | -1.3 | -138.1 | -67.0 | 75.4 |
| 8061 | ok | 0.09 | 7.04e-02 | 1.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.9 | -4.8 | -7.2 | -52.3 | -72.7 | 61.2 |
| 8062 | ok | 0.09 | 0.1 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.3 | 8.4 | 15.3 | 334.6 | 215.5 | -154.8 |
| 8063 | ok | 0.09 | 6.88e-02 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.5 | -7.6 | 6.2 | -230.1 | -182.3 | 63.6 |
| 8064 | ok | 0.09 | 5.18e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.8 | -5.6 | 3.8 | -146.2 | -131.1 | 60.5 |
| 8065 | ok | 0.09 | 4.85e-02 | 1.65e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.6 | -5.1 | 30.9 | -65.4 | -116.5 | -50.8 |
| 8066 | ok | 0.09 | 0.1 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.5 | -4.5 | -16.4 | 290.4 | 458.1 | 40.4 |
| 8067 | ok | 0.09 | 7.49e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.2 | -8.6 | 7.5 | -256.6 | -320.1 | 13.5 |
| 8068 | ok | 0.09 | 4.75e-02 | 1.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.5 | -7.2 | 2.2 | -158.6 | -203.3 | 17.0 |
| 8069 | ok | 0.09 | 6.87e-02 | 1.89e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.3 | -1.8 | 38.1 | -63.1 | -55.5 | -69.5 |
| 8070 | ok | 0.09 | 0.1 | 1.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.6 | 9.1 | -16.8 | 335.3 | 226.7 | 183.9 |
| 8071 | ok | 0.09 | 6.71e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.2 | -7.5 | -6.9 | -230.7 | -183.1 | -45.5 |
| 8072 | ok | 0.09 | 4.99e-02 | 1.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.9 | -5.9 | 2.1 | -146.2 | -128.2 | -44.8 |
| 8073 | ok | 0.09 | 6.43e-02 | 1.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.4 | -4.5 | 10.4 | -60.4 | -37.8 | -58.8 |
| 8074 | ok | 0.09 | 7.06e-02 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.1 | -10.9 | -0.7 | -243.1 | -85.2 | -48.2 |
| 8075 | ok | 0.09 | 6.19e-02 | 1.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.4 | -6.3 | -2.5 | -206.7 | -81.6 | -54.0 |
| 8076 | ok | 0.09 | 4.96e-02 | 1.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.3 | -4.9 | -8.10e-02 | -137.9 | -66.4 | -57.9 |
| 8077 | ok | 0.09 | 5.87e-02 | 1.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.8 | -5.3 | -34.6 | -56.4 | -48.0 | -41.8 |
| 8078 | ok | 0.09 | 6.58e-02 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.8 | -10.6 | 0.3 | -225.3 | 0.4 | -34.2 |
| 8079 | ok | 0.09 | 5.57e-02 | 1.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.1 | -4.7 | 2.9 | -182.9 | -17.3 | -44.6 |
| 8080 | ok | 0.09 | 4.64e-02 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.8 | -4.4 | 5.7 | -126.9 | -23.0 | -53.8 |
| 8081 | ok | 0.09 | 5.71e-02 | 1.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.2 | -2.5 | -28.1 | -63.9 | -36.0 | -50.4 |
| 8082 | ok | 0.09 | 7.37e-02 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.1 | -7.0 | 7.1 | -194.2 | 46.3 | -1.8 |
| 8083 | ok | 0.09 | 4.83e-02 | 1.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.6 | -4.5 | 13.5 | -155.2 | 20.3 | -25.3 |
| 8084 | ok | 0.09 | 4.26e-02 | 1.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.2 | -6.7 | 16.4 | -112.5 | 9.5 | -41.6 |
| 8085 | ok | 0.09 | 6.32e-02 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.3 | -2.3 | -21.7 | -66.1 | -24.3 | -50.2 |
| 8086 | ok | 0.09 | 9.11e-02 | 1.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.5 | -11.2 | 18.8 | -78.5 | 39.4 | 21.1 |
| 8087 | ok | 0.09 | 4.22e-02 | 1.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.0 | -6.1 | 15.0 | -119.8 | 35.4 | -5.1 |
| 8088 | ok | 0.09 | 3.77e-02 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.7 | -7.2 | 13.3 | -96.6 | 20.4 | -28.1 |
| 8089 | ok | 0.09 | 6.16e-02 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.8 | -2.7 | -21.9 | -66.4 | -13.5 | -47.7 |
| 8090 | ok | 0.09 | 0.1 | 2.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.7 | 2.6 | -44.0 | -44.9 | -39.8 | -81.7 |
| 8091 | ok | 0.09 | 0.2 | 6.15e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.9 | -30.6 | 12.0 | -8.4 | 26.2 | 61.1 |
| 8092 | ok | 0.09 | 7.37e-02 | 8.93e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.8 | -15.1 | 21.0 | -26.5 | 24.5 | 38.4 |
| 8093 | ok | 0.09 | 4.55e-02 | 8.65e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.3 | -10.9 | 22.6 | -43.8 | 16.3 | 22.9 |
| 8094 | ok | 0.09 | 3.31e-02 | 1.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.2 | -11.1 | 19.0 | -79.8 | 26.7 | -14.2 |
| 8095 | ok | 0.09 | 6.50e-02 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.0 | -5.0 | -21.8 | -62.8 | -5.7 | -42.5 |
| 8096 | ok | 0.09 | 0.1 | 2.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.5 | -0.5 | -42.7 | -50.2 | -27.0 | -77.6 |
| 8097 | ok | 0.09 | 0.1 | 1.61e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -0.5 | 26.8 | -1.7 | 29.1 | -4.5 | -44.8 |
| 8098 | ok | 0.09 | 9.61e-02 | 5.35e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.8 | 14.5 | 1.0 | 31.2 | -3.6 | -44.2 |
| 8099 | ok | 0.09 | 4.88e-02 | 6.00e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -17.4 | -11.7 | 20.1 | -40.0 | 10.8 | 16.3 |
| 8100 | ok | 0.09 | 3.65e-02 | 8.26e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.7 | -10.5 | 4.2 | -67.4 | 20.7 | -10.9 |
| 8101 | ok | 0.09 | 7.51e-02 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.9 | -15.1 | 32.6 | -56.8 | 21.0 | 20.5 |
| 8102 | ok | 0.09 | 0.1 | 1.83e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.6 | -5.6 | -44.2 | -52.0 | -14.1 | -70.8 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|----------|-------|-----------|--------|--------|--------|
| 8103 | ok | 0.09 | 9.05e-02 | 5.27e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -0.4 | 27.1 | -3.5 | 17.6 | -1.1 | -44.5 |
| 8104 | ok | 0.09 | 7.64e-02 | 3.19e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.5 | 13.6 | -0.2 | 21.9 | 28.9 | -33.2 |
| 8105 | ok | 0.09 | 5.46e-02 | 4.64e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.7 | -8.0 | 16.6 | -31.3 | 10.1 | 15.6 |
| 8106 | ok | 0.09 | 4.49e-02 | 6.57e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -23.8 | -11.5 | -0.1 | -58.0 | 20.1 | -6.1 |
| 8107 | ok | 0.09 | 7.61e-02 | 1.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.0 | -11.7 | 27.6 | -56.1 | 13.5 | 27.3 |
| 8108 | ok | 0.09 | 0.1 | 1.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.0 | -11.7 | 48.2 | -50.8 | 7.5 | 55.8 |
| 8109 | ok | 0.09 | 8.63e-02 | 3.49e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -0.9 | 23.8 | -2.8 | 15.8 | 32.1 | -30.2 |
| 8110 | ok | 0.09 | 6.56e-02 | 2.01e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.3 | 14.3 | -3.1 | 17.7 | 28.9 | -30.9 |
| 8111 | ok | 0.09 | 5.09e-02 | 3.54e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -9.3 | -8.4 | 8.4 | -87.9 | 0.5 | 30.5 |
| 8112 | ok | 0.09 | 4.75e-02 | 5.40e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.6 | -12.1 | 5.6 | -53.1 | 20.7 | 2.3 |
| 8113 | ok | 0.09 | 7.73e-02 | 1.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.1 | -8.0 | 23.2 | -57.2 | 6.5 | 33.2 |
| 8114 | ok | 0.09 | 0.1 | 1.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.9 | -5.1 | 43.2 | -52.5 | -4.9 | 65.1 |
| 8115 | ok | 0.09 | 8.12e-02 | 3.48e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.4 | 23.7 | 1.4 | -2.8 | 13.6 | 0.4 |
| 8116 | ok | 0.09 | 5.90e-02 | 2.10e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.7 | 10.3 | -7.0 | 60.5 | 39.0 | -33.7 |
| 8117 | ok | 0.09 | 4.80e-02 | 3.82e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -9.0 | -6.0 | -14.7 | -36.2 | 7.2 | 0.9 |
| 8118 | ok | 0.09 | 4.69e-02 | 6.48e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -16.9 | -8.7 | -12.8 | -39.4 | 14.2 | -0.9 |
| 8119 | ok | 0.09 | 7.72e-02 | 1.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.2 | -4.7 | 19.8 | -59.7 | -0.4 | 38.9 |
| 8120 | ok | 0.09 | 0.1 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.5 | 4.6 | 36.3 | 35.9 | 13.5 | -40.0 |
| 8121 | ok | 0.09 | 8.23e-02 | 4.84e-04 | 4.5 | 4.5 | 4.0 | 4.0 | 2.20e-02 | 24.1 | 4.5 | 5.6 | 6.2 | 20.3 |
| 8122 | ok | 0.09 | 6.43e-02 | 3.37e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -7.7 | -11.0 | -10.6 | -18.8 | 10.1 | -27.2 |
| 8123 | ok | 0.09 | 4.99e-02 | 5.29e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.4 | -12.0 | -15.6 | -25.9 | 16.8 | -21.5 |
| 8124 | ok | 0.09 | 4.86e-02 | 7.99e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.2 | -9.4 | -14.8 | -42.3 | 14.9 | 0.6 |
| 8125 | ok | 0.09 | 7.74e-02 | 1.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.7 | -2.0 | 18.0 | -63.2 | -7.4 | 44.7 |
| 8126 | ok | 0.09 | 0.1 | 2.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.1 | 8.6 | 36.2 | 38.7 | 11.9 | -40.6 |
| 8127 | ok | 0.09 | 0.1 | 1.71e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 2.4 | 31.7 | 7.5 | 7.4 | -2.7 | 29.0 |
| 8128 | ok | 0.09 | 7.68e-02 | 5.61e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -13.7 | -20.1 | -16.1 | -24.9 | 11.8 | -36.0 |
| 8129 | ok | 0.09 | 4.39e-02 | 7.55e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -22.2 | -12.9 | -18.6 | -32.6 | 20.8 | -20.9 |
| 8130 | ok | 0.09 | 4.82e-02 | 9.82e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.4 | -9.0 | -15.7 | -47.7 | 16.4 | 2.4 |
| 8131 | ok | 0.09 | 7.68e-02 | 1.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.7 | -22.7 | -46.9 | 26.0 | 12.3 | 26.9 |
| 8132 | ok | 0.09 | 0.1 | 2.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.2 | -30.9 | -72.3 | 35.9 | 13.1 | 50.1 |
| 8133 | ok | 0.09 | 0.2 | 5.99e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 31.7 | 55.5 | 23.4 | 10.5 | -13.5 | 72.9 |
| 8134 | ok | 0.09 | 5.21e-02 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -29.3 | -18.7 | -22.5 | -39.3 | 29.2 | -45.0 |
| 8135 | ok | 0.09 | 4.08e-02 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.4 | -11.9 | -19.8 | -43.0 | 25.6 | -17.9 |
| 8136 | ok | 0.09 | 4.56e-02 | 1.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.8 | -12.4 | -24.2 | 15.6 | 13.1 | 6.9 |
| 8137 | ok | 0.09 | 7.77e-02 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.5 | -20.2 | -49.6 | 26.1 | 11.3 | 33.0 |
| 8138 | ok | 0.09 | 8.69e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.2 | -16.7 | -30.9 | -70.1 | 17.8 | -29.5 |
| 8139 | ok | 0.09 | 4.14e-02 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.2 | -7.6 | -19.1 | 5.0 | 11.5 | 4.0 |
| 8140 | ok | 0.09 | 3.98e-02 | 1.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.9 | -9.8 | -23.7 | 14.0 | 11.5 | 9.0 |
| 8141 | ok | 0.09 | 5.81e-02 | 1.91e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.7 | -18.8 | -46.8 | -64.3 | 37.8 | 35.8 |
| 8142 | ok | 0.09 | 6.00e-02 | 1.75e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.9 | -10.3 | -12.1 | -0.2 | 2.9 | -1.1 |
| 8143 | ok | 0.09 | 4.83e-02 | 1.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.3 | -6.0 | -15.0 | -0.7 | 7.0 | 3.3 |
| 8144 | ok | 0.09 | 4.40e-02 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.0 | -6.7 | -12.3 | -110.4 | 9.6 | 46.4 |
| 8145 | ok | 0.09 | 6.42e-02 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.4 | -14.1 | -44.9 | -63.3 | 24.2 | 56.0 |
| 8146 | ok | 0.09 | 6.46e-02 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -69.5 | -16.1 | -2.6 | -4.7 | -8.5 | -8.7 |
| 8147 | ok | 0.09 | 5.57e-02 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -67.8 | -8.7 | -7.1 | -177.1 | -10.6 | 50.2 |
| 8148 | ok | 0.09 | 4.72e-02 | 1.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.5 | -6.1 | -6.9 | -123.3 | -18.1 | 58.7 |
| 8149 | ok | 0.09 | 7.11e-02 | 1.90e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.3 | -6.8 | 8.3 | -53.4 | -42.7 | 53.2 |
| 8150 | ok | 0.09 | 7.02e-02 | 1.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -67.5 | -14.5 | 1.1 | -15.8 | -24.2 | -20.8 |
| 8151 | ok | 0.09 | 6.18e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -67.8 | -10.4 | -1.4 | -198.1 | -71.7 | 60.4 |
| 8152 | ok | 0.09 | 5.01e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.2 | -7.1 | -1.2 | -133.0 | -59.3 | 62.5 |
| 8153 | ok | 0.09 | 7.22e-02 | 1.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.7 | -11.6 | 42.8 | -31.4 | -66.7 | -17.4 |
| 8154 | ok | 0.09 | 9.43e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.5 | 2.8 | 15.3 | 322.1 | 223.5 | -201.4 |
| 8155 | ok | 0.09 | 6.71e-02 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.1 | -10.8 | 6.4 | -222.6 | -167.6 | 54.7 |
| 8156 | ok | 0.09 | 5.06e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.7 | -7.3 | -0.4 | -26.5 | -36.8 | 14.1 |
| 8157 | ok | 0.09 | 4.94e-02 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.0 | -7.8 | -31.8 | -60.8 | -98.4 | 63.4 |
| 8158 | ok | 0.09 | 0.1 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.2 | -9.7 | 14.6 | 275.8 | 452.2 | -61.8 |
| 8159 | ok | 0.09 | 7.18e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.1 | -11.8 | 7.6 | -246.8 | -298.0 | 9.2 |
| 8160 | ok | 0.09 | 4.64e-02 | 1.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.4 | -9.6 | -3.2 | -152.4 | -190.6 | -4.0 |
| 8161 | ok | 0.09 | 6.71e-02 | 1.89e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.6 | -3.2 | 38.6 | -59.4 | -46.8 | -73.0 |
| 8162 | ok | 0.09 | 0.1 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.0 | 4.6 | -16.7 | 313.7 | 201.7 | 127.0 |
| 8163 | ok | 0.09 | 6.33e-02 | 1.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.4 | -10.7 | -7.1 | -220.1 | -167.2 | -46.2 |
| 8164 | ok | 0.09 | 4.73e-02 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.9 | -8.4 | -4.9 | -139.1 | -119.7 | -44.5 |
| 8165 | ok | 0.09 | 6.83e-02 | 1.91e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.9 | -6.1 | 10.4 | -56.4 | -32.9 | -59.6 |
| 8166 | ok | 0.09 | 6.62e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.7 | -14.9 | -0.7 | -228.3 | -75.1 | -45.5 |
| 8167 | ok | 0.09 | 5.83e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.2 | -9.6 | -2.82e-02 | -195.4 | -72.9 | -52.1 |
| 8168 | ok | 0.09 | 4.69e-02 | 1.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.8 | -7.3 | -0.2 | -130.4 | -58.9 | -58.0 |
| 8169 | ok | 0.09 | 6.62e-02 | 1.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.4 | -7.0 | -34.9 | -52.6 | -45.4 | -41.4 |
| 8170 | ok | 0.09 | 6.09e-02 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.8 | -14.7 | 0.3 | -209.5 | 4.9 | -32.6 |
| 8171 | ok | 0.09 | 5.26e-02 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.0 | -7.9 | 2.8 | -171.5 | -12.0 | -43.7 |
| 8172 | ok | 0.09 | 4.37e-02 | 1.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.6 | -6.7 | 5.7 | -119.3 | -18.4 | -53.2 |
| 8173 | ok | 0.09 | 7.44e-02 | 1.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.9 | -4.0 | -28.2 | -60.0 | -33.4 | -49.3 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-------|-------|-------|--------|-------|-------|
| 8174 | ok | 0.09 | 5.64e-02 | 1.57e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.5 | -9.9 | 11.3 | -182.8 | 48.5 | -1.5 |
| 8175 | ok | 0.09 | 4.57e-02 | 1.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.9 | -7.6 | 13.6 | -144.8 | 23.5 | -25.1 |
| 8176 | ok | 0.09 | 3.90e-02 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.2 | -9.0 | 16.6 | -105.4 | 12.2 | -40.7 |
| 8177 | ok | 0.09 | 6.98e-02 | 1.81e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.0 | -3.5 | -21.5 | -62.2 | -21.4 | -48.6 |
| 8178 | ok | 0.09 | 7.37e-02 | 1.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.7 | -10.9 | 20.0 | -123.5 | 61.6 | 33.2 |
| 8179 | ok | 0.09 | 4.13e-02 | 1.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.9 | -7.9 | 16.3 | -112.1 | 38.9 | -5.3 |
| 8180 | ok | 0.09 | 3.67e-02 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.7 | -9.5 | 13.8 | -90.2 | 22.5 | -27.1 |
| 8181 | ok | 0.09 | 7.29e-02 | 1.65e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.3 | -3.8 | -21.6 | -62.5 | -10.2 | -45.8 |
| 8182 | ok | 0.09 | 0.1 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.0 | 2.7 | -43.8 | -43.4 | -36.0 | -78.5 |
| 8183 | ok | 0.09 | 0.2 | 6.09e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -12.8 | -28.9 | 12.9 | -5.7 | 20.2 | 24.4 |
| 8184 | ok | 0.09 | 7.09e-02 | 9.88e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -10.0 | -16.4 | 16.7 | -48.3 | 35.9 | 44.9 |
| 8185 | ok | 0.09 | 5.04e-02 | 9.12e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -30.5 | -11.9 | 14.8 | -79.8 | 37.9 | 5.5 |
| 8186 | ok | 0.09 | 3.37e-02 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.2 | -12.0 | 13.8 | -75.6 | 27.0 | -15.3 |
| 8187 | ok | 0.09 | 7.83e-02 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.4 | -6.0 | -21.3 | -58.9 | -1.6 | -40.3 |
| 8188 | ok | 0.09 | 0.1 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.7 | -0.2 | -42.2 | -48.5 | -22.2 | -74.0 |
| 8189 | ok | 0.09 | 9.55e-02 | 1.43e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 2.3 | 26.5 | -8.7 | 9.1 | -2.6 | -26.7 |
| 8190 | ok | 0.09 | 8.70e-02 | 5.41e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -0.3 | 12.3 | -6.1 | 12.0 | 0.7 | -43.4 |
| 8191 | ok | 0.09 | 5.20e-02 | 6.46e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -16.2 | -12.5 | 12.3 | -56.4 | 34.0 | 9.5 |
| 8192 | ok | 0.09 | 3.89e-02 | 8.65e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.9 | -13.1 | 11.0 | -62.6 | 26.1 | -7.4 |
| 8193 | ok | 0.09 | 8.02e-02 | 1.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.3 | -17.4 | 33.5 | -54.2 | 20.0 | 22.7 |
| 8194 | ok | 0.09 | 0.1 | 1.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.4 | -19.8 | 55.4 | -49.2 | 15.5 | 48.0 |
| 8195 | ok | 0.09 | 6.08e-02 | 5.26e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.2 | 20.4 | -1.7 | -0.2 | 14.6 | -6.8 |
| 8196 | ok | 0.09 | 6.96e-02 | 3.18e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.6 | 3.6 | 1.3 | 1.3 | 14.6 | -39.5 |
| 8197 | ok | 0.09 | 5.39e-02 | 4.76e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.1 | -11.1 | 6.6 | -41.9 | 30.8 | 8.5 |
| 8198 | ok | 0.09 | 4.79e-02 | 6.92e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.1 | -13.6 | 0.6 | -52.8 | 24.4 | -3.8 |
| 8199 | ok | 0.09 | 8.48e-02 | 1.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.1 | -13.9 | 28.5 | -53.5 | 12.8 | 30.4 |
| 8200 | ok | 0.09 | 0.1 | 1.85e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.2 | -13.8 | 49.3 | -52.3 | 2.4 | 59.9 |
| 8201 | ok | 0.09 | 6.21e-02 | 5.11e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.4 | 20.9 | -1.4 | -0.2 | 17.8 | -6.7 |
| 8202 | ok | 0.09 | 5.51e-02 | 2.57e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.2 | 5.9 | -0.4 | 1.6 | 17.8 | -38.3 |
| 8203 | ok | 0.09 | 4.84e-02 | 4.36e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -9.0 | -10.6 | -15.7 | 37.6 | 14.5 | -33.0 |
| 8204 | ok | 0.09 | 4.99e-02 | 6.63e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -14.8 | -11.3 | -17.0 | 49.8 | 10.7 | -31.6 |
| 8205 | ok | 0.09 | 8.78e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.8 | -10.1 | 23.8 | -54.2 | 6.1 | 37.5 |
| 8206 | ok | 0.09 | 0.1 | 2.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.6 | 1.2 | 37.7 | 30.9 | 28.3 | -42.8 |
| 8207 | ok | 0.09 | 7.52e-02 | 9.00e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.5 | 21.0 | -1.2 | -0.2 | 21.4 | -6.4 |
| 8208 | ok | 0.09 | 5.46e-02 | 3.62e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -4.3 | -7.1 | -13.1 | 19.6 | 18.9 | -29.4 |
| 8209 | ok | 0.09 | 4.65e-02 | 5.36e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.5 | -15.4 | -18.3 | 34.8 | 14.2 | -29.3 |
| 8210 | ok | 0.09 | 5.24e-02 | 7.83e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -17.5 | -13.4 | -19.7 | 46.9 | 10.4 | -29.9 |
| 8211 | ok | 0.09 | 8.87e-02 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.4 | -6.5 | 20.0 | -55.9 | -0.2 | 44.8 |
| 8212 | ok | 0.09 | 0.1 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.6 | 7.4 | 34.6 | 32.0 | 26.5 | -41.4 |
| 8213 | ok | 0.09 | 9.42e-02 | 2.10e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 0.2 | 26.9 | 5.8 | -5.0 | 24.4 | -1.5 |
| 8214 | ok | 0.09 | 6.90e-02 | 5.29e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -6.0 | -15.3 | -15.1 | 20.1 | 18.8 | -24.2 |
| 8215 | ok | 0.09 | 4.45e-02 | 6.86e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -12.7 | -17.4 | -23.4 | 34.6 | 14.2 | -27.0 |
| 8216 | ok | 0.09 | 5.19e-02 | 9.29e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -22.0 | -14.8 | -21.8 | 45.8 | 9.5 | -28.6 |
| 8217 | ok | 0.09 | 8.73e-02 | 1.81e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.9 | -3.5 | 17.7 | -57.8 | -6.5 | 52.7 |
| 8218 | ok | 0.09 | 0.1 | 2.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.8 | 12.3 | 33.7 | 34.7 | 25.0 | -41.6 |
| 8219 | ok | 0.09 | 0.1 | 4.32e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 2.8 | 35.9 | 9.3 | -5.8 | 30.6 | -16.8 |
| 8220 | ok | 0.09 | 8.56e-02 | 7.93e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -9.8 | -26.0 | -19.7 | 22.9 | 17.2 | -19.3 |
| 8221 | ok | 0.09 | 3.97e-02 | 8.91e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -19.4 | -22.8 | -27.4 | 37.1 | 13.4 | -23.9 |
| 8222 | ok | 0.09 | 5.01e-02 | 1.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -28.3 | -15.1 | -22.8 | 46.1 | 13.3 | -28.1 |
| 8223 | ok | 0.09 | 8.35e-02 | 1.98e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.1 | -1.4 | 17.3 | -58.9 | -13.5 | 60.9 |
| 8224 | ok | 0.09 | 0.1 | 2.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.9 | 15.1 | 35.5 | 39.6 | 23.7 | -43.8 |
| 8225 | ok | 0.09 | 0.2 | 9.79e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 34.3 | 62.9 | 27.0 | -6.3 | 41.8 | -30.5 |
| 8226 | ok | 0.09 | 5.92e-02 | 1.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -22.7 | -39.6 | -29.4 | 33.2 | 16.1 | 7.9 |
| 8227 | ok | 0.09 | 3.20e-02 | 1.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.4 | -24.2 | -30.5 | 41.2 | 11.6 | -22.5 |
| 8228 | ok | 0.09 | 4.32e-02 | 1.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.8 | -14.3 | -21.7 | 47.1 | 12.7 | -28.2 |
| 8229 | ok | 0.09 | 7.76e-02 | 2.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.9 | -0.6 | 18.0 | -56.2 | -22.8 | 68.2 |
| 8230 | ok | 0.09 | 8.47e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.2 | -32.9 | -23.0 | 43.9 | -18.9 | 6.6 |
| 8231 | ok | 0.09 | 3.49e-02 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.0 | -22.6 | -30.2 | 52.7 | 10.7 | -19.1 |
| 8232 | ok | 0.09 | 3.66e-02 | 1.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.8 | -15.3 | -26.6 | 52.1 | 11.7 | -24.9 |
| 8233 | ok | 0.09 | 6.95e-02 | 2.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.8 | -0.7 | 22.9 | 22.0 | 35.4 | -14.8 |
| 8234 | ok | 0.09 | 5.66e-02 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -76.1 | -32.2 | -16.5 | 89.9 | -12.4 | -16.1 |
| 8235 | ok | 0.09 | 4.28e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.1 | -22.5 | -12.4 | 66.6 | 7.3 | -26.1 |
| 8236 | ok | 0.09 | 4.15e-02 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.7 | -13.8 | -11.5 | 12.6 | 19.5 | 4.5 |
| 8237 | ok | 0.09 | 6.54e-02 | 2.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.6 | -24.8 | -51.8 | 27.4 | 6.2 | 45.9 |
| 8238 | ok | 0.09 | 5.69e-02 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.1 | -38.4 | -8.0 | 77.2 | -2.6 | -22.4 |
| 8239 | ok | 0.09 | 4.83e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.3 | -22.2 | -10.3 | 64.9 | 7.2 | -27.9 |
| 8240 | ok | 0.09 | 4.52e-02 | 1.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.3 | -15.0 | -6.3 | 9.0 | 18.2 | 7.5 |
| 8241 | ok | 0.09 | 6.45e-02 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.5 | -20.9 | -49.4 | 28.6 | 1.7 | 64.1 |
| 8242 | ok | 0.09 | 6.17e-02 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.9 | -35.8 | -3.4 | -12.6 | 2.0 | -6.9 |
| 8243 | ok | 0.09 | 5.19e-02 | 1.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.4 | -25.4 | -3.4 | -19.6 | 8.5 | 2.6 |
| 8244 | ok | 0.09 | 4.70e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.4 | -19.6 | -15.2 | -1.7 | 6.4 | 18.8 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|-------|-------|-------|--------|--------|
| 8245 | ok | 0.09 | 8.00e-02 | 2.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.6 | -18.6 | -45.6 | 28.0 | -6.3 | 85.7 |
| 8246 | ok | 0.09 | 7.05e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.5 | -35.4 | 3.5 | -18.6 | -11.5 | -24.2 |
| 8247 | ok | 0.09 | 5.57e-02 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.1 | -25.6 | 0.3 | 55.9 | 94.1 | -93.7 |
| 8248 | ok | 0.09 | 4.66e-02 | 1.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.8 | -17.0 | 3.0 | 59.0 | 79.6 | -62.3 |
| 8249 | ok | 0.09 | 0.1 | 1.83e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.9 | -20.5 | -33.0 | 78.5 | 0.8 | 43.6 |
| 8250 | ok | 0.09 | 9.29e-02 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.4 | -38.3 | 9.4 | 51.5 | 234.3 | -100.8 |
| 8251 | ok | 0.09 | 6.95e-02 | 1.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.4 | -28.5 | 7.3 | 23.0 | 105.2 | -64.0 |
| 8252 | ok | 0.09 | 6.49e-02 | 1.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -67.8 | -17.4 | 18.7 | 38.5 | 68.6 | -61.2 |
| 8253 | ok | 0.09 | 7.42e-02 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.7 | -26.3 | -59.6 | 80.7 | 55.8 | 115.8 |
| 8254 | ok | 0.09 | 6.90e-02 | 1.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.2 | -40.6 | -26.4 | 53.4 | 174.1 | 22.2 |
| 8255 | ok | 0.09 | 5.57e-02 | 1.77e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.9 | -26.3 | -21.6 | 11.2 | 89.5 | -20.3 |
| 8256 | ok | 0.09 | 4.05e-02 | 1.77e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.8 | -17.6 | -11.5 | 17.2 | 58.0 | -29.5 |
| 8257 | ok | 0.09 | 7.39e-02 | 2.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.8 | -7.0 | 30.9 | 24.6 | -70.9 | -111.6 |
| 8258 | ok | 0.09 | 9.24e-02 | 2.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.3 | -41.6 | -20.0 | 84.0 | 42.8 | 27.2 |
| 8259 | ok | 0.09 | 6.99e-02 | 1.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -69.0 | -23.8 | -13.3 | 14.9 | 46.4 | 1.3 |
| 8260 | ok | 0.09 | 5.42e-02 | 1.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.6 | -17.4 | -4.9 | 12.2 | 26.3 | -15.2 |
| 8261 | ok | 0.09 | 8.60e-02 | 2.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.9 | -18.5 | -52.8 | 40.3 | -20.6 | 82.1 |
| 8262 | ok | 0.09 | 0.2 | 2.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.1 | -48.2 | 40.7 | -31.3 | -301.0 | 122.2 |
| 8263 | ok | 0.09 | 9.68e-02 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.4 | -22.0 | 29.7 | -45.1 | -221.2 | 117.0 |
| 8264 | ok | 0.09 | 7.42e-02 | 1.68e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.5 | -17.8 | 21.6 | 23.3 | 46.2 | 3.6 |
| 8265 | ok | 0.09 | 7.28e-02 | 2.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.8 | -1.8 | -27.8 | 96.9 | 107.1 | 71.4 |
| 8266 | ok | 0.09 | 0.1 | 2.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.3 | -12.7 | -25.2 | 359.1 | 97.2 | 232.2 |
| 8267 | ok | 0.09 | 5.85e-02 | 1.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -71.2 | -10.5 | -10.4 | 252.9 | 55.2 | 114.2 |
| 8268 | ok | 0.09 | 4.26e-02 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.3 | -7.7 | -9.2 | 129.6 | 61.9 | 97.4 |
| 8269 | ok | 0.09 | 9.79e-02 | 3.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -69.8 | 13.7 | -28.3 | 99.2 | 113.0 | 73.0 |
| 8270 | ok | 0.09 | 0.1 | 2.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -123.2 | -10.3 | -0.8 | 575.7 | 18.3 | 158.0 |
| 8271 | ok | 0.09 | 6.66e-02 | 2.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -106.1 | -1.2 | -0.4 | 323.6 | 41.8 | 88.1 |
| 8272 | ok | 0.09 | 4.59e-02 | 2.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -89.7 | 1.5 | 2.9 | 177.4 | 54.1 | 63.1 |
| 8273 | ok | 0.09 | 0.1 | 3.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.4 | 29.0 | -27.0 | 104.4 | 86.6 | 62.6 |
| 8274 | ok | 0.09 | 0.1 | 3.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -147.8 | -6.4 | 15.1 | 675.6 | -70.1 | 64.0 |
| 8275 | ok | 0.09 | 6.86e-02 | 2.85e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -121.0 | 4.9 | 26.3 | 319.6 | 66.0 | 45.5 |
| 8276 | ok | 0.09 | 6.08e-02 | 2.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -102.5 | 7.8 | 19.3 | 175.1 | 29.8 | 47.1 |
| 8281 | ok | 0.09 | 0.3 | 1.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -6.5 | -56.3 | 4.8 | 0.6 | -409.2 | 18.9 |
| 8282 | ok | 0.09 | 9.69e-02 | 2.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.8 | -51.5 | 37.5 | -9.4 | -213.1 | 96.1 |
| 8283 | ok | 0.09 | 0.1 | 6.77e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 3.1 | -28.5 | -3.0 | 2.8 | -253.2 | 12.4 |
| 8284 | ok | 0.09 | 8.46e-02 | 1.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -7.3 | -41.6 | 15.3 | -16.5 | -242.6 | 94.1 |
| 8285 | ok | 0.09 | 8.48e-02 | 4.12e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.8 | -22.0 | 1.4 | 1.7 | -89.2 | 39.1 |
| 8286 | ok | 0.09 | 6.84e-02 | 7.66e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.8 | -28.3 | 12.4 | -5.7 | -144.9 | 66.3 |
| 8287 | ok | 0.09 | 6.92e-02 | 3.06e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.2 | -16.3 | -0.5 | 7.8 | 8.9 | 35.6 |
| 8288 | ok | 0.09 | 5.73e-02 | 5.80e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -4.8 | -26.9 | 6.7 | 30.7 | 18.2 | 84.8 |
| 8289 | ok | 0.09 | 9.14e-02 | 3.04e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.0 | 22.7 | 1.6 | -8.4 | -10.8 | 9.1 |
| 8290 | ok | 0.09 | 8.29e-02 | 5.15e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -4.9 | -25.1 | 3.2 | 44.9 | 18.7 | 95.7 |
| 8291 | ok | 0.09 | 0.1 | 4.22e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 3.3 | 43.4 | 9.0 | -4.7 | 11.8 | 14.0 |
| 8292 | ok | 0.09 | 0.1 | 7.42e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.5 | -29.4 | -3.2 | 16.9 | 72.4 | 61.9 |
| 8293 | ok | 0.09 | 0.4 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | 56.1 | 96.4 | 40.5 | -89.8 | 118.8 | -3.3 |
| 8294 | ok | 0.09 | 0.1 | 1.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.0 | -32.9 | -40.8 | 65.7 | 65.6 | 121.7 |
| 8295 | ok | 0.09 | 6.83e-02 | 2.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.1 | -5.9 | -23.7 | 73.9 | 73.2 | 66.4 |
| 8296 | ok | 0.09 | 0.1 | 2.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.5 | 15.2 | -36.4 | 146.2 | 162.7 | 221.9 |
| 8297 | ok | 0.09 | 7.36e-02 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.5 | -33.7 | 30.7 | -27.7 | -160.6 | 108.2 |
| 8298 | ok | 0.09 | 5.67e-02 | 1.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.3 | -21.7 | 24.7 | -8.4 | -106.7 | 93.6 |
| 8299 | ok | 0.09 | 6.28e-02 | 1.93e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.3 | -5.0 | -11.9 | 71.1 | 73.6 | 62.4 |
| 8300 | ok | 0.09 | 0.1 | 2.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.7 | 23.3 | -27.9 | 127.9 | 131.3 | 189.1 |
| 8301 | ok | 0.09 | 5.26e-02 | 1.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -21.9 | -35.3 | 24.9 | -3.2 | -101.9 | 79.7 |
| 8302 | ok | 0.09 | 4.14e-02 | 1.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.1 | -30.9 | 27.4 | 9.1 | -80.5 | 64.9 |
| 8303 | ok | 0.09 | 7.02e-02 | 1.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -28.1 | -3.1 | -7.2 | 70.9 | 51.2 | 97.3 |
| 8304 | ok | 0.09 | 0.1 | 2.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -29.9 | 20.0 | -28.7 | 112.3 | 112.3 | 161.8 |
| 8305 | ok | 0.09 | 4.31e-02 | 9.87e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.1 | -28.8 | 16.7 | 25.7 | -73.5 | 81.8 |
| 8306 | ok | 0.09 | 4.56e-02 | 1.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -24.4 | -31.8 | 23.6 | 26.5 | -47.2 | 50.5 |
| 8307 | ok | 0.09 | 6.20e-02 | 1.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -25.8 | -6.8 | -10.4 | 74.1 | 55.3 | 83.7 |
| 8308 | ok | 0.09 | 0.1 | 2.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -29.7 | 11.8 | -33.9 | 99.2 | 102.0 | 140.4 |
| 8309 | ok | 0.09 | 5.58e-02 | 8.20e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -8.0 | -26.5 | 12.7 | 15.7 | -60.8 | 52.0 |
| 8310 | ok | 0.09 | 4.74e-02 | 9.95e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.0 | -30.6 | 19.0 | 42.7 | -20.7 | 44.0 |
| 8311 | ok | 0.09 | 6.39e-02 | 1.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -27.6 | -11.3 | -15.6 | 78.5 | 63.2 | 74.8 |
| 8312 | ok | 0.09 | 0.1 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.1 | 3.2 | -41.7 | 88.2 | 100.0 | 124.8 |
| 8313 | ok | 0.09 | 5.70e-02 | 7.05e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -14.3 | -30.2 | 7.2 | 71.5 | 15.5 | 101.6 |
| 8314 | ok | 0.09 | 4.17e-02 | 8.88e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.5 | -24.9 | 5.2 | 65.2 | 19.0 | 48.4 |
| 8315 | ok | 0.09 | 6.48e-02 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.4 | -13.6 | -21.3 | 84.6 | 75.5 | 70.1 |
| 8316 | ok | 0.09 | 0.1 | 2.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.9 | -1.9 | -50.8 | 78.9 | 106.2 | 115.2 |
| 8317 | ok | 0.09 | 6.32e-02 | 6.74e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.2 | -24.2 | -15.9 | 33.2 | 50.2 | 94.6 |
| 8318 | ok | 0.09 | 3.50e-02 | 8.39e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -29.1 | -23.2 | -0.6 | 87.3 | 40.1 | 50.8 |
| 8319 | ok | 0.09 | 6.93e-02 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.4 | -11.1 | -26.0 | 91.5 | 91.6 | 69.3 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------------|-------|------------|--------------|-----------------|---------------|---------------|----------------|----------------|------------|------------|-------------|------------|------------|-------------|
| 8320 | ok | 0.09 | 0.1 | 2.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.9 | -0.4 | -59.9 | 71.6 | 119.7 | 111.5 |
| 8321 | ok | 0.09 | 6.78e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.0 | -21.2 | -13.8 | 147.8 | 86.8 | 132.1 |
| 8322 | ok | 0.09 | 3.83e-02 | 1.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.6 | -17.0 | -11.4 | 104.8 | 68.2 | 93.3 |
| 8326 | ok | 0.09 | 0.2 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.4 | 39.4 | 24.6 | 381.2 | 647.6 | 6.8 |
| 8329 | ok | 0.09 | 0.1 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.5 | 4.8 | 11.3 | 238.1 | 350.4 | 98.5 |
| 8330 | ok | 0.09 | 8.84e-02 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.4 | 5.4 | -16.2 | 58.7 | 74.9 | 60.1 |
| 8331 | ok | 0.09 | 6.12e-02 | 1.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.3 | 4.0 | -17.3 | 55.2 | 25.4 | 53.3 |
| 8332 | ok | 0.09 | 9.70e-02 | 1.81e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.4 | 1.6 | -40.4 | -75.2 | -87.4 | 60.5 |
| 8345 | ok | 0.09 | 0.1 | 1.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.7 | -25.7 | 20.7 | 131.4 | 417.9 | -25.1 |
| 8347 | ok | 0.09 | 9.48e-02 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.1 | -47.2 | 3.3 | 34.6 | 227.6 | -53.6 |
| 8348 | ok | 0.09 | 7.13e-02 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.0 | -28.9 | 4.4 | 11.8 | 90.1 | -48.1 |
| 8349 | ok | 0.09 | 5.60e-02 | 1.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.1 | -18.9 | 9.2 | 26.3 | 50.9 | -40.0 |
| 8350 | ok | 0.09 | 8.37e-02 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.3 | -13.0 | 24.5 | 98.6 | 59.8 | -66.0 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | 0.09 | 0.39 | 0.07 | 4.52 | 4.52 | 4.00 | 4.00 | -331.02 | -153.70 | -88.44 | -256.64 | -470.49 | -238.86 |
| | | 0.09 | 0.39 | 0.07 | 4.52 | 4.52 | 4.00 | 4.00 | 56.06 | 96.42 | 129.89 | 1086.40 | 660.03 | 523.63 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 31 | ok | 0.46 | | | | | | |
| 32 | ok | 0.26 | | | | | | |
| 33 | ok | 0.31 | | | | | | |
| 34 | ok | 0.35 | | | | | | |
| 35 | ok | 0.51 | | | | | | |
| 36 | ok | 0.49 | | | | | | |
| 37 | ok | 0.51 | | | | | | |
| 39 | ok | 0.13 | | | | | | |
| 40 | ok | 0.58 | | | | | | |
| 3720 | ok | 0.19 | | | | | | |
| 3899 | ok | 0.33 | | | | | | |
| 3932 | ok | 0.41 | | | | | | |
| 3960 | ok | 0.46 | | | | | | |
| 3977 | ok | 0.23 | | | | | | |
| 3994 | ok | 0.26 | | | | | | |
| 4036 | ok | 0.31 | | | | | | |
| 4053 | ok | 0.31 | | | | | | |
| 4070 | ok | 0.73 | | | | | | |
| 4087 | ok | 1.00 | | | | | | |
| 4104 | ok | 0.60 | | | | | | |
| 4121 | ok | 0.37 | | | | | | |
| 4138 | ok | 0.29 | | | | | | |
| 4195 | ok | 0.51 | | | | | | |
| 4212 | ok | 0.24 | | | | | | |
| 4229 | ok | 0.42 | | | | | | |
| 4246 | ok | 0.97 | | | | | | |
| 4263 | ok | 1.11 | | | | | | |
| 4280 | ok | 1.11 | | | | | | |
| 4297 | ok | 0.56 | | | | | | |
| 4314 | ok | 0.32 | | | | | | |
| 4331 | ok | 0.46 | | | | | | |
| 4391 | ok | 0.54 | | | | | | |
| 4408 | ok | 0.76 | | | | | | |
| 4425 | ok | 0.76 | | | | | | |
| 4442 | ok | 0.62 | | | | | | |
| 4497 | ok | 0.46 | | | | | | |
| 4514 | ok | 0.34 | | | | | | |
| 4531 | ok | 0.60 | | | | | | |
| 4548 | ok | 1.18 | | | | | | |
| 4565 | ok | 1.18 | | | | | | |
| 4582 | ok | 0.96 | | | | | | |
| 4599 | ok | 0.38 | | | | | | |
| 4616 | ok | 0.26 | | | | | | |
| 4633 | ok | 0.56 | | | | | | |
| 4689 | ok | 0.57 | | | | | | |
| 6883 | ok | 0.37 | | | | | | |
| 6903 | ok | 0.30 | | | | | | |
| 6923 | ok | 0.67 | | | | | | |
| 6943 | ok | 0.67 | | | | | | |
| 7333 | ok | 0.24 | | | | | | |
| 7334 | ok | 0.11 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 7335 | ok | 0.13 | | | | | | |
| 7336 | ok | 0.12 | | | | | | |
| 7337 | ok | 0.06 | | | | | | |
| 7338 | ok | 0.09 | | | | | | |
| 7339 | ok | 0.10 | | | | | | |
| 7340 | ok | 0.13 | | | | | | |
| 7341 | ok | 0.19 | | | | | | |
| 7494 | ok | 0.14 | | | | | | |
| 7495 | ok | 0.14 | | | | | | |
| 7496 | ok | 0.14 | | | | | | |
| 7497 | ok | 0.24 | | | | | | |
| 7498 | ok | 0.20 | | | | | | |
| 7499 | ok | 0.15 | | | | | | |
| 7500 | ok | 0.13 | | | | | | |
| 7501 | ok | 0.13 | | | | | | |
| 7502 | ok | 0.23 | | | | | | |
| 7503 | ok | 0.17 | | | | | | |
| 7504 | ok | 0.13 | | | | | | |
| 7505 | ok | 0.13 | | | | | | |
| 7506 | ok | 0.13 | | | | | | |
| 7507 | ok | 0.08 | | | | | | |
| 7508 | ok | 0.11 | | | | | | |
| 7509 | ok | 0.14 | | | | | | |
| 7510 | ok | 0.18 | | | | | | |
| 7512 | ok | 0.18 | | | | | | |
| 7513 | ok | 0.14 | | | | | | |
| 7514 | ok | 0.13 | | | | | | |
| 7515 | ok | 0.11 | | | | | | |
| 7516 | ok | 0.14 | | | | | | |
| 7517 | ok | 0.27 | | | | | | |
| 7518 | ok | 0.23 | | | | | | |
| 7519 | ok | 0.19 | | | | | | |
| 7520 | ok | 0.12 | | | | | | |
| 7521 | ok | 0.14 | | | | | | |
| 7522 | ok | 0.15 | | | | | | |
| 7523 | ok | 0.17 | | | | | | |
| 7525 | ok | 0.17 | | | | | | |
| 7526 | ok | 0.13 | | | | | | |
| 7527 | ok | 0.10 | | | | | | |
| 7528 | ok | 0.08 | | | | | | |
| 7529 | ok | 0.06 | | | | | | |
| 7640 | ok | 0.11 | | | | | | |
| 7641 | ok | 0.14 | | | | | | |
| 7642 | ok | 0.20 | | | | | | |
| 7643 | ok | 0.20 | | | | | | |
| 7650 | ok | 0.23 | | | | | | |
| 7651 | ok | 0.18 | | | | | | |
| 7652 | ok | 0.17 | | | | | | |
| 7653 | ok | 0.27 | | | | | | |
| 7907 | ok | 0.43 | | | | | | |
| 7908 | ok | 0.33 | | | | | | |
| 7909 | ok | 0.26 | | | | | | |
| 7910 | ok | 0.26 | | | | | | |
| 7911 | ok | 0.43 | | | | | | |
| 7912 | ok | 0.33 | | | | | | |
| 7913 | ok | 0.26 | | | | | | |
| 7914 | ok | 0.26 | | | | | | |
| 7915 | ok | 0.43 | | | | | | |
| 7916 | ok | 0.41 | | | | | | |
| 7917 | ok | 0.24 | | | | | | |
| 7918 | ok | 0.18 | | | | | | |
| 7919 | ok | 0.18 | | | | | | |
| 7920 | ok | 0.15 | | | | | | |
| 7921 | ok | 0.15 | | | | | | |
| 7922 | ok | 0.18 | | | | | | |
| 7923 | ok | 0.13 | | | | | | |
| 7924 | ok | 0.15 | | | | | | |
| 7925 | ok | 0.11 | | | | | | |
| 7926 | ok | 0.14 | | | | | | |
| 7927 | ok | 0.10 | | | | | | |
| 7928 | ok | 0.13 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 7929 | ok | 0.09 | | | | | | |
| 7930 | ok | 0.10 | | | | | | |
| 7931 | ok | 0.07 | | | | | | |
| 7932 | ok | 0.11 | | | | | | |
| 7933 | ok | 0.26 | | | | | | |
| 7934 | ok | 0.07 | | | | | | |
| 7935 | ok | 0.07 | | | | | | |
| 7936 | ok | 0.07 | | | | | | |
| 7937 | ok | 0.05 | | | | | | |
| 7938 | ok | 0.12 | | | | | | |
| 7939 | ok | 0.23 | | | | | | |
| 7940 | ok | 0.06 | | | | | | |
| 7941 | ok | 0.05 | | | | | | |
| 7942 | ok | 0.05 | | | | | | |
| 7943 | ok | 0.04 | | | | | | |
| 7944 | ok | 0.12 | | | | | | |
| 7945 | ok | 0.21 | | | | | | |
| 7946 | ok | 0.06 | | | | | | |
| 7947 | ok | 0.04 | | | | | | |
| 7948 | ok | 0.04 | | | | | | |
| 7949 | ok | 0.03 | | | | | | |
| 7950 | ok | 0.12 | | | | | | |
| 7951 | ok | 0.23 | | | | | | |
| 7952 | ok | 0.10 | | | | | | |
| 7953 | ok | 0.04 | | | | | | |
| 7954 | ok | 0.04 | | | | | | |
| 7955 | ok | 0.04 | | | | | | |
| 7956 | ok | 0.13 | | | | | | |
| 7957 | ok | 0.29 | | | | | | |
| 7958 | ok | 0.12 | | | | | | |
| 7959 | ok | 0.07 | | | | | | |
| 7960 | ok | 0.06 | | | | | | |
| 7961 | ok | 0.07 | | | | | | |
| 7962 | ok | 0.12 | | | | | | |
| 7963 | ok | 0.10 | | | | | | |
| 7964 | ok | 0.09 | | | | | | |
| 7965 | ok | 0.11 | | | | | | |
| 7966 | ok | 0.16 | | | | | | |
| 7967 | ok | 0.15 | | | | | | |
| 7968 | ok | 0.13 | | | | | | |
| 7969 | ok | 0.16 | | | | | | |
| 7970 | ok | 0.31 | | | | | | |
| 7971 | ok | 0.24 | | | | | | |
| 7972 | ok | 0.19 | | | | | | |
| 7973 | ok | 0.23 | | | | | | |
| 7974 | ok | 0.56 | | | | | | |
| 7975 | ok | 0.33 | | | | | | |
| 7976 | ok | 0.25 | | | | | | |
| 7977 | ok | 0.19 | | | | | | |
| 7978 | ok | 0.65 | | | | | | |
| 7979 | ok | 0.32 | | | | | | |
| 7980 | ok | 0.23 | | | | | | |
| 7981 | ok | 0.14 | | | | | | |
| 7982 | ok | 0.42 | | | | | | |
| 7983 | ok | 0.22 | | | | | | |
| 7984 | ok | 0.17 | | | | | | |
| 7985 | ok | 0.09 | | | | | | |
| 7986 | ok | 0.27 | | | | | | |
| 7987 | ok | 0.14 | | | | | | |
| 7988 | ok | 0.11 | | | | | | |
| 7989 | ok | 0.06 | | | | | | |
| 7990 | ok | 0.16 | | | | | | |
| 7991 | ok | 0.10 | | | | | | |
| 7992 | ok | 0.08 | | | | | | |
| 7993 | ok | 0.04 | | | | | | |
| 7994 | ok | 0.13 | | | | | | |
| 7995 | ok | 0.07 | | | | | | |
| 7996 | ok | 0.05 | | | | | | |
| 7997 | ok | 0.03 | | | | | | |
| 7998 | ok | 0.11 | | | | | | |
| 7999 | ok | 0.35 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 8000 | ok | 0.13 | | | | | | |
| 8001 | ok | 0.06 | | | | | | |
| 8002 | ok | 0.04 | | | | | | |
| 8003 | ok | 0.03 | | | | | | |
| 8004 | ok | 0.10 | | | | | | |
| 8005 | ok | 0.22 | | | | | | |
| 8006 | ok | 0.11 | | | | | | |
| 8007 | ok | 0.06 | | | | | | |
| 8008 | ok | 0.04 | | | | | | |
| 8009 | ok | 0.03 | | | | | | |
| 8010 | ok | 0.09 | | | | | | |
| 8011 | ok | 0.13 | | | | | | |
| 8012 | ok | 0.07 | | | | | | |
| 8013 | ok | 0.05 | | | | | | |
| 8014 | ok | 0.04 | | | | | | |
| 8015 | ok | 0.03 | | | | | | |
| 8016 | ok | 0.08 | | | | | | |
| 8017 | ok | 0.13 | | | | | | |
| 8018 | ok | 0.04 | | | | | | |
| 8019 | ok | 0.04 | | | | | | |
| 8020 | ok | 0.04 | | | | | | |
| 8021 | ok | 0.03 | | | | | | |
| 8022 | ok | 0.07 | | | | | | |
| 8023 | ok | 0.18 | | | | | | |
| 8024 | ok | 0.07 | | | | | | |
| 8025 | ok | 0.04 | | | | | | |
| 8026 | ok | 0.04 | | | | | | |
| 8027 | ok | 0.03 | | | | | | |
| 8028 | ok | 0.06 | | | | | | |
| 8029 | ok | 0.25 | | | | | | |
| 8030 | ok | 0.10 | | | | | | |
| 8031 | ok | 0.05 | | | | | | |
| 8032 | ok | 0.04 | | | | | | |
| 8033 | ok | 0.03 | | | | | | |
| 8034 | ok | 0.05 | | | | | | |
| 8035 | ok | 0.36 | | | | | | |
| 8036 | ok | 0.14 | | | | | | |
| 8037 | ok | 0.06 | | | | | | |
| 8038 | ok | 0.04 | | | | | | |
| 8039 | ok | 0.03 | | | | | | |
| 8040 | ok | 0.05 | | | | | | |
| 8041 | ok | 0.51 | | | | | | |
| 8042 | ok | 0.16 | | | | | | |
| 8043 | ok | 0.07 | | | | | | |
| 8044 | ok | 0.05 | | | | | | |
| 8045 | ok | 0.05 | | | | | | |
| 8046 | ok | 0.16 | | | | | | |
| 8047 | ok | 0.09 | | | | | | |
| 8048 | ok | 0.07 | | | | | | |
| 8049 | ok | 0.08 | | | | | | |
| 8050 | ok | 0.14 | | | | | | |
| 8051 | ok | 0.12 | | | | | | |
| 8052 | ok | 0.10 | | | | | | |
| 8053 | ok | 0.12 | | | | | | |
| 8054 | ok | 0.24 | | | | | | |
| 8055 | ok | 0.17 | | | | | | |
| 8056 | ok | 0.14 | | | | | | |
| 8057 | ok | 0.17 | | | | | | |
| 8058 | ok | 0.37 | | | | | | |
| 8059 | ok | 0.25 | | | | | | |
| 8060 | ok | 0.20 | | | | | | |
| 8061 | ok | 0.23 | | | | | | |
| 8062 | ok | 0.59 | | | | | | |
| 8063 | ok | 0.37 | | | | | | |
| 8064 | ok | 0.28 | | | | | | |
| 8065 | ok | 0.23 | | | | | | |
| 8066 | ok | 0.59 | | | | | | |
| 8067 | ok | 0.37 | | | | | | |
| 8068 | ok | 0.28 | | | | | | |
| 8069 | ok | 0.23 | | | | | | |
| 8070 | ok | 0.58 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 8071 | ok | 0.37 | | | | | | |
| 8072 | ok | 0.28 | | | | | | |
| 8073 | ok | 0.17 | | | | | | |
| 8074 | ok | 0.36 | | | | | | |
| 8075 | ok | 0.25 | | | | | | |
| 8076 | ok | 0.20 | | | | | | |
| 8077 | ok | 0.12 | | | | | | |
| 8078 | ok | 0.24 | | | | | | |
| 8079 | ok | 0.17 | | | | | | |
| 8080 | ok | 0.14 | | | | | | |
| 8081 | ok | 0.08 | | | | | | |
| 8082 | ok | 0.13 | | | | | | |
| 8083 | ok | 0.12 | | | | | | |
| 8084 | ok | 0.10 | | | | | | |
| 8085 | ok | 0.05 | | | | | | |
| 8086 | ok | 0.14 | | | | | | |
| 8087 | ok | 0.09 | | | | | | |
| 8088 | ok | 0.07 | | | | | | |
| 8089 | ok | 0.03 | | | | | | |
| 8090 | ok | 0.07 | | | | | | |
| 8091 | ok | 0.49 | | | | | | |
| 8092 | ok | 0.14 | | | | | | |
| 8093 | ok | 0.08 | | | | | | |
| 8094 | ok | 0.05 | | | | | | |
| 8095 | ok | 0.03 | | | | | | |
| 8096 | ok | 0.06 | | | | | | |
| 8097 | ok | 0.32 | | | | | | |
| 8098 | ok | 0.12 | | | | | | |
| 8099 | ok | 0.07 | | | | | | |
| 8100 | ok | 0.04 | | | | | | |
| 8101 | ok | 0.03 | | | | | | |
| 8102 | ok | 0.05 | | | | | | |
| 8103 | ok | 0.19 | | | | | | |
| 8104 | ok | 0.08 | | | | | | |
| 8105 | ok | 0.06 | | | | | | |
| 8106 | ok | 0.04 | | | | | | |
| 8107 | ok | 0.03 | | | | | | |
| 8108 | ok | 0.05 | | | | | | |
| 8109 | ok | 0.13 | | | | | | |
| 8110 | ok | 0.05 | | | | | | |
| 8111 | ok | 0.05 | | | | | | |
| 8112 | ok | 0.04 | | | | | | |
| 8113 | ok | 0.03 | | | | | | |
| 8114 | ok | 0.05 | | | | | | |
| 8115 | ok | 0.12 | | | | | | |
| 8116 | ok | 0.05 | | | | | | |
| 8117 | ok | 0.05 | | | | | | |
| 8118 | ok | 0.04 | | | | | | |
| 8119 | ok | 0.03 | | | | | | |
| 8120 | ok | 0.06 | | | | | | |
| 8121 | ok | 0.19 | | | | | | |
| 8122 | ok | 0.07 | | | | | | |
| 8123 | ok | 0.06 | | | | | | |
| 8124 | ok | 0.04 | | | | | | |
| 8125 | ok | 0.03 | | | | | | |
| 8126 | ok | 0.07 | | | | | | |
| 8127 | ok | 0.32 | | | | | | |
| 8128 | ok | 0.11 | | | | | | |
| 8129 | ok | 0.07 | | | | | | |
| 8130 | ok | 0.04 | | | | | | |
| 8131 | ok | 0.03 | | | | | | |
| 8132 | ok | 0.08 | | | | | | |
| 8133 | ok | 0.51 | | | | | | |
| 8134 | ok | 0.14 | | | | | | |
| 8135 | ok | 0.08 | | | | | | |
| 8136 | ok | 0.05 | | | | | | |
| 8137 | ok | 0.05 | | | | | | |
| 8138 | ok | 0.14 | | | | | | |
| 8139 | ok | 0.10 | | | | | | |
| 8140 | ok | 0.07 | | | | | | |
| 8141 | ok | 0.08 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 8142 | ok | 0.14 | | | | | | |
| 8143 | ok | 0.12 | | | | | | |
| 8144 | ok | 0.10 | | | | | | |
| 8145 | ok | 0.12 | | | | | | |
| 8146 | ok | 0.24 | | | | | | |
| 8147 | ok | 0.16 | | | | | | |
| 8148 | ok | 0.13 | | | | | | |
| 8149 | ok | 0.16 | | | | | | |
| 8150 | ok | 0.36 | | | | | | |
| 8151 | ok | 0.24 | | | | | | |
| 8152 | ok | 0.19 | | | | | | |
| 8153 | ok | 0.22 | | | | | | |
| 8154 | ok | 0.58 | | | | | | |
| 8155 | ok | 0.36 | | | | | | |
| 8156 | ok | 0.27 | | | | | | |
| 8157 | ok | 0.22 | | | | | | |
| 8158 | ok | 0.58 | | | | | | |
| 8159 | ok | 0.36 | | | | | | |
| 8160 | ok | 0.27 | | | | | | |
| 8161 | ok | 0.22 | | | | | | |
| 8162 | ok | 0.54 | | | | | | |
| 8163 | ok | 0.35 | | | | | | |
| 8164 | ok | 0.27 | | | | | | |
| 8165 | ok | 0.16 | | | | | | |
| 8166 | ok | 0.33 | | | | | | |
| 8167 | ok | 0.23 | | | | | | |
| 8168 | ok | 0.19 | | | | | | |
| 8169 | ok | 0.12 | | | | | | |
| 8170 | ok | 0.22 | | | | | | |
| 8171 | ok | 0.16 | | | | | | |
| 8172 | ok | 0.13 | | | | | | |
| 8173 | ok | 0.08 | | | | | | |
| 8174 | ok | 0.12 | | | | | | |
| 8175 | ok | 0.12 | | | | | | |
| 8176 | ok | 0.10 | | | | | | |
| 8177 | ok | 0.05 | | | | | | |
| 8178 | ok | 0.17 | | | | | | |
| 8179 | ok | 0.09 | | | | | | |
| 8180 | ok | 0.07 | | | | | | |
| 8181 | ok | 0.04 | | | | | | |
| 8182 | ok | 0.06 | | | | | | |
| 8183 | ok | 0.57 | | | | | | |
| 8184 | ok | 0.17 | | | | | | |
| 8185 | ok | 0.08 | | | | | | |
| 8186 | ok | 0.05 | | | | | | |
| 8187 | ok | 0.03 | | | | | | |
| 8188 | ok | 0.08 | | | | | | |
| 8189 | ok | 0.42 | | | | | | |
| 8190 | ok | 0.15 | | | | | | |
| 8191 | ok | 0.06 | | | | | | |
| 8192 | ok | 0.04 | | | | | | |
| 8193 | ok | 0.03 | | | | | | |
| 8194 | ok | 0.09 | | | | | | |
| 8195 | ok | 0.31 | | | | | | |
| 8196 | ok | 0.12 | | | | | | |
| 8197 | ok | 0.05 | | | | | | |
| 8198 | ok | 0.04 | | | | | | |
| 8199 | ok | 0.03 | | | | | | |
| 8200 | ok | 0.10 | | | | | | |
| 8201 | ok | 0.25 | | | | | | |
| 8202 | ok | 0.08 | | | | | | |
| 8203 | ok | 0.04 | | | | | | |
| 8204 | ok | 0.04 | | | | | | |
| 8205 | ok | 0.03 | | | | | | |
| 8206 | ok | 0.11 | | | | | | |
| 8207 | ok | 0.20 | | | | | | |
| 8208 | ok | 0.06 | | | | | | |
| 8209 | ok | 0.04 | | | | | | |
| 8210 | ok | 0.04 | | | | | | |
| 8211 | ok | 0.03 | | | | | | |
| 8212 | ok | 0.12 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 8213 | ok | 0.16 | | | | | | |
| 8214 | ok | 0.05 | | | | | | |
| 8215 | ok | 0.04 | | | | | | |
| 8216 | ok | 0.04 | | | | | | |
| 8217 | ok | 0.03 | | | | | | |
| 8218 | ok | 0.12 | | | | | | |
| 8219 | ok | 0.12 | | | | | | |
| 8220 | ok | 0.08 | | | | | | |
| 8221 | ok | 0.05 | | | | | | |
| 8222 | ok | 0.04 | | | | | | |
| 8223 | ok | 0.03 | | | | | | |
| 8224 | ok | 0.13 | | | | | | |
| 8225 | ok | 0.13 | | | | | | |
| 8226 | ok | 0.11 | | | | | | |
| 8227 | ok | 0.06 | | | | | | |
| 8228 | ok | 0.04 | | | | | | |
| 8229 | ok | 0.03 | | | | | | |
| 8230 | ok | 0.12 | | | | | | |
| 8231 | ok | 0.06 | | | | | | |
| 8232 | ok | 0.04 | | | | | | |
| 8233 | ok | 0.05 | | | | | | |
| 8234 | ok | 0.18 | | | | | | |
| 8235 | ok | 0.07 | | | | | | |
| 8236 | ok | 0.06 | | | | | | |
| 8237 | ok | 0.08 | | | | | | |
| 8238 | ok | 0.25 | | | | | | |
| 8239 | ok | 0.09 | | | | | | |
| 8240 | ok | 0.08 | | | | | | |
| 8241 | ok | 0.10 | | | | | | |
| 8242 | ok | 0.32 | | | | | | |
| 8243 | ok | 0.13 | | | | | | |
| 8244 | ok | 0.11 | | | | | | |
| 8245 | ok | 0.13 | | | | | | |
| 8246 | ok | 0.43 | | | | | | |
| 8247 | ok | 0.18 | | | | | | |
| 8248 | ok | 0.14 | | | | | | |
| 8249 | ok | 0.27 | | | | | | |
| 8250 | ok | 0.55 | | | | | | |
| 8251 | ok | 0.24 | | | | | | |
| 8252 | ok | 0.18 | | | | | | |
| 8253 | ok | 0.22 | | | | | | |
| 8254 | ok | 0.44 | | | | | | |
| 8255 | ok | 0.31 | | | | | | |
| 8256 | ok | 0.22 | | | | | | |
| 8257 | ok | 0.19 | | | | | | |
| 8258 | ok | 0.44 | | | | | | |
| 8259 | ok | 0.29 | | | | | | |
| 8260 | ok | 0.22 | | | | | | |
| 8261 | ok | 0.19 | | | | | | |
| 8262 | ok | 0.44 | | | | | | |
| 8263 | ok | 0.29 | | | | | | |
| 8264 | ok | 0.22 | | | | | | |
| 8265 | ok | 0.10 | | | | | | |
| 8266 | ok | 0.30 | | | | | | |
| 8267 | ok | 0.20 | | | | | | |
| 8268 | ok | 0.14 | | | | | | |
| 8269 | ok | 0.14 | | | | | | |
| 8270 | ok | 0.30 | | | | | | |
| 8271 | ok | 0.25 | | | | | | |
| 8272 | ok | 0.18 | | | | | | |
| 8273 | ok | 0.18 | | | | | | |
| 8274 | ok | 0.43 | | | | | | |
| 8275 | ok | 0.41 | | | | | | |
| 8276 | ok | 0.24 | | | | | | |
| 8281 | ok | 0.31 | | | | | | |
| 8282 | ok | 0.29 | | | | | | |
| 8283 | ok | 0.19 | | | | | | |
| 8284 | ok | 0.18 | | | | | | |
| 8285 | ok | 0.17 | | | | | | |
| 8286 | ok | 0.15 | | | | | | |
| 8287 | ok | 0.18 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------------|-------|----------------|-----------------|------------------|----------------|-----------------|-------------|--------------|
| 8288 | ok | 0.13 | | | | | | |
| 8289 | ok | 0.21 | | | | | | |
| 8290 | ok | 0.13 | | | | | | |
| 8291 | ok | 0.30 | | | | | | |
| 8292 | ok | 0.13 | | | | | | |
| 8293 | ok | 0.37 | | | | | | |
| 8294 | ok | 0.19 | | | | | | |
| 8295 | ok | 0.13 | | | | | | |
| 8296 | ok | 0.15 | | | | | | |
| 8297 | ok | 0.21 | | | | | | |
| 8298 | ok | 0.15 | | | | | | |
| 8299 | ok | 0.13 | | | | | | |
| 8300 | ok | 0.13 | | | | | | |
| 8301 | ok | 0.17 | | | | | | |
| 8302 | ok | 0.14 | | | | | | |
| 8303 | ok | 0.10 | | | | | | |
| 8304 | ok | 0.10 | | | | | | |
| 8305 | ok | 0.12 | | | | | | |
| 8306 | ok | 0.11 | | | | | | |
| 8307 | ok | 0.08 | | | | | | |
| 8308 | ok | 0.07 | | | | | | |
| 8309 | ok | 0.09 | | | | | | |
| 8310 | ok | 0.08 | | | | | | |
| 8311 | ok | 0.06 | | | | | | |
| 8312 | ok | 0.08 | | | | | | |
| 8313 | ok | 0.07 | | | | | | |
| 8314 | ok | 0.07 | | | | | | |
| 8315 | ok | 0.05 | | | | | | |
| 8316 | ok | 0.08 | | | | | | |
| 8317 | ok | 0.09 | | | | | | |
| 8318 | ok | 0.07 | | | | | | |
| 8319 | ok | 0.07 | | | | | | |
| 8320 | ok | 0.10 | | | | | | |
| 8321 | ok | 0.15 | | | | | | |
| 8322 | ok | 0.10 | | | | | | |
| 8326 | ok | 1.00 | | | | | | |
| 8329 | ok | 0.65 | | | | | | |
| 8330 | ok | 0.33 | | | | | | |
| 8331 | ok | 0.25 | | | | | | |
| 8332 | ok | 0.23 | | | | | | |
| 8345 | ok | 0.76 | | | | | | |
| 8347 | ok | 0.55 | | | | | | |
| 8348 | ok | 0.31 | | | | | | |
| 8349 | ok | 0.22 | | | | | | |
| 8350 | ok | 0.27 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 1.18 | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 67 | 40.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|-----------|----------|--------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 1 | ok | 0.09 | 9.07e-02 | 1.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -96.7 | 3.6 | -27.3 | 48.9 | -351.3 | -99.7 |
| 2 | ok | 0.09 | 0.3 | 2.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -94.1 | -63.0 | -21.5 | 265.7 | 1711.1 | 41.2 |
| 3 | ok | 0.09 | 0.3 | 3.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.7 | -164.4 | 52.3 | -12.2 | -4.4 | 30.6 |
| 24 | ok | 0.09 | 0.2 | 9.97e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -39.2 | 23.3 | -5.6 | 88.3 | -50.7 | 74.6 |
| 25 | ok | 0.09 | 0.2 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.6 | -33.7 | 36.8 | -14.5 | -11.5 | 10.0 |
| 26 | ok | 0.09 | 0.4 | 1.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | 16.7 | 97.4 | 6.1 | 36.6 | -25.9 | -3.8 |
| 27 | ok | 0.09 | 0.2 | 6.52e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -20.2 | 43.4 | 9.3 | 70.9 | -35.3 | -23.8 |
| 28 | ok | 0.09 | 7.17e-02 | 7.14e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.8 | 14.6 | 10.9 | 2.1 | 74.2 | 2.4 |
| 29 | ok | 0.09 | 0.1 | 1.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.6 | -6.1 | -7.5 | 111.7 | 516.3 | -38.0 |
| 30 | ok | 0.09 | 0.3 | 1.98e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.5 | 12.8 | -59.8 | 6.1 | 1009.2 | 20.3 |
| 52 | ok | 0.09 | 9.90e-02 | 6.80e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -19.9 | 27.3 | 7.9 | 1.2 | 35.7 | 2.8 |
| 60 | ok | 0.09 | 0.2 | 6.80e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 11.5 | 22.4 | -11.6 | 728.4 | 338.8 | -143.8 |
| 86 | ok | 0.09 | 0.3 | 2.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -95.8 | -11.0 | -13.0 | 137.4 | 894.0 | -33.5 |
| 97 | ok | 0.09 | 7.78e-02 | 7.12e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.8 | 17.3 | 10.3 | 1.7 | 53.3 | 2.5 |
| 99 | ok | 0.09 | 8.71e-02 | 7.05e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -20.5 | 23.2 | 7.6 | 1.7 | 41.8 | 2.8 |
| 101 | ok | 0.09 | 0.2 | 7.13e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.1 | 50.6 | 8.4 | 74.1 | -37.7 | -20.4 |
| 103 | ok | 0.09 | 0.2 | 9.47e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -12.5 | 60.5 | 7.2 | 76.9 | -38.5 | -17.6 |
| 105 | ok | 0.09 | 0.3 | 1.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.0 | -47.9 | -1.0 | -51.8 | 19.1 | 2.4 |
| 107 | ok | 0.09 | 0.1 | 1.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.7 | -20.6 | -6.2 | -21.7 | 4.2 | 13.3 |
| 109 | ok | 0.09 | 0.1 | 9.56e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -43.1 | 22.6 | 2.2 | 173.8 | -95.7 | 1.7 |
| 111 | ok | 0.09 | 0.1 | 1.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.3 | 27.7 | 2.6 | 167.5 | -89.5 | 13.4 |
| 113 | ok | 0.09 | 3.49e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -73.4 | -14.5 | -15.0 | 41.9 | 38.3 | -105.5 |
| 115 | ok | 0.09 | 0.1 | 1.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.0 | -46.6 | -17.0 | 129.9 | 826.0 | -46.1 |
| 117 | ok | 0.09 | 7.13e-02 | 1.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.8 | -26.1 | -14.8 | 99.4 | 308.1 | -39.5 |
| 130 | ok | 0.09 | 9.43e-02 | 1.83e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.2 | -70.7 | 0.2 | 151.2 | 505.2 | 58.1 |
| 132 | ok | 0.09 | 6.32e-02 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.8 | -72.0 | 10.2 | 59.1 | 11.5 | 7.0 |
| 134 | ok | 0.09 | 4.45e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.8 | -63.3 | 12.4 | 50.1 | 6.2 | 6.9 |
| 136 | ok | 0.09 | 3.56e-02 | 1.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.0 | -54.9 | 9.7 | 43.4 | 1.1 | 6.2 |
| 138 | ok | 0.09 | 3.31e-02 | 1.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -20.1 | -54.9 | 18.2 | 67.5 | -15.8 | 45.8 |
| 140 | ok | 0.09 | 3.26e-02 | 1.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -19.6 | -51.2 | 15.3 | 68.6 | -18.7 | 44.9 |
| 142 | ok | 0.09 | 4.87e-02 | 1.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -18.9 | -53.1 | 13.4 | 2.9 | -1.2 | -12.8 |
| 144 | ok | 0.09 | 7.47e-02 | 1.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -23.8 | -61.7 | 17.1 | -2.99e-02 | 1.1 | -11.0 |
| 146 | ok | 0.09 | 0.1 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -27.6 | -66.4 | 17.4 | -3.1 | 0.9 | -9.2 |
| 148 | ok | 0.09 | 0.1 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.3 | -72.9 | 17.4 | -6.0 | 0.9 | -6.6 |
| 150 | ok | 0.09 | 0.2 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.4 | -82.2 | 17.3 | -8.6 | 0.9 | -2.8 |
| 152 | ok | 0.09 | 0.2 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.0 | -99.5 | 15.3 | -11.2 | 0.2 | 2.7 |
| 154 | ok | 0.09 | 0.3 | 2.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.1 | -126.4 | 16.9 | -14.0 | -2.4 | 24.8 |
| 716 | ok | 0.09 | 7.23e-02 | 7.37e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.8 | 12.3 | 11.0 | 2.8 | 95.0 | 38.8 |
| 728 | ok | 0.09 | 7.46e-02 | 8.21e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -36.3 | 7.4 | -6.1 | -51.9 | 120.3 | 52.2 |
| 740 | ok | 0.09 | 7.99e-02 | 9.72e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.8 | -11.9 | -9.0 | 107.1 | 213.4 | -66.2 |
| 752 | ok | 0.09 | 0.1 | 6.12e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -19.2 | 37.8 | 9.7 | 67.9 | -31.6 | -27.3 |
| 764 | ok | 0.09 | 0.1 | 6.06e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.8 | 36.7 | 6.2 | 64.8 | -29.4 | -28.1 |
| 776 | ok | 0.09 | 0.1 | 6.37e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.9 | 31.9 | 8.4 | 0.7 | 31.7 | 2.7 |
| 7304 | ok | 0.09 | 6.26e-02 | 4.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -157.5 | -66.9 | -63.1 | 250.3 | -172.8 | -3.6 |
| 7305 | ok | 0.09 | 0.1 | 4.50e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.8 | 30.4 | -3.3 | 214.8 | 179.1 | 33.0 |
| 7306 | ok | 0.09 | 0.2 | 3.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.1 | -58.7 | 89.2 | -5.0 | -24.6 | 9.8 |
| 7326 | ok | 0.09 | 0.1 | 1.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.1 | -21.2 | 54.4 | -1.5 | 4.07e-02 | 0.9 |
| 7327 | ok | 0.09 | 0.1 | 2.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.3 | 13.9 | -35.9 | -4.4 | -12.7 | -9.8 |
| 7328 | ok | 0.09 | 0.1 | 2.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.3 | 4.4 | 9.3 | 59.6 | 27.9 | -5.6 |
| 7329 | ok | 0.09 | 0.1 | 2.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.7 | -26.0 | -70.4 | 120.7 | -221.7 | 53.4 |
| 7330 | ok | 0.09 | 0.2 | 2.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.3 | 13.1 | 46.7 | 112.8 | 351.7 | -306.5 |
| 7331 | ok | 0.09 | 0.2 | 3.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.6 | 11.0 | 65.9 | 52.0 | 251.8 | -114.0 |
| 7332 | ok | 0.09 | 0.1 | 2.98e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.8 | -6.1 | 87.2 | -62.4 | -178.1 | 66.5 |
| 7350 | ok | 0.09 | 0.2 | 2.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.1 | 14.5 | 45.8 | 155.5 | 342.4 | -347.7 |
| 7357 | ok | 0.09 | 0.2 | 3.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -71.2 | 5.8 | 77.4 | 98.3 | 152.1 | -65.5 |
| 7358 | ok | 0.09 | 0.2 | 2.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.3 | 12.6 | 44.9 | 130.4 | 348.3 | -327.5 |
| 7359 | ok | 0.09 | 0.2 | 2.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.3 | 12.4 | 44.5 | 150.7 | 337.9 | -344.0 |
| 7360 | ok | 0.09 | 0.1 | 2.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.4 | -26.4 | -69.7 | 128.8 | -195.8 | 76.8 |
| 7361 | ok | 0.09 | 0.1 | 2.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.3 | -26.2 | -68.8 | -14.3 | -37.6 | -31.5 |
| 7362 | ok | 0.09 | 0.1 | 2.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.5 | 5.4 | 14.9 | 62.9 | 29.8 | -8.0 |
| 7363 | ok | 0.09 | 0.1 | 2.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.8 | 12.1 | -39.2 | -3.7 | -10.4 | -7.9 |
| 7364 | ok | 0.09 | 0.1 | 1.97e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.0 | -19.5 | 58.7 | -1.0 | 4.5 | -1.7 |
| 7365 | ok | 0.09 | 0.1 | 1.91e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.4 | -19.2 | 56.1 | -1.2 | 2.3 | -0.4 |
| 7366 | ok | 0.09 | 4.55e-02 | 1.98e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.5 | -8.0 | -16.1 | 217.2 | -89.8 | -73.6 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|----------|----------|-------|----------|--------|--------|
| 7367 | ok | 0.09 | 8.70e-02 | 1.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.2 | -4.0 | -26.4 | 233.5 | 256.8 | -27.4 |
| 7368 | ok | 0.09 | 4.80e-02 | 1.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.7 | -14.0 | -31.2 | 159.7 | 110.0 | -44.5 |
| 7370 | ok | 0.09 | 0.2 | 1.65e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.5 | 39.9 | 54.0 | -53.9 | -363.5 | 555.2 |
| 7371 | ok | 0.09 | 0.2 | 2.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.3 | -22.1 | 73.0 | -16.7 | -357.3 | 275.5 |
| 7372 | ok | 0.09 | 0.2 | 2.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.4 | 36.6 | -51.4 | 58.7 | 412.0 | 270.3 |
| 7373 | ok | 0.09 | 0.2 | 2.93e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.0 | 31.0 | -53.2 | 99.3 | 409.5 | 311.7 |
| 7374 | ok | 0.09 | 0.2 | 2.91e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.7 | 27.3 | -52.7 | 130.9 | 395.7 | 338.8 |
| 7375 | ok | 0.09 | 0.2 | 2.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.8 | 25.1 | -51.6 | 155.1 | 375.0 | 355.4 |
| 7376 | ok | 0.09 | 0.2 | 2.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.5 | 24.1 | -50.6 | 173.1 | 350.1 | 363.9 |
| 7377 | ok | 0.09 | 0.2 | 2.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.4 | 24.3 | -49.6 | 186.2 | 322.7 | 365.9 |
| 7378 | ok | 0.09 | 0.2 | 2.89e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.0 | -39.2 | 85.5 | 102.0 | -273.8 | -31.7 |
| 7379 | ok | 0.09 | 0.1 | 2.97e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.8 | 28.7 | -47.6 | 10.0 | 32.0 | 22.6 |
| 7380 | ok | 0.09 | 0.2 | 3.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.3 | 34.1 | -45.0 | 8.2 | 26.2 | 18.3 |
| 7381 | ok | 0.09 | 0.2 | 3.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.1 | -51.3 | 94.6 | -5.7 | -27.3 | 12.1 |
| 7382 | ok | 0.09 | 0.2 | 2.77e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.0 | 16.4 | 49.7 | 77.8 | 372.4 | -265.1 |
| 7383 | ok | 0.09 | 0.2 | 2.89e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.5 | 16.5 | 52.8 | 54.8 | 356.5 | -221.8 |
| 7384 | ok | 0.09 | 0.2 | 2.99e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.2 | 14.7 | 57.7 | 40.9 | 318.7 | -169.4 |
| 7385 | ok | 0.09 | 0.2 | 2.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.3 | 13.8 | 45.3 | 197.1 | 273.6 | -356.4 |
| 7386 | ok | 0.09 | 0.2 | 2.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.8 | 13.6 | 46.2 | 188.7 | 297.2 | -359.1 |
| 7387 | ok | 0.09 | 0.2 | 2.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.9 | 13.9 | 46.4 | 176.5 | 319.6 | -356.9 |
| 7655 | ok | 0.09 | 0.5 | 1.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -14.1 | -107.1 | 17.5 | -6.9 | -4.6 | 32.4 |
| 7656 | ok | 0.09 | 0.2 | 3.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.5 | -54.3 | 87.4 | -5.3 | -18.8 | 10.6 |
| 7657 | ok | 0.09 | 0.3 | 9.73e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 5.73e-02 | 71.7 | -4.3 | 6.3 | 6.6 | -14.4 |
| 7658 | ok | 0.09 | 0.2 | 2.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.7 | -53.6 | 80.5 | -3.8 | -13.5 | 7.6 |
| 7659 | ok | 0.09 | 0.2 | 6.13e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 0.3 | 77.0 | -6.5 | 4.2 | 6.6 | -14.3 |
| 7660 | ok | 0.09 | 0.2 | 2.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.3 | -50.1 | 73.8 | -3.5 | -11.0 | 6.7 |
| 7661 | ok | 0.09 | 0.2 | 3.89e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -0.9 | 71.3 | -5.3 | 4.3 | 8.3 | -5.5 |
| 7662 | ok | 0.09 | 0.1 | 2.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.6 | -44.6 | 67.3 | -3.2 | -8.7 | 5.8 |
| 7663 | ok | 0.09 | 0.2 | 2.07e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.2 | 66.4 | -5.0 | 4.7 | 8.4 | -3.9 |
| 7664 | ok | 0.09 | 0.1 | 2.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.5 | -38.0 | 61.5 | -2.8 | -6.5 | 4.7 |
| 7665 | ok | 0.09 | 0.2 | 7.84e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.9 | 60.6 | -6.0 | 6.2 | 6.7 | -1.9 |
| 7666 | ok | 0.09 | 0.1 | 2.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.3 | -31.3 | 57.2 | -2.4 | -4.3 | 3.5 |
| 7667 | ok | 0.09 | 0.2 | 4.74e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 24.9 | 52.5 | 21.9 | -0.1 | -11.6 | 30.0 |
| 7668 | ok | 0.09 | 0.1 | 1.90e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.9 | -25.4 | 54.7 | -1.9 | -2.2 | 2.2 |
| 7669 | ok | 0.09 | 0.3 | 4.43e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.8 | 61.8 | 1.3 | -1.4 | -40.0 | -20.5 |
| 7670 | ok | 0.09 | 0.1 | 1.98e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.7 | 13.7 | -33.0 | -5.2 | -15.0 | -11.7 |
| 7671 | ok | 0.09 | 0.2 | 3.69e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.3 | 67.4 | -1.6 | -3.3 | 11.4 | -10.2 |
| 7672 | ok | 0.09 | 0.1 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -29.6 | 7.0 | -32.5 | -7.0 | -19.5 | -15.5 |
| 7673 | ok | 0.09 | 0.2 | 3.39e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.5 | 68.6 | -1.5 | 9.69e-03 | -5.8 | -1.8 |
| 7674 | ok | 0.09 | 0.1 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.0 | -11.5 | -44.0 | -7.7 | -19.7 | -16.4 |
| 7675 | ok | 0.09 | 0.2 | 4.87e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -0.3 | 72.2 | 5.3 | 1.4 | -0.2 | -6.0 |
| 7676 | ok | 0.09 | 0.1 | 1.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.0 | -17.2 | -48.9 | -8.6 | -22.0 | -18.1 |
| 7677 | ok | 0.09 | 0.3 | 1.35e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 1.1 | 83.6 | 8.1 | 1.3 | -4.0 | -6.0 |
| 7678 | ok | 0.09 | 0.1 | 1.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -28.3 | 2.52e-02 | 3.9 | 52.8 | 24.2 | -1.7 |
| 7679 | ok | 0.09 | 0.4 | 7.63e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 25.8 | 117.9 | 23.5 | -0.7 | -15.6 | -7.1 |
| 7680 | ok | 0.09 | 0.1 | 1.98e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.0 | 2.6 | 5.4 | 56.1 | 26.1 | -3.5 |
| 7681 | ok | 0.09 | 0.2 | 4.86e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -0.2 | 66.3 | -2.2 | -5.5 | -4.4 | -13.4 |
| 7682 | ok | 0.09 | 0.1 | 1.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.9 | 11.3 | -31.7 | -6.1 | -17.2 | -13.6 |
| 7683 | ok | 0.09 | 0.1 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -84.8 | -12.8 | -28.1 | 88.1 | -441.4 | -97.0 |
| 7684 | ok | 0.09 | 7.87e-02 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -82.2 | -10.1 | -27.2 | 79.6 | -130.2 | -254.2 |
| 7685 | ok | 0.09 | 8.19e-02 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -82.5 | -7.0 | -28.3 | 78.0 | -344.8 | -63.9 |
| 7686 | ok | 0.09 | 7.02e-02 | 1.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -81.9 | -7.9 | -32.3 | 85.1 | -139.9 | -229.4 |
| 7687 | ok | 0.09 | 6.70e-02 | 1.98e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.7 | -8.1 | -29.2 | 57.7 | -283.8 | -53.2 |
| 7688 | ok | 0.09 | 6.48e-02 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -81.4 | -8.0 | -35.6 | 90.0 | -114.1 | -205.4 |
| 7689 | ok | 0.09 | 6.61e-02 | 2.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -97.3 | -16.1 | -32.8 | 40.4 | -290.1 | -40.5 |
| 7690 | ok | 0.09 | 6.26e-02 | 2.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -87.9 | -30.7 | -58.0 | 110.3 | -42.5 | -269.0 |
| 7691 | ok | 0.09 | 0.2 | 1.99e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.2 | -33.2 | -17.0 | 154.4 | 1175.8 | 30.9 |
| 7692 | ok | 0.09 | 0.2 | 1.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.2 | -1.7 | 9.3 | 148.2 | 751.9 | -79.6 |
| 7693 | ok | 0.09 | 8.69e-02 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.2 | -25.6 | -25.2 | 135.3 | 338.5 | -263.3 |
| 7694 | ok | 0.09 | 0.1 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.9 | -34.0 | -27.1 | 227.9 | 862.2 | -137.4 |
| 7695 | ok | 0.09 | 0.3 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.6 | -24.5 | -7.9 | 432.6 | 1626.7 | 83.6 |
| 7696 | ok | 0.09 | 0.1 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.8 | -55.8 | 14.3 | 212.3 | 504.7 | 288.5 |
| 7697 | ok | 0.09 | 9.53e-02 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.3 | -54.8 | 16.3 | 64.6 | 17.7 | 44.8 |
| 7698 | ok | 0.09 | 8.50e-02 | 1.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.0 | -49.4 | 18.9 | 52.3 | 9.4 | 39.4 |
| 7699 | ok | 0.09 | 7.80e-02 | 1.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.5 | -44.0 | 19.8 | 44.9 | 2.9 | 33.8 |
| 7700 | ok | 0.09 | 7.30e-02 | 1.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -20.0 | -45.5 | 21.3 | 69.5 | -13.2 | 54.5 |
| 7701 | ok | 0.09 | 6.89e-02 | 1.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -19.8 | -43.1 | 18.6 | 70.2 | -16.3 | 52.6 |
| 7702 | ok | 0.09 | 6.53e-02 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.9 | -32.6 | 14.4 | 30.4 | -8.3 | 20.5 |
| 7703 | ok | 0.09 | 6.34e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -23.1 | -49.1 | 11.1 | -2.1 | -0.7 | -11.6 |
| 7704 | ok | 0.09 | 8.57e-02 | 1.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -27.2 | -53.1 | 10.6 | -5.2 | -0.5 | -10.6 |
| 7705 | ok | 0.09 | 0.1 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.4 | -62.5 | 17.8 | -6.2 | 0.6 | -1.1 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-------|-------|-------|-------|--------|--------|
| 7706 | ok | 0.09 | 0.1 | 1.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.5 | -68.0 | 17.1 | -9.2 | 0.3 | 1.3 |
| 7707 | ok | 0.09 | 0.1 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.4 | -70.1 | 15.0 | -12.2 | -0.2 | 5.5 |
| 7708 | ok | 0.09 | 0.2 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -72.2 | -66.3 | 20.2 | -13.6 | -3.0 | 22.3 |
| 7709 | ok | 0.09 | 0.2 | 1.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.9 | -66.8 | 40.8 | -12.6 | -5.7 | 26.9 |
| 7710 | ok | 0.09 | 0.2 | 1.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -25.1 | -71.8 | 36.9 | -26.8 | -12.4 | 25.8 |
| 7711 | ok | 0.09 | 0.2 | 1.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -10.2 | -49.7 | 24.5 | -18.6 | -13.7 | 23.5 |
| 7712 | ok | 0.09 | 0.2 | 8.73e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -8.6 | -43.2 | 19.2 | -15.6 | -13.2 | 11.2 |
| 7713 | ok | 0.09 | 0.2 | 6.16e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.6 | 54.2 | -10.1 | 15.5 | 9.5 | -7.6 |
| 7714 | ok | 0.09 | 0.2 | 4.52e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -6.5 | 38.3 | -11.2 | 16.2 | 8.2 | -3.7 |
| 7715 | ok | 0.09 | 0.1 | 3.32e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -6.9 | 39.1 | -15.0 | 19.5 | 8.5 | -2.5 |
| 7716 | ok | 0.09 | 0.1 | 5.94e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.8 | 26.5 | -21.9 | 28.9 | 7.2 | 1.2 |
| 7717 | ok | 0.09 | 0.1 | 9.47e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 8.4 | 9.6 | 9.8 | 33.0 | -3.9 | 23.2 |
| 7718 | ok | 0.09 | 0.1 | 1.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.5 | 26.2 | 3.4 | 38.7 | -14.0 | -4.0 |
| 7719 | ok | 0.09 | 0.1 | 9.80e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -48.2 | 32.1 | 4.0 | 40.0 | -14.2 | -6.9 |
| 7720 | ok | 0.09 | 0.1 | 1.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.3 | 17.6 | 10.3 | -25.2 | -2.1 | 13.1 |
| 7721 | ok | 0.09 | 0.1 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | 3.8 | 30.5 | -7.5 | 20.6 | 3.1 | -11.3 |
| 7722 | ok | 0.09 | 0.2 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | 8.2 | 53.2 | 10.0 | -44.2 | -14.0 | -38.4 |
| 7723 | ok | 0.09 | 0.2 | 8.03e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 4.7 | 57.6 | 13.1 | -30.4 | -15.6 | -35.5 |
| 7724 | ok | 0.09 | 0.1 | 8.20e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -5.4 | 34.5 | 10.8 | 48.2 | -17.5 | -92.1 |
| 7725 | ok | 0.09 | 0.1 | 2.04e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.3 | 46.1 | 0.2 | 23.5 | 15.8 | -56.1 |
| 7726 | ok | 0.09 | 0.1 | 4.18e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.8 | 42.2 | 5.4 | 29.7 | 3.6 | -72.3 |
| 7727 | ok | 0.09 | 0.2 | 1.84e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.3 | 48.1 | 11.8 | 5.4 | 1.5 | -29.1 |
| 7728 | ok | 0.09 | 0.2 | 2.96e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.3 | 47.9 | 8.6 | 5.0 | 1.2 | -12.7 |
| 7729 | ok | 0.09 | 0.2 | 5.41e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 7.1 | 58.9 | 18.5 | -20.7 | -14.2 | -33.8 |
| 7730 | ok | 0.09 | 0.2 | 1.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.9 | -12.4 | -17.8 | 65.7 | -3.1 | 21.5 |
| 7731 | ok | 0.09 | 0.2 | 9.30e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.9 | 52.5 | 3.9 | 75.9 | -35.0 | -24.0 |
| 7732 | ok | 0.09 | 0.2 | 7.97e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.0 | 45.6 | 5.9 | 73.4 | -34.6 | -27.5 |
| 7733 | ok | 0.09 | 0.1 | 7.46e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -20.6 | 39.1 | 7.3 | 70.3 | -32.5 | -31.7 |
| 7734 | ok | 0.09 | 0.1 | 7.15e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -20.0 | 29.8 | 7.8 | 67.4 | -29.1 | -36.0 |
| 7735 | ok | 0.09 | 0.1 | 7.14e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -19.5 | 28.4 | 5.1 | 64.5 | -27.0 | -37.3 |
| 7736 | ok | 0.09 | 9.53e-02 | 7.37e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.8 | 26.6 | 3.6 | -49.4 | 28.7 | -4.2 |
| 7737 | ok | 0.09 | 8.21e-02 | 7.66e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.4 | -15.7 | -10.9 | 64.2 | -13.2 | -22.0 |
| 7738 | ok | 0.09 | 7.17e-02 | 7.84e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.7 | 18.4 | 3.8 | -42.5 | 38.7 | -2.9 |
| 7739 | ok | 0.09 | 7.20e-02 | 7.96e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.8 | 13.7 | 8.7 | 3.1 | 51.1 | -5.9 |
| 7740 | ok | 0.09 | 7.59e-02 | 8.12e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -36.2 | 4.7 | -5.9 | -87.6 | 86.3 | 168.5 |
| 7741 | ok | 0.09 | 8.09e-02 | 8.53e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.8 | -1.8 | -5.5 | 136.9 | 94.9 | -213.5 |
| 7742 | ok | 0.09 | 8.76e-02 | 9.42e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -37.5 | -4.6 | -9.2 | 138.4 | 180.2 | -204.0 |
| 7743 | ok | 0.09 | 9.81e-02 | 1.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.8 | -7.3 | -10.2 | 143.9 | 303.7 | -180.9 |
| 7744 | ok | 0.09 | 0.1 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.3 | -7.4 | -11.6 | 166.2 | 478.4 | -135.9 |
| 7745 | ok | 0.09 | 0.2 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -82.8 | -16.1 | -13.5 | 155.0 | 725.9 | 18.1 |
| 7746 | ok | 0.09 | 0.1 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.2 | -13.4 | -13.0 | 157.8 | 555.0 | -32.7 |
| 7747 | ok | 0.09 | 7.81e-02 | 1.74e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.1 | -17.3 | -34.1 | 151.8 | 274.7 | -261.7 |
| 7748 | ok | 0.09 | 0.1 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.8 | -21.1 | -24.7 | 223.2 | 654.4 | -176.1 |
| 7749 | ok | 0.09 | 0.2 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.6 | -23.2 | -14.8 | 307.8 | 1097.6 | 21.2 |
| 7750 | ok | 0.09 | 0.1 | 1.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.4 | -35.2 | 8.0 | 152.0 | 287.3 | 195.6 |
| 7751 | ok | 0.09 | 9.11e-02 | 1.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.5 | -37.8 | 16.9 | 52.3 | 26.0 | 56.9 |
| 7752 | ok | 0.09 | 8.27e-02 | 1.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.5 | -34.8 | 19.9 | 44.9 | 18.7 | 44.6 |
| 7753 | ok | 0.09 | 7.70e-02 | 1.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.9 | -31.6 | 20.5 | 40.0 | 9.5 | 37.5 |
| 7754 | ok | 0.09 | 7.31e-02 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.2 | -29.2 | 19.5 | 35.3 | 2.8 | 32.9 |
| 7755 | ok | 0.09 | 6.97e-02 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.2 | -27.5 | 18.2 | 30.8 | -2.5 | 29.2 |
| 7756 | ok | 0.09 | 6.66e-02 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.3 | -26.0 | 16.5 | 27.0 | -5.2 | 25.3 |
| 7757 | ok | 0.09 | 6.37e-02 | 1.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.0 | -24.6 | 14.7 | 24.0 | -6.3 | 21.4 |
| 7758 | ok | 0.09 | 6.98e-02 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.1 | -42.9 | 7.7 | -7.7 | -0.7 | -8.1 |
| 7759 | ok | 0.09 | 8.26e-02 | 1.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.5 | -45.9 | 7.3 | -10.3 | -1.0 | -6.4 |
| 7760 | ok | 0.09 | 9.27e-02 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.4 | -47.7 | 10.9 | -12.7 | -1.5 | -3.2 |
| 7761 | ok | 0.09 | 0.1 | 1.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.9 | -45.3 | 13.9 | -15.3 | -3.0 | 5.3 |
| 7762 | ok | 0.09 | 0.1 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.8 | -42.5 | 25.7 | -47.1 | -4.7 | 8.7 |
| 7763 | ok | 0.09 | 0.1 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.1 | -43.6 | 37.4 | -41.2 | -5.8 | 10.6 |
| 7764 | ok | 0.09 | 0.1 | 1.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.3 | -42.8 | 39.0 | -24.9 | -8.8 | 24.0 |
| 7765 | ok | 0.09 | 0.1 | 1.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -20.8 | -41.6 | 35.2 | -30.8 | -11.5 | 10.9 |
| 7766 | ok | 0.09 | 0.1 | 9.67e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -13.0 | -32.1 | 29.9 | -27.6 | -12.2 | 9.9 |
| 7767 | ok | 0.09 | 0.1 | 7.71e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.7 | -28.2 | 24.5 | -26.5 | -12.0 | 9.3 |
| 7768 | ok | 0.09 | 0.1 | 6.47e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -8.4 | -19.2 | 24.0 | -20.4 | -10.5 | 9.8 |
| 7769 | ok | 0.09 | 0.1 | 5.21e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -13.9 | 28.0 | -20.6 | 32.3 | 6.2 | -4.1 |
| 7770 | ok | 0.09 | 0.1 | 6.18e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -22.5 | 26.7 | -23.1 | 38.5 | 4.0 | -3.4 |
| 7771 | ok | 0.09 | 0.1 | 7.56e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.4 | 28.4 | -11.9 | 44.7 | -5.1 | -5.2 |
| 7772 | ok | 0.09 | 0.1 | 8.43e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -40.3 | 32.1 | -13.6 | 52.2 | -5.1 | -7.3 |
| 7773 | ok | 0.09 | 9.76e-02 | 9.26e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -41.8 | 27.5 | 3.6 | 155.1 | -49.6 | 3.6 |
| 7774 | ok | 0.09 | 9.44e-02 | 1.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.3 | 28.2 | 6.6 | 6.1 | -6.7 | -5.8 |
| 7775 | ok | 0.09 | 9.67e-02 | 9.36e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -40.3 | 17.0 | 26.8 | -42.4 | -9.4 | 17.9 |
| 7776 | ok | 0.09 | 0.1 | 9.62e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 7.6 | 35.0 | 10.0 | -45.3 | -11.1 | -34.4 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-------|-------|-------|-------|-------|--------|
| 7777 | ok | 0.09 | 0.1 | 8.23e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 0.9 | 34.3 | 11.1 | -29.2 | -10.6 | -33.6 |
| 7778 | ok | 0.09 | 0.1 | 7.88e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.0 | 14.6 | 29.5 | -37.7 | -10.6 | -6.9 |
| 7779 | ok | 0.09 | 0.1 | 4.09e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -14.1 | 18.6 | 20.9 | -30.5 | -12.5 | -9.2 |
| 7780 | ok | 0.09 | 0.1 | 5.56e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -16.4 | 16.6 | 26.4 | -33.3 | -12.7 | -8.2 |
| 7781 | ok | 0.09 | 0.1 | 3.66e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -6.5 | 27.4 | 9.8 | 4.6 | -0.9 | -29.3 |
| 7782 | ok | 0.09 | 0.1 | 4.94e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.2 | 36.4 | 16.4 | 2.8 | -1.8 | -16.1 |
| 7783 | ok | 0.09 | 0.1 | 6.35e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 3.0 | 33.9 | 17.6 | -35.1 | -11.1 | -31.0 |
| 7784 | ok | 0.09 | 0.1 | 1.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.9 | -5.9 | -20.1 | 65.1 | -2.2 | 14.5 |
| 7785 | ok | 0.09 | 0.1 | 9.01e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -36.8 | 21.6 | -6.4 | 152.7 | -51.9 | -82.1 |
| 7786 | ok | 0.09 | 0.1 | 8.73e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -37.7 | 17.2 | -8.3 | 153.9 | -56.3 | -102.9 |
| 7787 | ok | 0.09 | 0.1 | 8.46e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.0 | 30.4 | 2.6 | -53.0 | -7.8 | -13.5 |
| 7788 | ok | 0.09 | 9.43e-02 | 8.28e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -20.3 | 28.0 | 0.6 | -51.0 | -6.2 | -14.1 |
| 7789 | ok | 0.09 | 7.89e-02 | 8.27e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.1 | -18.0 | -8.2 | 67.0 | 2.3 | -22.4 |
| 7790 | ok | 0.09 | 7.06e-02 | 8.41e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.5 | -16.5 | -9.1 | 65.6 | -13.0 | -23.4 |
| 7791 | ok | 0.09 | 6.73e-02 | 8.61e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.0 | -14.8 | -9.7 | 64.3 | -7.1 | -23.4 |
| 7792 | ok | 0.09 | 7.02e-02 | 8.82e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.6 | 13.6 | 2.6 | -46.0 | 29.4 | -4.5 |
| 7793 | ok | 0.09 | 7.32e-02 | 9.06e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -35.4 | -0.2 | -7.6 | 138.4 | 10.8 | -206.9 |
| 7794 | ok | 0.09 | 7.62e-02 | 9.36e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -36.2 | -2.5 | -10.4 | 138.4 | 42.3 | -210.6 |
| 7795 | ok | 0.09 | 8.01e-02 | 9.87e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.1 | -5.3 | -11.3 | 139.4 | 89.4 | -208.3 |
| 7796 | ok | 0.09 | 8.48e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.7 | -7.9 | -12.1 | 142.6 | 158.2 | -195.7 |
| 7797 | ok | 0.09 | 9.10e-02 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.3 | -10.1 | -12.5 | 147.5 | 256.0 | -167.8 |
| 7798 | ok | 0.09 | 0.1 | 1.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.7 | -12.3 | -11.6 | 151.9 | 389.3 | -117.0 |
| 7799 | ok | 0.09 | 0.1 | 1.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.8 | -9.5 | -9.8 | 120.8 | 472.7 | 17.8 |
| 7800 | ok | 0.09 | 9.04e-02 | 1.68e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -67.6 | -11.8 | -12.8 | 120.6 | 386.2 | -18.6 |
| 7801 | ok | 0.09 | 7.43e-02 | 1.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.9 | -14.1 | -34.2 | 134.4 | 208.9 | -247.6 |
| 7802 | ok | 0.09 | 9.32e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.9 | -14.2 | -25.7 | 180.7 | 506.1 | -123.7 |
| 7803 | ok | 0.09 | 0.1 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.9 | -17.7 | -19.2 | 215.2 | 734.0 | 80.6 |
| 7804 | ok | 0.09 | 8.66e-02 | 9.88e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -35.5 | -21.3 | 6.7 | 106.3 | 229.0 | 175.4 |
| 7805 | ok | 0.09 | 8.36e-02 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.5 | -18.2 | 15.8 | 108.5 | 181.4 | 202.5 |
| 7806 | ok | 0.09 | 7.83e-02 | 1.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.1 | -14.2 | 19.3 | 108.9 | 108.9 | 217.3 |
| 7807 | ok | 0.09 | 7.59e-02 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.9 | -12.7 | 19.2 | 109.3 | 65.6 | 224.4 |
| 7808 | ok | 0.09 | 7.44e-02 | 1.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.5 | -15.3 | 17.5 | 30.1 | 12.8 | 36.3 |
| 7809 | ok | 0.09 | 7.26e-02 | 1.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.8 | -15.9 | 15.5 | 26.3 | 7.8 | 32.3 |
| 7810 | ok | 0.09 | 7.04e-02 | 1.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.8 | -16.2 | 13.8 | 22.9 | 4.3 | 28.1 |
| 7811 | ok | 0.09 | 6.80e-02 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.3 | -22.1 | 22.4 | 18.2 | -7.7 | 23.2 |
| 7812 | ok | 0.09 | 6.54e-02 | 1.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.2 | -21.7 | 21.6 | 16.0 | -8.6 | 19.5 |
| 7813 | ok | 0.09 | 6.25e-02 | 1.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.3 | -32.9 | 15.2 | 16.3 | -12.9 | 31.7 |
| 7814 | ok | 0.09 | 6.80e-02 | 1.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.5 | -31.7 | 17.4 | 15.4 | -12.3 | 27.3 |
| 7815 | ok | 0.09 | 7.51e-02 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.4 | -25.8 | 11.3 | 14.7 | -9.8 | 25.1 |
| 7816 | ok | 0.09 | 7.65e-02 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.4 | -28.4 | 27.4 | -50.1 | -4.6 | 7.9 |
| 7817 | ok | 0.09 | 7.66e-02 | 1.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.7 | -28.2 | 36.7 | -42.5 | -7.4 | 10.2 |
| 7818 | ok | 0.09 | 7.91e-02 | 1.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.3 | -29.0 | 39.2 | -36.0 | -7.8 | 10.8 |
| 7819 | ok | 0.09 | 8.71e-02 | 1.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -27.7 | -31.7 | 40.6 | -39.4 | -10.6 | 9.2 |
| 7820 | ok | 0.09 | 9.62e-02 | 1.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -20.2 | -28.1 | 37.4 | -37.2 | -11.0 | 8.8 |
| 7821 | ok | 0.09 | 9.93e-02 | 9.07e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.1 | -23.0 | 33.6 | -36.4 | -10.7 | 8.0 |
| 7822 | ok | 0.09 | 9.72e-02 | 8.09e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -14.3 | -17.7 | 24.4 | -37.2 | -10.4 | 7.5 |
| 7823 | ok | 0.09 | 0.1 | 6.80e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.9 | -14.1 | 23.8 | -39.4 | -9.9 | 6.7 |
| 7824 | ok | 0.09 | 0.1 | 5.87e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.8 | 20.9 | -23.9 | 43.8 | 4.1 | -6.0 |
| 7825 | ok | 0.09 | 9.74e-02 | 7.08e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.0 | 22.5 | -21.6 | 47.5 | 2.8 | -7.2 |
| 7826 | ok | 0.09 | 8.92e-02 | 8.15e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -30.0 | 16.2 | -3.0 | 51.3 | 2.0 | -9.4 |
| 7827 | ok | 0.09 | 7.40e-02 | 9.16e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -39.9 | 17.2 | 9.0 | 154.1 | -19.7 | -4.1 |
| 7828 | ok | 0.09 | 6.58e-02 | 9.71e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -39.1 | 20.6 | 3.5 | 150.6 | -18.3 | -6.3 |
| 7829 | ok | 0.09 | 7.93e-02 | 9.29e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.7 | 12.2 | 24.3 | -44.3 | -7.9 | 16.5 |
| 7830 | ok | 0.09 | 8.26e-02 | 9.04e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.3 | -4.3 | -26.9 | 50.3 | 2.3 | 12.7 |
| 7831 | ok | 0.09 | 8.89e-02 | 8.39e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.5 | -5.7 | -30.8 | 49.2 | 2.5 | 12.5 |
| 7832 | ok | 0.09 | 9.11e-02 | 8.01e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -29.0 | 11.5 | 27.8 | -38.3 | -8.6 | -7.9 |
| 7833 | ok | 0.09 | 0.1 | 5.55e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.7 | 12.8 | 21.7 | -41.6 | -11.6 | -10.2 |
| 7834 | ok | 0.09 | 9.65e-02 | 6.63e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.1 | 11.0 | 30.5 | -42.7 | -10.0 | -9.5 |
| 7835 | ok | 0.09 | 0.1 | 5.16e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -14.7 | 14.5 | 19.7 | -41.9 | -12.9 | -11.2 |
| 7836 | ok | 0.09 | 0.1 | 6.22e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.4 | 16.8 | 17.2 | -43.8 | -13.3 | -12.1 |
| 7837 | ok | 0.09 | 0.1 | 7.35e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.6 | -3.2 | -22.1 | 44.6 | 5.1 | 13.5 |
| 7838 | ok | 0.09 | 7.57e-02 | 9.49e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -42.1 | -5.2 | -24.5 | 59.3 | 0.5 | -7.8 |
| 7839 | ok | 0.09 | 7.82e-02 | 9.82e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -34.9 | 13.2 | -10.6 | 152.0 | -31.0 | -86.3 |
| 7840 | ok | 0.09 | 7.69e-02 | 9.84e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -36.4 | 12.1 | -10.7 | 155.8 | -24.3 | -106.6 |
| 7841 | ok | 0.09 | 6.93e-02 | 9.79e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -39.7 | 8.4 | -13.6 | 1.6 | -8.5 | -21.7 |
| 7842 | ok | 0.09 | 6.35e-02 | 9.75e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.9 | -15.1 | -10.7 | 66.6 | -1.4 | -20.9 |
| 7843 | ok | 0.09 | 6.63e-02 | 9.81e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.5 | -12.2 | -8.4 | 64.8 | -8.3 | -22.8 |
| 7844 | ok | 0.09 | 6.90e-02 | 9.96e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -40.5 | -0.7 | -15.3 | 137.6 | -41.9 | -164.5 |
| 7845 | ok | 0.09 | 7.22e-02 | 1.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.7 | -2.5 | -15.9 | 132.1 | -33.8 | -178.8 |
| 7846 | ok | 0.09 | 7.44e-02 | 1.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.8 | -4.3 | -17.1 | 126.4 | -25.7 | -188.5 |
| 7847 | ok | 0.09 | 7.66e-02 | 1.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.8 | -1.7 | -5.2 | 132.6 | 47.9 | -204.5 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|---------|---------|----------|---------|---------|---------|
| 7848 | ok | 0.09 | 7.80e-02 | 1.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.7 | -3.7 | -6.4 | 127.3 | 67.4 | -206.0 |
| 7849 | ok | 0.09 | 8.01e-02 | 1.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.1 | -5.9 | -6.9 | 124.1 | 101.9 | -200.5 |
| 7850 | ok | 0.09 | 8.20e-02 | 1.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.7 | -7.9 | -6.9 | 122.4 | 149.6 | -184.1 |
| 7851 | ok | 0.09 | 8.36e-02 | 1.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.9 | -9.9 | -6.6 | 121.6 | 215.2 | -150.7 |
| 7852 | ok | 0.09 | 8.55e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.0 | -11.5 | -6.2 | 120.7 | 299.0 | -93.3 |
| 7853 | ok | 0.09 | 7.84e-02 | 2.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.7 | -15.6 | -48.5 | 60.2 | 310.7 | 29.0 |
| 7854 | ok | 0.09 | 0.1 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.6 | -7.9 | 0.3 | 80.4 | 253.7 | -9.2 |
| 7855 | ok | 0.09 | 6.98e-02 | 1.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.6 | -21.1 | -40.6 | 147.2 | 140.2 | -247.6 |
| 7856 | ok | 0.09 | 7.62e-02 | 1.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.7 | -9.3 | -25.7 | 168.1 | 342.6 | -100.3 |
| 7857 | ok | 0.09 | 6.85e-02 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -27.4 | -2.9 | -17.9 | 162.0 | 370.6 | 78.7 |
| 7858 | ok | 0.09 | 7.52e-02 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -20.4 | -1.9 | 8.8 | 139.2 | 201.4 | 136.7 |
| 7859 | ok | 0.09 | 0.1 | 1.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -27.9 | 2.9 | 16.0 | 75.9 | 162.0 | 194.2 |
| 7860 | ok | 0.09 | 9.17e-02 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.8 | 18.9 | -4.9 | 52.8 | 260.0 | 166.4 |
| 7861 | ok | 0.09 | 9.72e-02 | 2.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.5 | 15.3 | -9.9 | 94.6 | 246.3 | 213.0 |
| 7862 | ok | 0.09 | 0.1 | 2.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.2 | 11.5 | -13.7 | 115.0 | 235.4 | 233.4 |
| 7863 | ok | 0.09 | 0.1 | 2.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.2 | 8.7 | -15.6 | 131.8 | 222.4 | 242.8 |
| 7864 | ok | 0.09 | 0.1 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.0 | 7.2 | -16.4 | 146.1 | 207.7 | 245.0 |
| 7865 | ok | 0.09 | 0.1 | 2.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.5 | 6.6 | -16.6 | 157.8 | 191.9 | 242.2 |
| 7866 | ok | 0.09 | 0.1 | 2.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.0 | 4.3 | -16.7 | 17.7 | 26.8 | 24.3 |
| 7867 | ok | 0.09 | 0.1 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.6 | 5.9 | -16.3 | 15.3 | 21.4 | 20.4 |
| 7868 | ok | 0.09 | 9.72e-02 | 2.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.7 | -22.9 | 18.1 | 12.6 | -7.4 | 29.3 |
| 7869 | ok | 0.09 | 9.25e-02 | 2.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.0 | -22.6 | 21.3 | 11.8 | -5.7 | 25.9 |
| 7870 | ok | 0.09 | 0.1 | 2.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.6 | -22.3 | 26.9 | 10.9 | -5.3 | 23.6 |
| 7871 | ok | 0.09 | 9.50e-02 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.2 | -21.3 | 35.1 | 9.9 | -4.4 | 22.1 |
| 7872 | ok | 0.09 | 0.1 | 2.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.9 | -20.7 | 41.8 | 9.1 | -3.8 | 21.6 |
| 7873 | ok | 0.09 | 0.1 | 2.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -29.5 | -15.8 | 33.8 | -39.7 | -7.7 | 8.6 |
| 7874 | ok | 0.09 | 0.1 | 1.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -27.7 | -22.2 | 39.1 | -37.5 | -9.1 | 8.2 |
| 7875 | ok | 0.09 | 0.1 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -22.1 | -20.0 | 35.9 | -36.7 | -9.2 | 7.8 |
| 7876 | ok | 0.09 | 0.1 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -20.7 | -22.3 | 50.2 | -45.3 | -10.8 | 9.6 |
| 7877 | ok | 0.09 | 0.1 | 1.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -19.5 | -18.3 | 45.2 | -46.4 | -9.4 | 9.6 |
| 7878 | ok | 0.09 | 0.1 | 1.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -18.6 | -7.4 | 6.7 | -48.4 | -9.4 | 8.0 |
| 7879 | ok | 0.09 | 0.1 | 1.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -28.3 | 14.6 | -36.2 | 50.2 | 4.6 | -11.0 |
| 7880 | ok | 0.09 | 0.1 | 1.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.2 | 14.5 | -33.2 | 51.7 | 3.3 | -12.4 |
| 7881 | ok | 0.09 | 9.50e-02 | 1.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.8 | 10.5 | 6.69e-02 | 164.7 | 4.7 | 23.2 |
| 7882 | ok | 0.09 | 8.69e-02 | 1.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.2 | 6.8 | 14.0 | 162.9 | 5.8 | -28.4 |
| 7883 | ok | 0.09 | 9.16e-02 | 1.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.0 | 2.7 | 21.3 | 19.7 | 1.0 | 2.7 |
| 7884 | ok | 0.09 | 9.64e-02 | 1.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.5 | -11.4 | -44.7 | 55.8 | -5.7 | -9.8 |
| 7885 | ok | 0.09 | 0.1 | 1.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.5 | -10.3 | -45.9 | 52.6 | -3.9 | -7.2 |
| 7886 | ok | 0.09 | 0.1 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.1 | 7.2 | 20.0 | 6.9 | -2.1 | -13.2 |
| 7887 | ok | 0.09 | 0.1 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -18.5 | 6.0 | 22.1 | -42.5 | -11.3 | -10.5 |
| 7888 | ok | 0.09 | 0.1 | 1.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -23.4 | 5.7 | 23.5 | -43.9 | -10.9 | -9.9 |
| 7889 | ok | 0.09 | 0.1 | 9.51e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -19.8 | 6.9 | 7.5 | -52.4 | -18.4 | -13.4 |
| 7890 | ok | 0.09 | 0.1 | 1.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -14.5 | 9.6 | 38.2 | -51.0 | -2.6 | -9.8 |
| 7891 | ok | 0.09 | 0.1 | 1.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -12.7 | 12.2 | 34.1 | -53.3 | -1.2 | -9.4 |
| 7892 | ok | 0.09 | 8.69e-02 | 1.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.2 | -12.1 | -41.8 | 58.8 | -7.5 | -13.0 |
| 7893 | ok | 0.09 | 8.86e-02 | 1.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.1 | -2.9 | -11.6 | 62.6 | 5.4 | -11.8 |
| 7894 | ok | 0.09 | 9.33e-02 | 1.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.0 | -4.0 | -7.1 | 65.0 | 5.3 | -14.9 |
| 7895 | ok | 0.09 | 9.75e-02 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.4 | 12.4 | 21.0 | -183.4 | -98.5 | 186.1 |
| 7896 | ok | 0.09 | 0.1 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.4 | -11.7 | -42.9 | 126.9 | -150.0 | -41.7 |
| 7897 | ok | 0.09 | 0.1 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.8 | -13.1 | -43.4 | 118.6 | -161.3 | -61.7 |
| 7898 | ok | 0.09 | 0.1 | 1.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.8 | 1.6 | -4.7 | 145.2 | 46.4 | -181.5 |
| 7899 | ok | 0.09 | 0.1 | 1.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.7 | 7.8 | 25.1 | -174.0 | -131.8 | 222.3 |
| 7900 | ok | 0.09 | 0.1 | 1.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.9 | 6.1 | 23.7 | -165.9 | -138.7 | 226.8 |
| 7901 | ok | 0.09 | 0.1 | 1.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.1 | 4.9 | 24.2 | -159.6 | -144.0 | 232.0 |
| 7902 | ok | 0.09 | 0.1 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.4 | 3.8 | 22.0 | -142.3 | -157.6 | 234.3 |
| 7903 | ok | 0.09 | 0.1 | 1.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.3 | 3.7 | 24.8 | -131.4 | -165.1 | 238.7 |
| 7904 | ok | 0.09 | 0.1 | 2.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.0 | 2.5 | 26.9 | -114.8 | -172.4 | 242.2 |
| 7905 | ok | 0.09 | 0.1 | 2.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.7 | -1.9 | 31.6 | -160.7 | -333.7 | 364.1 |
| 7906 | ok | 0.09 | 0.1 | 2.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.1 | -8.1 | -3.0 | 76.7 | 208.4 | -83.7 |
| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | | | | | | | | -157.51 | -164.40 | -70.45 | -183.39 | -441.38 | -359.08 |
| | | 0.09 | 0.46 | 0.04 | 4.52 | 4.52 | 4.00 | 4.00 | 25.84 | 117.88 | 94.56 | 728.37 | 1711.12 | 555.22 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 1 | ok | 0.88 | | | | | | |
| 2 | ok | 0.98 | | | | | | |
| 3 | ok | 0.17 | | | | | | |
| 24 | ok | 0.24 | | | | | | |
| 25 | ok | 0.24 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 26 | ok | 0.18 | | | | | | |
| 27 | ok | 0.19 | | | | | | |
| 28 | ok | 0.38 | | | | | | |
| 29 | ok | 0.68 | | | | | | |
| 30 | ok | 0.86 | | | | | | |
| 52 | ok | 0.29 | | | | | | |
| 60 | ok | 0.39 | | | | | | |
| 86 | ok | 0.86 | | | | | | |
| 97 | ok | 0.35 | | | | | | |
| 99 | ok | 0.32 | | | | | | |
| 101 | ok | 0.16 | | | | | | |
| 103 | ok | 0.13 | | | | | | |
| 105 | ok | 0.17 | | | | | | |
| 107 | ok | 0.22 | | | | | | |
| 109 | ok | 0.09 | | | | | | |
| 111 | ok | 0.23 | | | | | | |
| 113 | ok | 0.88 | | | | | | |
| 115 | ok | 0.98 | | | | | | |
| 117 | ok | 0.74 | | | | | | |
| 130 | ok | 0.71 | | | | | | |
| 132 | ok | 0.53 | | | | | | |
| 134 | ok | 0.46 | | | | | | |
| 136 | ok | 0.41 | | | | | | |
| 138 | ok | 0.38 | | | | | | |
| 140 | ok | 0.34 | | | | | | |
| 142 | ok | 0.31 | | | | | | |
| 144 | ok | 0.28 | | | | | | |
| 146 | ok | 0.25 | | | | | | |
| 148 | ok | 0.23 | | | | | | |
| 150 | ok | 0.20 | | | | | | |
| 152 | ok | 0.17 | | | | | | |
| 154 | ok | 0.14 | | | | | | |
| 716 | ok | 0.42 | | | | | | |
| 728 | ok | 0.47 | | | | | | |
| 740 | ok | 0.54 | | | | | | |
| 752 | ok | 0.21 | | | | | | |
| 764 | ok | 0.24 | | | | | | |
| 776 | ok | 0.26 | | | | | | |
| 7304 | ok | 0.36 | | | | | | |
| 7305 | ok | 0.39 | | | | | | |
| 7306 | ok | 0.08 | | | | | | |
| 7326 | ok | 0.04 | | | | | | |
| 7327 | ok | 0.04 | | | | | | |
| 7328 | ok | 0.07 | | | | | | |
| 7329 | ok | 0.10 | | | | | | |
| 7330 | ok | 0.16 | | | | | | |
| 7331 | ok | 0.22 | | | | | | |
| 7332 | ok | 0.33 | | | | | | |
| 7350 | ok | 0.14 | | | | | | |
| 7357 | ok | 0.33 | | | | | | |
| 7358 | ok | 0.16 | | | | | | |
| 7359 | ok | 0.15 | | | | | | |
| 7360 | ok | 0.09 | | | | | | |
| 7361 | ok | 0.08 | | | | | | |
| 7362 | ok | 0.07 | | | | | | |
| 7363 | ok | 0.04 | | | | | | |
| 7364 | ok | 0.04 | | | | | | |
| 7365 | ok | 0.04 | | | | | | |
| 7366 | ok | 0.36 | | | | | | |
| 7367 | ok | 0.19 | | | | | | |
| 7368 | ok | 0.13 | | | | | | |
| 7370 | ok | 0.22 | | | | | | |
| 7371 | ok | 0.22 | | | | | | |
| 7372 | ok | 0.21 | | | | | | |
| 7373 | ok | 0.21 | | | | | | |
| 7374 | ok | 0.20 | | | | | | |
| 7375 | ok | 0.19 | | | | | | |
| 7376 | ok | 0.18 | | | | | | |
| 7377 | ok | 0.16 | | | | | | |
| 7378 | ok | 0.15 | | | | | | |
| 7379 | ok | 0.13 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 7380 | ok | 0.11 | | | | | | |
| 7381 | ok | 0.10 | | | | | | |
| 7382 | ok | 0.17 | | | | | | |
| 7383 | ok | 0.17 | | | | | | |
| 7384 | ok | 0.18 | | | | | | |
| 7385 | ok | 0.11 | | | | | | |
| 7386 | ok | 0.12 | | | | | | |
| 7387 | ok | 0.13 | | | | | | |
| 7655 | ok | 0.17 | | | | | | |
| 7656 | ok | 0.07 | | | | | | |
| 7657 | ok | 0.10 | | | | | | |
| 7658 | ok | 0.07 | | | | | | |
| 7659 | ok | 0.06 | | | | | | |
| 7660 | ok | 0.06 | | | | | | |
| 7661 | ok | 0.09 | | | | | | |
| 7662 | ok | 0.06 | | | | | | |
| 7663 | ok | 0.14 | | | | | | |
| 7664 | ok | 0.05 | | | | | | |
| 7665 | ok | 0.19 | | | | | | |
| 7666 | ok | 0.05 | | | | | | |
| 7667 | ok | 0.24 | | | | | | |
| 7668 | ok | 0.04 | | | | | | |
| 7669 | ok | 0.24 | | | | | | |
| 7670 | ok | 0.04 | | | | | | |
| 7671 | ok | 0.12 | | | | | | |
| 7672 | ok | 0.05 | | | | | | |
| 7673 | ok | 0.09 | | | | | | |
| 7674 | ok | 0.05 | | | | | | |
| 7675 | ok | 0.08 | | | | | | |
| 7676 | ok | 0.06 | | | | | | |
| 7677 | ok | 0.12 | | | | | | |
| 7678 | ok | 0.06 | | | | | | |
| 7679 | ok | 0.18 | | | | | | |
| 7680 | ok | 0.06 | | | | | | |
| 7681 | ok | 0.17 | | | | | | |
| 7682 | ok | 0.05 | | | | | | |
| 7683 | ok | 0.81 | | | | | | |
| 7684 | ok | 0.81 | | | | | | |
| 7685 | ok | 0.54 | | | | | | |
| 7686 | ok | 0.54 | | | | | | |
| 7687 | ok | 0.46 | | | | | | |
| 7688 | ok | 0.46 | | | | | | |
| 7689 | ok | 0.40 | | | | | | |
| 7690 | ok | 0.40 | | | | | | |
| 7691 | ok | 0.86 | | | | | | |
| 7692 | ok | 0.86 | | | | | | |
| 7693 | ok | 0.74 | | | | | | |
| 7694 | ok | 0.98 | | | | | | |
| 7695 | ok | 0.98 | | | | | | |
| 7696 | ok | 0.71 | | | | | | |
| 7697 | ok | 0.53 | | | | | | |
| 7698 | ok | 0.46 | | | | | | |
| 7699 | ok | 0.41 | | | | | | |
| 7700 | ok | 0.38 | | | | | | |
| 7701 | ok | 0.34 | | | | | | |
| 7702 | ok | 0.31 | | | | | | |
| 7703 | ok | 0.28 | | | | | | |
| 7704 | ok | 0.25 | | | | | | |
| 7705 | ok | 0.23 | | | | | | |
| 7706 | ok | 0.20 | | | | | | |
| 7707 | ok | 0.17 | | | | | | |
| 7708 | ok | 0.13 | | | | | | |
| 7709 | ok | 0.11 | | | | | | |
| 7710 | ok | 0.11 | | | | | | |
| 7711 | ok | 0.07 | | | | | | |
| 7712 | ok | 0.06 | | | | | | |
| 7713 | ok | 0.09 | | | | | | |
| 7714 | ok | 0.14 | | | | | | |
| 7715 | ok | 0.19 | | | | | | |
| 7716 | ok | 0.23 | | | | | | |
| 7717 | ok | 0.23 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 7718 | ok | 0.12 | | | | | | |
| 7719 | ok | 0.08 | | | | | | |
| 7720 | ok | 0.11 | | | | | | |
| 7721 | ok | 0.21 | | | | | | |
| 7722 | ok | 0.14 | | | | | | |
| 7723 | ok | 0.14 | | | | | | |
| 7724 | ok | 0.21 | | | | | | |
| 7725 | ok | 0.12 | | | | | | |
| 7726 | ok | 0.17 | | | | | | |
| 7727 | ok | 0.08 | | | | | | |
| 7728 | ok | 0.06 | | | | | | |
| 7729 | ok | 0.09 | | | | | | |
| 7730 | ok | 0.10 | | | | | | |
| 7731 | ok | 0.13 | | | | | | |
| 7732 | ok | 0.16 | | | | | | |
| 7733 | ok | 0.19 | | | | | | |
| 7734 | ok | 0.21 | | | | | | |
| 7735 | ok | 0.24 | | | | | | |
| 7736 | ok | 0.26 | | | | | | |
| 7737 | ok | 0.29 | | | | | | |
| 7738 | ok | 0.32 | | | | | | |
| 7739 | ok | 0.35 | | | | | | |
| 7740 | ok | 0.38 | | | | | | |
| 7741 | ok | 0.42 | | | | | | |
| 7742 | ok | 0.47 | | | | | | |
| 7743 | ok | 0.54 | | | | | | |
| 7744 | ok | 0.68 | | | | | | |
| 7745 | ok | 0.45 | | | | | | |
| 7746 | ok | 0.45 | | | | | | |
| 7747 | ok | 0.55 | | | | | | |
| 7748 | ok | 0.73 | | | | | | |
| 7749 | ok | 0.73 | | | | | | |
| 7750 | ok | 0.43 | | | | | | |
| 7751 | ok | 0.27 | | | | | | |
| 7752 | ok | 0.19 | | | | | | |
| 7753 | ok | 0.14 | | | | | | |
| 7754 | ok | 0.10 | | | | | | |
| 7755 | ok | 0.08 | | | | | | |
| 7756 | ok | 0.06 | | | | | | |
| 7757 | ok | 0.06 | | | | | | |
| 7758 | ok | 0.05 | | | | | | |
| 7759 | ok | 0.05 | | | | | | |
| 7760 | ok | 0.05 | | | | | | |
| 7761 | ok | 0.05 | | | | | | |
| 7762 | ok | 0.06 | | | | | | |
| 7763 | ok | 0.07 | | | | | | |
| 7764 | ok | 0.07 | | | | | | |
| 7765 | ok | 0.07 | | | | | | |
| 7766 | ok | 0.06 | | | | | | |
| 7767 | ok | 0.06 | | | | | | |
| 7768 | ok | 0.07 | | | | | | |
| 7769 | ok | 0.07 | | | | | | |
| 7770 | ok | 0.07 | | | | | | |
| 7771 | ok | 0.07 | | | | | | |
| 7772 | ok | 0.06 | | | | | | |
| 7773 | ok | 0.05 | | | | | | |
| 7774 | ok | 0.06 | | | | | | |
| 7775 | ok | 0.07 | | | | | | |
| 7776 | ok | 0.08 | | | | | | |
| 7777 | ok | 0.08 | | | | | | |
| 7778 | ok | 0.08 | | | | | | |
| 7779 | ok | 0.07 | | | | | | |
| 7780 | ok | 0.08 | | | | | | |
| 7781 | ok | 0.06 | | | | | | |
| 7782 | ok | 0.06 | | | | | | |
| 7783 | ok | 0.07 | | | | | | |
| 7784 | ok | 0.06 | | | | | | |
| 7785 | ok | 0.06 | | | | | | |
| 7786 | ok | 0.05 | | | | | | |
| 7787 | ok | 0.05 | | | | | | |
| 7788 | ok | 0.05 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 7789 | ok | 0.06 | | | | | | |
| 7790 | ok | 0.06 | | | | | | |
| 7791 | ok | 0.07 | | | | | | |
| 7792 | ok | 0.07 | | | | | | |
| 7793 | ok | 0.09 | | | | | | |
| 7794 | ok | 0.11 | | | | | | |
| 7795 | ok | 0.15 | | | | | | |
| 7796 | ok | 0.19 | | | | | | |
| 7797 | ok | 0.26 | | | | | | |
| 7798 | ok | 0.35 | | | | | | |
| 7799 | ok | 0.38 | | | | | | |
| 7800 | ok | 0.38 | | | | | | |
| 7801 | ok | 0.41 | | | | | | |
| 7802 | ok | 0.50 | | | | | | |
| 7803 | ok | 0.50 | | | | | | |
| 7804 | ok | 0.29 | | | | | | |
| 7805 | ok | 0.18 | | | | | | |
| 7806 | ok | 0.14 | | | | | | |
| 7807 | ok | 0.09 | | | | | | |
| 7808 | ok | 0.05 | | | | | | |
| 7809 | ok | 0.03 | | | | | | |
| 7810 | ok | 0.03 | | | | | | |
| 7811 | ok | 0.04 | | | | | | |
| 7812 | ok | 0.04 | | | | | | |
| 7813 | ok | 0.05 | | | | | | |
| 7814 | ok | 0.05 | | | | | | |
| 7815 | ok | 0.05 | | | | | | |
| 7816 | ok | 0.05 | | | | | | |
| 7817 | ok | 0.06 | | | | | | |
| 7818 | ok | 0.06 | | | | | | |
| 7819 | ok | 0.06 | | | | | | |
| 7820 | ok | 0.06 | | | | | | |
| 7821 | ok | 0.06 | | | | | | |
| 7822 | ok | 0.06 | | | | | | |
| 7823 | ok | 0.07 | | | | | | |
| 7824 | ok | 0.07 | | | | | | |
| 7825 | ok | 0.07 | | | | | | |
| 7826 | ok | 0.06 | | | | | | |
| 7827 | ok | 0.06 | | | | | | |
| 7828 | ok | 0.06 | | | | | | |
| 7829 | ok | 0.07 | | | | | | |
| 7830 | ok | 0.07 | | | | | | |
| 7831 | ok | 0.07 | | | | | | |
| 7832 | ok | 0.07 | | | | | | |
| 7833 | ok | 0.06 | | | | | | |
| 7834 | ok | 0.07 | | | | | | |
| 7835 | ok | 0.06 | | | | | | |
| 7836 | ok | 0.06 | | | | | | |
| 7837 | ok | 0.07 | | | | | | |
| 7838 | ok | 0.06 | | | | | | |
| 7839 | ok | 0.06 | | | | | | |
| 7840 | ok | 0.06 | | | | | | |
| 7841 | ok | 0.05 | | | | | | |
| 7842 | ok | 0.05 | | | | | | |
| 7843 | ok | 0.05 | | | | | | |
| 7844 | ok | 0.05 | | | | | | |
| 7845 | ok | 0.05 | | | | | | |
| 7846 | ok | 0.05 | | | | | | |
| 7847 | ok | 0.04 | | | | | | |
| 7848 | ok | 0.06 | | | | | | |
| 7849 | ok | 0.09 | | | | | | |
| 7850 | ok | 0.14 | | | | | | |
| 7851 | ok | 0.20 | | | | | | |
| 7852 | ok | 0.27 | | | | | | |
| 7853 | ok | 0.37 | | | | | | |
| 7854 | ok | 0.37 | | | | | | |
| 7855 | ok | 0.27 | | | | | | |
| 7856 | ok | 0.29 | | | | | | |
| 7857 | ok | 0.29 | | | | | | |
| 7858 | ok | 0.28 | | | | | | |
| 7859 | ok | 0.19 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 7860 | ok | 0.17 | | | | | | |
| 7861 | ok | 0.10 | | | | | | |
| 7862 | ok | 0.06 | | | | | | |
| 7863 | ok | 0.04 | | | | | | |
| 7864 | ok | 0.03 | | | | | | |
| 7865 | ok | 0.04 | | | | | | |
| 7866 | ok | 0.04 | | | | | | |
| 7867 | ok | 0.05 | | | | | | |
| 7868 | ok | 0.05 | | | | | | |
| 7869 | ok | 0.05 | | | | | | |
| 7870 | ok | 0.05 | | | | | | |
| 7871 | ok | 0.06 | | | | | | |
| 7872 | ok | 0.06 | | | | | | |
| 7873 | ok | 0.06 | | | | | | |
| 7874 | ok | 0.06 | | | | | | |
| 7875 | ok | 0.06 | | | | | | |
| 7876 | ok | 0.06 | | | | | | |
| 7877 | ok | 0.06 | | | | | | |
| 7878 | ok | 0.06 | | | | | | |
| 7879 | ok | 0.06 | | | | | | |
| 7880 | ok | 0.06 | | | | | | |
| 7881 | ok | 0.06 | | | | | | |
| 7882 | ok | 0.06 | | | | | | |
| 7883 | ok | 0.06 | | | | | | |
| 7884 | ok | 0.06 | | | | | | |
| 7885 | ok | 0.06 | | | | | | |
| 7886 | ok | 0.06 | | | | | | |
| 7887 | ok | 0.06 | | | | | | |
| 7888 | ok | 0.06 | | | | | | |
| 7889 | ok | 0.06 | | | | | | |
| 7890 | ok | 0.06 | | | | | | |
| 7891 | ok | 0.06 | | | | | | |
| 7892 | ok | 0.06 | | | | | | |
| 7893 | ok | 0.06 | | | | | | |
| 7894 | ok | 0.06 | | | | | | |
| 7895 | ok | 0.05 | | | | | | |
| 7896 | ok | 0.05 | | | | | | |
| 7897 | ok | 0.05 | | | | | | |
| 7898 | ok | 0.05 | | | | | | |
| 7899 | ok | 0.05 | | | | | | |
| 7900 | ok | 0.05 | | | | | | |
| 7901 | ok | 0.06 | | | | | | |
| 7902 | ok | 0.08 | | | | | | |
| 7903 | ok | 0.10 | | | | | | |
| 7904 | ok | 0.14 | | | | | | |
| 7905 | ok | 0.18 | | | | | | |
| 7906 | ok | 0.23 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 0.98 | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 68 | 40.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|--------|--------|----------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 22 | ok | 0.09 | 0.3 | 3.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -74.8 | -46.2 | 93.2 | 46.5 | 507.2 | 6.06e-02 |
| 23 | ok | 0.09 | 0.1 | 2.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -90.8 | -23.7 | 24.2 | -71.0 | 261.2 | -122.6 |
| 43 | ok | 0.09 | 0.2 | 3.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.8 | -123.1 | 60.2 | -68.0 | -973.3 | 59.5 |
| 44 | ok | 0.09 | 6.76e-02 | 8.87e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.9 | -16.0 | -12.1 | -106.6 | 36.2 | 184.3 |
| 45 | ok | 0.09 | 6.71e-02 | 7.37e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.0 | 11.4 | 9.1 | 6.2 | -1.1 | 5.3 |
| 46 | ok | 0.09 | 7.01e-02 | 7.71e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.9 | 15.1 | 8.4 | -140.7 | 12.5 | 16.2 |
| 47 | ok | 0.09 | 9.19e-02 | 7.67e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.5 | 23.7 | -9.7 | -143.7 | 12.9 | -14.1 |
| 48 | ok | 0.09 | 0.1 | 9.60e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -41.6 | 32.6 | 8.9 | -147.3 | 25.5 | -9.0 |
| 49 | ok | 0.09 | 0.3 | 7.98e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 0.5 | 93.1 | 3.9 | -179.8 | -36.5 | -254.9 |
| 50 | ok | 0.09 | 6.10e-02 | 8.26e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -34.3 | 11.8 | -7.1 | -139.2 | 23.3 | 11.7 |
| 4786 | ok | 0.09 | 6.93e-02 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.1 | -22.4 | -9.8 | -106.9 | 47.9 | 201.3 |
| 4965 | ok | 0.09 | 5.76e-02 | 1.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.3 | -28.0 | -7.6 | -89.7 | -61.0 | 202.4 |
| 4998 | ok | 0.09 | 5.61e-02 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.0 | -33.2 | -6.2 | -88.8 | -87.7 | 202.3 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|----------|-----------|---------|-----------|---------|
| 5026 | ok | 0.09 | 0.3 | 2.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -15.7 | 21.9 | -59.5 | -77.3 | 587.3 | -119.8 |
| 5043 | ok | 0.09 | 0.1 | 1.90e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -93.7 | -32.3 | 10.1 | -129.0 | 473.6 | -159.7 |
| 5060 | ok | 0.09 | 8.55e-02 | 2.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -93.5 | -30.5 | 7.6 | -126.9 | 385.4 | -157.0 |
| 5102 | ok | 0.09 | 0.2 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.7 | 50.4 | 6.0 | -205.9 | 47.7 | -34.0 |
| 5119 | ok | 0.09 | 0.2 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.4 | 44.3 | 2.9 | -179.8 | 66.8 | -34.4 |
| 5136 | ok | 0.09 | 0.2 | 1.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.4 | 39.6 | 2.5 | -172.6 | 64.5 | -29.9 |
| 5153 | ok | 0.09 | 0.2 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.8 | 35.9 | 2.6 | -169.3 | 59.6 | -25.7 |
| 5170 | ok | 0.09 | 0.1 | 1.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.6 | 32.9 | 3.0 | -167.2 | 53.5 | -21.5 |
| 5187 | ok | 0.09 | 0.1 | 1.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.3 | 30.9 | 4.1 | -164.1 | 45.9 | -17.0 |
| 5204 | ok | 0.09 | 0.1 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.1 | 30.5 | 6.3 | -157.8 | 36.3 | -12.6 |
| 5261 | ok | 0.09 | 8.32e-02 | 9.55e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -40.6 | 18.9 | -8.4 | -152.6 | 19.6 | -11.3 |
| 5278 | ok | 0.09 | 7.74e-02 | 1.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.8 | 15.3 | -6.4 | -157.4 | 25.1 | -7.8 |
| 5295 | ok | 0.09 | 7.38e-02 | 1.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.3 | 13.0 | -4.8 | -158.9 | 28.9 | -4.4 |
| 5312 | ok | 0.09 | 7.09e-02 | 1.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.7 | 11.4 | -3.7 | -158.6 | 30.8 | -1.4 |
| 5329 | ok | 0.09 | 6.85e-02 | 1.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.8 | 10.4 | 1.0 | -157.9 | 31.3 | 1.5 |
| 5346 | ok | 0.09 | 6.64e-02 | 1.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.7 | 9.7 | 2.0 | -157.7 | 30.6 | 4.0 |
| 5363 | ok | 0.09 | 6.46e-02 | 1.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.3 | 9.6 | 3.2 | -157.2 | 28.5 | 6.9 |
| 5380 | ok | 0.09 | 6.68e-02 | 1.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.9 | 10.2 | 4.8 | -155.1 | 24.7 | 10.2 |
| 5397 | ok | 0.09 | 6.73e-02 | 9.55e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -41.0 | 11.9 | 6.9 | -149.8 | 19.1 | 13.6 |
| 5457 | ok | 0.09 | 6.44e-02 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.3 | -39.1 | -5.2 | -87.4 | -129.8 | 199.5 |
| 5474 | ok | 0.09 | 8.01e-02 | 1.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.1 | -47.0 | -4.7 | -86.5 | -192.1 | 192.7 |
| 5491 | ok | 0.09 | 0.1 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.1 | -59.8 | -5.1 | -89.2 | -282.4 | 182.3 |
| 5508 | ok | 0.09 | 0.2 | 1.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.4 | -82.9 | -6.4 | -111.1 | -442.8 | 152.0 |
| 5563 | ok | 0.09 | 5.62e-02 | 1.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.9 | 7.9 | -5.0 | -146.8 | 32.1 | 15.1 |
| 5580 | ok | 0.09 | 5.39e-02 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.2 | 5.7 | -2.8 | -150.1 | 39.3 | 19.1 |
| 5597 | ok | 0.09 | 5.29e-02 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.1 | 4.7 | -1.2 | -150.1 | 44.7 | 22.9 |
| 5614 | ok | 0.09 | 5.21e-02 | 1.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.0 | 4.2 | -5.29e-02 | -148.5 | 48.3 | 26.2 |
| 5631 | ok | 0.09 | 5.21e-02 | 1.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.7 | 4.2 | 0.9 | -146.8 | 50.7 | 29.1 |
| 5648 | ok | 0.09 | 5.22e-02 | 1.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.2 | 4.5 | -1.7 | -145.6 | 52.3 | 31.8 |
| 5665 | ok | 0.09 | 5.38e-02 | 1.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.6 | 4.0 | 0.3 | 4.5 | 0.2 | 5.5 |
| 5682 | ok | 0.09 | 5.62e-02 | 1.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.2 | 5.3 | 1.9 | 5.3 | -1.52e-02 | 5.4 |
| 5699 | ok | 0.09 | 6.07e-02 | 9.24e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -41.1 | 7.7 | 3.9 | 5.8 | -0.4 | 5.3 |
| 5766 | ok | 0.09 | 7.09e-02 | 6.59e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.5 | -11.1 | -12.4 | -52.7 | 23.6 | 32.8 |
| 5768 | ok | 0.09 | 7.43e-02 | 4.66e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -17.1 | -6.2 | -11.8 | -52.4 | 20.6 | 33.8 |
| 5770 | ok | 0.09 | 7.66e-02 | 3.42e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -12.0 | 16.4 | -2.5 | 13.6 | -16.7 | 5.3 |
| 5772 | ok | 0.09 | 7.79e-02 | 2.71e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -10.5 | 18.3 | -3.6 | 11.1 | -12.3 | 5.6 |
| 5774 | ok | 0.09 | 7.82e-02 | 2.38e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -10.1 | 19.5 | 2.7 | 7.7 | -7.3 | 6.3 |
| 5776 | ok | 0.09 | 8.03e-02 | 2.68e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.7 | 19.0 | 0.6 | 7.8 | -5.8 | 5.5 |
| 5778 | ok | 0.09 | 7.64e-02 | 3.58e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.2 | 17.7 | 3.0 | 7.0 | -3.6 | 5.3 |
| 5780 | ok | 0.09 | 7.01e-02 | 5.20e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -22.3 | 15.0 | 5.1 | 6.5 | -2.1 | 5.3 |
| 5809 | ok | 0.09 | 7.44e-02 | 5.97e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -23.8 | 15.8 | -6.9 | -129.5 | 15.2 | 9.6 |
| 5811 | ok | 0.09 | 8.28e-02 | 4.13e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -16.1 | 19.2 | -4.8 | -118.5 | 7.4 | 8.9 |
| 5813 | ok | 0.09 | 8.52e-02 | 3.05e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -12.2 | 21.4 | -2.5 | -108.8 | 0.8 | 9.7 |
| 5815 | ok | 0.09 | 8.51e-02 | 2.49e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -10.6 | 22.5 | -0.5 | -103.0 | -3.5 | 11.9 |
| 5817 | ok | 0.09 | 8.43e-02 | 2.36e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -10.5 | 22.9 | 1.5 | -102.9 | -4.9 | 14.6 |
| 5819 | ok | 0.09 | 8.23e-02 | 2.79e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.9 | 22.4 | 3.5 | -108.6 | -3.2 | 16.9 |
| 5821 | ok | 0.09 | 8.37e-02 | 3.76e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.2 | 21.0 | 2.5 | -118.7 | 0.9 | 17.8 |
| 5823 | ok | 0.09 | 7.26e-02 | 5.48e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -22.1 | 18.5 | 7.8 | -130.0 | 6.3 | 17.8 |
| 5849 | ok | 0.09 | 0.1 | 5.45e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.9 | 28.5 | -8.8 | -133.1 | 6.7 | -15.7 |
| 5851 | ok | 0.09 | 0.1 | 3.78e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.4 | 32.4 | -3.3 | -121.6 | 1.1 | -15.8 |
| 5853 | ok | 0.09 | 0.1 | 2.87e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -12.4 | 35.2 | -4.1 | -111.4 | -3.1 | -14.9 |
| 5855 | ok | 0.09 | 0.1 | 2.51e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.4 | 37.1 | -1.8 | -105.7 | -4.8 | -12.5 |
| 5857 | ok | 0.09 | 0.1 | 2.68e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.9 | 38.2 | 0.6 | -106.1 | -3.4 | -9.6 |
| 5859 | ok | 0.09 | 0.1 | 3.32e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -14.1 | 38.4 | 3.1 | -112.6 | 1.1 | -7.3 |
| 5861 | ok | 0.09 | 0.1 | 4.61e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -19.2 | 37.6 | 6.0 | -123.4 | 8.1 | -6.4 |
| 5863 | ok | 0.09 | 0.1 | 6.81e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.8 | 35.3 | 8.6 | -135.8 | 16.5 | -7.0 |
| 6983 | ok | 0.09 | 0.3 | 5.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -148.7 | -127.9 | -114.4 | -1034.5 | -1392.6 | -1022.8 |
| 7003 | ok | 0.09 | 0.2 | 4.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -193.0 | -50.4 | -6.5 | -1066.0 | -302.4 | -810.6 |
| 7023 | ok | 0.09 | 0.2 | 4.95e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -179.9 | -37.1 | 10.6 | -1271.4 | 42.4 | -810.7 |
| 7043 | ok | 0.09 | 0.2 | 7.91e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -362.9 | -22.2 | 3.0 | -1239.6 | 182.7 | -174.1 |
| 7324 | ok | 0.09 | 0.2 | 3.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -120.2 | -20.1 | -91.1 | -598.8 | -524.3 | -456.2 |
| 7325 | ok | 0.09 | 0.2 | 4.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.8 | 72.8 | -39.1 | -213.2 | -494.4 | -485.6 |
| 7342 | ok | 0.09 | 0.2 | 2.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -72.9 | -23.3 | 65.7 | -171.3 | -193.8 | 243.4 |
| 7343 | ok | 0.09 | 0.2 | 2.99e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.7 | 18.7 | 44.4 | -205.3 | -469.9 | 455.6 |
| 7344 | ok | 0.09 | 0.2 | 2.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.0 | -1.9 | -54.5 | 22.6 | 39.2 | 43.9 |
| 7345 | ok | 0.09 | 0.2 | 2.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.1 | 8.45e-02 | -51.8 | 322.9 | 58.9 | 364.2 |
| 7346 | ok | 0.09 | 0.2 | 2.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.3 | 8.4 | 47.6 | -30.9 | -54.9 | 58.2 |
| 7347 | ok | 0.09 | 0.2 | 2.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.0 | -11.3 | 71.2 | -43.4 | -95.4 | 90.4 |
| 7348 | ok | 0.09 | 0.2 | 2.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.3 | -8.9 | 72.8 | -195.3 | 281.7 | 140.4 |
| 7349 | ok | 0.09 | 0.2 | 2.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.8 | 5.7 | 48.3 | -8.8 | -24.0 | 20.9 |
| 7539 | ok | 0.09 | 0.2 | 3.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.8 | 22.4 | 46.4 | -181.2 | -491.2 | 436.1 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|-------|----------|--------|--------|---------|---------|--------|-------|-------|---------|--------|--------|
| 7540 | ok | 0.09 | 0.2 | 3.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.1 | 24.3 | 47.8 | -160.3 | -497.4 | 416.3 |
| 7541 | ok | 0.09 | 0.2 | 3.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.6 | 25.5 | 48.7 | -137.0 | -496.8 | 390.1 |
| 7542 | ok | 0.09 | 0.3 | 4.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -69.1 | 21.4 | -51.9 | -209.4 | -533.6 | -468.2 |
| 7543 | ok | 0.09 | 0.2 | 4.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.8 | 43.9 | -37.1 | -195.3 | -500.1 | -494.8 |
| 7544 | ok | 0.09 | 0.2 | 4.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.9 | 54.4 | -32.4 | -230.0 | -466.6 | -510.4 |
| 7545 | ok | 0.09 | 0.2 | 2.74e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.8 | 3.6 | 67.8 | -70.0 | -119.8 | 137.2 |
| 7546 | ok | 0.09 | 0.2 | 2.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.7 | 4.3 | 70.2 | -227.5 | 233.7 | 189.9 |
| 7547 | ok | 0.09 | 0.2 | 2.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.8 | -17.2 | -85.5 | -326.0 | -295.2 | -515.8 |
| 7548 | ok | 0.09 | 0.2 | 2.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.8 | -13.3 | -83.1 | -330.5 | -275.6 | -510.8 |
| 7549 | ok | 0.09 | 0.2 | 2.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.0 | -8.8 | -79.2 | -333.2 | -256.5 | -503.1 |
| 7550 | ok | 0.09 | 0.2 | 2.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.8 | -4.7 | -74.2 | -334.1 | -238.3 | -492.6 |
| 7551 | ok | 0.09 | 0.2 | 2.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.3 | -9.3 | 75.5 | -49.2 | -99.0 | 97.3 |
| 7552 | ok | 0.09 | 0.2 | 2.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.2 | 10.7 | 50.7 | -27.7 | -55.7 | 54.2 |
| 7553 | ok | 0.09 | 0.2 | 2.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.6 | 9.8 | 53.5 | -26.5 | -53.3 | 51.8 |
| 7554 | ok | 0.09 | 0.2 | 2.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.1 | 7.5 | 56.3 | -25.1 | -51.0 | 49.4 |
| 7555 | ok | 0.09 | 0.2 | 2.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.6 | 4.2 | 59.1 | -23.7 | -48.7 | 47.0 |
| 7556 | ok | 0.09 | 0.2 | 2.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.4 | -0.7 | 62.3 | 286.6 | -37.3 | -319.8 |
| 7557 | ok | 0.09 | 0.2 | 2.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.6 | -5.3 | -64.6 | 316.7 | 117.9 | 417.5 |
| 7558 | ok | 0.09 | 0.2 | 2.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.9 | -2.0 | -61.5 | 314.4 | 101.6 | 406.2 |
| 7559 | ok | 0.09 | 0.2 | 2.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.1 | 0.4 | -58.3 | 311.2 | 86.0 | 393.5 |
| 7560 | ok | 0.09 | 0.2 | 2.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.4 | 1.5 | -55.1 | 308.2 | 71.5 | 379.0 |
| 7561 | ok | 0.09 | 0.2 | 3.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.8 | 26.3 | 48.6 | -114.5 | -485.8 | 356.9 |
| 7562 | ok | 0.09 | 0.2 | 3.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.5 | 26.0 | 47.2 | -98.6 | -459.3 | 317.1 |
| 7563 | ok | 0.09 | 0.2 | 2.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.7 | 22.6 | 45.2 | -100.6 | -411.5 | 273.2 |
| 7564 | ok | 0.09 | 0.2 | 2.74e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.7 | 12.0 | 47.1 | -139.7 | -338.3 | 232.0 |
| 7565 | ok | 0.09 | 0.2 | 2.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.1 | 7.3 | 52.0 | -7.4 | -24.2 | 18.7 |
| 7566 | ok | 0.09 | 0.2 | 2.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.8 | 6.0 | 55.4 | -6.6 | -22.9 | 17.1 |
| 7567 | ok | 0.09 | 0.2 | 2.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.6 | 3.4 | 58.5 | -5.6 | -21.5 | 15.5 |
| 7568 | ok | 0.09 | 0.2 | 2.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.3 | -1.6 | 62.2 | 322.0 | 212.1 | -463.5 |
| 7569 | ok | 0.09 | 0.2 | 2.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.0 | -5.3 | 65.0 | 0.3 | -40.3 | 17.4 |
| 7570 | ok | 0.09 | 0.2 | 2.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.5 | -3.6 | -63.8 | 15.9 | 43.8 | 37.5 |
| 7571 | ok | 0.09 | 0.2 | 2.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.2 | -1.0 | -61.5 | 17.2 | 43.7 | 39.0 |
| 7572 | ok | 0.09 | 0.2 | 2.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.8 | 0.5 | -59.1 | 18.6 | 43.3 | 40.5 |
| 7573 | ok | 0.09 | 0.2 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.6 | 0.5 | -56.8 | 19.8 | 42.6 | 41.8 |
| 7575 | ok | 0.09 | 0.2 | 2.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.8 | 15.8 | 43.4 | -218.0 | -460.3 | 465.8 |
| 7576 | ok | 0.09 | 0.2 | 2.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.3 | 12.2 | 43.5 | -231.5 | -448.6 | 474.5 |
| 7577 | ok | 0.09 | 0.2 | 2.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.5 | -31.9 | -74.2 | -103.2 | 374.9 | 81.1 |
| 7578 | ok | 0.09 | 0.2 | 2.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.0 | -27.4 | -69.4 | -118.3 | 362.0 | 57.1 |
| 7579 | ok | 0.09 | 0.2 | 2.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.9 | -22.5 | -65.1 | -133.1 | 348.2 | 33.5 |
| 7580 | ok | 0.09 | 0.2 | 2.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.3 | -17.7 | -61.4 | -148.0 | 333.6 | 10.0 |
| 7581 | ok | 0.09 | 0.2 | 2.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.3 | -13.9 | 59.6 | 13.5 | -30.7 | 1.6 |
| 7582 | ok | 0.09 | 0.2 | 2.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.6 | -4.0 | -53.2 | 23.1 | 38.0 | 44.5 |
| 7583 | ok | 0.09 | 0.2 | 2.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.0 | 4.9 | 45.9 | -9.3 | -25.2 | 22.1 |
| 7584 | ok | 0.09 | 0.2 | 2.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.3 | 3.3 | 45.2 | -10.1 | -26.4 | 23.5 |
| 7585 | ok | 0.09 | 0.2 | 2.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.2 | -2.1 | 47.5 | -9.3 | -41.4 | 30.2 |
| 7586 | ok | 0.09 | 0.2 | 1.90e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.9 | -5.2 | 49.4 | -10.3 | -41.9 | 31.5 |
| 7587 | ok | 0.09 | 0.2 | 1.81e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.1 | -8.4 | 51.9 | -11.3 | -42.5 | 32.8 |
| 7588 | ok | 0.09 | 0.2 | 1.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.6 | -11.3 | 54.8 | -12.3 | -43.2 | 34.2 |
| 7589 | ok | 0.09 | 0.2 | 1.91e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.3 | -13.3 | 57.8 | -13.4 | -44.0 | 35.7 |
| 7590 | ok | 0.09 | 0.2 | 2.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.5 | -14.4 | 60.8 | 303.5 | 58.6 | -361.2 |
| 7591 | ok | 0.09 | 0.2 | 2.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.9 | 7.2 | 45.9 | -31.2 | -57.6 | 60.4 |
| 7592 | ok | 0.09 | 0.2 | 2.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.6 | 5.1 | 46.0 | -32.5 | -60.0 | 63.0 |
| 7593 | ok | 0.09 | 0.2 | 2.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.9 | 1.8 | 47.9 | -306.0 | 23.9 | 312.1 |
| 7594 | ok | 0.09 | 0.2 | 1.98e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.3 | -3.4 | 51.4 | -36.4 | -71.7 | 73.1 |
| 7595 | ok | 0.09 | 0.2 | 1.91e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.9 | -6.9 | 54.8 | -38.3 | -74.4 | 76.5 |
| 7596 | ok | 0.09 | 0.2 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.9 | -9.9 | 58.5 | -40.4 | -77.3 | 80.3 |
| 7597 | ok | 0.09 | 0.2 | 2.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.2 | -11.8 | 62.4 | -42.6 | -80.4 | 84.4 |
| 7598 | ok | 0.09 | 0.2 | 2.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.5 | -12.4 | 66.5 | -45.6 | -83.7 | 89.2 |
| 7645 | ok | 0.09 | 0.2 | 3.68e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -95.8 | -19.6 | 104.0 | 144.6 | 554.5 | -357.7 |
| 7646 | ok | 0.09 | 0.3 | 5.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -121.3 | -43.3 | 141.6 | 208.2 | 596.2 | -394.7 |
| 7647 | ok | 0.09 | 0.3 | 6.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -142.5 | -65.8 | 180.9 | 362.9 | 628.7 | -445.6 |
| 7648 | ok | 0.09 | 0.2 | 5.77e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -101.5 | -74.9 | 174.7 | 810.9 | 658.0 | -527.5 |
| 8361 | ok | 0.09 | 0.2 | 2.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -112.9 | -20.2 | 23.0 | 88.3 | 182.6 | -147.6 |
| 8362 | ok | 0.09 | 0.2 | 2.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -107.6 | -10.5 | 26.6 | -45.9 | 275.0 | -52.3 |
| 8363 | ok | 0.09 | 0.1 | 2.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -107.1 | -11.5 | 33.1 | -37.9 | 248.0 | -43.3 |
| 8364 | ok | 0.09 | 0.2 | 3.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -93.4 | -6.8 | 85.4 | 95.8 | 431.3 | 119.1 |
| 8365 | ok | 0.09 | 0.2 | 2.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -98.5 | -25.9 | 20.7 | -122.9 | 625.2 | -285.8 |
| 8366 | ok | 0.09 | 0.1 | 2.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -95.0 | -6.2 | 24.7 | -55.8 | 240.3 | -340.3 |
| 8367 | ok | 0.09 | 0.1 | 2.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -92.4 | -5.9 | 31.0 | -48.8 | 165.3 | -320.5 |
| 8368 | ok | 0.09 | 0.1 | 3.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -102.3 | 12.8 | -33.3 | -210.1 | -201.7 | -401.8 |
| 8369 | ok | 0.09 | 0.2 | 5.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -224.9 | 7.6 | 61.2 | -1140.3 | 88.4 | -45.2 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|-------|-------|--------|--------|--------|
| 8370 | ok | 0.09 | 0.1 | 4.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -201.5 | 1.7 | 57.3 | -773.8 | 33.5 | -52.9 |
| 8371 | ok | 0.09 | 8.50e-02 | 3.99e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -163.2 | 0.9 | 57.6 | -441.0 | 48.1 | -43.2 |
| 8372 | ok | 0.09 | 8.91e-02 | 3.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -135.4 | 16.3 | 6.0 | -308.1 | -251.0 | 96.6 |
| 8373 | ok | 0.09 | 0.1 | 3.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.3 | 22.6 | -14.1 | -150.2 | -226.9 | -360.7 |
| 8374 | ok | 0.09 | 0.1 | 2.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -95.3 | -12.0 | 14.2 | -128.3 | 540.3 | -264.7 |
| 8375 | ok | 0.09 | 0.1 | 2.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -88.0 | -6.2 | 26.8 | -112.0 | 362.1 | -290.7 |
| 8376 | ok | 0.09 | 0.1 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.1 | -9.7 | 44.0 | -66.8 | 169.9 | -303.2 |
| 8377 | ok | 0.09 | 0.1 | 3.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.5 | 31.7 | -6.7 | -160.8 | -225.2 | -349.1 |
| 8378 | ok | 0.09 | 0.1 | 2.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -88.1 | -4.0 | 22.7 | -106.6 | 372.6 | -247.3 |
| 8379 | ok | 0.09 | 0.1 | 2.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.6 | -2.3 | 29.4 | -97.3 | 306.7 | -271.7 |
| 8380 | ok | 0.09 | 0.1 | 2.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -73.9 | -9.4 | 48.1 | -82.8 | 140.7 | -272.8 |
| 8381 | ok | 0.09 | 0.2 | 3.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.5 | 38.9 | -11.3 | -187.9 | -222.1 | -337.0 |
| 8382 | ok | 0.09 | 0.1 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.0 | 16.3 | 44.5 | -95.0 | 191.3 | -193.4 |
| 8383 | ok | 0.09 | 0.1 | 1.74e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.6 | 7.8 | 38.9 | -85.1 | 134.5 | -242.3 |
| 8384 | ok | 0.09 | 0.1 | 1.93e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.6 | -7.6 | 48.1 | -95.1 | 106.8 | -241.5 |
| 8385 | ok | 0.09 | 0.2 | 2.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.7 | 41.7 | 0.5 | -176.6 | -239.8 | -314.0 |
| 8386 | ok | 0.09 | 0.2 | 4.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.4 | 61.9 | -41.6 | -254.8 | -449.2 | -492.6 |
| 8387 | ok | 0.09 | 0.2 | 1.23e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 25.1 | 73.0 | -16.0 | 25.5 | 113.5 | -34.2 |
| 8388 | ok | 0.09 | 0.1 | 7.96e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -7.6 | 17.4 | 24.0 | -31.2 | 96.0 | -179.3 |
| 8389 | ok | 0.09 | 0.1 | 1.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.8 | 8.2 | 35.1 | -75.4 | 78.7 | -207.5 |
| 8390 | ok | 0.09 | 0.1 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.5 | -5.8 | 44.5 | -101.6 | 75.8 | -208.3 |
| 8391 | ok | 0.09 | 0.2 | 2.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.6 | 35.1 | -6.1 | -194.2 | -233.1 | -308.5 |
| 8392 | ok | 0.09 | 0.2 | 4.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.3 | 45.4 | -45.6 | -268.1 | -422.1 | -492.1 |
| 8393 | ok | 0.09 | 0.2 | 3.40e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.5 | 74.6 | 1.2 | 3.2 | 49.2 | -30.5 |
| 8394 | ok | 0.09 | 0.2 | 3.37e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.6 | 37.5 | 14.1 | -23.1 | 40.8 | -185.5 |
| 8395 | ok | 0.09 | 0.1 | 7.56e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -20.1 | 15.1 | 26.8 | -69.3 | 39.1 | -194.8 |
| 8396 | ok | 0.09 | 0.1 | 1.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.1 | -0.8 | 35.9 | -106.6 | 49.4 | -191.0 |
| 8397 | ok | 0.09 | 0.2 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.3 | 26.9 | -14.5 | -204.2 | -228.1 | -305.1 |
| 8398 | ok | 0.09 | 0.2 | 3.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.8 | 27.3 | -51.9 | -275.2 | -402.7 | -493.6 |
| 8399 | ok | 0.09 | 0.2 | 3.09e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.3 | 83.4 | 1.5 | 3.7 | 15.2 | -33.5 |
| 8400 | ok | 0.09 | 0.2 | 1.71e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.0 | 49.2 | 6.3 | -24.4 | 9.3 | -196.9 |
| 8401 | ok | 0.09 | 0.1 | 4.91e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.7 | 23.0 | 17.6 | -74.6 | 14.8 | -196.0 |
| 8402 | ok | 0.09 | 0.1 | 9.33e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.4 | 13.2 | 15.8 | -127.9 | -29.0 | -200.4 |
| 8403 | ok | 0.09 | 0.2 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.4 | 18.3 | -23.6 | -215.3 | -221.9 | -304.7 |
| 8404 | ok | 0.09 | 0.2 | 3.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.9 | 10.2 | -60.2 | -281.8 | -386.8 | -498.4 |
| 8405 | ok | 0.09 | 0.3 | 3.31e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.1 | 90.3 | 1.9 | 6.4 | 5.2 | -36.9 |
| 8406 | ok | 0.09 | 0.2 | 1.74e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.6 | 55.1 | 6.5 | -31.3 | -2.9 | -213.4 |
| 8407 | ok | 0.09 | 0.1 | 3.72e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -14.6 | 28.0 | 9.7 | -136.5 | 4.1 | -382.8 |
| 8408 | ok | 0.09 | 0.1 | 7.31e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -23.0 | 13.2 | 11.8 | -205.2 | -20.9 | -366.4 |
| 8409 | ok | 0.09 | 0.1 | 1.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.1 | 10.7 | -32.6 | -228.7 | -213.7 | -305.1 |
| 8410 | ok | 0.09 | 0.2 | 2.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.0 | -4.0 | -69.3 | -289.6 | -371.5 | -505.0 |
| 8411 | ok | 0.09 | 0.3 | 1.56e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 12.2 | 99.4 | 12.7 | -23.2 | -21.6 | -247.2 |
| 8412 | ok | 0.09 | 0.2 | 3.36e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -5.4 | 52.5 | 1.2 | -96.0 | 19.4 | -403.2 |
| 8413 | ok | 0.09 | 0.1 | 4.89e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -17.6 | 30.8 | -1.9 | -181.2 | 6.6 | -391.8 |
| 8414 | ok | 0.09 | 0.1 | 7.09e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -26.0 | 14.9 | 0.8 | -235.2 | 8.2 | -358.0 |
| 8415 | ok | 0.09 | 0.1 | 1.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.9 | 4.9 | -40.1 | -243.3 | -204.0 | -303.9 |
| 8416 | ok | 0.09 | 0.2 | 7.09e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.4 | 54.1 | -11.9 | -145.3 | 59.8 | -251.7 |
| 8417 | ok | 0.09 | 0.1 | 7.84e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -26.6 | 33.2 | -7.3 | -155.3 | 18.2 | -203.6 |
| 8418 | ok | 0.09 | 9.74e-02 | 9.25e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -34.6 | 17.7 | -4.9 | -182.4 | -7.5 | -181.0 |
| 8419 | ok | 0.09 | 0.1 | 1.74e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.8 | -4.1 | -45.2 | 186.5 | 288.9 | 342.7 |
| 8420 | ok | 0.09 | 0.2 | 1.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.3 | 55.2 | -10.5 | -195.7 | 73.1 | -197.7 |
| 8421 | ok | 0.09 | 0.1 | 1.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.0 | 34.9 | -11.7 | -185.5 | 26.4 | -184.3 |
| 8422 | ok | 0.09 | 9.65e-02 | 1.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.3 | 18.8 | -14.0 | -207.3 | -24.3 | -175.8 |
| 8423 | ok | 0.09 | 0.1 | 1.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.8 | -4.0 | -47.4 | 209.2 | 274.0 | 341.7 |
| 8424 | ok | 0.09 | 0.2 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.6 | 43.6 | -3.5 | -200.3 | 58.9 | -163.9 |
| 8425 | ok | 0.09 | 0.1 | 1.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.5 | 34.0 | -8.8 | -203.9 | 28.0 | -161.4 |
| 8426 | ok | 0.09 | 9.48e-02 | 1.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.4 | 19.1 | -14.0 | -222.9 | -23.0 | -161.4 |
| 8427 | ok | 0.09 | 0.1 | 1.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.4 | 6.4 | -15.7 | -258.4 | -59.6 | -158.9 |
| 8428 | ok | 0.09 | 0.1 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.6 | 37.9 | -1.5 | -201.4 | 54.0 | -139.1 |
| 8429 | ok | 0.09 | 0.1 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.6 | 30.9 | -5.7 | -212.3 | 26.1 | -140.5 |
| 8430 | ok | 0.09 | 9.23e-02 | 1.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.5 | 18.4 | -12.2 | -233.1 | -22.0 | -145.8 |
| 8431 | ok | 0.09 | 0.1 | 1.85e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.8 | 1.7 | -45.2 | -283.7 | -160.5 | -282.1 |
| 8432 | ok | 0.09 | 0.1 | 1.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.9 | 34.1 | 2.5 | -201.0 | 48.9 | -119.0 |
| 8433 | ok | 0.09 | 0.1 | 1.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.2 | 28.2 | -3.2 | -216.4 | 23.0 | -121.6 |
| 8434 | ok | 0.09 | 8.95e-02 | 1.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.0 | 17.2 | -9.7 | -239.2 | -22.2 | -130.4 |
| 8435 | ok | 0.09 | 0.1 | 1.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.3 | 3.3 | -42.2 | -286.5 | -150.7 | -272.7 |
| 8436 | ok | 0.09 | 0.1 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.3 | 31.7 | 4.1 | -199.8 | 43.2 | -100.7 |
| 8437 | ok | 0.09 | 9.65e-02 | 1.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.0 | 26.1 | -0.6 | -217.7 | 18.8 | -104.7 |
| 8438 | ok | 0.09 | 8.65e-02 | 1.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.7 | 16.2 | -6.8 | -242.3 | -23.4 | -115.9 |
| 8439 | ok | 0.09 | 0.1 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.4 | 4.8 | -38.6 | -287.3 | -141.7 | -262.5 |
| 8440 | ok | 0.09 | 0.1 | 1.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.0 | 30.4 | 3.6 | -196.7 | 36.2 | -83.7 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-------|------|-------|--------|--------|--------|
| 8441 | ok | 0.09 | 9.04e-02 | 1.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.1 | 24.5 | 2.3 | -216.9 | 13.4 | -89.4 |
| 8442 | ok | 0.09 | 8.35e-02 | 1.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.7 | 15.1 | -3.8 | -243.4 | -25.4 | -102.6 |
| 8443 | ok | 0.09 | 0.1 | 1.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.3 | 5.3 | -34.8 | -287.0 | -134.2 | -251.3 |
| 8444 | ok | 0.09 | 0.1 | 1.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.9 | 29.8 | 6.9 | -190.9 | 27.3 | -68.5 |
| 8445 | ok | 0.09 | 9.65e-02 | 1.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.9 | 22.9 | 5.3 | -214.1 | 6.9 | -76.3 |
| 8446 | ok | 0.09 | 8.06e-02 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.0 | 13.6 | -0.8 | -243.0 | -28.3 | -90.8 |
| 8447 | ok | 0.09 | 0.1 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.2 | 3.8 | -29.5 | -286.1 | -130.1 | -235.1 |
| 8448 | ok | 0.09 | 0.1 | 1.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.3 | 28.3 | 9.7 | -181.9 | 16.9 | -56.5 |
| 8449 | ok | 0.09 | 9.38e-02 | 1.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.4 | 20.1 | 6.6 | -210.0 | -2.7 | -66.0 |
| 8450 | ok | 0.09 | 7.83e-02 | 1.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.4 | 11.9 | 0.7 | -240.8 | -31.7 | -81.8 |
| 8451 | ok | 0.09 | 0.1 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.8 | 4.4 | -32.3 | -295.6 | -115.4 | -246.1 |
| 8453 | ok | 0.09 | 0.1 | 8.06e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.1 | 26.5 | 9.7 | -172.8 | 7.8 | -49.6 |
| 8454 | ok | 0.09 | 9.13e-02 | 9.00e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.9 | 18.1 | 6.5 | -205.6 | -8.9 | -59.9 |
| 8455 | ok | 0.09 | 7.86e-02 | 1.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.2 | 10.3 | -0.4 | -240.8 | -35.7 | -79.2 |
| 8456 | ok | 0.09 | 0.1 | 1.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.0 | 0.6 | -30.1 | 257.7 | 174.9 | 278.8 |
| 8458 | ok | 0.09 | 0.1 | 6.23e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -23.1 | 25.5 | 9.2 | -163.3 | -1.2 | -46.1 |
| 8459 | ok | 0.09 | 8.88e-02 | 7.61e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.2 | 16.3 | 4.7 | -201.3 | -14.3 | -55.5 |
| 8460 | ok | 0.09 | 7.58e-02 | 9.11e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -39.3 | 8.8 | -1.7 | -240.2 | -37.4 | -73.9 |
| 8461 | ok | 0.09 | 0.1 | 1.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.2 | -1.3 | -30.7 | 258.0 | 168.4 | 273.0 |
| 8463 | ok | 0.09 | 0.1 | 4.90e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.1 | 25.1 | 5.9 | -155.3 | -8.4 | -45.9 |
| 8464 | ok | 0.09 | 8.44e-02 | 6.47e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.8 | 15.0 | 1.9 | -197.8 | -18.5 | -53.1 |
| 8465 | ok | 0.09 | 7.47e-02 | 8.15e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -35.8 | 7.3 | -3.8 | -238.8 | -39.1 | -70.2 |
| 8466 | ok | 0.09 | 0.1 | 1.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.6 | 1.7 | 30.1 | -264.3 | 14.2 | 127.8 |
| 8468 | ok | 0.09 | 0.1 | 4.15e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.5 | 24.7 | 2.5 | -150.7 | -13.1 | -48.6 |
| 8469 | ok | 0.09 | 7.86e-02 | 5.74e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -26.2 | 14.1 | -1.4 | -196.0 | -21.2 | -52.1 |
| 8470 | ok | 0.09 | 7.40e-02 | 7.54e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.5 | 6.1 | -6.4 | -238.3 | -40.0 | -67.5 |
| 8471 | ok | 0.09 | 0.1 | 1.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.8 | 3.5 | 27.2 | -266.9 | 8.3 | 132.1 |
| 8473 | ok | 0.09 | 9.77e-02 | 4.03e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -14.7 | 23.8 | -0.6 | -150.7 | -14.5 | -52.4 |
| 8474 | ok | 0.09 | 7.24e-02 | 5.71e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.4 | 13.3 | -4.7 | -196.4 | -22.2 | -51.9 |
| 8475 | ok | 0.09 | 7.38e-02 | 7.71e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.7 | 5.3 | -9.3 | -239.0 | -40.0 | -65.4 |
| 8476 | ok | 0.09 | 0.1 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.1 | 5.3 | 24.8 | -270.4 | 2.7 | 136.9 |
| 8478 | ok | 0.09 | 9.16e-02 | 4.51e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.8 | 22.5 | -3.7 | -155.3 | -12.5 | -55.4 |
| 8479 | ok | 0.09 | 6.65e-02 | 6.22e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -26.3 | 12.6 | -7.9 | -199.1 | -21.6 | -51.4 |
| 8480 | ok | 0.09 | 7.38e-02 | 8.24e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.3 | 4.7 | -12.2 | -240.8 | -39.1 | -63.2 |
| 8481 | ok | 0.09 | 0.1 | 1.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.3 | 7.0 | 23.1 | -274.8 | -2.6 | 142.6 |
| 8483 | ok | 0.09 | 8.53e-02 | 5.51e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.9 | 20.9 | -6.9 | -163.2 | -8.0 | -56.1 |
| 8484 | ok | 0.09 | 6.33e-02 | 7.11e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.8 | 12.1 | -10.7 | -203.5 | -19.4 | -49.8 |
| 8485 | ok | 0.09 | 7.40e-02 | 8.99e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -35.2 | 4.4 | -14.8 | -243.5 | -37.4 | -60.6 |
| 8486 | ok | 0.09 | 0.1 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.3 | 8.3 | 22.6 | -280.2 | -7.6 | 150.0 |
| 8488 | ok | 0.09 | 7.97e-02 | 6.95e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.4 | 19.7 | -9.4 | -172.5 | -2.1 | -53.7 |
| 8489 | ok | 0.09 | 6.40e-02 | 8.20e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.8 | 11.9 | -12.8 | -208.9 | -16.3 | -46.7 |
| 8490 | ok | 0.09 | 7.41e-02 | 9.83e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.0 | 4.5 | -16.7 | -246.6 | -34.9 | -57.2 |
| 8491 | ok | 0.09 | 0.1 | 1.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.5 | 8.8 | 20.1 | -281.5 | -14.8 | 143.9 |
| 8492 | ok | 0.09 | 7.66e-02 | 8.51e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.4 | 19.0 | -10.0 | -181.5 | 4.1 | -48.4 |
| 8493 | ok | 0.09 | 6.46e-02 | 9.29e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -37.7 | 11.8 | -13.5 | -214.4 | -12.6 | -41.9 |
| 8494 | ok | 0.09 | 7.41e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.7 | 4.6 | -17.5 | -250.6 | -31.6 | -52.4 |
| 8495 | ok | 0.09 | 0.1 | 1.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.6 | 9.8 | 22.7 | -281.9 | -17.5 | 159.1 |
| 8496 | ok | 0.09 | 7.46e-02 | 9.85e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.2 | 17.7 | -8.5 | -189.6 | 10.5 | -39.7 |
| 8497 | ok | 0.09 | 6.47e-02 | 1.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.6 | 11.5 | -12.9 | -219.7 | -8.4 | -34.6 |
| 8498 | ok | 0.09 | 7.33e-02 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.8 | 4.7 | -16.6 | -253.2 | -28.1 | -43.6 |
| 8499 | ok | 0.09 | 0.1 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.6 | 9.2 | 24.6 | -285.3 | -23.1 | 169.1 |
| 8500 | ok | 0.09 | 7.13e-02 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.4 | 15.7 | -8.7 | -195.0 | 15.5 | -28.9 |
| 8501 | ok | 0.09 | 6.44e-02 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.2 | 10.9 | -10.9 | -223.7 | -4.9 | -25.9 |
| 8502 | ok | 0.09 | 7.26e-02 | 1.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.4 | 4.6 | -15.2 | -255.4 | -25.3 | -36.1 |
| 8503 | ok | 0.09 | 0.1 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.1 | 7.5 | 26.8 | -288.5 | -30.0 | 178.3 |
| 8504 | ok | 0.09 | 6.70e-02 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.4 | 13.6 | -6.4 | -197.7 | 18.6 | -17.3 |
| 8505 | ok | 0.09 | 6.39e-02 | 1.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.4 | 9.9 | -8.7 | -226.3 | -2.3 | -16.2 |
| 8506 | ok | 0.09 | 7.19e-02 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.3 | 4.5 | -13.2 | -257.4 | -22.8 | -27.7 |
| 8507 | ok | 0.09 | 0.1 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.2 | 5.3 | 29.2 | -290.9 | -37.6 | 187.1 |
| 8508 | ok | 0.09 | 6.41e-02 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.2 | 12.0 | -4.6 | -198.4 | 20.2 | -5.8 |
| 8509 | ok | 0.09 | 6.32e-02 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.5 | 9.0 | -6.4 | -227.5 | -0.8 | -6.1 |
| 8510 | ok | 0.09 | 7.11e-02 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.3 | 4.3 | -11.0 | -258.4 | -20.8 | -18.6 |
| 8511 | ok | 0.09 | 0.1 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.5 | -5.2 | -37.7 | 278.4 | 82.1 | 217.9 |
| 8512 | ok | 0.09 | 6.20e-02 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.3 | 11.0 | -3.0 | -198.2 | 20.5 | 5.4 |
| 8513 | ok | 0.09 | 6.29e-02 | 1.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.7 | 8.5 | -0.5 | -227.6 | -0.4 | 5.9 |
| 8514 | ok | 0.09 | 7.03e-02 | 1.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.3 | 5.4 | 2.9 | -258.7 | -20.8 | 18.9 |
| 8515 | ok | 0.09 | 0.1 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.9 | -3.1 | -35.1 | 277.8 | 72.8 | 209.0 |
| 8516 | ok | 0.09 | 6.03e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.1 | 10.6 | 1.2 | -197.5 | 20.0 | 16.5 |
| 8517 | ok | 0.09 | 6.27e-02 | 1.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.4 | 8.1 | 1.7 | -226.8 | -1.1 | 16.2 |
| 8518 | ok | 0.09 | 6.98e-02 | 1.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.0 | 4.8 | 5.3 | -258.1 | -22.2 | 28.2 |
| 8519 | ok | 0.09 | 0.1 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.8 | -1.1 | -32.5 | 276.1 | 64.0 | 199.6 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-------|-----------|-------|--------|--------|--------|
| 8520 | ok | 0.09 | 5.89e-02 | 1.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.4 | 10.8 | 3.1 | -196.1 | 18.3 | 27.8 |
| 8521 | ok | 0.09 | 6.24e-02 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.3 | 8.0 | 4.0 | -224.9 | -2.6 | 26.2 |
| 8522 | ok | 0.09 | 6.99e-02 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.9 | 4.2 | 7.5 | -256.4 | -24.2 | 37.1 |
| 8523 | ok | 0.09 | 0.1 | 1.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.1 | 0.4 | -30.0 | 273.6 | 55.9 | 189.9 |
| 8524 | ok | 0.09 | 5.94e-02 | 1.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.4 | 11.5 | 5.4 | -192.8 | 15.1 | 39.1 |
| 8525 | ok | 0.09 | 6.21e-02 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.1 | 8.0 | 6.3 | -221.7 | -5.2 | 35.7 |
| 8526 | ok | 0.09 | 6.99e-02 | 1.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.7 | 4.7 | 3.6 | -253.1 | -23.2 | 33.8 |
| 8527 | ok | 0.09 | 0.1 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.8 | 0.9 | -27.6 | 270.8 | 49.1 | 179.5 |
| 8528 | ok | 0.09 | 6.00e-02 | 9.67e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.3 | 12.3 | 5.4 | -186.9 | 10.1 | 49.6 |
| 8529 | ok | 0.09 | 6.14e-02 | 9.87e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -39.2 | 8.4 | 5.2 | -217.1 | -8.0 | 44.2 |
| 8530 | ok | 0.09 | 6.98e-02 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.8 | 4.0 | 5.2 | -249.7 | -25.5 | 41.5 |
| 8531 | ok | 0.09 | 0.1 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.3 | -5.80e-02 | -24.8 | 270.0 | 44.9 | 164.9 |
| 8532 | ok | 0.09 | 5.90e-02 | 8.33e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.4 | 12.3 | 7.1 | -178.4 | 3.7 | 58.1 |
| 8533 | ok | 0.09 | 6.03e-02 | 8.90e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -34.2 | 7.6 | 6.3 | -211.3 | -12.0 | 51.3 |
| 8534 | ok | 0.09 | 6.99e-02 | 9.95e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -41.7 | 0.8 | 13.5 | -5.9 | -7.1 | 24.4 |
| 8535 | ok | 0.09 | 0.1 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.6 | -8.0 | 37.0 | 266.8 | 40.6 | -180.8 |
| 8536 | ok | 0.09 | 5.83e-02 | 6.77e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.3 | 11.8 | 6.8 | -169.2 | -2.4 | 63.2 |
| 8537 | ok | 0.09 | 5.90e-02 | 7.79e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.2 | 4.4 | 10.2 | -3.4 | -3.5 | 23.9 |
| 8538 | ok | 0.09 | 6.92e-02 | 9.12e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -37.6 | -1.8 | 12.7 | 231.7 | 22.6 | -24.4 |
| 8539 | ok | 0.09 | 0.1 | 1.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.3 | -7.7 | 34.7 | 266.4 | 48.6 | -183.1 |
| 8540 | ok | 0.09 | 6.30e-02 | 5.32e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.4 | 11.8 | 4.5 | -159.8 | -8.1 | 65.4 |
| 8541 | ok | 0.09 | 5.76e-02 | 6.69e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.8 | 6.0 | 6.4 | -199.6 | -18.1 | 58.7 |
| 8542 | ok | 0.09 | 6.86e-02 | 8.28e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -34.4 | -2.5 | 10.9 | 229.4 | 25.8 | -28.7 |
| 8543 | ok | 0.09 | 0.1 | 1.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.6 | -6.6 | 32.2 | 266.1 | 55.3 | -186.0 |
| 8544 | ok | 0.09 | 6.94e-02 | 4.28e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -14.9 | 12.2 | 1.6 | -151.9 | -12.4 | 64.7 |
| 8545 | ok | 0.09 | 5.64e-02 | 5.80e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.9 | 5.5 | 1.5 | -195.1 | -20.6 | 60.5 |
| 8546 | ok | 0.09 | 6.80e-02 | 7.52e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -30.8 | -4.5 | 8.2 | 382.1 | 51.5 | -69.7 |
| 8547 | ok | 0.09 | 0.1 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.6 | -5.0 | 29.6 | 266.3 | 61.3 | -189.2 |
| 8549 | ok | 0.09 | 7.41e-02 | 3.74e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -13.5 | 12.4 | -1.3 | -147.1 | -14.3 | 61.8 |
| 8550 | ok | 0.09 | 5.85e-02 | 5.28e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -20.5 | 5.2 | -1.5 | -192.0 | -21.1 | 61.0 |
| 8551 | ok | 0.09 | 6.76e-02 | 7.11e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -29.7 | -4.5 | 5.6 | 379.6 | 53.7 | -74.3 |
| 8552 | ok | 0.09 | 0.1 | 1.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.6 | -3.2 | 27.2 | 267.2 | 66.9 | -192.9 |
| 8554 | ok | 0.09 | 7.62e-02 | 3.95e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -13.7 | 12.1 | -4.0 | -146.8 | -13.0 | 58.2 |
| 8555 | ok | 0.09 | 6.27e-02 | 5.56e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -23.9 | 4.5 | -1.6 | -191.3 | -21.2 | 61.3 |
| 8556 | ok | 0.09 | 6.76e-02 | 7.49e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -29.7 | -4.3 | 3.0 | 378.9 | 54.5 | -78.8 |
| 8557 | ok | 0.09 | 0.1 | 1.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.5 | -1.3 | 25.3 | 269.1 | 72.3 | -197.3 |
| 8559 | ok | 0.09 | 7.74e-02 | 4.65e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.5 | 11.3 | -6.9 | -150.7 | -8.5 | 55.7 |
| 8560 | ok | 0.09 | 6.55e-02 | 6.25e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.6 | 4.4 | -4.5 | -192.5 | -18.6 | 62.2 |
| 8561 | ok | 0.09 | 6.80e-02 | 8.16e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -29.0 | -9.82e-02 | -6.0 | -230.1 | -25.2 | 61.9 |
| 8562 | ok | 0.09 | 0.1 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.1 | 2.7 | 23.3 | -283.6 | -118.1 | 240.7 |
| 8564 | ok | 0.09 | 7.77e-02 | 5.81e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -19.3 | 10.4 | -9.8 | -157.8 | -1.7 | 55.9 |
| 8565 | ok | 0.09 | 6.72e-02 | 7.26e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.9 | 4.4 | -7.1 | -195.4 | -14.6 | 64.5 |
| 8566 | ok | 0.09 | 6.88e-02 | 9.00e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.5 | 0.7 | -8.6 | -231.7 | -28.4 | 69.7 |
| 8567 | ok | 0.09 | 0.1 | 1.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.6 | 3.8 | 23.3 | -286.8 | -121.9 | 246.6 |
| 8569 | ok | 0.09 | 7.61e-02 | 7.34e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.6 | 9.8 | -9.8 | -166.2 | 6.7 | 59.4 |
| 8570 | ok | 0.09 | 6.70e-02 | 8.41e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.5 | 4.8 | -8.8 | -199.0 | -9.8 | 68.6 |
| 8571 | ok | 0.09 | 6.99e-02 | 9.89e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -37.7 | 1.6 | -4.0 | -234.5 | -36.6 | 86.7 |
| 8572 | ok | 0.09 | 0.1 | 1.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.2 | 4.0 | 21.5 | -281.6 | -132.9 | 242.4 |
| 8573 | ok | 0.09 | 7.19e-02 | 8.91e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.2 | 9.8 | -9.9 | -173.9 | 14.9 | 66.2 |
| 8574 | ok | 0.09 | 6.41e-02 | 9.51e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.6 | 5.3 | -9.1 | -202.5 | -4.3 | 74.4 |
| 8575 | ok | 0.09 | 7.07e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.1 | 2.1 | -4.9 | -234.6 | -33.5 | 90.3 |
| 8576 | ok | 0.09 | 0.1 | 1.68e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.7 | 4.8 | 24.6 | -282.0 | -137.4 | 253.8 |
| 8577 | ok | 0.09 | 5.57e-02 | 1.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.0 | 9.2 | -7.9 | -180.4 | 23.3 | 76.8 |
| 8578 | ok | 0.09 | 6.29e-02 | 1.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.6 | 5.9 | -8.4 | -205.3 | 4.0 | 83.2 |
| 8579 | ok | 0.09 | 7.26e-02 | 1.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.2 | 2.5 | -4.0 | -236.1 | -30.8 | 98.0 |
| 8580 | ok | 0.09 | 0.1 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.9 | 4.0 | 27.0 | -282.4 | -144.0 | 262.4 |
| 8581 | ok | 0.09 | 5.87e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.8 | 7.7 | -5.1 | -183.9 | 30.0 | 89.5 |
| 8582 | ok | 0.09 | 6.52e-02 | 1.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.1 | 5.6 | -6.2 | -207.0 | 9.2 | 93.9 |
| 8583 | ok | 0.09 | 7.46e-02 | 1.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.0 | 2.5 | -2.1 | -236.3 | -28.5 | 107.6 |
| 8584 | ok | 0.09 | 0.1 | 1.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.6 | 2.3 | 29.4 | -282.2 | -151.7 | 270.7 |
| 8585 | ok | 0.09 | 6.11e-02 | 1.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.3 | 6.4 | -5.3 | -184.7 | 34.8 | 103.0 |
| 8586 | ok | 0.09 | 6.73e-02 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.0 | 4.9 | -3.8 | -207.1 | 13.3 | 105.7 |
| 8587 | ok | 0.09 | 7.65e-02 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.9 | 2.1 | 0.2 | -235.6 | -26.9 | 118.1 |
| 8588 | ok | 0.09 | 0.1 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.7 | -2.0 | 32.7 | 279.9 | 124.8 | -250.2 |
| 8589 | ok | 0.09 | 6.31e-02 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.6 | 5.5 | -3.6 | -183.5 | 38.0 | 116.6 |
| 8590 | ok | 0.09 | 6.93e-02 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.8 | 4.3 | -1.6 | -205.9 | 16.5 | 118.2 |
| 8591 | ok | 0.09 | 7.85e-02 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.6 | 1.8 | -3.9 | -230.8 | -9.7 | 119.3 |
| 8592 | ok | 0.09 | 0.1 | 1.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.2 | -4.3 | 35.1 | 279.7 | 135.1 | -259.7 |
| 8593 | ok | 0.09 | 6.51e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.4 | 5.2 | 0.4 | -181.6 | 40.5 | 129.8 |
| 8594 | ok | 0.09 | 7.11e-02 | 1.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.8 | 4.0 | -2.3 | -203.9 | 17.6 | 131.2 |
| 8595 | ok | 0.09 | 8.03e-02 | 1.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.8 | 1.4 | -1.7 | -227.8 | -8.0 | 131.1 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-------|-------|----------|--------|--------|-----------|
| 8596 | ok | 0.09 | 0.1 | 1.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.2 | -6.4 | 37.2 | 278.3 | 146.0 | -268.7 |
| 8597 | ok | 0.09 | 6.72e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.8 | 5.4 | -0.7 | -179.4 | 42.1 | 143.3 |
| 8598 | ok | 0.09 | 7.29e-02 | 1.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.9 | 3.0 | 5.89e-02 | 5.7 | 1.4 | 23.3 |
| 8599 | ok | 0.09 | 8.21e-02 | 1.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.9 | -1.8 | 7.7 | 234.6 | 19.3 | -121.1 |
| 8600 | ok | 0.09 | 0.1 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.5 | -8.2 | 38.9 | 275.8 | 157.1 | -277.0 |
| 8601 | ok | 0.09 | 6.94e-02 | 1.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.9 | 5.5 | 4.6 | 5.5 | 0.4 | 23.7 |
| 8602 | ok | 0.09 | 7.47e-02 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.9 | 3.3 | 2.2 | 6.6 | 1.4 | 23.2 |
| 8603 | ok | 0.09 | 8.38e-02 | 1.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.8 | -2.1 | 9.8 | 231.4 | 20.1 | -133.9 |
| 8604 | ok | 0.09 | 0.1 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.9 | -9.5 | 39.8 | 271.9 | 168.4 | -284.3 |
| 8605 | ok | 0.09 | 7.15e-02 | 1.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.9 | 6.8 | 6.8 | 6.3 | 0.3 | 23.5 |
| 8606 | ok | 0.09 | 7.64e-02 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.8 | 3.7 | 4.3 | 7.5 | 1.2 | 23.0 |
| 8607 | ok | 0.09 | 8.52e-02 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.7 | -2.5 | 11.5 | 227.0 | 21.2 | -146.6 |
| 8608 | ok | 0.09 | 0.1 | 1.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.4 | -10.3 | 39.4 | 264.8 | 180.3 | -289.6 |
| 8609 | ok | 0.09 | 7.33e-02 | 9.50e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.7 | 7.9 | 6.6 | 7.0 | -0.1 | 23.3 |
| 8610 | ok | 0.09 | 7.77e-02 | 9.86e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -43.1 | 3.6 | 6.1 | 8.4 | 0.9 | 22.8 |
| 8611 | ok | 0.09 | 8.65e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.1 | -3.0 | 12.7 | 222.0 | 22.0 | -158.6 |
| 8612 | ok | 0.09 | 0.1 | 1.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.6 | -6.6 | 14.0 | 242.0 | 60.7 | -184.2 |
| 8613 | ok | 0.09 | 7.44e-02 | 8.13e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.7 | 8.2 | 8.1 | 7.6 | -0.8 | 23.1 |
| 8614 | ok | 0.09 | 7.88e-02 | 8.87e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -34.9 | 3.6 | 7.4 | 9.2 | -0.2 | 22.8 |
| 8615 | ok | 0.09 | 8.82e-02 | 1.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.8 | -3.7 | 13.3 | 217.0 | 24.6 | -172.1 |
| 8616 | ok | 0.09 | 0.1 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.6 | -7.0 | 13.8 | 238.3 | 63.3 | -196.2 |
| 8618 | ok | 0.09 | 7.48e-02 | 6.58e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.5 | 7.8 | 7.5 | 8.1 | -1.7 | 22.9 |
| 8619 | ok | 0.09 | 7.93e-02 | 7.75e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -29.9 | 2.7 | 6.7 | 10.0 | -1.1 | 22.5 |
| 8620 | ok | 0.09 | 8.89e-02 | 9.25e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.0 | -4.4 | 12.3 | 210.0 | 25.0 | -182.5 |
| 8621 | ok | 0.09 | 0.1 | 1.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.1 | -7.7 | 11.4 | 229.4 | 64.1 | -205.1 |
| 8623 | ok | 0.09 | 7.55e-02 | 5.16e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.6 | 7.9 | 4.9 | 8.9 | -3.1 | 22.8 |
| 8624 | ok | 0.09 | 7.96e-02 | 6.65e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.6 | 2.2 | 8.5 | 10.5 | -0.9 | 25.2 |
| 8625 | ok | 0.09 | 8.93e-02 | 8.38e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -35.0 | -5.1 | 10.0 | 203.4 | 25.4 | -191.7 |
| 8626 | ok | 0.09 | 0.1 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.6 | -7.9 | 8.6 | 221.3 | 64.4 | -213.6 |
| 8628 | ok | 0.09 | 8.07e-02 | 4.18e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -14.5 | 8.9 | 5.1 | 8.8 | -3.4 | 26.1 |
| 8629 | ok | 0.09 | 7.97e-02 | 5.79e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.5 | 1.4 | 12.4 | 97.8 | -20.1 | -46.9 |
| 8630 | ok | 0.09 | 8.97e-02 | 7.87e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.9 | -5.6 | 7.0 | 196.8 | 25.0 | -200.4 |
| 8631 | ok | 0.09 | 0.1 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.6 | -4.5 | 29.5 | 15.9 | -18.2 | 4.3 |
| 8633 | ok | 0.09 | 8.48e-02 | 3.97e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.9 | 6.5 | 9.9 | 81.0 | -26.5 | -48.0 |
| 8634 | ok | 0.09 | 8.00e-02 | 5.85e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -19.2 | -4.8 | -10.6 | -189.6 | 21.5 | 286.8 |
| 8635 | ok | 0.09 | 9.00e-02 | 8.28e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -30.0 | -6.0 | 5.5 | 308.0 | 45.4 | -356.6 |
| 8636 | ok | 0.09 | 0.1 | 1.65e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.9 | -3.4 | 27.5 | 19.9 | -20.5 | 3.0 |
| 8638 | ok | 0.09 | 8.86e-02 | 4.56e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -17.5 | 3.5 | -8.1 | -116.7 | 23.7 | 209.7 |
| 8639 | ok | 0.09 | 8.05e-02 | 6.52e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -20.6 | -6.3 | -13.4 | -174.8 | 22.3 | 287.3 |
| 8640 | ok | 0.09 | 9.05e-02 | 9.06e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -26.6 | -7.4 | -12.0 | -198.3 | -28.2 | 274.0 |
| 8641 | ok | 0.09 | 0.1 | 1.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.7 | -1.2 | 25.3 | 22.0 | -21.0 | -3.34e-02 |
| 8644 | ok | 0.09 | 8.31e-02 | 5.55e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -16.9 | -6.6 | -13.6 | -64.0 | 17.9 | 55.4 |
| 8645 | ok | 0.09 | 8.15e-02 | 7.57e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -22.9 | -7.9 | -16.1 | -161.9 | 23.2 | 287.2 |
| 8646 | ok | 0.09 | 9.13e-02 | 1.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -28.5 | -8.0 | -14.5 | -182.8 | -29.7 | 275.3 |
| 8647 | ok | 0.09 | 0.1 | 1.93e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.0 | -23.5 | -51.6 | -107.3 | 223.5 | 134.4 |
| 8649 | ok | 0.09 | 7.91e-02 | 6.94e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.5 | -8.1 | -16.3 | -130.2 | 28.7 | 286.6 |
| 8650 | ok | 0.09 | 8.31e-02 | 8.84e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -26.4 | -9.4 | -18.3 | -150.9 | 24.5 | 286.7 |
| 8651 | ok | 0.09 | 9.23e-02 | 1.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.2 | -8.7 | -16.6 | -168.2 | -31.4 | 276.1 |
| 8652 | ok | 0.09 | 0.1 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.0 | -25.5 | -55.3 | -95.0 | 229.2 | 149.6 |
| 8654 | ok | 0.09 | 8.07e-02 | 8.61e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.3 | -10.9 | -17.7 | -125.4 | 31.2 | 284.8 |
| 8655 | ok | 0.09 | 8.53e-02 | 1.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.8 | -11.0 | -19.8 | -141.4 | 26.9 | 285.9 |
| 8656 | ok | 0.09 | 9.36e-02 | 1.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.3 | -9.3 | -18.0 | -154.5 | -33.5 | 276.3 |
| 8657 | ok | 0.09 | 0.1 | 2.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.3 | -26.9 | -58.7 | -79.2 | 234.1 | 163.0 |
| 8658 | ok | 0.09 | 8.48e-02 | 1.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.7 | -14.0 | -17.5 | -122.0 | 36.6 | 283.4 |
| 8659 | ok | 0.09 | 8.79e-02 | 1.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.5 | -10.4 | -17.3 | 15.4 | -1.3 | -0.8 |
| 8660 | ok | 0.09 | 9.48e-02 | 1.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.6 | -10.2 | -18.7 | -141.5 | -36.9 | 275.8 |
| 8661 | ok | 0.09 | 0.1 | 2.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.6 | -29.0 | -60.0 | -68.5 | 238.3 | 183.7 |
| 8662 | ok | 0.09 | 8.97e-02 | 1.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.8 | -17.9 | -15.9 | -102.8 | 48.4 | 306.6 |
| 8663 | ok | 0.09 | 9.10e-02 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.3 | -13.5 | -20.8 | 17.8 | 6.3 | 0.6 |
| 8664 | ok | 0.09 | 9.65e-02 | 1.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.8 | -11.5 | -18.5 | -128.6 | -42.3 | 297.6 |
| 8665 | ok | 0.09 | 0.1 | 2.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.5 | -4.1 | -12.6 | -112.3 | -104.9 | 272.9 |
| 8666 | ok | 0.09 | 9.44e-02 | 1.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.6 | -22.7 | -13.9 | -101.3 | -61.9 | 305.0 |
| 8667 | ok | 0.09 | 9.42e-02 | 1.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.1 | -16.6 | -19.5 | 20.5 | 17.7 | 3.9 |
| 8668 | ok | 0.09 | 9.80e-02 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.2 | -13.1 | -17.7 | -116.4 | -51.3 | 294.5 |
| 8669 | ok | 0.09 | 0.1 | 2.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.4 | -4.6 | -12.2 | -97.9 | -114.6 | 270.1 |
| 8670 | ok | 0.09 | 9.91e-02 | 1.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.3 | -27.8 | -12.6 | -100.4 | -87.7 | 301.2 |
| 8671 | ok | 0.09 | 9.77e-02 | 1.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.5 | -21.6 | -16.9 | -101.4 | -79.0 | 298.9 |
| 8672 | ok | 0.09 | 9.94e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.6 | -10.2 | -13.7 | -108.0 | -89.8 | 272.8 |
| 8673 | ok | 0.09 | 0.1 | 2.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.4 | -5.6 | -11.4 | -83.2 | -127.3 | 259.8 |
| 8674 | ok | 0.09 | 0.1 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.3 | -33.0 | -12.0 | -100.2 | -128.4 | 293.6 |
| 8675 | ok | 0.09 | 0.1 | 1.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.1 | -20.2 | -14.1 | -103.9 | -94.0 | 278.1 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-----------|-------|-------|---------|--------|--------|
| 8676 | ok | 0.09 | 0.1 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.4 | -12.3 | -12.7 | -97.6 | -115.9 | 266.3 |
| 8677 | ok | 0.09 | 0.1 | 2.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.8 | -7.0 | -9.8 | -68.8 | -144.0 | 238.3 |
| 8678 | ok | 0.09 | 0.1 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.0 | -38.2 | -12.1 | -101.2 | -189.6 | 280.8 |
| 8679 | ok | 0.09 | 0.1 | 1.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.2 | -23.3 | -16.8 | -95.4 | -145.7 | 272.4 |
| 8680 | ok | 0.09 | 0.1 | 2.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.5 | -8.8 | -6.9 | -55.3 | -165.4 | 201.5 |
| 8681 | ok | 0.09 | 0.1 | 1.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.7 | -41.9 | -12.4 | -105.4 | -284.5 | 259.5 |
| 8682 | ok | 0.09 | 0.1 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.3 | -24.8 | -16.0 | -84.2 | -223.2 | 249.9 |
| 8683 | ok | 0.09 | 0.1 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.8 | -15.6 | -8.3 | -68.1 | -201.7 | 219.5 |
| 8684 | ok | 0.09 | 0.1 | 2.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.4 | -10.9 | -2.7 | -41.2 | -187.4 | 148.1 |
| 8685 | ok | 0.09 | 0.1 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -67.9 | -44.0 | -19.6 | -83.9 | -412.4 | 252.6 |
| 8686 | ok | 0.09 | 0.1 | 1.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.2 | -26.6 | -13.8 | -66.1 | -315.0 | 197.3 |
| 8687 | ok | 0.09 | 0.1 | 1.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.3 | -18.4 | -4.8 | -43.5 | -249.5 | 167.1 |
| 8688 | ok | 0.09 | 0.1 | 2.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.6 | -21.6 | -54.6 | 19.2 | -150.8 | -182.7 |
| 8689 | ok | 0.09 | 0.2 | 1.73e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.7 | -7.9 | 24.6 | -126.5 | -871.9 | 89.7 |
| 8690 | ok | 0.09 | 0.1 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.3 | -25.7 | 29.6 | -87.8 | -582.6 | 81.4 |
| 8691 | ok | 0.09 | 0.1 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.3 | -18.5 | 23.9 | -52.9 | -372.3 | 79.0 |
| 8692 | ok | 0.09 | 9.89e-02 | 3.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.4 | -18.3 | -57.7 | -171.0 | -390.8 | -275.5 |
| 8693 | ok | 0.09 | 0.2 | 3.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -125.6 | -26.6 | -51.6 | -620.7 | -360.3 | -635.4 |
| 8694 | ok | 0.09 | 0.1 | 2.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -112.1 | -16.5 | -30.6 | -416.5 | -192.5 | -453.6 |
| 8695 | ok | 0.09 | 9.44e-02 | 2.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -101.4 | -13.9 | -23.4 | -264.2 | -157.3 | -346.8 |
| 8696 | ok | 0.09 | 9.80e-02 | 4.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -106.9 | 5.9 | -55.1 | -225.7 | -354.5 | -246.5 |
| 8697 | ok | 0.09 | 0.2 | 4.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -194.0 | -17.0 | 0.1 | -925.2 | -221.8 | -570.7 |
| 8698 | ok | 0.09 | 0.1 | 3.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -156.5 | -6.6 | -7.8 | -602.5 | -101.9 | -448.4 |
| 8699 | ok | 0.09 | 9.85e-02 | 2.99e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -133.1 | -2.9 | -7.5 | -367.8 | -106.3 | -330.6 |
| 8700 | ok | 0.09 | 0.1 | 4.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -131.4 | -44.6 | 97.0 | -7.9 | 405.1 | -408.2 |
| 8701 | ok | 0.09 | 0.2 | 4.91e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -225.2 | -22.1 | 4.4 | -1076.0 | 99.7 | -580.3 |
| 8702 | ok | 0.09 | 0.1 | 4.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -184.0 | -2.8 | 23.2 | -732.0 | 30.1 | -405.6 |
| 8703 | ok | 0.09 | 9.74e-02 | 3.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -154.9 | -3.6 | 31.3 | -423.4 | 70.0 | -305.8 |
| 8708 | ok | 0.09 | 0.2 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | 35.9 | -29.6 | -13.9 | 28.4 | -592.7 | -32.3 |
| 8709 | ok | 0.09 | 0.1 | 2.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.4 | -57.2 | 44.5 | -51.5 | -633.9 | -53.6 |
| 8710 | ok | 0.09 | 0.1 | 4.62e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.0 | -18.3 | 3.8 | -6.6 | -297.0 | -36.0 |
| 8711 | ok | 0.09 | 9.68e-02 | 8.77e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -5.2 | -30.5 | 16.4 | -36.4 | -430.4 | -142.8 |
| 8712 | ok | 0.09 | 9.88e-02 | 2.04e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -5.96e-02 | 26.5 | -3.7 | 16.7 | 57.4 | -2.5 |
| 8713 | ok | 0.09 | 7.65e-02 | 6.03e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.0 | -20.9 | 10.7 | -34.5 | -319.5 | -200.6 |
| 8714 | ok | 0.09 | 9.67e-02 | 8.07e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -0.9 | 28.2 | 2.4 | -4.0 | 1.6 | -50.4 |
| 8715 | ok | 0.09 | 8.93e-02 | 4.63e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -5.4 | -19.2 | 7.5 | -51.3 | -194.3 | -140.4 |
| 8716 | ok | 0.09 | 0.1 | 4.55e-04 | 4.5 | 4.5 | 4.0 | 4.0 | 0.3 | 34.5 | 3.5 | -5.7 | -10.1 | -64.0 |
| 8717 | ok | 0.09 | 0.1 | 4.09e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -5.3 | -16.6 | 4.5 | -49.6 | -157.4 | -157.3 |
| 8718 | ok | 0.09 | 0.2 | 1.33e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 3.9 | 47.2 | 9.1 | -12.6 | -159.9 | -111.2 |
| 8719 | ok | 0.09 | 0.2 | 6.26e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -9.0 | -22.6 | -4.8 | -103.4 | -288.1 | -391.3 |
| 8720 | ok | 0.09 | 0.4 | 5.42e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 67.5 | 92.3 | 43.5 | 138.9 | -322.0 | -122.7 |
| 8721 | ok | 0.09 | 0.2 | 2.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.5 | -80.5 | -59.9 | -331.7 | -630.9 | -746.0 |
| 8722 | ok | 0.09 | 9.78e-02 | 2.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.9 | -2.7 | -24.7 | -64.5 | -244.8 | -22.8 |
| 8723 | ok | 0.09 | 0.1 | 2.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.1 | -42.0 | 87.1 | 76.3 | 61.4 | 27.5 |
| 8724 | ok | 0.09 | 0.1 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.7 | -27.4 | 24.7 | -67.8 | -472.6 | -33.5 |
| 8725 | ok | 0.09 | 7.56e-02 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.5 | -20.9 | 15.4 | -46.6 | -334.6 | -15.0 |
| 8726 | ok | 0.09 | 8.48e-02 | 1.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.6 | -5.0 | -17.4 | -60.9 | -259.8 | -71.6 |
| 8727 | ok | 0.09 | 0.1 | 2.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.5 | -41.3 | 78.5 | 113.7 | 80.6 | -115.5 |
| 8728 | ok | 0.09 | 7.89e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -18.6 | -29.5 | 22.1 | -66.6 | -346.7 | -125.7 |
| 8729 | ok | 0.09 | 5.99e-02 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.7 | -23.7 | 13.0 | -56.0 | -268.7 | -101.3 |
| 8730 | ok | 0.09 | 9.04e-02 | 1.74e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.6 | -6.6 | -17.9 | -46.1 | -241.4 | -79.5 |
| 8731 | ok | 0.09 | 0.1 | 2.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.5 | -32.2 | 72.0 | 108.7 | 190.2 | -209.4 |
| 8732 | ok | 0.09 | 6.98e-02 | 8.58e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -12.2 | -28.6 | 15.0 | -70.3 | -257.3 | -187.4 |
| 8733 | ok | 0.09 | 5.95e-02 | 1.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -26.0 | -26.6 | 7.6 | -66.3 | -211.0 | -163.1 |
| 8734 | ok | 0.09 | 8.68e-02 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.3 | -14.7 | -25.0 | -54.5 | -254.8 | -126.9 |
| 8735 | ok | 0.09 | 0.1 | 2.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.2 | -21.4 | 65.3 | 99.1 | 269.1 | -249.9 |
| 8736 | ok | 0.09 | 7.65e-02 | 7.26e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -10.5 | -28.5 | 8.6 | -84.1 | -203.1 | -237.4 |
| 8737 | ok | 0.09 | 6.17e-02 | 8.54e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.1 | -29.4 | 0.3 | -82.0 | -175.2 | -208.9 |
| 8738 | ok | 0.09 | 8.90e-02 | 1.77e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.3 | -33.2 | -43.3 | -80.8 | -331.0 | -197.1 |
| 8739 | ok | 0.09 | 0.1 | 2.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.4 | -33.0 | -80.0 | -34.4 | -482.7 | -218.3 |
| 8740 | ok | 0.09 | 7.95e-02 | 6.88e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -13.5 | -27.8 | -3.5 | -109.1 | -195.5 | -288.1 |
| 8741 | ok | 0.09 | 6.83e-02 | 9.53e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -30.2 | -30.2 | -13.3 | -99.3 | -172.9 | -250.3 |
| 8742 | ok | 0.09 | 8.80e-02 | 2.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.0 | -36.8 | -51.3 | -106.0 | -356.0 | -229.5 |
| 8743 | ok | 0.09 | 0.1 | 2.97e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.7 | 5.7 | 56.8 | 127.4 | 471.6 | -351.0 |
| 8744 | ok | 0.09 | 8.93e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -26.2 | -34.0 | -17.1 | -170.5 | -203.9 | -348.8 |
| 8745 | ok | 0.09 | 7.67e-02 | 1.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.7 | -30.7 | -21.8 | -136.8 | -171.2 | -285.1 |
| 8746 | ok | 0.09 | 9.47e-02 | 2.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.6 | -32.5 | -57.0 | -137.1 | -380.2 | -257.3 |
| 8747 | ok | 0.09 | 0.2 | 3.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.6 | -5.2 | 77.3 | 118.9 | 501.5 | -334.2 |
| 8748 | ok | 0.09 | 0.1 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.9 | -31.3 | -30.1 | -276.0 | -227.6 | -408.6 |
| 8749 | ok | 0.09 | 8.61e-02 | 1.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.4 | -25.3 | -27.1 | -191.8 | -173.6 | -319.0 |
| 9841 | ok | 0.09 | 0.1 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.3 | -14.2 | -11.1 | -85.0 | -152.8 | 250.0 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|-------|----------|--------|--------|---------|---------|---------|---------|---------|----------|----------|----------|
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | 0.09 | 0.45 | 0.08 | 4.52 | 4.52 | 4.00 | 4.00 | -362.86 | -127.90 | -114.40 | -1271.36 | -1392.63 | -1022.77 |
| | | | | | | | | | 67.48 | 99.43 | 180.87 | 810.87 | 658.01 | 474.50 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 22 | ok | 0.84 | | | | | | |
| 23 | ok | 0.64 | | | | | | |
| 43 | ok | 0.89 | | | | | | |
| 44 | ok | 0.61 | | | | | | |
| 45 | ok | 0.62 | | | | | | |
| 46 | ok | 0.35 | | | | | | |
| 47 | ok | 0.41 | | | | | | |
| 48 | ok | 0.36 | | | | | | |
| 49 | ok | 0.96 | | | | | | |
| 50 | ok | 0.27 | | | | | | |
| 4786 | ok | 0.62 | | | | | | |
| 4965 | ok | 0.64 | | | | | | |
| 4998 | ok | 0.65 | | | | | | |
| 5026 | ok | 0.84 | | | | | | |
| 5043 | ok | 0.74 | | | | | | |
| 5060 | ok | 0.66 | | | | | | |
| 5102 | ok | 0.90 | | | | | | |
| 5119 | ok | 0.73 | | | | | | |
| 5136 | ok | 0.61 | | | | | | |
| 5153 | ok | 0.53 | | | | | | |
| 5170 | ok | 0.47 | | | | | | |
| 5187 | ok | 0.42 | | | | | | |
| 5204 | ok | 0.39 | | | | | | |
| 5261 | ok | 0.39 | | | | | | |
| 5278 | ok | 0.36 | | | | | | |
| 5295 | ok | 0.32 | | | | | | |
| 5312 | ok | 0.28 | | | | | | |
| 5329 | ok | 0.24 | | | | | | |
| 5346 | ok | 0.25 | | | | | | |
| 5363 | ok | 0.28 | | | | | | |
| 5380 | ok | 0.31 | | | | | | |
| 5397 | ok | 0.33 | | | | | | |
| 5457 | ok | 0.67 | | | | | | |
| 5474 | ok | 0.68 | | | | | | |
| 5491 | ok | 0.70 | | | | | | |
| 5508 | ok | 0.89 | | | | | | |
| 5563 | ok | 0.28 | | | | | | |
| 5580 | ok | 0.29 | | | | | | |
| 5597 | ok | 0.33 | | | | | | |
| 5614 | ok | 0.38 | | | | | | |
| 5631 | ok | 0.43 | | | | | | |
| 5648 | ok | 0.48 | | | | | | |
| 5665 | ok | 0.53 | | | | | | |
| 5682 | ok | 0.57 | | | | | | |
| 5699 | ok | 0.61 | | | | | | |
| 5766 | ok | 0.61 | | | | | | |
| 5768 | ok | 0.61 | | | | | | |
| 5770 | ok | 0.62 | | | | | | |
| 5772 | ok | 0.63 | | | | | | |
| 5774 | ok | 0.64 | | | | | | |
| 5776 | ok | 0.64 | | | | | | |
| 5778 | ok | 0.64 | | | | | | |
| 5780 | ok | 0.64 | | | | | | |
| 5809 | ok | 0.28 | | | | | | |
| 5811 | ok | 0.29 | | | | | | |
| 5813 | ok | 0.31 | | | | | | |
| 5815 | ok | 0.32 | | | | | | |
| 5817 | ok | 0.33 | | | | | | |
| 5819 | ok | 0.34 | | | | | | |
| 5821 | ok | 0.35 | | | | | | |
| 5823 | ok | 0.35 | | | | | | |
| 5849 | ok | 0.42 | | | | | | |
| 5851 | ok | 0.42 | | | | | | |
| 5853 | ok | 0.41 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 5855 | ok | 0.40 | | | | | | |
| 5857 | ok | 0.39 | | | | | | |
| 5859 | ok | 0.37 | | | | | | |
| 5861 | ok | 0.36 | | | | | | |
| 5863 | ok | 0.35 | | | | | | |
| 6983 | ok | 0.59 | | | | | | |
| 7003 | ok | 0.59 | | | | | | |
| 7023 | ok | 0.50 | | | | | | |
| 7043 | ok | 0.50 | | | | | | |
| 7324 | ok | 0.44 | | | | | | |
| 7325 | ok | 0.44 | | | | | | |
| 7342 | ok | 0.38 | | | | | | |
| 7343 | ok | 0.48 | | | | | | |
| 7344 | ok | 0.42 | | | | | | |
| 7345 | ok | 0.19 | | | | | | |
| 7346 | ok | 0.24 | | | | | | |
| 7347 | ok | 0.34 | | | | | | |
| 7348 | ok | 0.47 | | | | | | |
| 7349 | ok | 0.25 | | | | | | |
| 7539 | ok | 0.48 | | | | | | |
| 7540 | ok | 0.48 | | | | | | |
| 7541 | ok | 0.47 | | | | | | |
| 7542 | ok | 0.44 | | | | | | |
| 7543 | ok | 0.43 | | | | | | |
| 7544 | ok | 0.44 | | | | | | |
| 7545 | ok | 0.46 | | | | | | |
| 7546 | ok | 0.45 | | | | | | |
| 7547 | ok | 0.43 | | | | | | |
| 7548 | ok | 0.41 | | | | | | |
| 7549 | ok | 0.40 | | | | | | |
| 7550 | ok | 0.38 | | | | | | |
| 7551 | ok | 0.36 | | | | | | |
| 7552 | ok | 0.22 | | | | | | |
| 7553 | ok | 0.21 | | | | | | |
| 7554 | ok | 0.19 | | | | | | |
| 7555 | ok | 0.18 | | | | | | |
| 7556 | ok | 0.17 | | | | | | |
| 7557 | ok | 0.16 | | | | | | |
| 7558 | ok | 0.16 | | | | | | |
| 7559 | ok | 0.17 | | | | | | |
| 7560 | ok | 0.18 | | | | | | |
| 7561 | ok | 0.45 | | | | | | |
| 7562 | ok | 0.44 | | | | | | |
| 7563 | ok | 0.42 | | | | | | |
| 7564 | ok | 0.39 | | | | | | |
| 7565 | ok | 0.25 | | | | | | |
| 7566 | ok | 0.27 | | | | | | |
| 7567 | ok | 0.29 | | | | | | |
| 7568 | ok | 0.31 | | | | | | |
| 7569 | ok | 0.33 | | | | | | |
| 7570 | ok | 0.35 | | | | | | |
| 7571 | ok | 0.37 | | | | | | |
| 7572 | ok | 0.39 | | | | | | |
| 7573 | ok | 0.40 | | | | | | |
| 7575 | ok | 0.48 | | | | | | |
| 7576 | ok | 0.48 | | | | | | |
| 7577 | ok | 0.48 | | | | | | |
| 7578 | ok | 0.47 | | | | | | |
| 7579 | ok | 0.46 | | | | | | |
| 7580 | ok | 0.46 | | | | | | |
| 7581 | ok | 0.45 | | | | | | |
| 7582 | ok | 0.43 | | | | | | |
| 7583 | ok | 0.24 | | | | | | |
| 7584 | ok | 0.23 | | | | | | |
| 7585 | ok | 0.23 | | | | | | |
| 7586 | ok | 0.23 | | | | | | |
| 7587 | ok | 0.22 | | | | | | |
| 7588 | ok | 0.21 | | | | | | |
| 7589 | ok | 0.21 | | | | | | |
| 7590 | ok | 0.20 | | | | | | |
| 7591 | ok | 0.25 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 7592 | ok | 0.26 | | | | | | |
| 7593 | ok | 0.28 | | | | | | |
| 7594 | ok | 0.29 | | | | | | |
| 7595 | ok | 0.30 | | | | | | |
| 7596 | ok | 0.31 | | | | | | |
| 7597 | ok | 0.32 | | | | | | |
| 7598 | ok | 0.33 | | | | | | |
| 7645 | ok | 0.19 | | | | | | |
| 7646 | ok | 0.27 | | | | | | |
| 7647 | ok | 0.35 | | | | | | |
| 7648 | ok | 0.35 | | | | | | |
| 8361 | ok | 0.84 | | | | | | |
| 8362 | ok | 0.58 | | | | | | |
| 8363 | ok | 0.58 | | | | | | |
| 8364 | ok | 0.53 | | | | | | |
| 8365 | ok | 0.84 | | | | | | |
| 8366 | ok | 0.58 | | | | | | |
| 8367 | ok | 0.58 | | | | | | |
| 8368 | ok | 0.53 | | | | | | |
| 8369 | ok | 0.50 | | | | | | |
| 8370 | ok | 0.22 | | | | | | |
| 8371 | ok | 0.22 | | | | | | |
| 8372 | ok | 0.27 | | | | | | |
| 8373 | ok | 0.36 | | | | | | |
| 8374 | ok | 0.74 | | | | | | |
| 8375 | ok | 0.42 | | | | | | |
| 8376 | ok | 0.36 | | | | | | |
| 8377 | ok | 0.28 | | | | | | |
| 8378 | ok | 0.66 | | | | | | |
| 8379 | ok | 0.33 | | | | | | |
| 8380 | ok | 0.27 | | | | | | |
| 8381 | ok | 0.21 | | | | | | |
| 8382 | ok | 0.57 | | | | | | |
| 8383 | ok | 0.26 | | | | | | |
| 8384 | ok | 0.20 | | | | | | |
| 8385 | ok | 0.13 | | | | | | |
| 8386 | ok | 0.46 | | | | | | |
| 8387 | ok | 0.68 | | | | | | |
| 8388 | ok | 0.44 | | | | | | |
| 8389 | ok | 0.19 | | | | | | |
| 8390 | ok | 0.13 | | | | | | |
| 8391 | ok | 0.09 | | | | | | |
| 8392 | ok | 0.47 | | | | | | |
| 8393 | ok | 0.72 | | | | | | |
| 8394 | ok | 0.46 | | | | | | |
| 8395 | ok | 0.14 | | | | | | |
| 8396 | ok | 0.08 | | | | | | |
| 8397 | ok | 0.07 | | | | | | |
| 8398 | ok | 0.47 | | | | | | |
| 8399 | ok | 0.76 | | | | | | |
| 8400 | ok | 0.49 | | | | | | |
| 8401 | ok | 0.11 | | | | | | |
| 8402 | ok | 0.07 | | | | | | |
| 8403 | ok | 0.07 | | | | | | |
| 8404 | ok | 0.47 | | | | | | |
| 8405 | ok | 0.83 | | | | | | |
| 8406 | ok | 0.53 | | | | | | |
| 8407 | ok | 0.10 | | | | | | |
| 8408 | ok | 0.07 | | | | | | |
| 8409 | ok | 0.07 | | | | | | |
| 8410 | ok | 0.47 | | | | | | |
| 8411 | ok | 0.96 | | | | | | |
| 8412 | ok | 0.55 | | | | | | |
| 8413 | ok | 0.09 | | | | | | |
| 8414 | ok | 0.07 | | | | | | |
| 8415 | ok | 0.07 | | | | | | |
| 8416 | ok | 0.55 | | | | | | |
| 8417 | ok | 0.08 | | | | | | |
| 8418 | ok | 0.07 | | | | | | |
| 8419 | ok | 0.07 | | | | | | |
| 8420 | ok | 0.44 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 8421 | ok | 0.07 | | | | | | |
| 8422 | ok | 0.07 | | | | | | |
| 8423 | ok | 0.07 | | | | | | |
| 8424 | ok | 0.38 | | | | | | |
| 8425 | ok | 0.06 | | | | | | |
| 8426 | ok | 0.07 | | | | | | |
| 8427 | ok | 0.07 | | | | | | |
| 8428 | ok | 0.33 | | | | | | |
| 8429 | ok | 0.07 | | | | | | |
| 8430 | ok | 0.07 | | | | | | |
| 8431 | ok | 0.07 | | | | | | |
| 8432 | ok | 0.29 | | | | | | |
| 8433 | ok | 0.07 | | | | | | |
| 8434 | ok | 0.07 | | | | | | |
| 8435 | ok | 0.07 | | | | | | |
| 8436 | ok | 0.26 | | | | | | |
| 8437 | ok | 0.07 | | | | | | |
| 8438 | ok | 0.07 | | | | | | |
| 8439 | ok | 0.07 | | | | | | |
| 8440 | ok | 0.23 | | | | | | |
| 8441 | ok | 0.07 | | | | | | |
| 8442 | ok | 0.07 | | | | | | |
| 8443 | ok | 0.07 | | | | | | |
| 8444 | ok | 0.20 | | | | | | |
| 8445 | ok | 0.07 | | | | | | |
| 8446 | ok | 0.07 | | | | | | |
| 8447 | ok | 0.07 | | | | | | |
| 8448 | ok | 0.18 | | | | | | |
| 8449 | ok | 0.08 | | | | | | |
| 8450 | ok | 0.08 | | | | | | |
| 8451 | ok | 0.08 | | | | | | |
| 8453 | ok | 0.17 | | | | | | |
| 8454 | ok | 0.08 | | | | | | |
| 8455 | ok | 0.08 | | | | | | |
| 8456 | ok | 0.08 | | | | | | |
| 8458 | ok | 0.16 | | | | | | |
| 8459 | ok | 0.08 | | | | | | |
| 8460 | ok | 0.08 | | | | | | |
| 8461 | ok | 0.08 | | | | | | |
| 8463 | ok | 0.15 | | | | | | |
| 8464 | ok | 0.08 | | | | | | |
| 8465 | ok | 0.08 | | | | | | |
| 8466 | ok | 0.08 | | | | | | |
| 8468 | ok | 0.16 | | | | | | |
| 8469 | ok | 0.08 | | | | | | |
| 8470 | ok | 0.08 | | | | | | |
| 8471 | ok | 0.08 | | | | | | |
| 8473 | ok | 0.16 | | | | | | |
| 8474 | ok | 0.08 | | | | | | |
| 8475 | ok | 0.08 | | | | | | |
| 8476 | ok | 0.08 | | | | | | |
| 8478 | ok | 0.16 | | | | | | |
| 8479 | ok | 0.08 | | | | | | |
| 8480 | ok | 0.08 | | | | | | |
| 8481 | ok | 0.08 | | | | | | |
| 8483 | ok | 0.16 | | | | | | |
| 8484 | ok | 0.08 | | | | | | |
| 8485 | ok | 0.08 | | | | | | |
| 8486 | ok | 0.08 | | | | | | |
| 8488 | ok | 0.16 | | | | | | |
| 8489 | ok | 0.08 | | | | | | |
| 8490 | ok | 0.08 | | | | | | |
| 8491 | ok | 0.08 | | | | | | |
| 8492 | ok | 0.16 | | | | | | |
| 8493 | ok | 0.08 | | | | | | |
| 8494 | ok | 0.08 | | | | | | |
| 8495 | ok | 0.08 | | | | | | |
| 8496 | ok | 0.15 | | | | | | |
| 8497 | ok | 0.08 | | | | | | |
| 8498 | ok | 0.08 | | | | | | |
| 8499 | ok | 0.08 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 8500 | ok | 0.14 | | | | | | |
| 8501 | ok | 0.08 | | | | | | |
| 8502 | ok | 0.08 | | | | | | |
| 8503 | ok | 0.08 | | | | | | |
| 8504 | ok | 0.13 | | | | | | |
| 8505 | ok | 0.08 | | | | | | |
| 8506 | ok | 0.08 | | | | | | |
| 8507 | ok | 0.08 | | | | | | |
| 8508 | ok | 0.12 | | | | | | |
| 8509 | ok | 0.08 | | | | | | |
| 8510 | ok | 0.08 | | | | | | |
| 8511 | ok | 0.08 | | | | | | |
| 8512 | ok | 0.11 | | | | | | |
| 8513 | ok | 0.08 | | | | | | |
| 8514 | ok | 0.08 | | | | | | |
| 8515 | ok | 0.08 | | | | | | |
| 8516 | ok | 0.10 | | | | | | |
| 8517 | ok | 0.08 | | | | | | |
| 8518 | ok | 0.08 | | | | | | |
| 8519 | ok | 0.08 | | | | | | |
| 8520 | ok | 0.10 | | | | | | |
| 8521 | ok | 0.08 | | | | | | |
| 8522 | ok | 0.08 | | | | | | |
| 8523 | ok | 0.08 | | | | | | |
| 8524 | ok | 0.10 | | | | | | |
| 8525 | ok | 0.08 | | | | | | |
| 8526 | ok | 0.08 | | | | | | |
| 8527 | ok | 0.08 | | | | | | |
| 8528 | ok | 0.11 | | | | | | |
| 8529 | ok | 0.08 | | | | | | |
| 8530 | ok | 0.08 | | | | | | |
| 8531 | ok | 0.08 | | | | | | |
| 8532 | ok | 0.11 | | | | | | |
| 8533 | ok | 0.08 | | | | | | |
| 8534 | ok | 0.08 | | | | | | |
| 8535 | ok | 0.08 | | | | | | |
| 8536 | ok | 0.11 | | | | | | |
| 8537 | ok | 0.08 | | | | | | |
| 8538 | ok | 0.08 | | | | | | |
| 8539 | ok | 0.08 | | | | | | |
| 8540 | ok | 0.11 | | | | | | |
| 8541 | ok | 0.08 | | | | | | |
| 8542 | ok | 0.08 | | | | | | |
| 8543 | ok | 0.08 | | | | | | |
| 8544 | ok | 0.11 | | | | | | |
| 8545 | ok | 0.08 | | | | | | |
| 8546 | ok | 0.08 | | | | | | |
| 8547 | ok | 0.08 | | | | | | |
| 8549 | ok | 0.11 | | | | | | |
| 8550 | ok | 0.08 | | | | | | |
| 8551 | ok | 0.08 | | | | | | |
| 8552 | ok | 0.08 | | | | | | |
| 8554 | ok | 0.10 | | | | | | |
| 8555 | ok | 0.08 | | | | | | |
| 8556 | ok | 0.08 | | | | | | |
| 8557 | ok | 0.08 | | | | | | |
| 8559 | ok | 0.10 | | | | | | |
| 8560 | ok | 0.08 | | | | | | |
| 8561 | ok | 0.08 | | | | | | |
| 8562 | ok | 0.08 | | | | | | |
| 8564 | ok | 0.10 | | | | | | |
| 8565 | ok | 0.08 | | | | | | |
| 8566 | ok | 0.08 | | | | | | |
| 8567 | ok | 0.08 | | | | | | |
| 8569 | ok | 0.10 | | | | | | |
| 8570 | ok | 0.08 | | | | | | |
| 8571 | ok | 0.08 | | | | | | |
| 8572 | ok | 0.08 | | | | | | |
| 8573 | ok | 0.11 | | | | | | |
| 8574 | ok | 0.08 | | | | | | |
| 8575 | ok | 0.08 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 8576 | ok | 0.07 | | | | | | |
| 8577 | ok | 0.12 | | | | | | |
| 8578 | ok | 0.08 | | | | | | |
| 8579 | ok | 0.08 | | | | | | |
| 8580 | ok | 0.07 | | | | | | |
| 8581 | ok | 0.14 | | | | | | |
| 8582 | ok | 0.08 | | | | | | |
| 8583 | ok | 0.08 | | | | | | |
| 8584 | ok | 0.07 | | | | | | |
| 8585 | ok | 0.16 | | | | | | |
| 8586 | ok | 0.08 | | | | | | |
| 8587 | ok | 0.08 | | | | | | |
| 8588 | ok | 0.07 | | | | | | |
| 8589 | ok | 0.18 | | | | | | |
| 8590 | ok | 0.08 | | | | | | |
| 8591 | ok | 0.08 | | | | | | |
| 8592 | ok | 0.07 | | | | | | |
| 8593 | ok | 0.19 | | | | | | |
| 8594 | ok | 0.08 | | | | | | |
| 8595 | ok | 0.08 | | | | | | |
| 8596 | ok | 0.07 | | | | | | |
| 8597 | ok | 0.21 | | | | | | |
| 8598 | ok | 0.08 | | | | | | |
| 8599 | ok | 0.07 | | | | | | |
| 8600 | ok | 0.07 | | | | | | |
| 8601 | ok | 0.23 | | | | | | |
| 8602 | ok | 0.08 | | | | | | |
| 8603 | ok | 0.07 | | | | | | |
| 8604 | ok | 0.07 | | | | | | |
| 8605 | ok | 0.25 | | | | | | |
| 8606 | ok | 0.07 | | | | | | |
| 8607 | ok | 0.07 | | | | | | |
| 8608 | ok | 0.07 | | | | | | |
| 8609 | ok | 0.27 | | | | | | |
| 8610 | ok | 0.07 | | | | | | |
| 8611 | ok | 0.07 | | | | | | |
| 8612 | ok | 0.07 | | | | | | |
| 8613 | ok | 0.28 | | | | | | |
| 8614 | ok | 0.07 | | | | | | |
| 8615 | ok | 0.07 | | | | | | |
| 8616 | ok | 0.07 | | | | | | |
| 8618 | ok | 0.29 | | | | | | |
| 8619 | ok | 0.07 | | | | | | |
| 8620 | ok | 0.07 | | | | | | |
| 8621 | ok | 0.07 | | | | | | |
| 8623 | ok | 0.30 | | | | | | |
| 8624 | ok | 0.07 | | | | | | |
| 8625 | ok | 0.07 | | | | | | |
| 8626 | ok | 0.07 | | | | | | |
| 8628 | ok | 0.31 | | | | | | |
| 8629 | ok | 0.07 | | | | | | |
| 8630 | ok | 0.06 | | | | | | |
| 8631 | ok | 0.07 | | | | | | |
| 8633 | ok | 0.31 | | | | | | |
| 8634 | ok | 0.07 | | | | | | |
| 8635 | ok | 0.06 | | | | | | |
| 8636 | ok | 0.07 | | | | | | |
| 8638 | ok | 0.32 | | | | | | |
| 8639 | ok | 0.07 | | | | | | |
| 8640 | ok | 0.06 | | | | | | |
| 8641 | ok | 0.07 | | | | | | |
| 8644 | ok | 0.33 | | | | | | |
| 8645 | ok | 0.07 | | | | | | |
| 8646 | ok | 0.05 | | | | | | |
| 8647 | ok | 0.08 | | | | | | |
| 8649 | ok | 0.34 | | | | | | |
| 8650 | ok | 0.07 | | | | | | |
| 8651 | ok | 0.05 | | | | | | |
| 8652 | ok | 0.08 | | | | | | |
| 8654 | ok | 0.37 | | | | | | |
| 8655 | ok | 0.07 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 8656 | ok | 0.04 | | | | | | |
| 8657 | ok | 0.08 | | | | | | |
| 8658 | ok | 0.39 | | | | | | |
| 8659 | ok | 0.08 | | | | | | |
| 8660 | ok | 0.03 | | | | | | |
| 8661 | ok | 0.08 | | | | | | |
| 8662 | ok | 0.43 | | | | | | |
| 8663 | ok | 0.09 | | | | | | |
| 8664 | ok | 0.03 | | | | | | |
| 8665 | ok | 0.09 | | | | | | |
| 8666 | ok | 0.47 | | | | | | |
| 8667 | ok | 0.11 | | | | | | |
| 8668 | ok | 0.05 | | | | | | |
| 8669 | ok | 0.11 | | | | | | |
| 8670 | ok | 0.51 | | | | | | |
| 8671 | ok | 0.13 | | | | | | |
| 8672 | ok | 0.07 | | | | | | |
| 8673 | ok | 0.14 | | | | | | |
| 8674 | ok | 0.56 | | | | | | |
| 8675 | ok | 0.17 | | | | | | |
| 8676 | ok | 0.11 | | | | | | |
| 8677 | ok | 0.18 | | | | | | |
| 8678 | ok | 0.61 | | | | | | |
| 8679 | ok | 0.23 | | | | | | |
| 8680 | ok | 0.22 | | | | | | |
| 8681 | ok | 0.70 | | | | | | |
| 8682 | ok | 0.30 | | | | | | |
| 8683 | ok | 0.22 | | | | | | |
| 8684 | ok | 0.27 | | | | | | |
| 8685 | ok | 0.89 | | | | | | |
| 8686 | ok | 0.41 | | | | | | |
| 8687 | ok | 0.28 | | | | | | |
| 8688 | ok | 0.27 | | | | | | |
| 8689 | ok | 0.89 | | | | | | |
| 8690 | ok | 0.41 | | | | | | |
| 8691 | ok | 0.28 | | | | | | |
| 8692 | ok | 0.21 | | | | | | |
| 8693 | ok | 0.59 | | | | | | |
| 8694 | ok | 0.35 | | | | | | |
| 8695 | ok | 0.26 | | | | | | |
| 8696 | ok | 0.22 | | | | | | |
| 8697 | ok | 0.59 | | | | | | |
| 8698 | ok | 0.35 | | | | | | |
| 8699 | ok | 0.26 | | | | | | |
| 8700 | ok | 0.27 | | | | | | |
| 8701 | ok | 0.50 | | | | | | |
| 8702 | ok | 0.25 | | | | | | |
| 8703 | ok | 0.24 | | | | | | |
| 8708 | ok | 0.51 | | | | | | |
| 8709 | ok | 0.51 | | | | | | |
| 8710 | ok | 0.36 | | | | | | |
| 8711 | ok | 0.36 | | | | | | |
| 8712 | ok | 0.31 | | | | | | |
| 8713 | ok | 0.31 | | | | | | |
| 8714 | ok | 0.29 | | | | | | |
| 8715 | ok | 0.29 | | | | | | |
| 8716 | ok | 0.31 | | | | | | |
| 8717 | ok | 0.28 | | | | | | |
| 8718 | ok | 0.41 | | | | | | |
| 8719 | ok | 0.28 | | | | | | |
| 8720 | ok | 0.42 | | | | | | |
| 8721 | ok | 0.27 | | | | | | |
| 8722 | ok | 0.22 | | | | | | |
| 8723 | ok | 0.21 | | | | | | |
| 8724 | ok | 0.35 | | | | | | |
| 8725 | ok | 0.27 | | | | | | |
| 8726 | ok | 0.19 | | | | | | |
| 8727 | ok | 0.17 | | | | | | |
| 8728 | ok | 0.27 | | | | | | |
| 8729 | ok | 0.22 | | | | | | |
| 8730 | ok | 0.17 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 8731 | ok | 0.16 | | | | | | |
| 8732 | ok | 0.19 | | | | | | |
| 8733 | ok | 0.17 | | | | | | |
| 8734 | ok | 0.13 | | | | | | |
| 8735 | ok | 0.13 | | | | | | |
| 8736 | ok | 0.12 | | | | | | |
| 8737 | ok | 0.13 | | | | | | |
| 8738 | ok | 0.11 | | | | | | |
| 8739 | ok | 0.11 | | | | | | |
| 8740 | ok | 0.09 | | | | | | |
| 8741 | ok | 0.11 | | | | | | |
| 8742 | ok | 0.14 | | | | | | |
| 8743 | ok | 0.13 | | | | | | |
| 8744 | ok | 0.15 | | | | | | |
| 8745 | ok | 0.14 | | | | | | |
| 8746 | ok | 0.17 | | | | | | |
| 8747 | ok | 0.16 | | | | | | |
| 8748 | ok | 0.27 | | | | | | |
| 8749 | ok | 0.21 | | | | | | |
| 9841 | ok | 0.16 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 0.96 | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 69 | 40.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|-------|----------|--------|--------|---------|---------|---------|--------|---------|---------|----------|---------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 21 | ok | 0.09 | 0.3 | 3.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -155.1 | 21.6 | -46.9 | -669.9 | 540.9 | -616.7 |
| 22 | ok | 0.09 | 0.2 | 3.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -128.1 | 54.7 | -27.8 | 80.4 | 116.4 | -69.0 |
| 2775 | ok | 0.09 | 0.2 | 2.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.0 | 25.7 | -27.5 | 65.3 | 249.8 | -106.3 |
| 2776 | ok | 0.09 | 0.2 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -70.7 | 29.2 | -23.1 | 20.0 | 563.9 | -140.1 |
| 2777 | ok | 0.09 | 0.3 | 2.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -67.7 | 26.8 | -22.7 | 358.8 | 464.5 | -28.2 |
| 7323 | ok | 0.09 | 0.2 | 3.81e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -93.6 | 5.0 | 120.1 | 410.3 | 565.3 | -312.6 |
| 7324 | ok | 0.09 | 0.2 | 4.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -87.9 | -49.3 | -127.8 | -350.6 | -474.6 | -181.3 |
| 7469 | ok | 0.09 | 0.3 | 5.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -108.0 | -41.2 | -151.7 | -201.7 | -771.7 | -510.2 |
| 7470 | ok | 0.09 | 0.3 | 5.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -110.9 | -39.9 | -155.1 | -229.7 | -836.5 | -507.6 |
| 7471 | ok | 0.09 | 0.2 | 4.77e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -93.0 | 9.3 | 119.3 | 179.4 | 747.0 | -402.3 |
| 8361 | ok | 0.09 | 0.2 | 2.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -101.6 | -15.7 | -18.2 | -54.4 | -1171.2 | -29.8 |
| 8362 | ok | 0.09 | 0.2 | 2.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -101.8 | -2.5 | -22.6 | 3.9 | -276.5 | -74.8 |
| 8363 | ok | 0.09 | 0.1 | 2.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -100.4 | -2.5 | -23.4 | -18.5 | -229.0 | -63.6 |
| 8364 | ok | 0.09 | 0.1 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -92.2 | 1.5 | -32.3 | -69.5 | -247.1 | -46.3 |
| 8750 | ok | 0.09 | 0.2 | 2.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -90.1 | -14.0 | -17.6 | -22.5 | -776.4 | -301.2 |
| 8751 | ok | 0.09 | 0.1 | 2.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -95.3 | -6.7 | -18.5 | -32.4 | -338.5 | -354.9 |
| 8752 | ok | 0.09 | 0.1 | 2.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -93.9 | -7.1 | -19.4 | -38.6 | -283.8 | -329.5 |
| 8753 | ok | 0.09 | 0.1 | 3.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -94.7 | -30.0 | -77.3 | -130.8 | -586.5 | -258.9 |
| 8754 | ok | 0.09 | 0.2 | 2.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -84.4 | 15.5 | -29.8 | 56.8 | 480.9 | -417.7 |
| 8755 | ok | 0.09 | 0.1 | 2.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -93.3 | 3.6 | -25.6 | 26.3 | 190.6 | -456.4 |
| 8756 | ok | 0.09 | 0.1 | 2.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -100.0 | 3.5 | -9.1 | 34.0 | 203.9 | -417.4 |
| 8757 | ok | 0.09 | 0.1 | 3.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -99.9 | 13.9 | 54.0 | 95.8 | 519.6 | -384.5 |
| 8758 | ok | 0.09 | 0.2 | 2.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -101.1 | 6.5 | -37.1 | -64.8 | 368.6 | -646.9 |
| 8759 | ok | 0.09 | 0.2 | 2.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -101.3 | 9.7 | -23.0 | 15.0 | 453.6 | -396.6 |
| 8760 | ok | 0.09 | 0.1 | 2.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -99.3 | 6.3 | -18.4 | 39.8 | 354.6 | -344.9 |
| 8761 | ok | 0.09 | 0.1 | 3.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -99.0 | 9.0 | 54.5 | 136.8 | 590.0 | -371.1 |
| 8762 | ok | 0.09 | 0.3 | 2.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -105.1 | 18.0 | -21.4 | -290.7 | 1112.3 | -225.9 |
| 8763 | ok | 0.09 | 0.2 | 2.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -102.9 | 15.9 | -23.1 | 32.0 | 781.3 | -153.9 |
| 8764 | ok | 0.09 | 0.2 | 2.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -100.2 | 11.7 | -15.4 | 67.9 | 577.8 | -124.0 |
| 8765 | ok | 0.09 | 0.1 | 3.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -94.3 | 8.3 | 3.4 | 83.9 | 439.4 | -106.5 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | | | | | | | | -155.08 | -49.29 | -155.07 | -669.93 | -1171.15 | -646.92 |
| | | 0.09 | 0.33 | 0.05 | 4.52 | 4.52 | 4.00 | 4.00 | -67.73 | 54.71 | 120.06 | 410.27 | 1112.34 | -28.15 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 21 | ok | 0.81 | | | | | | |
| 22 | ok | 1.04 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 2775 | ok | 0.82 | | | | | | |
| 2776 | ok | 1.04 | | | | | | |
| 2777 | ok | 0.82 | | | | | | |
| 7323 | ok | 0.36 | | | | | | |
| 7324 | ok | 0.46 | | | | | | |
| 7469 | ok | 0.35 | | | | | | |
| 7470 | ok | 0.46 | | | | | | |
| 7471 | ok | 0.36 | | | | | | |
| 8361 | ok | 0.77 | | | | | | |
| 8362 | ok | 0.55 | | | | | | |
| 8363 | ok | 0.48 | | | | | | |
| 8364 | ok | 0.42 | | | | | | |
| 8750 | ok | 0.77 | | | | | | |
| 8751 | ok | 0.55 | | | | | | |
| 8752 | ok | 0.48 | | | | | | |
| 8753 | ok | 0.42 | | | | | | |
| 8754 | ok | 0.67 | | | | | | |
| 8755 | ok | 0.36 | | | | | | |
| 8756 | ok | 0.30 | | | | | | |
| 8757 | ok | 0.28 | | | | | | |
| 8758 | ok | 0.68 | | | | | | |
| 8759 | ok | 0.44 | | | | | | |
| 8760 | ok | 0.41 | | | | | | |
| 8761 | ok | 0.38 | | | | | | |
| 8762 | ok | 0.68 | | | | | | |
| 8763 | ok | 0.44 | | | | | | |
| 8764 | ok | 0.41 | | | | | | |
| 8765 | ok | 0.38 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 1.04 | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 71 | 40.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|--------|--------|-------|
| 30 | ok | 0.09 | 0.2 | 3.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 31 | ok | 0.09 | 0.2 | 2.97e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -119.0 | -56.6 | 45.2 | -510.4 | 633.7 | 510.0 |
| 2680 | ok | 0.09 | 0.1 | 2.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -125.9 | -105.7 | 23.5 | 36.5 | -317.6 | 53.1 |
| 2681 | ok | 0.09 | 0.1 | 2.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -69.2 | -53.8 | 26.7 | 61.2 | 11.1 | 118.5 |
| 2682 | ok | 0.09 | 0.1 | 2.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -106.6 | -94.9 | 24.7 | 24.8 | -233.9 | 56.5 |
| 2682 | ok | 0.09 | 0.1 | 2.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.8 | -41.4 | 18.5 | 289.2 | 484.0 | 26.9 |
| 7332 | ok | 0.09 | 0.2 | 2.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.3 | 12.8 | -79.6 | 300.6 | 389.5 | 259.2 |
| 7333 | ok | 0.09 | 0.2 | 4.75e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.0 | -74.4 | 136.6 | -150.6 | -436.4 | 152.1 |
| 7464 | ok | 0.09 | 0.2 | 4.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.6 | 32.5 | -70.3 | 118.2 | 457.1 | 325.6 |
| 7465 | ok | 0.09 | 0.2 | 4.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.6 | 44.2 | -67.5 | 174.5 | 349.6 | 293.5 |
| 7466 | ok | 0.09 | 0.2 | 4.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.8 | 19.2 | -76.1 | 135.3 | 448.3 | 276.9 |
| 7691 | ok | 0.09 | 0.2 | 2.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.2 | -28.0 | 18.2 | -190.2 | 914.4 | 175.0 |
| 7745 | ok | 0.09 | 0.1 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -85.0 | -24.9 | 20.6 | 19.3 | 597.1 | 115.4 |
| 7799 | ok | 0.09 | 9.64e-02 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -82.5 | -19.7 | 16.7 | 46.1 | 431.9 | 81.7 |
| 7853 | ok | 0.09 | 8.05e-02 | 2.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.2 | -12.1 | 3.0 | 71.8 | 318.9 | 63.5 |
| 7907 | ok | 0.09 | 0.1 | 2.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -97.2 | -46.9 | 29.0 | -39.5 | -503.5 | 132.8 |
| 7908 | ok | 0.09 | 7.83e-02 | 2.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -91.4 | -29.1 | 31.3 | -55.9 | -435.4 | 133.4 |
| 7909 | ok | 0.09 | 6.68e-02 | 2.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.6 | -22.2 | 32.8 | -49.5 | -341.1 | 123.7 |
| 7910 | ok | 0.09 | 8.78e-02 | 2.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.9 | -24.9 | 50.6 | -30.4 | -260.6 | 97.1 |
| 9030 | ok | 0.09 | 0.1 | 2.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.9 | -44.4 | 31.7 | -48.5 | 200.2 | 500.8 |
| 9031 | ok | 0.09 | 9.33e-02 | 2.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.3 | -27.9 | 21.0 | 12.1 | 303.2 | 272.7 |
| 9032 | ok | 0.09 | 7.67e-02 | 2.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -84.2 | -19.1 | 14.3 | 35.4 | 265.8 | 225.6 |
| 9033 | ok | 0.09 | 8.79e-02 | 3.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -76.7 | -1.4 | -30.0 | 89.3 | 300.4 | 278.8 |
| 9034 | ok | 0.09 | 9.52e-02 | 2.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -81.5 | -39.0 | 20.7 | 61.2 | 38.5 | 295.6 |
| 9035 | ok | 0.09 | 8.08e-02 | 2.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.0 | -27.9 | 22.5 | 26.7 | 58.0 | 290.4 |
| 9036 | ok | 0.09 | 7.03e-02 | 2.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -84.5 | -17.5 | 18.4 | 26.0 | 85.4 | 265.6 |
| 9037 | ok | 0.09 | 8.17e-02 | 3.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.0 | 6.3 | -24.5 | 74.2 | 287.3 | 256.1 |
| 9038 | ok | 0.09 | 9.09e-02 | 2.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -97.4 | -48.8 | 25.8 | -22.9 | -388.5 | 225.9 |
| 9039 | ok | 0.09 | 7.42e-02 | 2.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -89.1 | -30.6 | 29.4 | -38.5 | -337.9 | 223.9 |
| 9040 | ok | 0.09 | 6.84e-02 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -85.6 | -21.5 | 31.0 | -33.8 | -254.5 | 216.0 |
| 9041 | ok | 0.09 | 9.06e-02 | 3.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -88.4 | -55.3 | 86.2 | -48.2 | -336.0 | 232.4 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|-------|----------|--------|--------|---------|---------|---------|---------|--------|---------|---------|--------|
| | | | | | | | | | -125.89 | -105.71 | -79.64 | -510.40 | -503.46 | 26.94 |
| | | 0.09 | 0.24 | 0.05 | 4.52 | 4.52 | 4.00 | 4.00 | -50.77 | 44.15 | 136.63 | 300.61 | 914.38 | 510.05 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 30 | ok | 0.68 | | | | | | |
| 31 | ok | 0.59 | | | | | | |
| 2680 | ok | 0.67 | | | | | | |
| 2681 | ok | 0.61 | | | | | | |
| 2682 | ok | 0.68 | | | | | | |
| 7332 | ok | 0.27 | | | | | | |
| 7333 | ok | 0.29 | | | | | | |
| 7464 | ok | 0.25 | | | | | | |
| 7465 | ok | 0.29 | | | | | | |
| 7466 | ok | 0.27 | | | | | | |
| 7691 | ok | 0.68 | | | | | | |
| 7745 | ok | 0.45 | | | | | | |
| 7799 | ok | 0.36 | | | | | | |
| 7853 | ok | 0.29 | | | | | | |
| 7907 | ok | 0.55 | | | | | | |
| 7908 | ok | 0.38 | | | | | | |
| 7909 | ok | 0.32 | | | | | | |
| 7910 | ok | 0.26 | | | | | | |
| 9030 | ok | 0.68 | | | | | | |
| 9031 | ok | 0.45 | | | | | | |
| 9032 | ok | 0.36 | | | | | | |
| 9033 | ok | 0.29 | | | | | | |
| 9034 | ok | 0.63 | | | | | | |
| 9035 | ok | 0.36 | | | | | | |
| 9036 | ok | 0.30 | | | | | | |
| 9037 | ok | 0.23 | | | | | | |
| 9038 | ok | 0.56 | | | | | | |
| 9039 | ok | 0.38 | | | | | | |
| 9040 | ok | 0.32 | | | | | | |
| 9041 | ok | 0.26 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 0.68 | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 72 | 40.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|-------|--------|-------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 2 | ok | 0.09 | 0.4 | 8.54e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -36.4 | 103.4 | -19.8 | 11.5 | -760.9 | -0.4 |
| 6 | ok | 0.09 | 0.4 | 4.39e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.7 | 125.8 | 21.3 | 12.6 | -634.8 | -0.3 |
| 7 | ok | 0.09 | 0.1 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.4 | 25.6 | -12.1 | 3.0 | -30.4 | -61.8 |
| 8 | ok | 0.09 | 0.1 | 1.68e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.3 | 13.0 | -20.9 | 13.0 | 87.6 | -57.3 |
| 9 | ok | 0.09 | 0.1 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.2 | -17.0 | -6.2 | 18.6 | 113.1 | -61.9 |
| 10 | ok | 0.09 | 0.2 | 2.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -106.6 | -34.0 | -8.0 | 25.5 | 112.3 | -50.1 |
| 11 | ok | 0.09 | 0.3 | 2.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -98.0 | -83.3 | 27.7 | -33.8 | 76.4 | 19.7 |
| 12 | ok | 0.09 | 7.78e-02 | 4.99e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -204.4 | -111.8 | -53.2 | 6.9 | 87.4 | -9.1 |
| 13 | ok | 0.09 | 7.77e-02 | 4.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -176.5 | -106.7 | 49.0 | 16.3 | 79.3 | -17.0 |
| 14 | ok | 0.09 | 0.2 | 4.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -144.6 | -159.5 | -32.8 | -25.0 | 78.2 | 4.7 |
| 15 | ok | 0.09 | 6.77e-02 | 6.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -138.9 | -197.6 | 110.7 | -14.7 | 121.0 | 63.5 |
| 16 | ok | 0.09 | 0.5 | 5.94e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 53.4 | 163.5 | 43.5 | 11.0 | -275.7 | 57.7 |
| 921 | ok | 0.09 | 0.1 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.8 | 23.9 | -17.7 | 5.7 | 18.4 | -61.9 |
| 923 | ok | 0.09 | 0.1 | 1.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.7 | 21.0 | -20.2 | 8.3 | 52.2 | -61.0 |
| 925 | ok | 0.09 | 0.1 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.1 | 17.0 | -21.6 | 10.7 | 74.3 | -59.4 |
| 927 | ok | 0.09 | 0.1 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.8 | -19.0 | -9.4 | 21.3 | 117.6 | -58.8 |
| 929 | ok | 0.09 | 0.1 | 1.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.6 | -21.9 | -10.4 | 23.5 | 117.3 | -55.5 |
| 931 | ok | 0.09 | 0.2 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -90.7 | -27.0 | -10.8 | 25.2 | 114.8 | -52.5 |
| 1157 | ok | 0.09 | 0.2 | 2.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -94.8 | 32.6 | -6.2 | 2.8 | -322.2 | -52.0 |
| 1158 | ok | 0.09 | 0.1 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.5 | 28.2 | -10.9 | -1.1 | -188.7 | -58.4 |
| 1159 | ok | 0.09 | 0.1 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.1 | 26.9 | -11.1 | 0.4 | -97.5 | -60.8 |
| 1163 | ok | 0.09 | 0.1 | 1.75e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.7 | 28.4 | -21.5 | 52.3 | 56.6 | -1.7 |
| 1165 | ok | 0.09 | 0.2 | 2.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -117.8 | -94.1 | 4.8 | -62.8 | 69.8 | 15.2 |
| 1269 | ok | 0.09 | 9.45e-02 | 4.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -203.8 | -119.8 | 1.0 | 30.2 | 84.7 | -11.2 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|-------|-------|--------|-------|--------|
| 9126 | ok | 0.09 | 9.46e-02 | 2.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -102.9 | -32.0 | -34.7 | 129.8 | 78.1 | 93.3 |
| 9127 | ok | 0.09 | 0.1 | 2.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -99.3 | -27.8 | -38.9 | 170.5 | 60.7 | 87.0 |
| 9128 | ok | 0.09 | 0.1 | 2.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -88.3 | -67.0 | -60.9 | 123.8 | 107.8 | 106.1 |
| 9129 | ok | 0.09 | 8.14e-02 | 2.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -85.4 | -42.5 | -56.2 | 147.3 | 88.1 | 94.9 |
| 9130 | ok | 0.09 | 8.90e-02 | 2.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -85.6 | -35.7 | -41.4 | 117.6 | 71.8 | 73.3 |
| 9131 | ok | 0.09 | 0.1 | 2.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -88.4 | -32.2 | -42.3 | 154.3 | 54.7 | 67.3 |
| 9132 | ok | 0.09 | 9.77e-02 | 2.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.7 | -59.0 | -48.6 | 80.7 | 98.8 | 88.6 |
| 9133 | ok | 0.09 | 0.5 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | 61.0 | 118.2 | 46.0 | 1.1 | 62.5 | 16.7 |
| 9134 | ok | 0.09 | 7.00e-02 | 1.97e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.4 | -47.1 | -51.7 | 145.1 | 95.5 | 72.2 |
| 9135 | ok | 0.09 | 8.15e-02 | 2.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.1 | -41.5 | -38.0 | 107.1 | 66.1 | 53.4 |
| 9136 | ok | 0.09 | 9.57e-02 | 2.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.8 | -37.4 | -39.2 | 140.4 | 49.5 | 49.0 |
| 9137 | ok | 0.09 | 0.1 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.1 | -31.6 | -38.0 | 157.6 | 45.1 | 11.3 |
| 9138 | ok | 0.09 | 0.2 | 1.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -20.0 | -54.7 | -31.9 | 66.8 | 111.7 | 61.2 |
| 9139 | ok | 0.09 | 0.2 | 6.71e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -0.2 | -38.1 | -8.1 | -10.4 | 46.2 | 2.4 |
| 9140 | ok | 0.09 | 5.74e-02 | 1.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.7 | -43.4 | -38.1 | 87.2 | 82.9 | 58.9 |
| 9141 | ok | 0.09 | 7.43e-02 | 1.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.8 | -44.6 | -25.6 | 99.4 | 61.6 | 34.2 |
| 9142 | ok | 0.09 | 9.17e-02 | 1.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.0 | -40.9 | -29.7 | 130.1 | 45.6 | 31.9 |
| 9143 | ok | 0.09 | 0.1 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.3 | -35.7 | -31.5 | 143.9 | 40.6 | 8.9 |
| 9144 | ok | 0.09 | 7.64e-02 | 7.38e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -10.6 | -24.2 | 12.8 | 22.6 | 82.2 | -3.1 |
| 9145 | ok | 0.09 | 0.1 | 1.69e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.7 | 36.9 | 7.1 | 10.0 | 77.8 | -26.1 |
| 9146 | ok | 0.09 | 8.23e-02 | 1.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -25.7 | -41.6 | 18.5 | 56.9 | 69.2 | -2.8 |
| 9147 | ok | 0.09 | 7.41e-02 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.1 | -39.2 | 20.2 | 89.0 | 54.4 | -2.2 |
| 9148 | ok | 0.09 | 9.15e-02 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.2 | -35.5 | 12.8 | 122.3 | 42.8 | -4.6 |
| 9149 | ok | 0.09 | 0.1 | 1.89e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.6 | -33.5 | -14.0 | 136.5 | 38.7 | 4.3 |
| 9150 | ok | 0.09 | 0.1 | 8.52e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -7.1 | -17.0 | -1.5 | 22.4 | 83.8 | 14.7 |
| 9151 | ok | 0.09 | 0.2 | 3.37e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.2 | 37.1 | 4.9 | 7.0 | 78.9 | 9.5 |
| 9152 | ok | 0.09 | 8.27e-02 | 1.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -23.4 | -42.4 | -4.6 | 60.6 | 74.4 | 17.1 |
| 9153 | ok | 0.09 | 7.10e-02 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.9 | -44.5 | -6.4 | 94.5 | 58.9 | 15.6 |
| 9154 | ok | 0.09 | 8.99e-02 | 1.57e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.4 | -41.3 | -16.9 | 124.1 | 43.4 | 15.7 |
| 9155 | ok | 0.09 | 0.1 | 1.89e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -76.3 | -36.4 | -22.7 | 136.8 | 38.4 | 6.6 |
| 9156 | ok | 0.09 | 9.06e-02 | 3.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -107.5 | -24.9 | 63.7 | 33.7 | 82.7 | -45.6 |
| 9157 | ok | 0.09 | 8.28e-02 | 2.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -95.4 | -27.7 | 44.6 | 64.9 | 69.4 | -37.2 |
| 9158 | ok | 0.09 | 8.91e-02 | 2.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -95.0 | -24.6 | 34.0 | 94.9 | 57.2 | -33.6 |
| 9159 | ok | 0.09 | 9.97e-02 | 2.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -93.8 | -22.4 | 30.6 | 125.4 | 44.7 | -32.9 |
| 9160 | ok | 0.09 | 7.19e-02 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -20.9 | -74.5 | 48.1 | 21.5 | 87.4 | -24.8 |
| 9161 | ok | 0.09 | 0.3 | 3.93e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -6.9 | 6.8 | 2.6 | -1.9 | 81.4 | -4.5 |
| 9162 | ok | 0.09 | 7.34e-02 | 1.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.1 | -40.0 | 37.6 | 59.7 | 69.2 | -20.8 |
| 9163 | ok | 0.09 | 8.15e-02 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.6 | -34.0 | 32.3 | 91.0 | 55.5 | -18.3 |
| 9164 | ok | 0.09 | 9.53e-02 | 2.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.6 | -29.7 | 30.8 | 119.9 | 42.1 | -18.1 |
| 9165 | ok | 0.09 | 0.1 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.7 | -25.1 | 27.2 | 138.0 | 40.1 | -6.5 |
| 9166 | ok | 0.09 | 9.46e-02 | 3.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -154.6 | -35.8 | 17.5 | 46.2 | 77.6 | -54.0 |
| 9167 | ok | 0.09 | 8.91e-02 | 2.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -123.8 | -21.7 | 27.9 | 69.7 | 69.5 | -47.9 |
| 9168 | ok | 0.09 | 9.34e-02 | 2.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -112.9 | -18.1 | 25.6 | 98.2 | 58.6 | -44.7 |
| 9169 | ok | 0.09 | 0.1 | 2.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -105.0 | -16.4 | 25.5 | 129.6 | 46.4 | -44.7 |
| 9170 | ok | 0.09 | 9.50e-02 | 3.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -150.7 | -48.2 | 7.0 | 52.1 | 76.0 | -58.9 |
| 9171 | ok | 0.09 | 9.20e-02 | 3.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -137.0 | -21.0 | 10.7 | 73.3 | 69.8 | -57.1 |
| 9172 | ok | 0.09 | 9.58e-02 | 2.73e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -123.4 | -14.6 | 13.2 | 101.0 | 59.9 | -55.2 |
| 9173 | ok | 0.09 | 0.1 | 2.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -111.2 | -12.7 | 16.0 | 133.0 | 47.7 | -56.4 |
| 9174 | ok | 0.09 | 9.40e-02 | 3.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -148.9 | -52.2 | -1.4 | -246.6 | 121.2 | -61.2 |
| 9175 | ok | 0.09 | 9.22e-02 | 3.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -138.3 | -23.6 | -2.9 | -205.5 | 68.8 | -64.7 |
| 9176 | ok | 0.09 | 9.64e-02 | 2.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -125.4 | -14.8 | -1.3 | -187.8 | 29.0 | -65.1 |
| 9177 | ok | 0.09 | 0.1 | 2.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -113.0 | -11.2 | 5.1 | 135.4 | 48.8 | -68.5 |
| 9178 | ok | 0.09 | 9.21e-02 | 3.58e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -158.7 | -45.1 | -5.9 | 49.1 | 79.1 | -69.0 |
| 9179 | ok | 0.09 | 9.01e-02 | 3.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -141.9 | -16.5 | -15.5 | 72.5 | 72.2 | -75.7 |
| 9180 | ok | 0.09 | 9.53e-02 | 2.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -126.1 | -10.8 | -16.5 | 101.9 | 61.8 | -78.1 |
| 9181 | ok | 0.09 | 0.1 | 2.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -112.3 | -8.5 | -10.1 | 135.8 | 49.2 | -83.8 |
| 9182 | ok | 0.09 | 8.81e-02 | 3.90e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -166.7 | -29.7 | -20.1 | 40.4 | 83.8 | -75.0 |
| 9183 | ok | 0.09 | 8.50e-02 | 3.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -130.7 | -14.6 | -35.3 | 68.9 | 74.0 | -85.9 |
| 9184 | ok | 0.09 | 9.24e-02 | 2.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -117.2 | -12.1 | -30.6 | 100.4 | 62.3 | -89.2 |
| 9185 | ok | 0.09 | 0.1 | 2.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -106.3 | -10.3 | -20.4 | 134.8 | 49.2 | -96.3 |
| 9186 | ok | 0.09 | 0.1 | 3.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -119.8 | -8.0 | -66.6 | 27.7 | 92.2 | -88.5 |
| 9187 | ok | 0.09 | 9.86e-02 | 2.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -102.3 | -18.5 | -53.4 | 64.8 | 75.6 | -97.9 |
| 9188 | ok | 0.09 | 9.64e-02 | 2.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -99.9 | -16.8 | -40.5 | 98.5 | 62.6 | -101.1 |
| 9189 | ok | 0.09 | 0.1 | 2.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -96.0 | -14.2 | -27.3 | 132.9 | 48.9 | -109.0 |
| 9190 | ok | 0.09 | 0.1 | 2.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.5 | -72.6 | -72.4 | 21.6 | 94.1 | -106.8 |
| 9191 | ok | 0.09 | 0.4 | 5.44e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 57.9 | 32.2 | 28.4 | -5.4 | 86.7 | -20.0 |
| 9192 | ok | 0.09 | 0.1 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.5 | -29.6 | -51.9 | 61.6 | 76.7 | -112.0 |
| 9193 | ok | 0.09 | 0.1 | 2.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.5 | -23.2 | -42.2 | 96.6 | 62.6 | -114.2 |
| 9194 | ok | 0.09 | 0.1 | 2.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.3 | -19.4 | -29.6 | 130.7 | 48.4 | -122.4 |
| 9195 | ok | 0.09 | 0.1 | 2.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.5 | -16.0 | -18.4 | 154.5 | 47.1 | -28.7 |
| 9196 | ok | 0.09 | 0.1 | 9.69e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -8.2 | -24.8 | -21.2 | -40.1 | 21.3 | -178.6 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|----------|-------|-------|--------|--------|--------|
| 9197 | ok | 0.09 | 0.2 | 9.22e-04 | 4.5 | 4.5 | 4.0 | 4.0 | 4.8 | 39.7 | 4.1 | -2.9 | 90.9 | -21.1 |
| 9198 | ok | 0.09 | 0.1 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.5 | -30.8 | -38.5 | 59.9 | 77.4 | -127.0 |
| 9199 | ok | 0.09 | 0.1 | 1.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.9 | -27.3 | -35.2 | 95.5 | 62.6 | -127.9 |
| 9200 | ok | 0.09 | 9.91e-02 | 2.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -72.1 | -23.6 | -26.0 | 128.9 | 48.0 | -135.8 |
| 9201 | ok | 0.09 | 0.1 | 2.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.3 | -20.9 | -17.3 | 150.0 | 45.6 | -31.2 |
| 9202 | ok | 0.09 | 0.2 | 5.56e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -8.1 | -2.9 | -10.5 | 23.3 | 91.8 | -126.5 |
| 9203 | ok | 0.09 | 0.2 | 1.46e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 0.2 | 61.6 | -8.7 | 8.9 | 87.3 | -39.7 |
| 9204 | ok | 0.09 | 0.1 | 1.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -24.2 | -25.1 | -20.8 | 60.0 | 78.2 | -142.3 |
| 9205 | ok | 0.09 | 0.1 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.8 | -27.6 | -23.8 | 95.6 | 62.9 | -142.0 |
| 9206 | ok | 0.09 | 9.93e-02 | 1.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.2 | -25.6 | -18.8 | 128.2 | 47.9 | -149.1 |
| 9207 | ok | 0.09 | 0.1 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -74.7 | -24.2 | -13.7 | 147.1 | 44.7 | -33.5 |
| 9208 | ok | 0.09 | 0.1 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.4 | -42.7 | 37.2 | 7.4 | 64.7 | -92.6 |
| 9209 | ok | 0.09 | 0.4 | 8.30e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 0.2 | 78.6 | -8.9 | 10.5 | 85.5 | -42.0 |
| 9210 | ok | 0.09 | 8.74e-02 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.2 | -23.5 | 28.9 | 143.8 | 79.5 | -116.5 |
| 9211 | ok | 0.09 | 8.85e-02 | 1.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.0 | -20.3 | 28.4 | 168.3 | 67.7 | -115.0 |
| 9212 | ok | 0.09 | 0.1 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.2 | -21.8 | -3.2 | 131.9 | 49.8 | -176.0 |
| 9213 | ok | 0.09 | 0.1 | 1.89e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.9 | -25.7 | 5.4 | 166.3 | 51.4 | -37.7 |
| 9214 | ok | 0.09 | 0.2 | 8.25e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -10.2 | -7.9 | -43.7 | 32.1 | -131.3 | |
| 9215 | ok | 0.09 | 0.3 | 3.13e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 1.35e-02 | 64.2 | -7.3 | 9.4 | 89.3 | -41.4 |
| 9216 | ok | 0.09 | 0.1 | 8.75e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.6 | -18.8 | -6.2 | 61.8 | 79.2 | -156.1 |
| 9217 | ok | 0.09 | 8.64e-02 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.6 | -24.6 | -11.8 | 96.9 | 63.8 | -156.4 |
| 9218 | ok | 0.09 | 0.1 | 1.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.4 | -24.8 | -10.4 | 129.1 | 48.5 | -162.5 |
| 9219 | ok | 0.09 | 0.1 | 1.97e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -73.2 | -25.3 | -9.0 | 146.7 | 44.7 | -35.7 |
| 9220 | ok | 0.09 | 0.2 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -72.3 | -27.3 | 30.9 | -19.8 | 68.4 | -103.0 |
| 9221 | ok | 0.09 | 8.67e-02 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.3 | -19.1 | 34.0 | 156.9 | 82.9 | -127.3 |
| 9222 | ok | 0.09 | 9.31e-02 | 1.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.5 | -16.1 | 27.6 | 181.0 | 69.9 | -125.0 |
| 9223 | ok | 0.09 | 0.1 | 1.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -71.8 | -17.4 | 1.2 | 136.5 | 51.9 | -189.7 |
| 9224 | ok | 0.09 | 0.2 | 2.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -84.4 | -34.3 | 11.3 | -47.5 | 69.6 | -114.8 |
| 9225 | ok | 0.09 | 9.63e-02 | 1.97e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.7 | -15.5 | 22.4 | 170.7 | 79.7 | -139.3 |
| 9226 | ok | 0.09 | 9.65e-02 | 1.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.2 | -12.8 | 21.6 | 194.0 | 71.6 | -136.0 |
| 9227 | ok | 0.09 | 0.1 | 1.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.0 | -13.1 | 2.1 | 142.8 | 54.8 | -203.7 |
| 9228 | ok | 0.09 | 0.2 | 2.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -99.9 | -12.9 | -7.4 | 48.8 | 112.3 | -225.2 |
| 9229 | ok | 0.09 | 0.1 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.8 | -15.9 | 9.8 | 184.6 | 77.8 | -151.1 |
| 9230 | ok | 0.09 | 9.83e-02 | 1.93e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -87.8 | -10.4 | -1.0 | 129.5 | 83.7 | -221.8 |
| 9231 | ok | 0.09 | 0.1 | 1.89e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -82.7 | -9.7 | 0.7 | 150.1 | 58.2 | -218.1 |
| 9232 | ok | 0.09 | 0.1 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -89.3 | -17.4 | -12.1 | 50.4 | 115.6 | -239.5 |
| 9233 | ok | 0.09 | 0.1 | 2.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -88.5 | -10.6 | -8.6 | 91.7 | 102.8 | -243.7 |
| 9234 | ok | 0.09 | 9.86e-02 | 1.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -89.2 | -10.7 | -2.7 | 137.0 | 88.4 | -240.1 |
| 9235 | ok | 0.09 | 0.1 | 1.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -85.2 | -7.9 | -3.3 | 159.4 | 62.8 | -234.7 |
| 9236 | ok | 0.09 | 0.1 | 1.93e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.7 | -18.3 | -12.4 | 50.1 | 118.5 | -254.4 |
| 9237 | ok | 0.09 | 0.1 | 1.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.3 | -12.9 | -11.9 | 94.3 | 106.4 | -260.2 |
| 9238 | ok | 0.09 | 9.75e-02 | 1.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.8 | -11.7 | -7.1 | 143.7 | 93.1 | -257.9 |
| 9239 | ok | 0.09 | 0.1 | 2.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -85.5 | -7.1 | -6.9 | 168.7 | 67.7 | -251.8 |
| 9240 | ok | 0.09 | 0.1 | 1.85e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -76.1 | -16.6 | -11.5 | 48.4 | 119.2 | -269.2 |
| 9241 | ok | 0.09 | 0.1 | 1.91e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.1 | -13.1 | -13.2 | 95.0 | 108.2 | -276.4 |
| 9242 | ok | 0.09 | 9.54e-02 | 1.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.8 | -12.1 | -9.8 | 148.9 | 96.7 | -275.5 |
| 9243 | ok | 0.09 | 0.1 | 2.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -84.4 | -6.8 | -10.2 | 177.6 | 72.5 | -269.3 |
| 9244 | ok | 0.09 | 0.1 | 1.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -74.1 | -14.0 | -9.3 | 45.5 | 115.2 | -283.2 |
| 9245 | ok | 0.09 | 0.1 | 1.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -76.0 | -12.2 | -11.5 | 93.6 | 106.4 | -291.4 |
| 9246 | ok | 0.09 | 9.24e-02 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -81.2 | -11.5 | -15.9 | 152.1 | 97.8 | -291.6 |
| 9247 | ok | 0.09 | 0.1 | 2.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -82.7 | -6.8 | -13.4 | 185.4 | 76.9 | -286.6 |
| 9248 | ok | 0.09 | 0.1 | 1.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.2 | -12.8 | -11.0 | 43.5 | 105.6 | -267.3 |
| 9249 | ok | 0.09 | 0.1 | 1.83e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -73.4 | -11.2 | -12.9 | 90.5 | 101.0 | -301.7 |
| 9250 | ok | 0.09 | 8.96e-02 | 1.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.3 | -10.5 | -14.0 | 152.0 | 95.8 | -301.5 |
| 9251 | ok | 0.09 | 0.1 | 2.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -81.5 | -6.2 | -14.4 | 189.8 | 78.6 | -300.1 |
| 9252 | ok | 0.09 | 0.1 | 1.73e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.8 | 11.4 | -23.1 | 32.3 | 89.2 | -261.0 |
| 9253 | ok | 0.09 | 0.1 | 1.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -73.6 | -5.4 | -18.3 | -121.5 | 96.3 | -405.8 |
| 9254 | ok | 0.09 | 9.07e-02 | 1.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.1 | -6.8 | -22.7 | -77.5 | 76.2 | -399.1 |
| 9255 | ok | 0.09 | 0.1 | 1.97e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.4 | -5.6 | -15.0 | 191.8 | 77.7 | -313.2 |
| 9256 | ok | 0.09 | 0.1 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.6 | 12.4 | -23.8 | 28.1 | 76.2 | -269.2 |
| 9257 | ok | 0.09 | 0.1 | 1.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -69.1 | -4.4 | -18.8 | -114.5 | 74.7 | -425.4 |
| 9258 | ok | 0.09 | 9.26e-02 | 1.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.7 | -5.4 | -22.6 | -66.1 | 62.9 | -416.7 |
| 9259 | ok | 0.09 | 9.71e-02 | 1.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -76.4 | -5.2 | -16.7 | 191.8 | 73.9 | -327.8 |
| 9260 | ok | 0.09 | 0.1 | 1.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.1 | 13.6 | -22.5 | 22.8 | 54.4 | -274.7 |
| 9261 | ok | 0.09 | 0.1 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.9 | -3.2 | -18.4 | -110.5 | 36.5 | -438.0 |
| 9262 | ok | 0.09 | 9.46e-02 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.4 | -4.4 | -22.7 | -57.8 | 36.3 | -429.8 |
| 9263 | ok | 0.09 | 9.13e-02 | 1.90e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -73.8 | -4.5 | -16.8 | 186.1 | 63.3 | -339.3 |
| 9264 | ok | 0.09 | 0.1 | 1.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.5 | 15.8 | -20.0 | 16.1 | 21.0 | -276.7 |
| 9265 | ok | 0.09 | 0.1 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.2 | -1.2 | -17.5 | -110.0 | -24.6 | -441.4 |
| 9266 | ok | 0.09 | 9.70e-02 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.7 | -3.0 | -20.0 | -54.6 | -9.9 | -432.6 |
| 9267 | ok | 0.09 | 8.96e-02 | 1.85e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -71.2 | -3.5 | -16.8 | 172.9 | 42.3 | -345.3 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|---------|---------|--------|---------|---------|---------|
| 9268 | ok | 0.09 | 0.1 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.0 | 19.1 | -15.5 | 7.8 | -27.6 | -274.0 |
| 9269 | ok | 0.09 | 0.1 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.0 | 12.9 | -19.5 | 28.9 | -15.8 | -281.8 |
| 9270 | ok | 0.09 | 0.1 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.3 | 2.3 | -21.0 | 75.8 | -21.1 | -307.5 |
| 9271 | ok | 0.09 | 9.09e-02 | 1.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.2 | -2.6 | -16.8 | 150.9 | 7.9 | -343.1 |
| 9272 | ok | 0.09 | 0.1 | 1.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.0 | 23.5 | -15.2 | -2.5 | -95.4 | -265.2 |
| 9273 | ok | 0.09 | 0.1 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.7 | 16.9 | -23.4 | 11.3 | -75.2 | -272.5 |
| 9274 | ok | 0.09 | 0.1 | 1.58e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.7 | 3.8 | -22.3 | 50.3 | -87.9 | -289.4 |
| 9275 | ok | 0.09 | 9.21e-02 | 1.73e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.4 | -2.4 | -17.2 | 119.3 | -41.6 | -329.0 |
| 9276 | ok | 0.09 | 0.1 | 1.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.7 | 30.7 | -17.7 | -15.5 | -191.2 | -246.4 |
| 9277 | ok | 0.09 | 0.1 | 1.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.7 | 18.8 | -28.0 | -10.4 | -157.6 | -253.1 |
| 9278 | ok | 0.09 | 0.1 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.6 | 7.8 | -28.6 | 27.4 | -115.9 | -256.6 |
| 9279 | ok | 0.09 | 9.14e-02 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.9 | -3.9 | -18.4 | 78.8 | -102.5 | -295.8 |
| 9280 | ok | 0.09 | 0.2 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.5 | 38.9 | -33.9 | -46.0 | -329.4 | -215.3 |
| 9281 | ok | 0.09 | 0.1 | 1.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.5 | 20.3 | -33.0 | -32.8 | -274.5 | -209.1 |
| 9282 | ok | 0.09 | 0.1 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.3 | 5.7 | -32.1 | 4.3 | -192.6 | -209.9 |
| 9283 | ok | 0.09 | 8.49e-02 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.7 | -7.4 | -21.4 | 32.7 | -158.2 | -224.5 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | | | | | | | | -204.35 | -197.56 | -72.40 | -246.56 | -760.86 | -441.45 |
| | | 0.09 | 0.49 | 0.06 | 4.52 | 4.52 | 4.00 | 4.00 | 60.95 | 163.51 | 110.66 | 616.64 | 162.65 | 387.89 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 2 | ok | 0.97 | | | | | | |
| 6 | ok | 1.04 | | | | | | |
| 7 | ok | 0.65 | | | | | | |
| 8 | ok | 0.54 | | | | | | |
| 9 | ok | 0.49 | | | | | | |
| 10 | ok | 0.29 | | | | | | |
| 11 | ok | 0.46 | | | | | | |
| 12 | ok | 0.74 | | | | | | |
| 13 | ok | 0.74 | | | | | | |
| 14 | ok | 0.46 | | | | | | |
| 15 | ok | 0.60 | | | | | | |
| 16 | ok | 0.77 | | | | | | |
| 921 | ok | 0.61 | | | | | | |
| 923 | ok | 0.59 | | | | | | |
| 925 | ok | 0.56 | | | | | | |
| 927 | ok | 0.46 | | | | | | |
| 929 | ok | 0.42 | | | | | | |
| 931 | ok | 0.36 | | | | | | |
| 1157 | ok | 1.04 | | | | | | |
| 1158 | ok | 0.83 | | | | | | |
| 1159 | ok | 0.72 | | | | | | |
| 1163 | ok | 0.51 | | | | | | |
| 1165 | ok | 0.46 | | | | | | |
| 1269 | ok | 0.74 | | | | | | |
| 1284 | ok | 0.47 | | | | | | |
| 1299 | ok | 0.23 | | | | | | |
| 1314 | ok | 0.49 | | | | | | |
| 1329 | ok | 0.74 | | | | | | |
| 1359 | ok | 0.45 | | | | | | |
| 1374 | ok | 0.24 | | | | | | |
| 1389 | ok | 0.28 | | | | | | |
| 1404 | ok | 0.33 | | | | | | |
| 1419 | ok | 0.37 | | | | | | |
| 1434 | ok | 0.40 | | | | | | |
| 1449 | ok | 0.44 | | | | | | |
| 1464 | ok | 0.47 | | | | | | |
| 1479 | ok | 0.53 | | | | | | |
| 1494 | ok | 0.60 | | | | | | |
| 1526 | ok | 0.97 | | | | | | |
| 7305 | ok | 0.30 | | | | | | |
| 7308 | ok | 0.32 | | | | | | |
| 7309 | ok | 0.32 | | | | | | |
| 7310 | ok | 0.32 | | | | | | |
| 7311 | ok | 0.29 | | | | | | |
| 7312 | ok | 0.23 | | | | | | |
| 7313 | ok | 0.20 | | | | | | |
| 7314 | ok | 0.14 | | | | | | |
| 7315 | ok | 0.10 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 7316 | ok | 0.14 | | | | | | |
| 7317 | ok | 0.32 | | | | | | |
| 7318 | ok | 0.27 | | | | | | |
| 7388 | ok | 0.33 | | | | | | |
| 7389 | ok | 0.33 | | | | | | |
| 7390 | ok | 0.33 | | | | | | |
| 7391 | ok | 0.28 | | | | | | |
| 7392 | ok | 0.26 | | | | | | |
| 7393 | ok | 0.24 | | | | | | |
| 7394 | ok | 0.32 | | | | | | |
| 7395 | ok | 0.30 | | | | | | |
| 7396 | ok | 0.31 | | | | | | |
| 7397 | ok | 0.30 | | | | | | |
| 7398 | ok | 0.21 | | | | | | |
| 7399 | ok | 0.12 | | | | | | |
| 7400 | ok | 0.11 | | | | | | |
| 7401 | ok | 0.11 | | | | | | |
| 7402 | ok | 0.11 | | | | | | |
| 7403 | ok | 0.11 | | | | | | |
| 7404 | ok | 0.16 | | | | | | |
| 7405 | ok | 0.17 | | | | | | |
| 7406 | ok | 0.19 | | | | | | |
| 7407 | ok | 0.21 | | | | | | |
| 7408 | ok | 0.23 | | | | | | |
| 7409 | ok | 0.25 | | | | | | |
| 7410 | ok | 0.26 | | | | | | |
| 7411 | ok | 0.28 | | | | | | |
| 7412 | ok | 0.29 | | | | | | |
| 7413 | ok | 0.31 | | | | | | |
| 7414 | ok | 0.30 | | | | | | |
| 7695 | ok | 0.97 | | | | | | |
| 7749 | ok | 0.62 | | | | | | |
| 7803 | ok | 0.49 | | | | | | |
| 7857 | ok | 0.40 | | | | | | |
| 9042 | ok | 0.97 | | | | | | |
| 9043 | ok | 0.62 | | | | | | |
| 9044 | ok | 0.49 | | | | | | |
| 9045 | ok | 0.40 | | | | | | |
| 9046 | ok | 1.04 | | | | | | |
| 9047 | ok | 0.64 | | | | | | |
| 9048 | ok | 0.50 | | | | | | |
| 9049 | ok | 0.41 | | | | | | |
| 9050 | ok | 0.77 | | | | | | |
| 9051 | ok | 0.44 | | | | | | |
| 9052 | ok | 0.35 | | | | | | |
| 9053 | ok | 0.30 | | | | | | |
| 9054 | ok | 0.59 | | | | | | |
| 9055 | ok | 0.59 | | | | | | |
| 9056 | ok | 0.32 | | | | | | |
| 9057 | ok | 0.28 | | | | | | |
| 9058 | ok | 0.28 | | | | | | |
| 9059 | ok | 0.28 | | | | | | |
| 9060 | ok | 0.56 | | | | | | |
| 9061 | ok | 0.56 | | | | | | |
| 9062 | ok | 0.24 | | | | | | |
| 9063 | ok | 0.22 | | | | | | |
| 9064 | ok | 0.31 | | | | | | |
| 9065 | ok | 0.31 | | | | | | |
| 9066 | ok | 0.56 | | | | | | |
| 9067 | ok | 0.56 | | | | | | |
| 9068 | ok | 0.19 | | | | | | |
| 9069 | ok | 0.17 | | | | | | |
| 9070 | ok | 0.32 | | | | | | |
| 9071 | ok | 0.32 | | | | | | |
| 9072 | ok | 0.57 | | | | | | |
| 9073 | ok | 0.57 | | | | | | |
| 9074 | ok | 0.15 | | | | | | |
| 9075 | ok | 0.14 | | | | | | |
| 9076 | ok | 0.33 | | | | | | |
| 9077 | ok | 0.33 | | | | | | |
| 9078 | ok | 0.58 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 9079 | ok | 0.59 | | | | | | |
| 9080 | ok | 0.14 | | | | | | |
| 9081 | ok | 0.14 | | | | | | |
| 9082 | ok | 0.33 | | | | | | |
| 9083 | ok | 0.33 | | | | | | |
| 9084 | ok | 0.58 | | | | | | |
| 9085 | ok | 0.13 | | | | | | |
| 9086 | ok | 0.13 | | | | | | |
| 9087 | ok | 0.32 | | | | | | |
| 9088 | ok | 0.45 | | | | | | |
| 9089 | ok | 0.13 | | | | | | |
| 9090 | ok | 0.13 | | | | | | |
| 9091 | ok | 0.31 | | | | | | |
| 9092 | ok | 0.38 | | | | | | |
| 9093 | ok | 0.12 | | | | | | |
| 9094 | ok | 0.12 | | | | | | |
| 9095 | ok | 0.29 | | | | | | |
| 9096 | ok | 0.32 | | | | | | |
| 9097 | ok | 0.12 | | | | | | |
| 9098 | ok | 0.12 | | | | | | |
| 9099 | ok | 0.26 | | | | | | |
| 9100 | ok | 0.28 | | | | | | |
| 9101 | ok | 0.12 | | | | | | |
| 9102 | ok | 0.12 | | | | | | |
| 9103 | ok | 0.24 | | | | | | |
| 9104 | ok | 0.25 | | | | | | |
| 9105 | ok | 0.12 | | | | | | |
| 9106 | ok | 0.12 | | | | | | |
| 9107 | ok | 0.21 | | | | | | |
| 9108 | ok | 0.22 | | | | | | |
| 9109 | ok | 0.12 | | | | | | |
| 9110 | ok | 0.12 | | | | | | |
| 9111 | ok | 0.19 | | | | | | |
| 9112 | ok | 0.19 | | | | | | |
| 9113 | ok | 0.12 | | | | | | |
| 9114 | ok | 0.12 | | | | | | |
| 9115 | ok | 0.16 | | | | | | |
| 9116 | ok | 0.15 | | | | | | |
| 9117 | ok | 0.11 | | | | | | |
| 9118 | ok | 0.12 | | | | | | |
| 9119 | ok | 0.14 | | | | | | |
| 9120 | ok | 0.17 | | | | | | |
| 9121 | ok | 0.11 | | | | | | |
| 9122 | ok | 0.11 | | | | | | |
| 9123 | ok | 0.13 | | | | | | |
| 9124 | ok | 0.20 | | | | | | |
| 9125 | ok | 0.11 | | | | | | |
| 9126 | ok | 0.11 | | | | | | |
| 9127 | ok | 0.12 | | | | | | |
| 9128 | ok | 0.27 | | | | | | |
| 9129 | ok | 0.13 | | | | | | |
| 9130 | ok | 0.12 | | | | | | |
| 9131 | ok | 0.11 | | | | | | |
| 9132 | ok | 0.27 | | | | | | |
| 9133 | ok | 0.46 | | | | | | |
| 9134 | ok | 0.13 | | | | | | |
| 9135 | ok | 0.12 | | | | | | |
| 9136 | ok | 0.11 | | | | | | |
| 9137 | ok | 0.13 | | | | | | |
| 9138 | ok | 0.18 | | | | | | |
| 9139 | ok | 0.25 | | | | | | |
| 9140 | ok | 0.13 | | | | | | |
| 9141 | ok | 0.12 | | | | | | |
| 9142 | ok | 0.11 | | | | | | |
| 9143 | ok | 0.12 | | | | | | |
| 9144 | ok | 0.19 | | | | | | |
| 9145 | ok | 0.43 | | | | | | |
| 9146 | ok | 0.13 | | | | | | |
| 9147 | ok | 0.12 | | | | | | |
| 9148 | ok | 0.11 | | | | | | |
| 9149 | ok | 0.10 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 9150 | ok | 0.13 | | | | | | |
| 9151 | ok | 0.25 | | | | | | |
| 9152 | ok | 0.13 | | | | | | |
| 9153 | ok | 0.12 | | | | | | |
| 9154 | ok | 0.11 | | | | | | |
| 9155 | ok | 0.11 | | | | | | |
| 9156 | ok | 0.27 | | | | | | |
| 9157 | ok | 0.13 | | | | | | |
| 9158 | ok | 0.12 | | | | | | |
| 9159 | ok | 0.11 | | | | | | |
| 9160 | ok | 0.27 | | | | | | |
| 9161 | ok | 0.68 | | | | | | |
| 9162 | ok | 0.13 | | | | | | |
| 9163 | ok | 0.12 | | | | | | |
| 9164 | ok | 0.11 | | | | | | |
| 9165 | ok | 0.10 | | | | | | |
| 9166 | ok | 0.21 | | | | | | |
| 9167 | ok | 0.10 | | | | | | |
| 9168 | ok | 0.10 | | | | | | |
| 9169 | ok | 0.11 | | | | | | |
| 9170 | ok | 0.18 | | | | | | |
| 9171 | ok | 0.09 | | | | | | |
| 9172 | ok | 0.10 | | | | | | |
| 9173 | ok | 0.11 | | | | | | |
| 9174 | ok | 0.13 | | | | | | |
| 9175 | ok | 0.09 | | | | | | |
| 9176 | ok | 0.10 | | | | | | |
| 9177 | ok | 0.11 | | | | | | |
| 9178 | ok | 0.18 | | | | | | |
| 9179 | ok | 0.09 | | | | | | |
| 9180 | ok | 0.10 | | | | | | |
| 9181 | ok | 0.11 | | | | | | |
| 9182 | ok | 0.23 | | | | | | |
| 9183 | ok | 0.11 | | | | | | |
| 9184 | ok | 0.11 | | | | | | |
| 9185 | ok | 0.11 | | | | | | |
| 9186 | ok | 0.29 | | | | | | |
| 9187 | ok | 0.13 | | | | | | |
| 9188 | ok | 0.12 | | | | | | |
| 9189 | ok | 0.12 | | | | | | |
| 9190 | ok | 0.29 | | | | | | |
| 9191 | ok | 0.72 | | | | | | |
| 9192 | ok | 0.15 | | | | | | |
| 9193 | ok | 0.13 | | | | | | |
| 9194 | ok | 0.13 | | | | | | |
| 9195 | ok | 0.15 | | | | | | |
| 9196 | ok | 0.26 | | | | | | |
| 9197 | ok | 0.52 | | | | | | |
| 9198 | ok | 0.15 | | | | | | |
| 9199 | ok | 0.13 | | | | | | |
| 9200 | ok | 0.14 | | | | | | |
| 9201 | ok | 0.17 | | | | | | |
| 9202 | ok | 0.19 | | | | | | |
| 9203 | ok | 0.36 | | | | | | |
| 9204 | ok | 0.14 | | | | | | |
| 9205 | ok | 0.13 | | | | | | |
| 9206 | ok | 0.15 | | | | | | |
| 9207 | ok | 0.18 | | | | | | |
| 9208 | ok | 0.31 | | | | | | |
| 9209 | ok | 0.46 | | | | | | |
| 9210 | ok | 0.14 | | | | | | |
| 9211 | ok | 0.13 | | | | | | |
| 9212 | ok | 0.17 | | | | | | |
| 9213 | ok | 0.19 | | | | | | |
| 9214 | ok | 0.25 | | | | | | |
| 9215 | ok | 0.30 | | | | | | |
| 9216 | ok | 0.14 | | | | | | |
| 9217 | ok | 0.13 | | | | | | |
| 9218 | ok | 0.16 | | | | | | |
| 9219 | ok | 0.19 | | | | | | |
| 9220 | ok | 0.31 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------------|-------|----------------|-----------------|------------------|----------------|-----------------|-------------|--------------|
| 9221 | ok | 0.13 | | | | | | |
| 9222 | ok | 0.12 | | | | | | |
| 9223 | ok | 0.18 | | | | | | |
| 9224 | ok | 0.26 | | | | | | |
| 9225 | ok | 0.11 | | | | | | |
| 9226 | ok | 0.11 | | | | | | |
| 9227 | ok | 0.19 | | | | | | |
| 9228 | ok | 0.22 | | | | | | |
| 9229 | ok | 0.10 | | | | | | |
| 9230 | ok | 0.11 | | | | | | |
| 9231 | ok | 0.21 | | | | | | |
| 9232 | ok | 0.25 | | | | | | |
| 9233 | ok | 0.10 | | | | | | |
| 9234 | ok | 0.11 | | | | | | |
| 9235 | ok | 0.23 | | | | | | |
| 9236 | ok | 0.30 | | | | | | |
| 9237 | ok | 0.10 | | | | | | |
| 9238 | ok | 0.11 | | | | | | |
| 9239 | ok | 0.25 | | | | | | |
| 9240 | ok | 0.34 | | | | | | |
| 9241 | ok | 0.11 | | | | | | |
| 9242 | ok | 0.11 | | | | | | |
| 9243 | ok | 0.27 | | | | | | |
| 9244 | ok | 0.37 | | | | | | |
| 9245 | ok | 0.11 | | | | | | |
| 9246 | ok | 0.12 | | | | | | |
| 9247 | ok | 0.29 | | | | | | |
| 9248 | ok | 0.40 | | | | | | |
| 9249 | ok | 0.11 | | | | | | |
| 9250 | ok | 0.12 | | | | | | |
| 9251 | ok | 0.30 | | | | | | |
| 9252 | ok | 0.44 | | | | | | |
| 9253 | ok | 0.12 | | | | | | |
| 9254 | ok | 0.12 | | | | | | |
| 9255 | ok | 0.32 | | | | | | |
| 9256 | ok | 0.49 | | | | | | |
| 9257 | ok | 0.12 | | | | | | |
| 9258 | ok | 0.13 | | | | | | |
| 9259 | ok | 0.33 | | | | | | |
| 9260 | ok | 0.54 | | | | | | |
| 9261 | ok | 0.14 | | | | | | |
| 9262 | ok | 0.14 | | | | | | |
| 9263 | ok | 0.33 | | | | | | |
| 9264 | ok | 0.59 | | | | | | |
| 9265 | ok | 0.19 | | | | | | |
| 9266 | ok | 0.18 | | | | | | |
| 9267 | ok | 0.33 | | | | | | |
| 9268 | ok | 0.65 | | | | | | |
| 9269 | ok | 0.24 | | | | | | |
| 9270 | ok | 0.22 | | | | | | |
| 9271 | ok | 0.32 | | | | | | |
| 9272 | ok | 0.72 | | | | | | |
| 9273 | ok | 0.31 | | | | | | |
| 9274 | ok | 0.28 | | | | | | |
| 9275 | ok | 0.31 | | | | | | |
| 9276 | ok | 0.83 | | | | | | |
| 9277 | ok | 0.43 | | | | | | |
| 9278 | ok | 0.35 | | | | | | |
| 9279 | ok | 0.31 | | | | | | |
| 9280 | ok | 1.04 | | | | | | |
| 9281 | ok | 0.64 | | | | | | |
| 9282 | ok | 0.50 | | | | | | |
| 9283 | ok | 0.41 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 1.04 | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 73 | 40.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|--------|----------|-----------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 5 | ok | 0.09 | 8.90e-02 | 2.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -96.4 | 4.1 | -28.9 | -17.3 | 317.2 | 98.7 |
| 6 | ok | 0.09 | 0.2 | 2.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -91.8 | -85.6 | -24.9 | -137.4 | -1455.3 | -18.3 |
| 17 | ok | 0.09 | 0.1 | 8.97e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -35.5 | -18.0 | 17.0 | 11.1 | 0.4 | 7.6 |
| 18 | ok | 0.09 | 0.1 | 6.08e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.0 | 19.0 | -16.9 | -63.5 | 5.4 | -3.5 |
| 19 | ok | 0.09 | 0.1 | 6.52e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.5 | 36.8 | 2.0 | -16.7 | -0.4 | 0.1 |
| 20 | ok | 0.09 | 8.75e-02 | 1.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.6 | 16.9 | -14.4 | -135.5 | 43.4 | 31.4 |
| 21 | ok | 0.09 | 0.3 | 2.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.0 | 10.6 | -76.5 | -0.7 | -1148.1 | -6.8 |
| 1807 | ok | 0.09 | 4.43e-02 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.8 | -15.1 | -18.0 | 5.4 | -49.3 | 117.9 |
| 1809 | ok | 0.09 | 0.1 | 1.75e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.6 | -55.7 | -19.1 | -26.2 | -760.4 | 50.6 |
| 1811 | ok | 0.09 | 7.30e-02 | 1.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.2 | -35.9 | -18.8 | 7.8 | -354.5 | 71.2 |
| 1996 | ok | 0.09 | 9.81e-02 | 7.24e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -26.5 | 24.5 | -13.9 | -126.2 | 44.6 | 27.3 |
| 2000 | ok | 0.09 | 0.1 | 5.43e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -17.3 | 31.1 | -10.9 | -114.8 | 42.5 | 24.8 |
| 2004 | ok | 0.09 | 0.1 | 4.02e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -13.0 | 35.7 | -7.9 | -105.1 | 39.2 | 24.3 |
| 2008 | ok | 0.09 | 0.1 | 3.01e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.2 | 39.0 | -5.3 | -100.7 | 37.1 | 25.2 |
| 2012 | ok | 0.09 | 0.1 | 2.85e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -10.9 | 41.0 | -6.5 | -103.3 | 37.3 | 26.0 |
| 2016 | ok | 0.09 | 0.1 | 4.03e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -13.0 | 40.1 | -1.4 | -13.0 | -1.8 | 0.2 |
| 2020 | ok | 0.09 | 0.1 | 5.36e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -17.7 | 38.9 | 1.1 | -14.9 | -1.0 | 0.2 |
| 2024 | ok | 0.09 | 0.1 | 5.00e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -26.4 | 20.9 | -13.2 | -56.4 | 5.8 | -3.7 |
| 2028 | ok | 0.09 | 0.1 | 3.70e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.5 | 26.0 | -12.9 | -51.0 | 4.5 | -4.4 |
| 2032 | ok | 0.09 | 0.1 | 2.57e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -10.3 | 37.6 | 6.7 | -98.7 | 31.3 | -20.5 |
| 2036 | ok | 0.09 | 0.1 | 3.17e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -10.5 | 35.6 | 5.1 | -96.0 | 32.3 | -19.5 |
| 2040 | ok | 0.09 | 0.1 | 4.12e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.9 | 32.6 | 7.3 | -100.0 | 36.7 | -18.5 |
| 2044 | ok | 0.09 | 0.1 | 5.40e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.3 | 28.5 | 9.8 | -108.9 | 43.9 | -18.9 |
| 2048 | ok | 0.09 | 0.1 | 6.87e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -22.0 | 23.1 | 15.7 | -119.2 | 52.3 | -20.8 |
| 2126 | ok | 0.09 | 0.3 | 3.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -133.1 | -24.5 | -24.3 | -167.2 | -927.4 | 26.2 |
| 2141 | ok | 0.09 | 9.95e-02 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -76.7 | -15.4 | -11.3 | -127.4 | -525.7 | 32.8 |
| 2156 | ok | 0.09 | 6.06e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.3 | -11.1 | -11.4 | -120.1 | -303.1 | 42.6 |
| 2171 | ok | 0.09 | 4.51e-02 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.5 | -8.0 | -12.2 | -122.8 | -166.4 | 46.7 |
| 2186 | ok | 0.09 | 4.99e-02 | 1.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.6 | -5.4 | -12.9 | -34.5 | -96.9 | -6.1 |
| 2201 | ok | 0.09 | 5.74e-02 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.3 | -16.1 | -13.3 | -25.3 | -13.4 | 12.9 |
| 2216 | ok | 0.09 | 6.70e-02 | 1.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.4 | -15.4 | -15.5 | -22.8 | -2.4 | 14.0 |
| 2231 | ok | 0.09 | 7.83e-02 | 1.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.0 | -13.0 | -13.7 | -20.5 | 5.9 | 14.4 |
| 2246 | ok | 0.09 | 0.1 | 7.58e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.5 | 34.0 | 1.1 | -18.8 | 0.4 | -1.29e-02 |
| 2261 | ok | 0.09 | 0.1 | 7.80e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.6 | 36.7 | -0.9 | -140.2 | 55.7 | 11.6 |
| 2276 | ok | 0.09 | 0.1 | 7.67e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.8 | 35.9 | 2.8 | -138.7 | 56.3 | 7.9 |
| 2291 | ok | 0.09 | 0.1 | 7.51e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.2 | 35.4 | 2.7 | -136.4 | 55.7 | 4.6 |
| 2306 | ok | 0.09 | 0.1 | 7.41e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.3 | 35.0 | 2.6 | -134.9 | 54.9 | 1.7 |
| 2321 | ok | 0.09 | 0.1 | 7.41e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.1 | 34.7 | -1.5 | -134.8 | 54.3 | -1.4 |
| 2336 | ok | 0.09 | 0.1 | 7.52e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.7 | 34.6 | -1.7 | -135.8 | 53.5 | -4.5 |
| 2351 | ok | 0.09 | 0.1 | 7.53e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.4 | 34.8 | -2.2 | -136.3 | 51.7 | -8.4 |
| 2366 | ok | 0.09 | 0.1 | 7.18e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.2 | 35.6 | 1.3 | -134.0 | 48.1 | -12.3 |
| 2407 | ok | 0.09 | 9.49e-02 | 1.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.4 | -22.5 | 13.3 | 9.9 | 0.3 | 11.3 |
| 2422 | ok | 0.09 | 8.31e-02 | 9.84e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -36.0 | -24.7 | 10.9 | 8.6 | 0.2 | 15.3 |
| 2437 | ok | 0.09 | 7.22e-02 | 9.49e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.1 | -25.7 | 10.0 | 7.2 | 0.1 | 19.0 |
| 2452 | ok | 0.09 | 6.00e-02 | 9.27e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.6 | -26.4 | 9.7 | 5.7 | 4.69e-02 | 21.8 |
| 2467 | ok | 0.09 | 4.61e-02 | 9.25e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.1 | -23.7 | 11.7 | -54.9 | 21.6 | -35.6 |
| 2482 | ok | 0.09 | 3.42e-02 | 9.44e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.7 | -26.7 | 14.9 | -51.5 | 20.7 | -36.3 |
| 2497 | ok | 0.09 | 3.30e-02 | 9.90e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.4 | -27.6 | 14.8 | -15.7 | 3.5 | -4.0 |
| 2512 | ok | 0.09 | 3.23e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.1 | -32.3 | 11.5 | -15.5 | -2.5 | -4.9 |
| 2527 | ok | 0.09 | 3.30e-02 | 1.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.9 | -41.2 | 11.5 | -13.4 | -4.4 | -5.3 |
| 2542 | ok | 0.09 | 3.78e-02 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.5 | -51.4 | 11.0 | -10.8 | -4.0 | -5.9 |
| 2557 | ok | 0.09 | 5.04e-02 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.3 | -62.8 | 13.6 | -8.4 | 3.5 | -6.8 |
| 2572 | ok | 0.09 | 7.05e-02 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.1 | -74.7 | 7.2 | -9.4 | 24.6 | -7.0 |
| 2587 | ok | 0.09 | 9.89e-02 | 2.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.5 | -87.7 | 1.8 | -50.7 | 60.1 | 13.1 |
| 7307 | ok | 0.09 | 6.95e-02 | 4.68e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -174.1 | -75.3 | -74.9 | -287.0 | 159.8 | -4.7 |
| 7308 | ok | 0.09 | 0.1 | 5.97e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -26.7 | 36.3 | -4.6 | -258.5 | -164.2 | -43.6 |
| 7319 | ok | 0.09 | 0.2 | 3.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.1 | 30.0 | -37.8 | -21.0 | -26.8 | -35.1 |
| 7320 | ok | 0.09 | 0.1 | 2.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.2 | 2.5 | -53.2 | -18.9 | -23.2 | -34.1 |
| 7321 | ok | 0.09 | 0.2 | 2.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.2 | -16.1 | -66.1 | -26.1 | -14.2 | -34.7 |
| 7322 | ok | 0.09 | 0.2 | 3.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.0 | 31.2 | 47.2 | -234.3 | -304.8 | 410.1 |
| 7323 | ok | 0.09 | 0.2 | 3.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -96.6 | -8.5 | 116.2 | 241.3 | 405.3 | -201.0 |
| 7416 | ok | 0.09 | 4.90e-02 | 2.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.6 | -8.9 | -20.4 | -211.8 | 92.2 | 59.1 |
| 7417 | ok | 0.09 | 8.98e-02 | 1.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.0 | -3.8 | -34.4 | -286.0 | -261.1 | 26.9 |
| 7418 | ok | 0.09 | 5.00e-02 | 1.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.0 | -15.0 | -40.2 | -176.8 | -102.0 | 38.8 |
| 7420 | ok | 0.09 | 0.2 | 3.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.1 | -50.1 | -97.2 | -150.6 | 237.3 | -75.8 |
| 7421 | ok | 0.09 | 0.2 | 3.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.0 | -47.0 | -90.4 | -21.3 | -19.5 | -28.2 |
| 7422 | ok | 0.09 | 0.2 | 2.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.7 | -42.6 | -84.3 | -22.0 | -16.7 | -29.3 |
| 7423 | ok | 0.09 | 0.2 | 2.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.7 | -37.2 | -78.4 | -22.7 | -15.0 | -30.2 |
| 7424 | ok | 0.09 | 0.2 | 2.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.1 | -31.4 | -73.0 | -23.3 | -14.1 | -31.1 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|-------|--------|--------|---------|--------|
| 7425 | ok | 0.09 | 0.2 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.3 | -25.7 | -68.7 | -23.9 | -13.8 | -32.1 |
| 7426 | ok | 0.09 | 0.2 | 2.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.6 | -20.6 | -66.0 | -24.6 | -14.0 | -33.2 |
| 7427 | ok | 0.09 | 0.1 | 2.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.4 | 3.6 | -48.6 | -21.3 | -21.9 | -34.7 |
| 7428 | ok | 0.09 | 0.1 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.2 | 7.0 | -44.4 | -20.7 | -22.4 | -34.0 |
| 7429 | ok | 0.09 | 0.2 | 2.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.1 | 11.4 | -41.1 | -20.5 | -22.9 | -33.6 |
| 7430 | ok | 0.09 | 0.2 | 2.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.3 | 16.1 | -38.5 | -20.3 | -23.4 | -33.4 |
| 7431 | ok | 0.09 | 0.2 | 2.68e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.8 | 20.7 | -36.7 | -20.3 | -24.1 | -33.5 |
| 7432 | ok | 0.09 | 0.2 | 2.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.8 | 24.8 | -35.9 | -20.3 | -24.8 | -33.8 |
| 7433 | ok | 0.09 | 0.2 | 2.98e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.3 | 27.9 | -36.3 | -20.5 | -25.8 | -34.3 |
| 7434 | ok | 0.09 | 0.2 | 3.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.5 | -29.7 | -132.7 | -62.2 | -117.6 | -89.2 |
| 7435 | ok | 0.09 | 0.2 | 3.99e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -73.5 | 22.6 | 83.3 | -34.8 | -190.5 | 92.5 |
| 7436 | ok | 0.09 | 0.2 | 3.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.2 | 30.7 | 72.9 | -48.6 | -277.1 | 177.5 |
| 7437 | ok | 0.09 | 0.2 | 3.95e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.1 | 35.7 | 66.6 | -81.1 | -325.4 | 250.3 |
| 7438 | ok | 0.09 | 0.2 | 3.93e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.2 | 38.4 | 62.4 | -118.4 | -347.3 | 307.0 |
| 7439 | ok | 0.09 | 0.2 | 3.90e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.4 | 39.7 | 58.9 | -152.9 | -352.0 | 348.2 |
| 7440 | ok | 0.09 | 0.2 | 3.83e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.0 | 39.7 | 55.5 | -181.6 | -346.1 | 376.3 |
| 7441 | ok | 0.09 | 0.2 | 3.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.1 | 38.0 | 51.8 | -203.3 | -333.8 | 393.0 |
| 7442 | ok | 0.09 | 0.2 | 2.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.0 | -10.5 | -63.4 | -23.0 | -16.1 | -34.5 |
| 7443 | ok | 0.09 | 0.2 | 2.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.3 | -0.7 | -60.2 | -21.9 | -12.0 | -31.3 |
| 7444 | ok | 0.09 | 0.1 | 2.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.0 | -1.1 | -60.2 | -21.9 | -12.9 | -31.9 |
| 7445 | ok | 0.09 | 0.1 | 2.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.9 | -2.9 | -62.1 | -24.3 | -16.2 | -36.4 |
| 7446 | ok | 0.09 | 0.1 | 2.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.5 | -3.5 | -62.0 | -24.0 | -17.5 | -36.8 |
| 7447 | ok | 0.09 | 0.1 | 2.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.1 | -4.2 | -61.7 | -23.6 | -18.7 | -36.9 |
| 7448 | ok | 0.09 | 0.1 | 2.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.6 | -4.5 | -61.0 | -23.1 | -19.8 | -36.8 |
| 7449 | ok | 0.09 | 0.1 | 2.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.1 | -4.1 | -59.9 | -22.5 | -20.8 | -36.4 |
| 7450 | ok | 0.09 | 0.1 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.4 | -2.6 | -58.4 | -22.2 | -21.4 | -36.1 |
| 7451 | ok | 0.09 | 0.2 | 3.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.7 | 32.9 | -40.5 | -20.9 | -28.7 | -35.8 |
| 7452 | ok | 0.09 | 0.2 | 3.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.0 | 34.5 | -42.8 | -21.1 | -30.6 | -36.7 |
| 7453 | ok | 0.09 | 0.2 | 3.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.4 | 34.8 | -44.6 | -21.5 | -32.5 | -38.0 |
| 7454 | ok | 0.09 | 0.2 | 3.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.4 | -50.2 | 98.0 | -114.5 | 335.3 | 6.7 |
| 7455 | ok | 0.09 | 0.2 | 3.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.2 | 34.6 | -48.5 | -210.1 | -384.9 | -424.3 |
| 7456 | ok | 0.09 | 0.2 | 3.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.4 | 35.9 | -49.6 | -191.3 | -399.4 | -411.1 |
| 7457 | ok | 0.09 | 0.2 | 3.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.5 | 38.0 | -50.8 | -168.3 | -409.5 | -391.2 |
| 7458 | ok | 0.09 | 0.2 | 3.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.0 | 41.1 | -51.7 | -141.0 | -413.8 | -363.5 |
| 7459 | ok | 0.09 | 0.2 | 3.57e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.6 | 45.6 | -51.6 | -109.1 | -410.4 | -326.6 |
| 7460 | ok | 0.09 | 0.2 | 3.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.0 | 51.5 | -49.1 | -72.6 | -397.4 | -278.9 |
| 7461 | ok | 0.09 | 0.2 | 3.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.2 | 57.1 | -42.9 | -24.7 | -373.4 | -217.1 |
| 7462 | ok | 0.09 | 0.2 | 2.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.2 | 29.3 | 72.4 | -53.6 | 327.2 | -469.9 |
| 7463 | ok | 0.09 | 0.2 | 9.22e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 8.4 | 25.1 | -11.2 | -720.0 | -389.5 | 122.4 |
| 8762 | ok | 0.09 | 0.3 | 2.77e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -110.9 | -44.1 | -36.4 | -162.6 | -1380.4 | -80.5 |
| 8763 | ok | 0.09 | 0.2 | 2.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -108.7 | -21.0 | -17.8 | -195.3 | -874.2 | -44.3 |
| 8764 | ok | 0.09 | 0.1 | 2.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -106.3 | -19.1 | -14.5 | -164.8 | -607.3 | -36.2 |
| 8765 | ok | 0.09 | 8.65e-02 | 2.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -95.7 | -22.2 | -47.5 | -107.5 | -465.3 | -23.6 |
| 9046 | ok | 0.09 | 0.2 | 1.68e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.2 | -31.8 | -17.8 | -217.4 | -1354.6 | -24.2 |
| 9047 | ok | 0.09 | 0.2 | 1.57e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.8 | -26.2 | -26.5 | -169.6 | -936.6 | -26.2 |
| 9048 | ok | 0.09 | 0.1 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.1 | -16.0 | -27.1 | -126.3 | -592.8 | -28.7 |
| 9049 | ok | 0.09 | 7.71e-02 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.6 | -13.9 | -31.3 | -154.2 | -307.8 | -82.5 |
| 9284 | ok | 0.09 | 0.1 | 1.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.6 | -12.7 | -30.0 | -78.2 | 415.1 | 97.4 |
| 9285 | ok | 0.09 | 7.83e-02 | 2.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -74.4 | -7.4 | -35.4 | -13.3 | 424.6 | 45.0 |
| 9286 | ok | 0.09 | 6.46e-02 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.7 | -8.2 | -37.4 | -24.6 | 345.4 | 38.0 |
| 9287 | ok | 0.09 | 7.11e-02 | 2.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -107.9 | -17.2 | -40.1 | -49.9 | 280.7 | 35.3 |
| 9288 | ok | 0.09 | 0.1 | 2.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -83.1 | -19.2 | -22.5 | -92.1 | -268.9 | -49.8 |
| 9289 | ok | 0.09 | 0.2 | 1.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.5 | 4.7 | 19.3 | -166.9 | -796.2 | 67.5 |
| 9290 | ok | 0.09 | 0.1 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.5 | -25.5 | -12.8 | -189.4 | -614.1 | -27.6 |
| 9291 | ok | 0.09 | 9.31e-02 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -85.0 | -19.0 | -13.7 | -157.1 | -433.4 | -43.6 |
| 9292 | ok | 0.09 | 0.1 | 2.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -74.9 | -9.7 | -5.8 | -99.2 | -208.0 | 56.5 |
| 9293 | ok | 0.09 | 0.1 | 2.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -92.5 | -14.1 | -18.2 | -190.9 | -493.4 | 112.2 |
| 9294 | ok | 0.09 | 0.1 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -72.4 | -20.5 | -11.3 | -179.5 | -412.0 | 94.2 |
| 9295 | ok | 0.09 | 8.79e-02 | 1.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -74.3 | -15.9 | -16.4 | -151.6 | -304.1 | 72.4 |
| 9296 | ok | 0.09 | 0.1 | 2.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -70.6 | 7.2 | 29.2 | -114.9 | -233.5 | 128.6 |
| 9297 | ok | 0.09 | 9.75e-02 | 1.58e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.2 | -13.0 | -14.2 | -164.2 | -300.4 | 163.2 |
| 9298 | ok | 0.09 | 9.20e-02 | 1.65e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.7 | -13.8 | -16.9 | -175.2 | -256.5 | 150.1 |
| 9299 | ok | 0.09 | 8.51e-02 | 1.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -70.6 | -11.6 | -11.3 | -151.1 | -210.8 | 134.1 |
| 9300 | ok | 0.09 | 0.1 | 2.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.5 | 13.0 | 23.7 | -128.3 | -230.6 | 178.4 |
| 9301 | ok | 0.09 | 8.78e-02 | 1.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.6 | -9.5 | -15.2 | -159.3 | -168.9 | 187.3 |
| 9302 | ok | 0.09 | 8.59e-02 | 1.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.5 | -10.6 | -18.9 | -169.4 | -150.9 | 178.9 |
| 9303 | ok | 0.09 | 8.38e-02 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.6 | -8.0 | -14.0 | -152.8 | -140.8 | 169.1 |
| 9304 | ok | 0.09 | 0.1 | 2.73e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.7 | 17.3 | 20.1 | -145.0 | -223.7 | 211.9 |
| 9305 | ok | 0.09 | 8.15e-02 | 1.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.9 | -5.6 | -16.2 | -159.5 | -82.5 | 195.3 |
| 9306 | ok | 0.09 | 8.12e-02 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.8 | -6.9 | -20.4 | -166.5 | -80.9 | 189.9 |
| 9307 | ok | 0.09 | 8.20e-02 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.0 | -4.4 | -16.1 | -155.9 | -93.4 | 184.1 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-------|------|-------|--------|--------|--------|
| 9308 | ok | 0.09 | 0.1 | 2.68e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.9 | 20.4 | 17.5 | -161.9 | -214.4 | 232.5 |
| 9309 | ok | 0.09 | 7.65e-02 | 1.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.1 | -1.2 | -14.4 | -161.7 | -25.7 | 192.1 |
| 9310 | ok | 0.09 | 7.72e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.0 | -2.9 | -21.8 | -165.8 | -35.5 | 189.2 |
| 9311 | ok | 0.09 | 7.98e-02 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.2 | -1.1 | -17.8 | -160.4 | -62.2 | 186.5 |
| 9312 | ok | 0.09 | 0.1 | 2.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.3 | 22.4 | 15.4 | -177.1 | -203.9 | 243.4 |
| 9313 | ok | 0.09 | 7.17e-02 | 1.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.0 | 3.0 | -19.2 | -161.6 | 7.1 | 164.5 |
| 9314 | ok | 0.09 | 7.32e-02 | 1.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.1 | 0.9 | -20.0 | -166.1 | -9.4 | 179.2 |
| 9315 | ok | 0.09 | 7.71e-02 | 1.58e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.2 | 1.8 | -19.3 | -165.3 | -42.1 | 181.2 |
| 9316 | ok | 0.09 | 0.1 | 2.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.4 | 22.9 | 13.4 | -189.5 | -192.8 | 247.3 |
| 9317 | ok | 0.09 | 6.73e-02 | 1.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.7 | 7.9 | -21.6 | -160.4 | 26.1 | 150.9 |
| 9318 | ok | 0.09 | 6.92e-02 | 1.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.7 | 4.2 | -22.1 | -165.8 | 10.3 | 168.8 |
| 9319 | ok | 0.09 | 7.43e-02 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.4 | 3.8 | -20.5 | -169.8 | -29.9 | 171.7 |
| 9320 | ok | 0.09 | 0.1 | 2.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.2 | 21.0 | 10.2 | -196.8 | -181.7 | 246.3 |
| 9321 | ok | 0.09 | 8.00e-02 | 1.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.4 | 11.5 | -23.7 | -22.6 | -18.0 | -9.3 |
| 9322 | ok | 0.09 | 7.98e-02 | 1.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.5 | 6.7 | -22.9 | -164.6 | 17.9 | 155.2 |
| 9323 | ok | 0.09 | 8.10e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.1 | -4.2 | -31.9 | -21.7 | -15.6 | -7.2 |
| 9324 | ok | 0.09 | 0.1 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.6 | 19.4 | 13.8 | -211.9 | -167.3 | 249.9 |
| 9325 | ok | 0.09 | 9.11e-02 | 9.29e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.8 | 15.4 | -22.3 | -150.8 | 36.8 | 135.5 |
| 9326 | ok | 0.09 | 8.73e-02 | 1.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.6 | 8.5 | -24.6 | -162.8 | 18.4 | 143.5 |
| 9327 | ok | 0.09 | 8.69e-02 | 1.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.6 | -2.9 | -30.6 | -20.4 | -11.3 | -6.3 |
| 9328 | ok | 0.09 | 0.1 | 2.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.4 | 17.7 | 14.2 | -215.7 | -158.7 | 245.7 |
| 9329 | ok | 0.09 | 9.82e-02 | 7.25e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.3 | 18.4 | -16.4 | -142.9 | 34.5 | 125.3 |
| 9330 | ok | 0.09 | 9.00e-02 | 9.34e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.8 | 9.8 | -18.9 | -160.5 | 19.3 | 133.0 |
| 9331 | ok | 0.09 | 8.82e-02 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.6 | 3.7 | -22.1 | -176.6 | -2.3 | 135.0 |
| 9332 | ok | 0.09 | 0.1 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.7 | 15.4 | 15.9 | -220.0 | -149.6 | 241.8 |
| 9333 | ok | 0.09 | 0.1 | 5.68e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -16.7 | 21.7 | -12.4 | -136.3 | 30.7 | 118.6 |
| 9334 | ok | 0.09 | 9.02e-02 | 7.86e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.5 | 11.5 | -15.0 | -159.2 | 17.7 | 124.3 |
| 9335 | ok | 0.09 | 8.65e-02 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.1 | 4.5 | -18.5 | -179.2 | -2.7 | 125.6 |
| 9336 | ok | 0.09 | 0.1 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.1 | 1.6 | -7.8 | -207.2 | -46.8 | 137.0 |
| 9337 | ok | 0.09 | 0.1 | 4.67e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -14.6 | 24.6 | -11.2 | -133.7 | 28.1 | 114.7 |
| 9338 | ok | 0.09 | 8.87e-02 | 6.72e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -22.2 | 13.4 | -10.9 | -159.7 | 16.4 | 116.8 |
| 9339 | ok | 0.09 | 8.28e-02 | 9.33e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -29.9 | 5.5 | -14.5 | -182.3 | -3.3 | 116.8 |
| 9340 | ok | 0.09 | 0.1 | 1.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.3 | 1.4 | -4.0 | -212.5 | -45.0 | 128.7 |
| 9341 | ok | 0.09 | 0.1 | 4.13e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -14.1 | 26.6 | -7.7 | -136.2 | 28.4 | 111.2 |
| 9342 | ok | 0.09 | 8.47e-02 | 6.01e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.5 | 15.1 | -6.9 | -162.4 | 15.9 | 109.7 |
| 9343 | ok | 0.09 | 7.68e-02 | 8.44e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.9 | 3.8 | -15.1 | -182.5 | 16.2 | 96.3 |
| 9344 | ok | 0.09 | 0.1 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.6 | -0.6 | 19.5 | 69.6 | 6.4 | -21.8 |
| 9345 | ok | 0.09 | 0.1 | 4.81e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.2 | 27.9 | -1.7 | -142.7 | 31.2 | 105.9 |
| 9346 | ok | 0.09 | 8.06e-02 | 5.87e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -23.2 | 8.3 | 18.7 | 61.1 | 6.9 | -25.4 |
| 9347 | ok | 0.09 | 6.93e-02 | 7.91e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.4 | 3.8 | 20.4 | 69.4 | 6.2 | -23.8 |
| 9348 | ok | 0.09 | 0.1 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.9 | -1.6 | 11.5 | 72.0 | 4.8 | -23.3 |
| 9349 | ok | 0.09 | 9.21e-02 | 5.73e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.5 | 13.7 | 19.7 | 56.3 | 0.9 | -24.6 |
| 9350 | ok | 0.09 | 7.37e-02 | 6.67e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.5 | 8.8 | 19.6 | 64.1 | 0.4 | -23.8 |
| 9351 | ok | 0.09 | 6.37e-02 | 8.06e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -30.5 | 4.4 | 21.2 | 72.2 | 6.0 | -21.9 |
| 9352 | ok | 0.09 | 0.1 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.6 | -0.8 | 11.7 | 75.3 | 4.7 | -20.8 |
| 9353 | ok | 0.09 | 8.41e-02 | 6.77e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -29.0 | 27.2 | 2.9 | -17.9 | -0.8 | -1.4 |
| 9354 | ok | 0.09 | 6.59e-02 | 7.57e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.2 | 9.3 | 18.8 | 67.1 | 0.6 | -21.7 |
| 9355 | ok | 0.09 | 6.31e-02 | 8.78e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.8 | 4.7 | 20.4 | 75.0 | 5.8 | -19.7 |
| 9356 | ok | 0.09 | 9.49e-02 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.3 | 0.9 | 7.6 | -33.6 | -5.9 | 21.1 |
| 9357 | ok | 0.09 | 8.93e-02 | 7.93e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.3 | 28.2 | 2.9 | -19.5 | 0.1 | -2.0 |
| 9358 | ok | 0.09 | 5.94e-02 | 8.40e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -37.1 | 9.8 | 16.3 | 70.8 | 0.2 | -18.2 |
| 9359 | ok | 0.09 | 6.11e-02 | 9.13e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -36.9 | 5.2 | 15.2 | 71.8 | 4.2 | -17.6 |
| 9360 | ok | 0.09 | 9.69e-02 | 1.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.2 | 5.2 | -28.4 | -20.1 | -7.7 | -15.6 |
| 9361 | ok | 0.09 | 9.09e-02 | 8.28e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.0 | 29.9 | 0.5 | -169.8 | 46.5 | 52.9 |
| 9362 | ok | 0.09 | 6.13e-02 | 8.74e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -39.2 | 18.9 | 1.6 | -20.5 | -0.6 | -3.9 |
| 9363 | ok | 0.09 | 6.04e-02 | 9.42e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -41.9 | 11.0 | -1.5 | -20.9 | -2.6 | -5.2 |
| 9364 | ok | 0.09 | 9.37e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.4 | 4.6 | -28.6 | -20.2 | -8.2 | -16.1 |
| 9365 | ok | 0.09 | 9.08e-02 | 8.26e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.5 | 29.3 | 2.9 | -170.0 | 46.7 | 36.8 |
| 9366 | ok | 0.09 | 6.23e-02 | 8.82e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -35.3 | 21.0 | 0.2 | -188.8 | 24.4 | 37.6 |
| 9367 | ok | 0.09 | 5.96e-02 | 9.59e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.3 | 12.1 | 0.8 | -209.4 | 2.2 | 37.9 |
| 9368 | ok | 0.09 | 9.04e-02 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.9 | 2.8 | 7.7 | -233.8 | -22.9 | 47.6 |
| 9369 | ok | 0.09 | 8.97e-02 | 8.17e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.0 | 28.8 | 2.6 | -168.9 | 45.9 | 21.9 |
| 9370 | ok | 0.09 | 6.25e-02 | 8.80e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -36.0 | 20.8 | 3.0 | -189.3 | 24.5 | 22.9 |
| 9371 | ok | 0.09 | 5.86e-02 | 9.57e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.8 | 12.1 | 0.6 | -210.6 | 2.4 | 24.1 |
| 9372 | ok | 0.09 | 8.69e-02 | 1.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.9 | 3.7 | -31.1 | -232.5 | -11.4 | -144.0 |
| 9373 | ok | 0.09 | 8.85e-02 | 8.07e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.1 | 28.4 | -0.6 | -167.9 | 45.0 | 8.1 |
| 9374 | ok | 0.09 | 6.23e-02 | 8.70e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -36.1 | 20.6 | -0.5 | -189.2 | 23.8 | 8.8 |
| 9375 | ok | 0.09 | 5.78e-02 | 9.44e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -42.2 | 11.2 | 6.0 | -211.2 | 0.5 | 18.8 |
| 9376 | ok | 0.09 | 8.34e-02 | 1.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.6 | 3.4 | -31.3 | -234.5 | -25.7 | -156.3 |
| 9377 | ok | 0.09 | 8.86e-02 | 8.05e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.9 | 28.3 | -0.8 | -167.6 | 44.5 | -5.7 |
| 9378 | ok | 0.09 | 6.33e-02 | 8.64e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -35.8 | 20.5 | 2.2 | -188.7 | 23.2 | -5.5 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-------|-------|-------|--------|--------|--------|
| 9379 | ok | 0.09 | 5.71e-02 | 9.31e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -41.7 | 11.6 | -4.1 | -210.4 | 1.2 | -14.5 |
| 9380 | ok | 0.09 | 8.60e-02 | 1.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.7 | 1.6 | 32.5 | -230.0 | -5.6 | 136.1 |
| 9381 | ok | 0.09 | 8.90e-02 | 8.07e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.2 | 28.4 | -1.2 | -167.7 | 43.9 | -19.9 |
| 9382 | ok | 0.09 | 6.41e-02 | 8.58e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -34.9 | 20.5 | -1.4 | -187.6 | 22.5 | -19.5 |
| 9383 | ok | 0.09 | 5.73e-02 | 9.20e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -37.7 | 12.0 | 1.3 | -208.9 | 1.3 | -19.4 |
| 9384 | ok | 0.09 | 8.90e-02 | 1.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.2 | 2.6 | -5.9 | -101.9 | -7.3 | 3.2 |
| 9385 | ok | 0.09 | 8.89e-02 | 7.98e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -30.7 | 28.7 | -1.9 | -166.7 | 42.6 | -35.1 |
| 9386 | ok | 0.09 | 6.54e-02 | 8.40e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.2 | 20.3 | 1.2 | -185.6 | 21.0 | -33.6 |
| 9387 | ok | 0.09 | 5.75e-02 | 8.97e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -39.7 | 10.7 | 4.9 | -205.7 | 4.6 | -21.3 |
| 9388 | ok | 0.09 | 8.68e-02 | 1.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.7 | 2.0 | -13.5 | -98.2 | -10.1 | -0.5 |
| 9389 | ok | 0.09 | 9.05e-02 | 7.53e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.4 | 28.8 | 0.2 | -163.2 | 39.5 | -50.4 |
| 9390 | ok | 0.09 | 6.70e-02 | 7.97e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -35.9 | 14.1 | -15.2 | -87.8 | 1.6 | -2.3 |
| 9391 | ok | 0.09 | 5.78e-02 | 8.62e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -37.6 | 9.6 | 4.8 | -202.6 | 5.2 | -34.4 |
| 9392 | ok | 0.09 | 9.72e-02 | 1.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.4 | 1.8 | -16.0 | -93.8 | -10.4 | -3.6 |
| 9393 | ok | 0.09 | 9.12e-02 | 6.37e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.4 | 18.3 | -17.8 | -73.4 | 3.7 | -6.5 |
| 9394 | ok | 0.09 | 6.69e-02 | 7.11e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.0 | 13.6 | -17.6 | -82.5 | 0.7 | -5.3 |
| 9395 | ok | 0.09 | 5.91e-02 | 8.21e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -33.2 | 8.3 | -17.4 | -92.3 | -8.0 | -4.7 |
| 9396 | ok | 0.09 | 9.76e-02 | 1.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.8 | 2.5 | -16.6 | -90.7 | -11.0 | -6.2 |
| 9397 | ok | 0.09 | 9.05e-02 | 5.39e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.5 | 18.4 | -18.6 | -68.3 | 2.5 | -8.2 |
| 9398 | ok | 0.09 | 6.52e-02 | 6.25e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.3 | 13.1 | -16.3 | -78.5 | -8.7 | -7.4 |
| 9399 | ok | 0.09 | 5.92e-02 | 7.51e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -32.3 | 6.8 | 8.2 | -192.7 | 5.4 | -55.6 |
| 9400 | ok | 0.09 | 9.91e-02 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.6 | 2.0 | -16.3 | -87.5 | -11.2 | -8.5 |
| 9401 | ok | 0.09 | 8.48e-02 | 4.50e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -22.2 | 18.6 | -14.4 | -63.2 | 2.8 | -8.7 |
| 9402 | ok | 0.09 | 7.58e-02 | 5.59e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -22.8 | 12.7 | -15.5 | -75.0 | -8.7 | -9.0 |
| 9403 | ok | 0.09 | 6.16e-02 | 7.77e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.3 | 5.4 | 11.2 | -189.7 | 6.3 | -63.8 |
| 9404 | ok | 0.09 | 0.1 | 1.58e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.6 | 10.6 | -15.2 | -16.5 | -11.8 | -17.2 |
| 9405 | ok | 0.09 | 9.48e-02 | 4.14e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -13.2 | 24.8 | 5.2 | -132.3 | 22.5 | -86.7 |
| 9406 | ok | 0.09 | 8.15e-02 | 5.94e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -20.0 | 14.4 | 6.7 | -161.5 | 10.8 | -85.0 |
| 9407 | ok | 0.09 | 6.86e-02 | 8.29e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.0 | 5.7 | 8.7 | -187.4 | -1.2 | -81.1 |
| 9408 | ok | 0.09 | 0.1 | 1.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.0 | 12.7 | -12.7 | -16.5 | -12.0 | -17.2 |
| 9409 | ok | 0.09 | 9.68e-02 | 4.73e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -13.4 | 23.1 | 10.8 | -130.0 | 23.4 | -89.4 |
| 9410 | ok | 0.09 | 8.54e-02 | 6.65e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -20.3 | 13.0 | 10.1 | -159.0 | 12.2 | -91.1 |
| 9411 | ok | 0.09 | 7.27e-02 | 9.07e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -27.2 | 5.7 | 13.5 | -185.6 | -6.3 | -91.8 |
| 9412 | ok | 0.09 | 0.1 | 1.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.2 | 14.7 | -10.6 | -16.6 | -12.2 | -17.3 |
| 9413 | ok | 0.09 | 9.65e-02 | 5.67e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.0 | 20.7 | 11.3 | -132.3 | 28.2 | -92.5 |
| 9414 | ok | 0.09 | 8.31e-02 | 7.63e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.9 | 11.5 | 13.5 | -158.7 | 15.3 | -97.8 |
| 9415 | ok | 0.09 | 7.57e-02 | 1.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -26.1 | -1.4 | 24.2 | -28.0 | -2.7 | -46.3 |
| 9416 | ok | 0.09 | 0.1 | 1.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.8 | 17.2 | -10.0 | -17.9 | -14.9 | -20.0 |
| 9417 | ok | 0.09 | 9.44e-02 | 7.00e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -18.5 | 17.9 | 14.5 | -138.3 | 35.7 | -98.6 |
| 9418 | ok | 0.09 | 8.38e-02 | 8.82e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.1 | 10.1 | 16.6 | -159.9 | 20.0 | -106.1 |
| 9419 | ok | 0.09 | 7.72e-02 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -28.3 | -5.6 | 33.7 | -25.9 | -0.5 | -45.6 |
| 9420 | ok | 0.09 | 0.1 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.1 | 18.4 | -9.5 | -18.3 | -15.3 | -20.4 |
| 9421 | ok | 0.09 | 8.95e-02 | 8.60e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.1 | 15.4 | 19.7 | -145.5 | 44.0 | -108.8 |
| 9422 | ok | 0.09 | 8.22e-02 | 1.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -29.3 | 9.1 | 21.6 | -161.9 | 24.3 | -116.7 |
| 9423 | ok | 0.09 | 7.67e-02 | 1.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.0 | -4.6 | 27.6 | -21.4 | 1.3 | -46.9 |
| 9424 | ok | 0.09 | 0.1 | 2.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.2 | 19.2 | -8.4 | -18.5 | -16.1 | -20.8 |
| 9425 | ok | 0.09 | 8.01e-02 | 1.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.5 | -10.5 | 20.9 | 51.7 | 1.4 | 10.5 |
| 9426 | ok | 0.09 | 7.71e-02 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.7 | -4.4 | 24.5 | -20.1 | 9.7 | -47.5 |
| 9427 | ok | 0.09 | 7.35e-02 | 1.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.3 | -5.4 | 26.0 | -20.1 | 5.9 | -47.1 |
| 9428 | ok | 0.09 | 0.1 | 2.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.0 | 19.8 | -9.2 | -18.9 | -16.9 | -21.4 |
| 9429 | ok | 0.09 | 7.19e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.3 | -13.6 | 17.2 | 53.1 | 1.3 | 15.0 |
| 9430 | ok | 0.09 | 6.90e-02 | 1.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.1 | -6.4 | 21.7 | -19.2 | 11.1 | -47.9 |
| 9431 | ok | 0.09 | 6.83e-02 | 1.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.9 | -6.6 | 23.7 | -19.0 | 6.2 | -47.6 |
| 9432 | ok | 0.09 | 0.1 | 2.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.4 | 19.6 | -10.6 | -19.5 | -17.8 | -22.3 |
| 9433 | ok | 0.09 | 6.49e-02 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.4 | -16.9 | 14.1 | 53.7 | 1.0 | 19.8 |
| 9434 | ok | 0.09 | 6.41e-02 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.8 | -8.7 | 24.0 | -18.3 | 11.4 | -48.5 |
| 9435 | ok | 0.09 | 7.07e-02 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.1 | -6.0 | 24.7 | -18.1 | 5.5 | -48.4 |
| 9436 | ok | 0.09 | 0.1 | 2.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.3 | 18.7 | -11.5 | -20.2 | -18.9 | -23.3 |
| 9437 | ok | 0.09 | 6.43e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.7 | -15.8 | 14.5 | -15.5 | 21.4 | -49.9 |
| 9438 | ok | 0.09 | 6.67e-02 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.5 | -11.7 | 17.1 | -15.1 | 13.3 | -50.4 |
| 9439 | ok | 0.09 | 7.30e-02 | 1.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.6 | -1.1 | 18.0 | -17.6 | -2.4 | -14.5 |
| 9440 | ok | 0.09 | 0.1 | 2.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.9 | 17.6 | -12.0 | -20.9 | -20.2 | -24.3 |
| 9441 | ok | 0.09 | 6.71e-02 | 1.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.3 | -18.1 | 17.0 | -15.1 | 21.3 | -51.5 |
| 9442 | ok | 0.09 | 6.91e-02 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.9 | -7.4 | 18.7 | -18.3 | 1.2 | -14.3 |
| 9443 | ok | 0.09 | 7.49e-02 | 1.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.8 | -3.2 | 17.9 | -18.2 | -2.6 | -15.5 |
| 9444 | ok | 0.09 | 0.1 | 2.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.3 | 17.8 | -13.2 | -182.1 | -213.7 | -277.3 |
| 9445 | ok | 0.09 | 6.96e-02 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -28.5 | -19.5 | 15.2 | -55.9 | 19.6 | -40.1 |
| 9446 | ok | 0.09 | 7.12e-02 | 1.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.6 | -12.1 | 23.2 | -18.4 | 1.5 | -15.4 |
| 9447 | ok | 0.09 | 7.66e-02 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.9 | -5.3 | 18.5 | -18.7 | -3.1 | -16.4 |
| 9448 | ok | 0.09 | 0.1 | 2.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.2 | 17.7 | -13.0 | -167.6 | -222.7 | -276.0 |
| 9449 | ok | 0.09 | 7.21e-02 | 1.10e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.9 | -19.3 | 16.3 | -17.3 | 3.6 | -14.7 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|---------|--------|---------|---------|----------|---------|
| 9450 | ok | 0.09 | 7.32e-02 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.9 | -14.4 | 21.1 | -18.4 | 0.3 | -16.5 |
| 9451 | ok | 0.09 | 7.79e-02 | 1.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.0 | -7.1 | 19.5 | -19.2 | -4.0 | -17.2 |
| 9452 | ok | 0.09 | 0.1 | 2.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.9 | 18.2 | -12.5 | -150.9 | -230.3 | -270.5 |
| 9453 | ok | 0.09 | 7.46e-02 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.8 | -21.9 | 20.9 | -17.8 | -0.3 | -18.0 |
| 9454 | ok | 0.09 | 7.50e-02 | 1.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.9 | -17.4 | 22.3 | -18.1 | -1.8 | -16.9 |
| 9455 | ok | 0.09 | 7.87e-02 | 1.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.2 | -8.6 | 21.0 | -19.7 | -5.3 | -17.5 |
| 9456 | ok | 0.09 | 0.1 | 2.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.1 | 19.6 | -11.4 | -132.4 | -236.3 | -259.7 |
| 9457 | ok | 0.09 | 7.73e-02 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.8 | -27.6 | 19.5 | -15.9 | -2.6 | -19.1 |
| 9458 | ok | 0.09 | 7.68e-02 | 1.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.9 | -20.9 | 24.1 | -17.0 | -4.1 | -17.1 |
| 9459 | ok | 0.09 | 7.91e-02 | 1.58e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.4 | -9.7 | 23.0 | -20.2 | -7.4 | -17.2 |
| 9460 | ok | 0.09 | 0.1 | 2.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.7 | 22.0 | -9.1 | -112.7 | -240.8 | -241.8 |
| 9461 | ok | 0.09 | 8.04e-02 | 1.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.2 | -34.1 | 20.7 | -13.0 | -4.6 | -20.5 |
| 9462 | ok | 0.09 | 7.85e-02 | 1.44e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.9 | -24.8 | 25.9 | -14.6 | -6.9 | -17.1 |
| 9463 | ok | 0.09 | 7.89e-02 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.9 | -8.7 | 24.8 | -99.2 | -53.6 | -233.2 |
| 9464 | ok | 0.09 | 0.1 | 2.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.4 | 25.1 | -5.0 | -90.2 | -245.1 | -213.6 |
| 9465 | ok | 0.09 | 8.45e-02 | 1.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.1 | -41.4 | 21.2 | -8.7 | -4.6 | -23.1 |
| 9466 | ok | 0.09 | 8.08e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.8 | -29.2 | 27.1 | -10.0 | -9.9 | -18.1 |
| 9467 | ok | 0.09 | 7.82e-02 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.2 | -9.8 | 26.4 | -87.7 | -81.2 | -223.5 |
| 9468 | ok | 0.09 | 0.1 | 2.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.5 | 26.9 | -3.8 | -59.9 | -251.9 | -160.0 |
| 9469 | ok | 0.09 | 9.02e-02 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.8 | -49.3 | 23.5 | -3.4 | 1.3 | -28.6 |
| 9470 | ok | 0.09 | 8.44e-02 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.9 | -34.6 | 27.4 | -2.2 | -9.6 | -23.9 |
| 9471 | ok | 0.09 | 7.85e-02 | 1.65e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.8 | -12.8 | 26.5 | -78.3 | -124.8 | -205.3 |
| 9472 | ok | 0.09 | 0.1 | 2.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -28.4 | -3.5 | 10.5 | -99.9 | -351.2 | -97.0 |
| 9473 | ok | 0.09 | 9.95e-02 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.2 | -58.0 | 19.5 | 3.5 | 17.6 | -39.7 |
| 9474 | ok | 0.09 | 9.10e-02 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.5 | -38.6 | 23.8 | 10.1 | -0.4 | -35.2 |
| 9475 | ok | 0.09 | 8.20e-02 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.9 | -18.2 | 23.8 | -64.8 | -191.1 | -181.9 |
| 9476 | ok | 0.09 | 8.30e-02 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -28.3 | -2.2 | 17.4 | -129.3 | -208.0 | -116.0 |
| 9477 | ok | 0.09 | 0.1 | 1.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.4 | -67.6 | 22.3 | -4.0 | 61.2 | -60.9 |
| 9478 | ok | 0.09 | 9.95e-02 | 1.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.4 | -40.6 | 17.6 | 28.9 | 28.5 | -49.8 |
| 9479 | ok | 0.09 | 8.26e-02 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.1 | -22.2 | 15.9 | -54.1 | -217.0 | -151.5 |
| 9480 | ok | 0.09 | 7.61e-02 | 1.73e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.6 | -10.0 | -33.2 | -139.9 | -284.2 | 111.2 |
| 9481 | ok | 0.09 | 0.1 | 2.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.2 | -37.2 | -31.2 | -81.8 | -745.9 | 184.0 |
| 9482 | ok | 0.09 | 0.1 | 1.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.3 | -25.0 | -32.1 | -111.8 | -587.2 | 160.8 |
| 9483 | ok | 0.09 | 8.24e-02 | 1.76e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.8 | -16.8 | -34.1 | -108.4 | -419.2 | 137.5 |
| 9484 | ok | 0.09 | 6.93e-02 | 2.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.6 | -23.0 | -49.7 | -135.5 | -123.7 | 213.6 |
| 9485 | ok | 0.09 | 8.70e-02 | 1.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.4 | -28.5 | -32.5 | -28.8 | -336.4 | 278.3 |
| 9486 | ok | 0.09 | 7.53e-02 | 2.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.9 | -19.5 | -40.7 | -75.2 | -250.6 | 257.1 |
| 9487 | ok | 0.09 | 7.26e-02 | 2.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.9 | -15.8 | -41.9 | -91.7 | -184.2 | 223.4 |
| 9488 | ok | 0.09 | 6.03e-02 | 3.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -98.8 | -33.4 | -68.6 | -114.7 | 46.9 | 229.5 |
| 9489 | ok | 0.09 | 8.35e-02 | 1.93e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -82.3 | -9.9 | -30.7 | -19.8 | 126.0 | 292.1 |
| 9490 | ok | 0.09 | 7.20e-02 | 2.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -74.5 | -11.7 | -41.5 | -63.6 | 102.9 | 284.4 |
| 9491 | ok | 0.09 | 6.47e-02 | 2.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.1 | -10.4 | -47.8 | -73.8 | 86.2 | 240.3 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | 0.09 | 0.33 | 0.05 | 4.52 | 4.52 | 4.00 | 4.00 | -174.13 | -87.71 | -132.67 | -720.05 | -1455.33 | -469.87 |
| | | 0.09 | 0.33 | 0.05 | 4.52 | 4.52 | 4.00 | 4.00 | 8.42 | 57.09 | 116.24 | 241.34 | 424.61 | 410.13 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 5 | ok | 0.83 | | | | | | |
| 6 | ok | 0.91 | | | | | | |
| 17 | ok | 0.24 | | | | | | |
| 18 | ok | 0.21 | | | | | | |
| 19 | ok | 0.27 | | | | | | |
| 20 | ok | 0.28 | | | | | | |
| 21 | ok | 0.83 | | | | | | |
| 1807 | ok | 0.83 | | | | | | |
| 1809 | ok | 0.91 | | | | | | |
| 1811 | ok | 0.71 | | | | | | |
| 1996 | ok | 0.27 | | | | | | |
| 2000 | ok | 0.27 | | | | | | |
| 2004 | ok | 0.27 | | | | | | |
| 2008 | ok | 0.27 | | | | | | |
| 2012 | ok | 0.28 | | | | | | |
| 2016 | ok | 0.28 | | | | | | |
| 2020 | ok | 0.28 | | | | | | |
| 2024 | ok | 0.22 | | | | | | |
| 2028 | ok | 0.22 | | | | | | |
| 2032 | ok | 0.22 | | | | | | |
| 2036 | ok | 0.22 | | | | | | |
| 2040 | ok | 0.22 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 2044 | ok | 0.21 | | | | | | |
| 2048 | ok | 0.22 | | | | | | |
| 2126 | ok | 0.83 | | | | | | |
| 2141 | ok | 0.66 | | | | | | |
| 2156 | ok | 0.53 | | | | | | |
| 2171 | ok | 0.46 | | | | | | |
| 2186 | ok | 0.41 | | | | | | |
| 2201 | ok | 0.36 | | | | | | |
| 2216 | ok | 0.32 | | | | | | |
| 2231 | ok | 0.30 | | | | | | |
| 2246 | ok | 0.25 | | | | | | |
| 2261 | ok | 0.22 | | | | | | |
| 2276 | ok | 0.19 | | | | | | |
| 2291 | ok | 0.15 | | | | | | |
| 2306 | ok | 0.11 | | | | | | |
| 2321 | ok | 0.10 | | | | | | |
| 2336 | ok | 0.13 | | | | | | |
| 2351 | ok | 0.16 | | | | | | |
| 2366 | ok | 0.19 | | | | | | |
| 2407 | ok | 0.26 | | | | | | |
| 2422 | ok | 0.29 | | | | | | |
| 2437 | ok | 0.32 | | | | | | |
| 2452 | ok | 0.36 | | | | | | |
| 2467 | ok | 0.39 | | | | | | |
| 2482 | ok | 0.42 | | | | | | |
| 2497 | ok | 0.44 | | | | | | |
| 2512 | ok | 0.46 | | | | | | |
| 2527 | ok | 0.47 | | | | | | |
| 2542 | ok | 0.47 | | | | | | |
| 2557 | ok | 0.48 | | | | | | |
| 2572 | ok | 0.52 | | | | | | |
| 2587 | ok | 0.66 | | | | | | |
| 7307 | ok | 0.36 | | | | | | |
| 7308 | ok | 0.42 | | | | | | |
| 7319 | ok | 0.21 | | | | | | |
| 7320 | ok | 0.11 | | | | | | |
| 7321 | ok | 0.16 | | | | | | |
| 7322 | ok | 0.24 | | | | | | |
| 7323 | ok | 0.29 | | | | | | |
| 7416 | ok | 0.36 | | | | | | |
| 7417 | ok | 0.26 | | | | | | |
| 7418 | ok | 0.15 | | | | | | |
| 7420 | ok | 0.23 | | | | | | |
| 7421 | ok | 0.22 | | | | | | |
| 7422 | ok | 0.22 | | | | | | |
| 7423 | ok | 0.21 | | | | | | |
| 7424 | ok | 0.20 | | | | | | |
| 7425 | ok | 0.18 | | | | | | |
| 7426 | ok | 0.17 | | | | | | |
| 7427 | ok | 0.13 | | | | | | |
| 7428 | ok | 0.14 | | | | | | |
| 7429 | ok | 0.15 | | | | | | |
| 7430 | ok | 0.17 | | | | | | |
| 7431 | ok | 0.18 | | | | | | |
| 7432 | ok | 0.19 | | | | | | |
| 7433 | ok | 0.20 | | | | | | |
| 7434 | ok | 0.29 | | | | | | |
| 7435 | ok | 0.24 | | | | | | |
| 7436 | ok | 0.25 | | | | | | |
| 7437 | ok | 0.25 | | | | | | |
| 7438 | ok | 0.25 | | | | | | |
| 7439 | ok | 0.25 | | | | | | |
| 7440 | ok | 0.25 | | | | | | |
| 7441 | ok | 0.25 | | | | | | |
| 7442 | ok | 0.14 | | | | | | |
| 7443 | ok | 0.13 | | | | | | |
| 7444 | ok | 0.11 | | | | | | |
| 7445 | ok | 0.09 | | | | | | |
| 7446 | ok | 0.07 | | | | | | |
| 7447 | ok | 0.06 | | | | | | |
| 7448 | ok | 0.06 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 7449 | ok | 0.08 | | | | | | |
| 7450 | ok | 0.09 | | | | | | |
| 7451 | ok | 0.23 | | | | | | |
| 7452 | ok | 0.24 | | | | | | |
| 7453 | ok | 0.25 | | | | | | |
| 7454 | ok | 0.26 | | | | | | |
| 7455 | ok | 0.28 | | | | | | |
| 7456 | ok | 0.28 | | | | | | |
| 7457 | ok | 0.29 | | | | | | |
| 7458 | ok | 0.29 | | | | | | |
| 7459 | ok | 0.29 | | | | | | |
| 7460 | ok | 0.28 | | | | | | |
| 7461 | ok | 0.28 | | | | | | |
| 7462 | ok | 0.28 | | | | | | |
| 7463 | ok | 0.42 | | | | | | |
| 8762 | ok | 0.83 | | | | | | |
| 8763 | ok | 0.45 | | | | | | |
| 8764 | ok | 0.35 | | | | | | |
| 8765 | ok | 0.32 | | | | | | |
| 9046 | ok | 0.91 | | | | | | |
| 9047 | ok | 0.58 | | | | | | |
| 9048 | ok | 0.39 | | | | | | |
| 9049 | ok | 0.33 | | | | | | |
| 9284 | ok | 0.83 | | | | | | |
| 9285 | ok | 0.52 | | | | | | |
| 9286 | ok | 0.43 | | | | | | |
| 9287 | ok | 0.37 | | | | | | |
| 9288 | ok | 0.32 | | | | | | |
| 9289 | ok | 0.83 | | | | | | |
| 9290 | ok | 0.45 | | | | | | |
| 9291 | ok | 0.35 | | | | | | |
| 9292 | ok | 0.24 | | | | | | |
| 9293 | ok | 0.66 | | | | | | |
| 9294 | ok | 0.35 | | | | | | |
| 9295 | ok | 0.27 | | | | | | |
| 9296 | ok | 0.18 | | | | | | |
| 9297 | ok | 0.53 | | | | | | |
| 9298 | ok | 0.25 | | | | | | |
| 9299 | ok | 0.19 | | | | | | |
| 9300 | ok | 0.12 | | | | | | |
| 9301 | ok | 0.46 | | | | | | |
| 9302 | ok | 0.18 | | | | | | |
| 9303 | ok | 0.13 | | | | | | |
| 9304 | ok | 0.08 | | | | | | |
| 9305 | ok | 0.41 | | | | | | |
| 9306 | ok | 0.13 | | | | | | |
| 9307 | ok | 0.08 | | | | | | |
| 9308 | ok | 0.06 | | | | | | |
| 9309 | ok | 0.36 | | | | | | |
| 9310 | ok | 0.10 | | | | | | |
| 9311 | ok | 0.05 | | | | | | |
| 9312 | ok | 0.04 | | | | | | |
| 9313 | ok | 0.32 | | | | | | |
| 9314 | ok | 0.08 | | | | | | |
| 9315 | ok | 0.04 | | | | | | |
| 9316 | ok | 0.05 | | | | | | |
| 9317 | ok | 0.28 | | | | | | |
| 9318 | ok | 0.06 | | | | | | |
| 9319 | ok | 0.05 | | | | | | |
| 9320 | ok | 0.05 | | | | | | |
| 9321 | ok | 0.24 | | | | | | |
| 9322 | ok | 0.06 | | | | | | |
| 9323 | ok | 0.05 | | | | | | |
| 9324 | ok | 0.05 | | | | | | |
| 9325 | ok | 0.21 | | | | | | |
| 9326 | ok | 0.06 | | | | | | |
| 9327 | ok | 0.05 | | | | | | |
| 9328 | ok | 0.06 | | | | | | |
| 9329 | ok | 0.19 | | | | | | |
| 9330 | ok | 0.06 | | | | | | |
| 9331 | ok | 0.06 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 9332 | ok | 0.06 | | | | | | |
| 9333 | ok | 0.18 | | | | | | |
| 9334 | ok | 0.06 | | | | | | |
| 9335 | ok | 0.06 | | | | | | |
| 9336 | ok | 0.06 | | | | | | |
| 9337 | ok | 0.17 | | | | | | |
| 9338 | ok | 0.06 | | | | | | |
| 9339 | ok | 0.06 | | | | | | |
| 9340 | ok | 0.06 | | | | | | |
| 9341 | ok | 0.17 | | | | | | |
| 9342 | ok | 0.07 | | | | | | |
| 9343 | ok | 0.06 | | | | | | |
| 9344 | ok | 0.06 | | | | | | |
| 9345 | ok | 0.17 | | | | | | |
| 9346 | ok | 0.07 | | | | | | |
| 9347 | ok | 0.06 | | | | | | |
| 9348 | ok | 0.06 | | | | | | |
| 9349 | ok | 0.16 | | | | | | |
| 9350 | ok | 0.07 | | | | | | |
| 9351 | ok | 0.06 | | | | | | |
| 9352 | ok | 0.06 | | | | | | |
| 9353 | ok | 0.15 | | | | | | |
| 9354 | ok | 0.06 | | | | | | |
| 9355 | ok | 0.06 | | | | | | |
| 9356 | ok | 0.06 | | | | | | |
| 9357 | ok | 0.14 | | | | | | |
| 9358 | ok | 0.07 | | | | | | |
| 9359 | ok | 0.06 | | | | | | |
| 9360 | ok | 0.07 | | | | | | |
| 9361 | ok | 0.12 | | | | | | |
| 9362 | ok | 0.07 | | | | | | |
| 9363 | ok | 0.07 | | | | | | |
| 9364 | ok | 0.07 | | | | | | |
| 9365 | ok | 0.10 | | | | | | |
| 9366 | ok | 0.07 | | | | | | |
| 9367 | ok | 0.07 | | | | | | |
| 9368 | ok | 0.07 | | | | | | |
| 9369 | ok | 0.09 | | | | | | |
| 9370 | ok | 0.07 | | | | | | |
| 9371 | ok | 0.07 | | | | | | |
| 9372 | ok | 0.07 | | | | | | |
| 9373 | ok | 0.08 | | | | | | |
| 9374 | ok | 0.07 | | | | | | |
| 9375 | ok | 0.07 | | | | | | |
| 9376 | ok | 0.07 | | | | | | |
| 9377 | ok | 0.08 | | | | | | |
| 9378 | ok | 0.07 | | | | | | |
| 9379 | ok | 0.07 | | | | | | |
| 9380 | ok | 0.07 | | | | | | |
| 9381 | ok | 0.08 | | | | | | |
| 9382 | ok | 0.07 | | | | | | |
| 9383 | ok | 0.07 | | | | | | |
| 9384 | ok | 0.07 | | | | | | |
| 9385 | ok | 0.09 | | | | | | |
| 9386 | ok | 0.07 | | | | | | |
| 9387 | ok | 0.07 | | | | | | |
| 9388 | ok | 0.06 | | | | | | |
| 9389 | ok | 0.11 | | | | | | |
| 9390 | ok | 0.07 | | | | | | |
| 9391 | ok | 0.07 | | | | | | |
| 9392 | ok | 0.07 | | | | | | |
| 9393 | ok | 0.12 | | | | | | |
| 9394 | ok | 0.07 | | | | | | |
| 9395 | ok | 0.07 | | | | | | |
| 9396 | ok | 0.07 | | | | | | |
| 9397 | ok | 0.12 | | | | | | |
| 9398 | ok | 0.07 | | | | | | |
| 9399 | ok | 0.07 | | | | | | |
| 9400 | ok | 0.07 | | | | | | |
| 9401 | ok | 0.13 | | | | | | |
| 9402 | ok | 0.07 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 9403 | ok | 0.07 | | | | | | |
| 9404 | ok | 0.07 | | | | | | |
| 9405 | ok | 0.13 | | | | | | |
| 9406 | ok | 0.07 | | | | | | |
| 9407 | ok | 0.07 | | | | | | |
| 9408 | ok | 0.06 | | | | | | |
| 9409 | ok | 0.13 | | | | | | |
| 9410 | ok | 0.07 | | | | | | |
| 9411 | ok | 0.07 | | | | | | |
| 9412 | ok | 0.06 | | | | | | |
| 9413 | ok | 0.13 | | | | | | |
| 9414 | ok | 0.07 | | | | | | |
| 9415 | ok | 0.06 | | | | | | |
| 9416 | ok | 0.06 | | | | | | |
| 9417 | ok | 0.14 | | | | | | |
| 9418 | ok | 0.06 | | | | | | |
| 9419 | ok | 0.06 | | | | | | |
| 9420 | ok | 0.06 | | | | | | |
| 9421 | ok | 0.16 | | | | | | |
| 9422 | ok | 0.06 | | | | | | |
| 9423 | ok | 0.06 | | | | | | |
| 9424 | ok | 0.06 | | | | | | |
| 9425 | ok | 0.18 | | | | | | |
| 9426 | ok | 0.06 | | | | | | |
| 9427 | ok | 0.06 | | | | | | |
| 9428 | ok | 0.06 | | | | | | |
| 9429 | ok | 0.20 | | | | | | |
| 9430 | ok | 0.06 | | | | | | |
| 9431 | ok | 0.06 | | | | | | |
| 9432 | ok | 0.05 | | | | | | |
| 9433 | ok | 0.23 | | | | | | |
| 9434 | ok | 0.06 | | | | | | |
| 9435 | ok | 0.05 | | | | | | |
| 9436 | ok | 0.05 | | | | | | |
| 9437 | ok | 0.26 | | | | | | |
| 9438 | ok | 0.06 | | | | | | |
| 9439 | ok | 0.05 | | | | | | |
| 9440 | ok | 0.05 | | | | | | |
| 9441 | ok | 0.29 | | | | | | |
| 9442 | ok | 0.06 | | | | | | |
| 9443 | ok | 0.05 | | | | | | |
| 9444 | ok | 0.04 | | | | | | |
| 9445 | ok | 0.32 | | | | | | |
| 9446 | ok | 0.06 | | | | | | |
| 9447 | ok | 0.04 | | | | | | |
| 9448 | ok | 0.04 | | | | | | |
| 9449 | ok | 0.34 | | | | | | |
| 9450 | ok | 0.06 | | | | | | |
| 9451 | ok | 0.04 | | | | | | |
| 9452 | ok | 0.03 | | | | | | |
| 9453 | ok | 0.37 | | | | | | |
| 9454 | ok | 0.07 | | | | | | |
| 9455 | ok | 0.03 | | | | | | |
| 9456 | ok | 0.05 | | | | | | |
| 9457 | ok | 0.40 | | | | | | |
| 9458 | ok | 0.08 | | | | | | |
| 9459 | ok | 0.02 | | | | | | |
| 9460 | ok | 0.07 | | | | | | |
| 9461 | ok | 0.42 | | | | | | |
| 9462 | ok | 0.10 | | | | | | |
| 9463 | ok | 0.05 | | | | | | |
| 9464 | ok | 0.11 | | | | | | |
| 9465 | ok | 0.45 | | | | | | |
| 9466 | ok | 0.13 | | | | | | |
| 9467 | ok | 0.09 | | | | | | |
| 9468 | ok | 0.20 | | | | | | |
| 9469 | ok | 0.48 | | | | | | |
| 9470 | ok | 0.18 | | | | | | |
| 9471 | ok | 0.17 | | | | | | |
| 9472 | ok | 0.28 | | | | | | |
| 9473 | ok | 0.52 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 9474 | ok | 0.24 | | | | | | |
| 9475 | ok | 0.24 | | | | | | |
| 9476 | ok | 0.33 | | | | | | |
| 9477 | ok | 0.66 | | | | | | |
| 9478 | ok | 0.32 | | | | | | |
| 9479 | ok | 0.26 | | | | | | |
| 9480 | ok | 0.26 | | | | | | |
| 9481 | ok | 0.91 | | | | | | |
| 9482 | ok | 0.58 | | | | | | |
| 9483 | ok | 0.39 | | | | | | |
| 9484 | ok | 0.24 | | | | | | |
| 9485 | ok | 0.71 | | | | | | |
| 9486 | ok | 0.47 | | | | | | |
| 9487 | ok | 0.34 | | | | | | |
| 9488 | ok | 0.37 | | | | | | |
| 9489 | ok | 0.83 | | | | | | |
| 9490 | ok | 0.52 | | | | | | |
| 9491 | ok | 0.43 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 0.91 | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 74 | 40.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|--------|--------|--------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 40 | ok | 0.09 | 0.3 | 9.33e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.7 | 83.4 | -37.3 | 23.7 | 119.2 | 23.0 |
| 43 | ok | 0.09 | 0.4 | 6.13e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -9.8 | 117.3 | 17.5 | 0.5 | -76.0 | -17.3 |
| 5886 | ok | 0.09 | 0.2 | 7.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -237.5 | -228.6 | 62.0 | 201.3 | -40.9 | -109.9 |
| 5887 | ok | 0.09 | 0.6 | 2.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | 44.0 | 149.1 | 11.3 | 178.1 | -125.0 | 14.9 |
| 5888 | ok | 0.09 | 0.1 | 5.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -182.5 | -41.9 | 98.2 | 227.1 | 58.9 | -132.2 |
| 5894 | ok | 0.09 | 0.2 | 4.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -168.0 | 11.1 | 93.2 | 229.9 | 54.0 | -134.8 |
| 6002 | ok | 0.09 | 0.4 | 1.99e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -70.9 | -88.4 | -3.9 | -264.9 | 115.6 | 21.2 |
| 6004 | ok | 0.09 | 0.3 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -74.8 | -90.3 | -4.8 | -239.6 | 120.5 | 20.0 |
| 6005 | ok | 0.09 | 0.3 | 1.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.6 | -57.4 | -4.2 | -216.6 | 6.2 | 72.6 |
| 6006 | ok | 0.09 | 0.2 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -29.9 | 42.6 | 19.8 | 220.5 | -13.8 | -101.0 |
| 6007 | ok | 0.09 | 0.2 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.6 | 30.3 | 21.0 | 190.6 | -5.7 | -115.2 |
| 6008 | ok | 0.09 | 0.1 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.9 | 28.7 | 18.7 | 156.4 | -3.8 | -117.6 |
| 6009 | ok | 0.09 | 9.03e-02 | 1.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.6 | -10.4 | 14.3 | 16.8 | 24.7 | -13.0 |
| 6010 | ok | 0.09 | 6.81e-02 | 1.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.1 | -9.1 | 14.4 | 147.0 | 77.2 | -98.0 |
| 6011 | ok | 0.09 | 6.73e-02 | 1.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.2 | -9.4 | 21.1 | 5.1 | 39.3 | -12.1 |
| 6012 | ok | 0.09 | 9.25e-02 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.8 | -22.7 | 18.6 | -7.5 | 61.6 | -13.9 |
| 6013 | ok | 0.09 | 0.2 | 2.83e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.2 | -17.0 | 78.4 | -24.5 | 117.1 | 18.5 |
| 6014 | ok | 0.09 | 0.1 | 4.69e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -199.4 | -207.5 | 9.6 | 346.0 | -66.3 | -8.6 |
| 6015 | ok | 0.09 | 0.1 | 3.93e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -154.3 | -161.3 | 21.3 | 284.3 | -105.0 | 2.3 |
| 6017 | ok | 0.09 | 0.1 | 3.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -135.9 | -146.1 | 14.0 | 250.7 | -106.5 | 12.5 |
| 6019 | ok | 0.09 | 0.1 | 3.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -121.9 | -135.5 | 7.7 | 223.2 | -98.7 | 19.5 |
| 6021 | ok | 0.09 | 1.00e-01 | 2.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -109.7 | -126.5 | 2.6 | 199.1 | -88.3 | 24.6 |
| 6023 | ok | 0.09 | 9.35e-02 | 2.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -98.8 | -117.8 | -1.5 | 177.7 | -77.3 | 28.5 |
| 6025 | ok | 0.09 | 8.79e-02 | 2.47e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -89.1 | -109.1 | -4.8 | 158.4 | -66.5 | 31.6 |
| 6027 | ok | 0.09 | 8.27e-02 | 2.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.6 | -100.3 | -11.1 | 140.9 | -56.0 | 34.0 |
| 6029 | ok | 0.09 | 7.82e-02 | 2.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -73.2 | -91.3 | -13.2 | 125.1 | -45.7 | 35.9 |
| 6031 | ok | 0.09 | 7.42e-02 | 2.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.8 | -82.2 | -14.8 | 110.6 | -35.1 | 37.4 |
| 6033 | ok | 0.09 | 7.06e-02 | 1.85e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.3 | -73.2 | -16.0 | 97.5 | -23.6 | 38.5 |
| 6035 | ok | 0.09 | 6.72e-02 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.8 | -64.3 | -16.8 | 85.5 | -10.3 | 39.1 |
| 6037 | ok | 0.09 | 6.44e-02 | 1.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.9 | -55.6 | -13.7 | 74.7 | 6.4 | 39.3 |
| 6039 | ok | 0.09 | 6.22e-02 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.9 | -47.2 | -14.1 | 64.9 | 28.2 | 39.0 |
| 6041 | ok | 0.09 | 6.09e-02 | 1.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.4 | -39.3 | -14.2 | 56.0 | 58.1 | 38.0 |
| 6043 | ok | 0.09 | 6.12e-02 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.6 | -31.9 | -14.1 | 47.8 | 99.8 | 36.3 |
| 6045 | ok | 0.09 | 6.60e-02 | 1.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.2 | -25.5 | -14.0 | 40.2 | 159.3 | 33.5 |
| 6047 | ok | 0.09 | 8.14e-02 | 1.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.7 | -20.6 | -13.7 | 32.4 | 245.2 | 29.5 |
| 6049 | ok | 0.09 | 0.1 | 1.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.4 | 13.1 | -15.4 | -5.1 | -70.6 | 35.4 |
| 6051 | ok | 0.09 | 0.2 | 1.94e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.0 | 22.0 | -6.3 | -37.1 | -110.1 | 27.0 |
| 7341 | ok | 0.09 | 0.1 | 3.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.3 | -40.1 | 92.5 | 24.5 | 32.9 | -11.6 |
| 7342 | ok | 0.09 | 0.1 | 3.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.5 | -54.9 | -98.8 | -72.6 | -29.8 | -103.6 |
| 7599 | ok | 0.09 | 0.2 | 5.43e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -90.9 | -87.0 | 158.9 | 134.7 | 35.7 | -173.7 |
| 7600 | ok | 0.09 | 0.2 | 2.45e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.0 | 32.5 | 25.9 | 35.2 | 51.3 | -61.4 |
| 7601 | ok | 0.09 | 0.2 | 3.22e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.9 | -62.3 | 89.6 | 65.0 | 86.0 | -113.7 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-------|-------|--------|--------|--------|--------|
| 7602 | ok | 0.09 | 0.2 | 1.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.7 | -15.8 | 52.1 | 43.4 | 62.3 | -77.6 |
| 7603 | ok | 0.09 | 0.2 | 2.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.9 | 32.8 | 32.9 | 33.2 | 54.6 | -61.5 |
| 7604 | ok | 0.09 | 0.2 | 2.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.5 | 32.7 | 36.5 | 43.1 | 71.2 | -81.3 |
| 7605 | ok | 0.09 | 0.2 | 2.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.7 | 27.4 | 43.2 | 40.0 | 74.2 | -80.6 |
| 7606 | ok | 0.09 | 0.2 | 2.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.4 | -20.5 | -74.8 | -118.3 | 348.2 | -6.9 |
| 7607 | ok | 0.09 | 0.2 | 2.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.4 | 14.6 | 53.7 | -211.6 | -402.9 | 441.0 |
| 7608 | ok | 0.09 | 0.2 | 2.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.2 | -9.2 | 62.0 | 8.8 | 40.6 | -30.6 |
| 7609 | ok | 0.09 | 0.2 | 2.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.2 | 1.1 | -66.5 | -44.3 | 422.7 | 141.0 |
| 7610 | ok | 0.09 | 0.2 | 2.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.9 | -15.2 | 75.6 | -126.3 | -464.8 | 370.3 |
| 7611 | ok | 0.09 | 0.2 | 2.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.2 | -25.7 | 85.0 | 16.9 | 73.7 | -53.0 |
| 7612 | ok | 0.09 | 0.2 | 3.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.7 | -37.1 | 95.6 | 13.7 | 65.1 | -41.1 |
| 7613 | ok | 0.09 | 0.2 | 3.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -70.1 | -43.8 | 102.7 | 15.3 | 51.3 | -27.1 |
| 7614 | ok | 0.09 | 0.2 | 5.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -76.0 | 55.2 | -55.2 | 149.3 | 9.1 | 157.5 |
| 7615 | ok | 0.09 | 0.2 | 4.75e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.7 | 44.9 | -79.3 | 148.0 | 29.4 | 181.7 |
| 7616 | ok | 0.09 | 0.2 | 4.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.8 | 22.9 | -96.5 | 153.4 | 54.1 | 204.1 |
| 7617 | ok | 0.09 | 0.2 | 3.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.4 | 1.2 | -109.0 | 156.3 | 80.1 | 223.1 |
| 7618 | ok | 0.09 | 0.2 | 3.73e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.8 | -18.0 | -117.7 | 156.3 | 106.5 | 238.0 |
| 7619 | ok | 0.09 | 0.2 | 3.99e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.1 | -33.8 | -123.5 | 153.5 | 132.1 | 248.6 |
| 7620 | ok | 0.09 | 0.2 | 4.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.3 | -46.3 | -127.1 | 148.3 | 156.1 | 254.9 |
| 7621 | ok | 0.09 | 0.3 | 4.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.4 | -56.1 | -129.9 | 152.7 | 158.0 | 259.8 |
| 7622 | ok | 0.09 | 0.3 | 4.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.5 | -64.5 | -132.1 | 146.0 | 178.0 | 260.8 |
| 7623 | ok | 0.09 | 0.3 | 4.58e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.4 | -71.0 | -133.4 | 138.1 | 195.7 | 259.0 |
| 7624 | ok | 0.09 | 0.3 | 4.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.0 | -76.1 | -133.8 | 129.3 | 211.1 | 254.7 |
| 7625 | ok | 0.09 | 0.3 | 4.68e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.6 | -80.1 | -133.8 | 119.6 | 224.2 | 248.3 |
| 7626 | ok | 0.09 | 0.3 | 4.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.2 | -83.4 | -133.5 | 109.0 | 235.1 | 240.0 |
| 7627 | ok | 0.09 | 0.3 | 4.73e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.1 | -86.4 | -133.3 | 97.6 | 243.8 | 229.7 |
| 7628 | ok | 0.09 | 0.2 | 4.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.6 | -89.5 | -133.6 | 85.1 | 250.0 | 217.3 |
| 7629 | ok | 0.09 | 0.2 | 4.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -81.2 | -93.0 | -134.9 | 71.5 | 253.5 | 202.7 |
| 7630 | ok | 0.09 | 0.2 | 5.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -84.3 | -96.7 | -137.8 | 56.7 | 253.4 | 185.2 |
| 7631 | ok | 0.09 | 0.2 | 5.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -89.1 | -99.4 | -142.3 | 41.6 | 248.5 | 164.1 |
| 7632 | ok | 0.09 | 0.2 | 5.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.0 | 61.5 | 48.3 | -48.1 | -207.7 | 149.8 |
| 7633 | ok | 0.09 | 0.2 | 5.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.1 | 55.2 | 49.6 | -93.0 | -147.3 | 114.5 |
| 8261 | ok | 0.09 | 8.35e-02 | 1.60e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.5 | -6.4 | 31.6 | 25.5 | 53.5 | 1.1 |
| 8262 | ok | 0.09 | 0.2 | 2.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.2 | -45.5 | 38.6 | 69.5 | 111.0 | 4.8 |
| 8263 | ok | 0.09 | 0.2 | 1.57e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.2 | -3.8 | 29.4 | 49.2 | 106.5 | -1.1 |
| 8264 | ok | 0.09 | 0.1 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.8 | -4.8 | 24.3 | 36.4 | 76.7 | -2.9 |
| 8688 | ok | 0.09 | 0.1 | 1.59e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.4 | 12.1 | 5.0 | 61.2 | 328.4 | 27.1 |
| 8689 | ok | 0.09 | 0.3 | 1.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.2 | 2.3 | -39.8 | -4.9 | -109.8 | 34.6 |
| 8690 | ok | 0.09 | 0.2 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.9 | 14.1 | -32.7 | 21.3 | -42.2 | 25.5 |
| 8691 | ok | 0.09 | 0.1 | 1.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.3 | 2.1 | -30.4 | 41.9 | 103.3 | 16.3 |
| 9492 | ok | 0.09 | 0.2 | 1.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.0 | -11.4 | 31.2 | -9.2 | -14.4 | 115.6 |
| 9493 | ok | 0.09 | 0.1 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.0 | 0.8 | 26.0 | 39.5 | 69.8 | -14.8 |
| 9494 | ok | 0.09 | 0.1 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.0 | -4.7 | 29.7 | 33.4 | 55.6 | -18.1 |
| 9495 | ok | 0.09 | 0.1 | 2.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.9 | -25.8 | 62.3 | 25.6 | 53.9 | -20.8 |
| 9496 | ok | 0.09 | 0.1 | 1.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.1 | -3.9 | 14.4 | 7.3 | 63.3 | -28.8 |
| 9497 | ok | 0.09 | 0.1 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.8 | 1.3 | 19.5 | 27.8 | 47.1 | -27.0 |
| 9498 | ok | 0.09 | 0.1 | 1.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.9 | -4.9 | 25.7 | 28.8 | 38.8 | -29.0 |
| 9499 | ok | 0.09 | 0.1 | 2.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.2 | -24.6 | 60.1 | 25.7 | 51.4 | -30.3 |
| 9500 | ok | 0.09 | 0.1 | 1.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.5 | -4.3 | 13.6 | 13.3 | 38.6 | -41.3 |
| 9501 | ok | 0.09 | 0.1 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.5 | 0.2 | 13.1 | 24.0 | 30.1 | -37.7 |
| 9502 | ok | 0.09 | 0.1 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -63.0 | -3.5 | 20.4 | 26.4 | 26.6 | -36.9 |
| 9503 | ok | 0.09 | 0.1 | 2.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.4 | -18.8 | 53.2 | 25.7 | 50.4 | -38.7 |
| 9504 | ok | 0.09 | 0.1 | 1.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.1 | -8.8 | 9.4 | 18.9 | 44.3 | -43.2 |
| 9505 | ok | 0.09 | 0.1 | 1.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.1 | -6.3 | 11.6 | 25.8 | 35.8 | -38.8 |
| 9506 | ok | 0.09 | 0.1 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.9 | -4.3 | 8.5 | 24.8 | 27.0 | -37.0 |
| 9507 | ok | 0.09 | 0.2 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.2 | 2.1 | -27.5 | -67.0 | 226.8 | 195.2 |
| 9508 | ok | 0.09 | 0.1 | 1.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.1 | 11.3 | 21.3 | 140.1 | 19.2 | -46.7 |
| 9509 | ok | 0.09 | 0.1 | 1.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.1 | 4.5 | 7.3 | 27.0 | 8.5 | -47.2 |
| 9510 | ok | 0.09 | 0.1 | 1.27e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.6 | -4.6 | 11.0 | 25.9 | 20.5 | -42.2 |
| 9511 | ok | 0.09 | 0.2 | 1.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.1 | -6.0 | 39.0 | -163.1 | -259.5 | 290.1 |
| 9512 | ok | 0.09 | 0.1 | 1.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.2 | 20.1 | 20.1 | 165.5 | 6.0 | -126.6 |
| 9513 | ok | 0.09 | 0.1 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.3 | -27.0 | 7.9 | -125.3 | 2.5 | 118.9 |
| 9514 | ok | 0.09 | 0.1 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.9 | -19.0 | 7.4 | -130.2 | 0.6 | 110.9 |
| 9515 | ok | 0.09 | 0.2 | 1.56e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.7 | -12.9 | 16.0 | -13.5 | 2.8 | 95.2 |
| 9516 | ok | 0.09 | 0.1 | 1.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.3 | 30.2 | 18.6 | 193.2 | -4.6 | -116.0 |
| 9517 | ok | 0.09 | 0.1 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.8 | -30.5 | -0.3 | -161.1 | 3.9 | 104.0 |
| 9518 | ok | 0.09 | 0.1 | 1.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.2 | -21.2 | 5.0 | -147.9 | 1.6 | 92.5 |
| 9519 | ok | 0.09 | 0.2 | 1.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -51.9 | -7.5 | -39.2 | -130.2 | 225.0 | 109.9 |
| 9520 | ok | 0.09 | 0.2 | 1.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -28.3 | 41.8 | 16.5 | 223.2 | -12.1 | -100.5 |
| 9521 | ok | 0.09 | 0.1 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.8 | -28.8 | -0.7 | -185.6 | 1.1 | 93.0 |
| 9522 | ok | 0.09 | 0.1 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.1 | -20.5 | 10.0 | -16.6 | 2.7 | 76.6 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|-------|----------|--------|--------|---------|---------|-------|-------|-------|--------|--------|-------|
| 9523 | ok | 0.09 | 0.2 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.6 | 16.3 | 21.4 | -214.8 | -198.1 | 283.9 |
| 9524 | ok | 0.09 | 0.2 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -48.0 | -45.8 | 1.2 | -194.0 | 6.5 | 74.9 |
| 9525 | ok | 0.09 | 0.2 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.8 | -31.7 | -2.8 | -204.4 | 2.3 | 65.3 |
| 9526 | ok | 0.09 | 0.1 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.6 | -20.9 | -2.8 | -174.2 | 1.3 | 45.6 |
| 9527 | ok | 0.09 | 0.2 | 1.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.3 | 18.5 | 17.5 | 38.5 | 41.7 | -52.6 |
| 9528 | ok | 0.09 | 0.3 | 1.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -71.6 | -52.5 | -10.1 | -242.2 | 113.8 | 6.8 |
| 9529 | ok | 0.09 | 0.2 | 1.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.8 | -30.9 | -9.1 | -219.4 | 56.3 | 21.2 |
| 9530 | ok | 0.09 | 0.1 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.5 | -19.8 | -11.1 | -174.9 | 28.6 | 24.3 |
| 9531 | ok | 0.09 | 0.2 | 1.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.6 | 23.9 | 12.1 | 40.2 | 39.9 | -51.3 |
| 9532 | ok | 0.09 | 0.3 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -67.5 | -50.8 | -12.4 | -269.7 | 107.4 | 12.6 |
| 9533 | ok | 0.09 | 0.2 | 1.35e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.4 | -31.7 | -10.6 | -204.3 | 60.1 | 20.9 |
| 9534 | ok | 0.09 | 0.1 | 1.19e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.4 | -21.1 | -12.5 | -158.5 | 31.5 | 20.4 |
| 9535 | ok | 0.09 | 0.1 | 1.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.7 | 27.2 | 7.5 | 40.5 | 38.3 | -49.3 |
| 9536 | ok | 0.09 | 0.3 | 1.70e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -74.3 | -47.8 | -25.1 | -145.1 | 103.7 | 4.4 |
| 9537 | ok | 0.09 | 0.2 | 1.37e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.4 | -30.3 | -22.5 | -143.1 | 56.0 | 2.6 |
| 9538 | ok | 0.09 | 0.1 | 1.16e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.5 | -20.6 | -22.1 | -131.4 | 28.8 | 22.6 |
| 9539 | ok | 0.09 | 0.1 | 1.75e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.4 | 22.5 | 3.9 | 29.1 | 30.0 | -37.0 |
| 9540 | ok | 0.09 | 0.3 | 1.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | 29.9 | 89.2 | 18.4 | 91.3 | -57.7 | -4.3 |
| 9541 | ok | 0.09 | 0.6 | 1.82e-02 | 4.5 | 4.5 | 4.0 | 4.0 | 41.4 | 179.8 | 36.7 | 11.4 | -69.1 | 9.4 |
| 9542 | ok | 0.09 | 0.2 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.1 | -29.9 | -33.2 | -77.4 | 47.2 | 2.5 |
| 9543 | ok | 0.09 | 0.1 | 1.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -38.7 | -18.5 | -23.9 | -15.3 | 25.7 | 24.3 |
| 9544 | ok | 0.09 | 0.1 | 1.66e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.5 | 22.4 | 2.3 | 28.7 | 29.2 | -36.4 |
| 9545 | ok | 0.09 | 0.2 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.2 | 29.8 | 20.8 | 36.0 | 48.7 | -60.8 |
| 9546 | ok | 0.09 | 0.4 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | 1.7 | 103.6 | 8.3 | 20.2 | -19.7 | -6.8 |
| 9547 | ok | 0.09 | 0.4 | 8.08e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 2.6 | 130.3 | 12.0 | 13.7 | -34.0 | -2.8 |
| 9548 | ok | 0.09 | 0.2 | 9.78e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 1.7 | 68.3 | 11.9 | 28.6 | -0.7 | -16.3 |
| 9549 | ok | 0.09 | 0.2 | 1.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.8 | -20.1 | -26.2 | -14.2 | 17.7 | 1.4 |
| 9550 | ok | 0.09 | 0.1 | 1.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -26.4 | 21.9 | 3.3 | 28.2 | 28.7 | -36.1 |
| 9551 | ok | 0.09 | 0.2 | 2.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -27.9 | 27.6 | 18.7 | 35.1 | 48.3 | -59.7 |
| 9552 | ok | 0.09 | 0.3 | 7.71e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.3 | 88.7 | 9.0 | 13.4 | 10.1 | -15.4 |
| 9553 | ok | 0.09 | 0.4 | 4.98e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -0.7 | 108.0 | 3.0 | -13.4 | -8.1 | -40.3 |
| 9554 | ok | 0.09 | 0.2 | 8.50e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 3.1 | 69.8 | 16.4 | 23.8 | -7.0 | -17.5 |
| 9555 | ok | 0.09 | 0.2 | 9.02e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.0 | -20.8 | -28.1 | -7.9 | 11.7 | 3.4 |
| 9556 | ok | 0.09 | 0.2 | 1.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -23.4 | 17.9 | 3.2 | 18.7 | 21.2 | -25.5 |
| 9557 | ok | 0.09 | 0.2 | 2.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -25.8 | 24.0 | 18.9 | 34.8 | 48.1 | -59.2 |
| 9558 | ok | 0.09 | 0.3 | 5.54e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.7 | 83.4 | 7.8 | 9.4 | 12.2 | -21.3 |
| 9559 | ok | 0.09 | 0.4 | 3.25e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.0 | 103.4 | 2.4 | -10.3 | -11.9 | -34.9 |
| 9560 | ok | 0.09 | 0.2 | 6.92e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -4.8 | 63.0 | 11.3 | 22.0 | 9.2 | -19.4 |
| 9561 | ok | 0.09 | 0.2 | 7.92e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -4.8 | 46.3 | 18.1 | 30.5 | 5.4 | -19.7 |
| 9562 | ok | 0.09 | 0.2 | 1.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -21.5 | 17.2 | 4.8 | 18.5 | 21.6 | -25.8 |
| 9563 | ok | 0.09 | 0.2 | 1.86e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -13.7 | 13.0 | 41.0 | 42.7 | 25.1 | -70.4 |
| 9564 | ok | 0.09 | 0.3 | 4.03e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.5 | 79.0 | 6.9 | -26.4 | -16.4 | -55.8 |
| 9565 | ok | 0.09 | 0.3 | 1.91e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.0 | 105.3 | 4.5 | -7.8 | -10.9 | -34.7 |
| 9566 | ok | 0.09 | 0.2 | 5.62e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -6.4 | 59.3 | 10.8 | -44.4 | -12.2 | -54.8 |
| 9567 | ok | 0.09 | 0.2 | 6.94e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -7.8 | 44.7 | 19.3 | 29.9 | 8.9 | -20.4 |
| 9568 | ok | 0.09 | 0.2 | 1.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -11.7 | 24.1 | 17.7 | 32.3 | 10.2 | -49.6 |
| 9569 | ok | 0.09 | 0.2 | 1.73e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -15.2 | 9.2 | 42.7 | 42.1 | 25.2 | -72.5 |
| 9570 | ok | 0.09 | 0.3 | 2.91e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.6 | 79.9 | 9.7 | -23.5 | -15.6 | -55.3 |
| 9571 | ok | 0.09 | 0.3 | 8.31e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.4 | 104.0 | -1.5 | -0.8 | 11.2 | -4.3 |
| 9572 | ok | 0.09 | 0.2 | 4.45e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -6.8 | 60.3 | 14.8 | -39.1 | -10.8 | -54.9 |
| 9573 | ok | 0.09 | 0.2 | 6.05e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -10.2 | 42.2 | 20.4 | 30.2 | 10.4 | -51.6 |
| 9574 | ok | 0.09 | 0.2 | 1.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -13.2 | 22.3 | 19.1 | 32.5 | 10.8 | -50.3 |
| 9575 | ok | 0.09 | 0.2 | 1.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -26.7 | -8.2 | 39.3 | 33.3 | 35.2 | -51.8 |
| 9576 | ok | 0.09 | 0.2 | 2.14e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -4.3 | 74.2 | 10.5 | -23.6 | -16.6 | -21.0 |
| 9577 | ok | 0.09 | 0.3 | 3.90e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -0.6 | 103.7 | -1.8 | -1.4 | 10.0 | -5.1 |
| 9578 | ok | 0.09 | 0.2 | 3.70e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -8.8 | 56.0 | 16.1 | -36.9 | -12.0 | -21.8 |
| 9579 | ok | 0.09 | 0.2 | 5.44e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -12.8 | 39.5 | 20.7 | -46.6 | -8.3 | -21.4 |
| 9580 | ok | 0.09 | 0.1 | 1.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -14.8 | 21.3 | 14.5 | 32.4 | 5.4 | -47.9 |
| 9581 | ok | 0.09 | 0.2 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -29.2 | -9.9 | 43.8 | 44.8 | 52.9 | -72.7 |
| 9582 | ok | 0.09 | 0.2 | 2.21e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -8.5 | 69.7 | 5.6 | 13.8 | 12.3 | -35.0 |
| 9583 | ok | 0.09 | 0.3 | 5.34e-04 | 4.5 | 4.5 | 4.0 | 4.0 | 6.1 | 103.4 | -3.6 | -8.3 | 4.8 | -4.4 |
| 9584 | ok | 0.09 | 0.2 | 4.31e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -16.3 | 52.8 | 10.2 | 23.9 | 10.1 | -30.5 |
| 9585 | ok | 0.09 | 0.1 | 5.73e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -15.8 | 37.2 | 21.7 | -40.9 | -8.2 | -20.0 |
| 9586 | ok | 0.09 | 0.1 | 1.00e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -24.8 | 14.3 | 14.7 | 20.5 | 24.0 | -28.7 |
| 9587 | ok | 0.09 | 0.2 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.8 | -12.2 | 47.3 | 45.6 | 54.3 | -74.6 |
| 9588 | ok | 0.09 | 0.2 | 1.49e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.7 | 36.5 | 47.4 | 59.6 | 44.8 | -81.3 |
| 9589 | ok | 0.09 | 0.3 | 2.96e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 81.1 | 111.0 | -31.6 | -105.1 | -27.8 | 31.9 |
| 9590 | ok | 0.09 | 0.2 | 6.35e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -26.0 | 53.1 | 10.5 | 29.2 | 12.8 | -29.7 |
| 9591 | ok | 0.09 | 0.1 | 6.77e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.6 | 36.8 | 12.8 | 30.5 | 13.2 | -27.9 |
| 9592 | ok | 0.09 | 0.1 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -28.8 | 18.6 | 13.0 | 34.9 | 16.5 | -29.4 |
| 9593 | ok | 0.09 | 0.2 | 1.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.6 | -13.5 | 50.3 | 46.8 | 55.9 | -77.2 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|-------|-------|-------|--------|-------|--------|
| 9594 | ok | 0.09 | 0.3 | 1.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.7 | 116.7 | 14.6 | 42.2 | -43.7 | -49.1 |
| 9595 | ok | 0.09 | 0.2 | 7.58e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -34.3 | 56.8 | 6.3 | 33.0 | 8.8 | -26.1 |
| 9596 | ok | 0.09 | 0.1 | 7.25e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -31.7 | 36.6 | 10.4 | 32.0 | 13.9 | -27.6 |
| 9597 | ok | 0.09 | 0.1 | 1.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -34.5 | 12.7 | 32.8 | 40.0 | 37.3 | -48.0 |
| 9598 | ok | 0.09 | 0.2 | 1.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.4 | 31.2 | -38.1 | 49.6 | 46.5 | 24.8 |
| 9599 | ok | 0.09 | 0.3 | 3.33e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 83.6 | 113.4 | 34.5 | -109.7 | -27.0 | -44.2 |
| 9600 | ok | 0.09 | 0.1 | 5.77e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -24.6 | 49.4 | -2.1 | 29.2 | 12.7 | -23.1 |
| 9601 | ok | 0.09 | 0.1 | 6.44e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.7 | 33.2 | 7.2 | 31.2 | 14.0 | -27.4 |
| 9602 | ok | 0.09 | 0.1 | 1.05e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.4 | 8.3 | 29.9 | 38.3 | 40.3 | -47.5 |
| 9603 | ok | 0.09 | 0.2 | 1.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.1 | -18.8 | 54.4 | 47.3 | 64.3 | -81.6 |
| 9604 | ok | 0.09 | 0.2 | 1.85e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -8.5 | 64.4 | 0.3 | 14.0 | 14.9 | -18.4 |
| 9605 | ok | 0.09 | 0.2 | 6.19e-04 | 4.5 | 4.5 | 4.0 | 4.0 | 6.6 | 95.3 | 3.8 | -9.7 | 10.4 | -5.2 |
| 9606 | ok | 0.09 | 0.1 | 3.51e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.6 | 43.7 | -4.5 | 21.7 | 12.2 | -30.6 |
| 9607 | ok | 0.09 | 9.86e-02 | 5.36e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -23.2 | 28.2 | 8.4 | 29.5 | 14.9 | -28.6 |
| 9608 | ok | 0.09 | 0.1 | 1.09e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -31.2 | 3.6 | 31.7 | 39.5 | 41.9 | -49.9 |
| 9609 | ok | 0.09 | 0.2 | 1.89e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.0 | -23.9 | 56.1 | 49.5 | 67.1 | -85.0 |
| 9610 | ok | 0.09 | 0.2 | 1.26e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.0 | 65.0 | 4.8 | 7.4 | 16.4 | -26.3 |
| 9611 | ok | 0.09 | 0.2 | 3.61e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -0.6 | 91.1 | 1.9 | -1.6 | 15.4 | -4.5 |
| 9612 | ok | 0.09 | 0.1 | 2.83e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -9.0 | 42.3 | 2.9 | 19.5 | 13.9 | -33.8 |
| 9613 | ok | 0.09 | 9.05e-02 | 5.11e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -20.3 | 24.0 | 12.2 | 28.6 | 16.0 | -30.6 |
| 9614 | ok | 0.09 | 0.1 | 1.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.1 | -1.9 | 34.8 | 40.4 | 43.7 | -52.2 |
| 9615 | ok | 0.09 | 0.2 | 2.03e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.2 | -30.8 | 59.4 | 51.4 | 70.0 | -88.5 |
| 9616 | ok | 0.09 | 0.1 | 1.32e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -2.3 | 61.4 | 3.3 | 6.6 | 17.9 | -32.0 |
| 9617 | ok | 0.09 | 0.2 | 3.25e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -1.4 | 87.1 | -1.6 | 2.8 | -18.7 | 1.8 |
| 9618 | ok | 0.09 | 0.1 | 3.08e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.8 | 39.3 | 11.3 | 18.9 | 14.7 | -32.2 |
| 9619 | ok | 0.09 | 8.61e-02 | 5.67e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -19.9 | 20.4 | 16.8 | 29.2 | 16.9 | -33.3 |
| 9620 | ok | 0.09 | 0.1 | 1.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.4 | -7.8 | 39.2 | 41.8 | 45.8 | -54.9 |
| 9621 | ok | 0.09 | 0.2 | 2.25e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.1 | -38.6 | 64.7 | 53.5 | 73.2 | -92.5 |
| 9622 | ok | 0.09 | 0.1 | 1.58e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -5.0 | 57.3 | 2.8 | 8.1 | 18.5 | -39.5 |
| 9623 | ok | 0.09 | 0.2 | 3.60e-04 | 4.5 | 4.5 | 4.0 | 4.0 | -0.5 | 83.4 | -1.9 | -1.8 | 18.5 | -7.5 |
| 9624 | ok | 0.09 | 0.1 | 3.89e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -9.8 | 35.0 | 12.4 | 20.7 | 14.8 | -37.1 |
| 9625 | ok | 0.09 | 8.37e-02 | 6.90e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -21.9 | 16.7 | 21.7 | 31.1 | 17.7 | -36.1 |
| 9626 | ok | 0.09 | 0.1 | 1.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -32.5 | -13.6 | 44.6 | 43.9 | 47.9 | -57.9 |
| 9627 | ok | 0.09 | 0.2 | 2.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -39.3 | -46.2 | 71.6 | 55.7 | 76.6 | -96.9 |
| 9628 | ok | 0.09 | 0.2 | 2.56e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -9.1 | 49.2 | 8.2 | 15.4 | 20.2 | -52.8 |
| 9629 | ok | 0.09 | 0.2 | 6.41e-04 | 4.5 | 4.5 | 4.0 | 4.0 | 7.2 | 79.5 | -4.0 | -10.1 | 15.3 | -6.9 |
| 9630 | ok | 0.09 | 0.1 | 5.70e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -16.9 | 32.9 | 15.6 | -72.0 | 3.6 | 24.4 |
| 9631 | ok | 0.09 | 8.57e-02 | 8.66e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -26.4 | 13.4 | 26.5 | 34.4 | 18.3 | -38.7 |
| 9632 | ok | 0.09 | 0.1 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -36.4 | -18.7 | 50.1 | 46.7 | 50.1 | -61.0 |
| 9633 | ok | 0.09 | 0.2 | 2.78e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -42.9 | -52.7 | 79.0 | 58.3 | 80.1 | -101.9 |
| 9634 | ok | 0.09 | 0.1 | 1.77e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.1 | -4.4 | 55.2 | 51.7 | 54.1 | -92.6 |
| 9635 | ok | 0.09 | 0.3 | 3.68e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 94.2 | 84.3 | -39.3 | -113.1 | -24.0 | 34.9 |
| 9636 | ok | 0.09 | 0.1 | 8.59e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -25.2 | 34.2 | 22.3 | -89.3 | 27.8 | 18.5 |
| 9637 | ok | 0.09 | 9.32e-02 | 1.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -33.1 | 11.1 | 29.3 | 38.6 | 19.1 | -40.7 |
| 9638 | ok | 0.09 | 0.1 | 1.92e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -41.2 | -23.2 | 54.6 | 49.9 | 52.3 | -64.2 |
| 9639 | ok | 0.09 | 0.2 | 3.02e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.4 | -58.0 | 85.2 | 61.1 | 83.5 | -107.3 |
| 9640 | ok | 0.09 | 0.3 | 1.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.5 | 91.2 | 20.0 | 50.3 | -37.4 | -72.4 |
| 9641 | ok | 0.09 | 0.1 | 9.96e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -38.5 | 31.4 | 15.2 | 41.3 | 16.0 | -48.4 |
| 9642 | ok | 0.09 | 0.1 | 1.11e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -37.6 | 7.6 | 27.9 | 42.3 | 19.7 | -42.1 |
| 9643 | ok | 0.09 | 0.1 | 2.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.4 | -28.2 | 57.2 | 53.1 | 54.4 | -67.5 |
| 9644 | ok | 0.09 | 0.2 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.2 | -8.1 | -37.6 | 53.9 | 57.5 | 2.3 |
| 9645 | ok | 0.09 | 0.3 | 3.76e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 89.3 | 75.7 | 37.4 | -112.0 | -20.3 | -50.0 |
| 9646 | ok | 0.09 | 0.1 | 7.46e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -28.1 | 20.4 | 6.7 | 38.7 | 20.0 | -47.6 |
| 9647 | ok | 0.09 | 0.1 | 1.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -30.1 | 8.7 | 18.5 | -115.5 | 4.0 | -21.1 |
| 9648 | ok | 0.09 | 0.1 | 2.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.6 | -35.0 | 59.7 | 56.5 | 55.7 | -71.5 |
| 9649 | ok | 0.09 | 0.2 | 3.38e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.6 | -66.1 | 93.3 | 71.1 | 86.4 | -121.5 |
| 9650 | ok | 0.09 | 0.2 | 4.61e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -3.6 | 25.3 | 8.3 | 12.0 | 20.3 | -44.8 |
| 9651 | ok | 0.09 | 0.2 | 1.98e-03 | 4.5 | 4.5 | 4.0 | 4.0 | 3.8 | 62.8 | -0.2 | -8.2 | 1.5 | -6.3 |
| 9652 | ok | 0.09 | 0.1 | 6.35e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -16.2 | 11.2 | 9.6 | 34.4 | 19.3 | -49.8 |
| 9653 | ok | 0.09 | 0.1 | 1.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -29.7 | -9.6 | 30.0 | 45.4 | 20.4 | -46.5 |
| 9654 | ok | 0.09 | 0.1 | 2.36e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.7 | -42.3 | 64.4 | 61.2 | 55.6 | -76.9 |
| 9655 | ok | 0.09 | 0.2 | 3.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -55.7 | -73.9 | 96.3 | 73.8 | 88.3 | -128.0 |
| 9656 | ok | 0.09 | 0.2 | 8.09e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -5.3 | -41.9 | 16.1 | 17.1 | 19.2 | -20.3 |
| 9657 | ok | 0.09 | 0.2 | 6.00e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.0 | 63.5 | -2.2 | -4.1 | -3.6 | -5.5 |
| 9658 | ok | 0.09 | 0.1 | 9.97e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -13.5 | -15.8 | 25.5 | 33.9 | 14.4 | -54.5 |
| 9659 | ok | 0.09 | 0.1 | 1.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -25.8 | -28.0 | 42.9 | 52.7 | 18.3 | -53.5 |
| 9660 | ok | 0.09 | 0.2 | 2.88e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.0 | -63.6 | 77.1 | 70.9 | 54.2 | -86.5 |
| 9661 | ok | 0.09 | 0.2 | 4.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.4 | -95.0 | 110.9 | 83.4 | 87.5 | -144.3 |
| 9662 | ok | 0.09 | 0.2 | 6.16e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -4.8 | -24.9 | 15.4 | 18.1 | 20.8 | -18.2 |
| 9663 | ok | 0.09 | 0.2 | 3.86e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.1 | 69.8 | -4.4 | -4.0 | -3.6 | -5.1 |
| 9664 | ok | 0.09 | 0.1 | 7.86e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -11.9 | -27.5 | 24.9 | 35.0 | 17.3 | -20.8 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|-------|--------|--------|--------|
| 9665 | ok | 0.09 | 0.1 | 1.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -26.4 | -18.8 | 35.9 | 48.0 | 19.8 | -49.8 |
| 9666 | ok | 0.09 | 0.2 | 2.58e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.4 | -52.5 | 69.8 | 65.3 | 55.5 | -81.4 |
| 9667 | ok | 0.09 | 0.2 | 3.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.7 | -83.8 | 102.2 | 78.2 | 88.7 | -135.7 |
| 9668 | ok | 0.09 | 0.2 | 1.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -5.4 | -48.6 | 20.0 | 19.2 | 18.4 | -25.3 |
| 9669 | ok | 0.09 | 0.2 | 8.37e-03 | 4.5 | 4.5 | 4.0 | 4.0 | -1.4 | -49.4 | 3.0 | 2.7 | 15.1 | -8.3 |
| 9670 | ok | 0.09 | 0.1 | 1.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -15.4 | -30.7 | 35.5 | 39.9 | 12.5 | -61.5 |
| 9671 | ok | 0.09 | 0.1 | 1.84e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -28.3 | -37.6 | 50.7 | 60.3 | 15.3 | -57.1 |
| 9672 | ok | 0.09 | 0.2 | 3.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.2 | -74.6 | 85.8 | 78.5 | 51.0 | -91.7 |
| 9673 | ok | 0.09 | 0.2 | 4.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -61.0 | -105.6 | 122.1 | 89.7 | 84.0 | -153.3 |
| 9674 | ok | 0.09 | 0.2 | 1.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -6.4 | -39.5 | 19.8 | 20.1 | 10.7 | -70.1 |
| 9675 | ok | 0.09 | 0.2 | 1.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -1.4 | -56.7 | 5.1 | 3.8 | 12.7 | -9.5 |
| 9676 | ok | 0.09 | 0.1 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -20.5 | -45.0 | 44.0 | 50.0 | 6.4 | -68.4 |
| 9677 | ok | 0.09 | 8.90e-02 | 2.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -35.3 | -46.6 | 59.5 | 71.5 | 10.2 | -59.8 |
| 9678 | ok | 0.09 | 0.2 | 3.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.8 | -83.9 | 95.4 | 88.2 | 45.6 | -96.2 |
| 9679 | ok | 0.09 | 0.2 | 4.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.9 | -113.3 | 134.9 | 97.0 | 77.5 | -162.1 |
| 9680 | ok | 0.09 | 0.2 | 1.91e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -13.4 | -65.4 | 34.2 | 31.5 | 0.6 | -83.5 |
| 9681 | ok | 0.09 | 0.3 | 1.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | 5.6 | -37.0 | -4.5 | -6.7 | -5.0 | -16.3 |
| 9682 | ok | 0.09 | 0.1 | 2.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -29.1 | -57.6 | 55.9 | 66.9 | -3.5 | -76.3 |
| 9683 | ok | 0.09 | 7.67e-02 | 2.61e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.3 | -52.9 | 68.3 | 87.3 | 3.3 | -60.3 |
| 9684 | ok | 0.09 | 0.1 | 3.98e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.5 | -89.1 | 104.2 | 100.2 | 37.7 | -99.0 |
| 9685 | ok | 0.09 | 0.2 | 5.29e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -70.5 | -115.1 | 147.2 | 105.0 | 67.4 | -169.3 |
| 9686 | ok | 0.09 | 0.1 | 4.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -40.1 | -140.8 | 85.6 | 48.5 | 14.0 | -130.3 |
| 9687 | ok | 0.09 | 0.5 | 2.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | 71.1 | -46.5 | -37.2 | -53.4 | -55.1 | 2.3 |
| 9688 | ok | 0.09 | 0.1 | 2.95e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -64.1 | -66.1 | 68.4 | 98.6 | -16.5 | -80.4 |
| 9689 | ok | 0.09 | 8.41e-02 | 2.98e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -71.7 | -53.7 | 72.9 | 107.9 | -5.0 | -56.9 |
| 9690 | ok | 0.09 | 0.1 | 4.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.8 | -88.2 | 109.3 | 113.9 | 27.8 | -98.8 |
| 9691 | ok | 0.09 | 0.2 | 5.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.2 | -108.7 | 155.4 | 113.8 | 53.3 | -173.5 |
| 9692 | ok | 0.09 | 0.2 | 4.18e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -133.4 | -57.6 | 77.9 | 154.8 | -46.8 | -149.3 |
| 9693 | ok | 0.09 | 0.1 | 3.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -106.9 | -55.6 | 62.0 | 139.5 | -35.0 | -72.0 |
| 9694 | ok | 0.09 | 9.14e-02 | 3.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -97.4 | -49.1 | 67.8 | 131.1 | -13.9 | -47.8 |
| 9695 | ok | 0.09 | 0.1 | 4.24e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -92.5 | -81.3 | 106.5 | 129.3 | 16.5 | -92.4 |
| 9696 | ok | 0.09 | 0.1 | 4.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -178.4 | -85.5 | 26.3 | 240.0 | -113.5 | -101.0 |
| 9697 | ok | 0.09 | 0.1 | 3.42e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -135.3 | -59.9 | 45.3 | 173.1 | -47.2 | -51.9 |
| 9698 | ok | 0.09 | 9.71e-02 | 3.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -115.3 | -46.9 | 55.8 | 150.1 | -21.8 | -35.8 |
| 9699 | ok | 0.09 | 0.1 | 4.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -108.6 | -64.7 | 106.0 | 140.1 | 0.2 | -97.4 |
| 9700 | ok | 0.09 | 0.1 | 3.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -142.8 | -111.5 | 10.7 | 258.4 | -105.4 | -22.9 |
| 9701 | ok | 0.09 | 0.1 | 3.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -134.8 | -63.6 | 20.4 | 195.1 | -58.4 | -20.6 |
| 9702 | ok | 0.09 | 0.1 | 2.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -121.0 | -47.5 | 36.1 | 164.7 | -29.3 | -14.3 |
| 9703 | ok | 0.09 | 0.1 | 3.85e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -99.9 | -2.1 | -29.6 | 154.8 | 10.1 | 83.3 |
| 9704 | ok | 0.09 | 0.1 | 2.91e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -128.2 | -109.1 | 4.9 | 242.4 | -100.3 | 22.9 |
| 9705 | ok | 0.09 | 0.1 | 2.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -123.3 | -72.2 | 6.4 | 199.6 | -61.3 | 13.5 |
| 9706 | ok | 0.09 | 0.1 | 2.67e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -115.1 | -45.0 | 1.7 | 171.8 | -26.2 | 21.3 |
| 9707 | ok | 0.09 | 0.1 | 3.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -100.5 | -17.0 | -45.2 | 161.6 | 22.6 | 102.0 |
| 9708 | ok | 0.09 | 0.1 | 2.62e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -115.7 | -105.1 | -0.7 | 221.9 | -91.8 | 56.2 |
| 9709 | ok | 0.09 | 0.1 | 2.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -112.1 | -75.0 | -2.3 | 193.1 | -59.5 | 42.9 |
| 9710 | ok | 0.09 | 0.1 | 2.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -108.2 | -50.6 | -10.1 | 171.3 | -24.7 | 43.7 |
| 9711 | ok | 0.09 | 0.2 | 3.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -98.3 | -31.2 | -57.1 | 164.1 | 36.9 | 119.0 |
| 9712 | ok | 0.09 | 0.1 | 2.48e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -104.5 | -100.4 | -5.6 | 201.4 | -81.8 | 81.7 |
| 9713 | ok | 0.09 | 0.1 | 2.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -102.0 | -74.9 | -9.0 | 181.9 | -55.0 | 67.5 |
| 9714 | ok | 0.09 | 0.1 | 2.34e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -97.4 | -51.6 | -9.8 | 164.0 | -32.3 | 57.2 |
| 9715 | ok | 0.09 | 0.2 | 3.06e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -94.8 | -43.0 | -66.0 | 162.6 | 52.0 | 133.8 |
| 9716 | ok | 0.09 | 0.1 | 2.40e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -94.5 | -95.1 | -10.0 | 181.9 | -71.4 | 101.8 |
| 9717 | ok | 0.09 | 0.1 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -92.9 | -72.8 | -16.9 | 168.4 | -49.6 | 87.8 |
| 9718 | ok | 0.09 | 0.1 | 2.33e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -93.0 | -50.8 | -8.3 | 153.8 | -37.5 | 70.2 |
| 9719 | ok | 0.09 | 0.2 | 3.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -91.1 | -51.8 | -72.7 | 158.0 | 67.3 | 145.8 |
| 9720 | ok | 0.09 | 0.1 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -85.7 | -89.4 | -13.6 | 163.7 | -61.3 | 118.0 |
| 9721 | ok | 0.09 | 0.1 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -84.9 | -69.7 | -21.4 | 154.5 | -43.2 | 104.8 |
| 9722 | ok | 0.09 | 0.1 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -86.1 | -48.3 | -14.2 | 142.7 | -36.1 | 86.7 |
| 9723 | ok | 0.09 | 0.2 | 3.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -87.5 | -51.5 | -78.6 | 158.8 | 71.5 | 150.0 |
| 9724 | ok | 0.09 | 0.1 | 2.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.8 | -83.1 | -19.1 | 146.8 | -51.5 | 131.0 |
| 9725 | ok | 0.09 | 0.1 | 2.21e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.9 | -65.9 | -24.9 | 140.5 | -36.6 | 118.9 |
| 9726 | ok | 0.09 | 0.1 | 2.32e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.0 | -45.4 | -18.8 | 130.7 | -34.2 | 100.9 |
| 9727 | ok | 0.09 | 0.2 | 3.39e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -84.9 | -56.5 | -82.9 | 151.2 | 85.3 | 157.2 |
| 9728 | ok | 0.09 | 0.1 | 2.14e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -71.0 | -76.5 | -21.4 | 131.2 | -41.7 | 141.5 |
| 9729 | ok | 0.09 | 0.1 | 2.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -71.9 | -61.5 | -27.6 | 127.0 | -29.7 | 130.5 |
| 9730 | ok | 0.09 | 0.1 | 2.31e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -74.9 | -42.2 | -22.3 | 118.3 | -31.7 | 113.2 |
| 9731 | ok | 0.09 | 0.2 | 3.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -82.6 | -59.8 | -86.1 | 142.5 | 97.8 | 162.2 |
| 9732 | ok | 0.09 | 0.1 | 2.04e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.2 | -69.8 | -23.1 | 117.0 | -31.7 | 149.7 |
| 9733 | ok | 0.09 | 0.1 | 2.12e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.8 | -56.9 | -29.5 | 114.2 | -22.4 | 139.8 |
| 9734 | ok | 0.09 | 0.1 | 2.30e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -71.4 | -33.5 | -26.9 | -124.3 | 35.5 | -124.3 |
| 9735 | ok | 0.09 | 0.2 | 3.50e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -80.5 | -61.8 | -88.3 | 133.0 | 109.0 | 165.2 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------------|-------|------------|--------------|-----------------|---------------|---------------|----------------|----------------|------------|------------|-------------|------------|------------|-------------|
| 9736 | ok | 0.09 | 0.1 | 1.95e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.2 | -62.9 | -24.3 | 104.0 | -20.8 | 155.8 |
| 9737 | ok | 0.09 | 0.1 | 2.07e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.4 | -52.0 | -30.8 | 102.3 | -14.2 | 147.0 |
| 9738 | ok | 0.09 | 0.1 | 2.28e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.9 | -47.7 | -41.3 | 100.3 | 12.7 | 138.7 |
| 9739 | ok | 0.09 | 0.2 | 3.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.6 | -62.9 | -89.7 | 122.9 | 118.9 | 166.5 |
| 9740 | ok | 0.09 | 0.1 | 1.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -56.1 | -56.0 | -25.0 | 92.4 | -8.1 | 159.8 |
| 9741 | ok | 0.09 | 0.1 | 2.01e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.7 | -47.1 | -31.5 | 91.6 | -4.4 | 151.9 |
| 9742 | ok | 0.09 | 0.1 | 2.26e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -68.7 | -36.0 | -48.1 | 96.6 | 13.2 | 132.6 |
| 9743 | ok | 0.09 | 0.2 | 3.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.0 | -63.3 | -90.6 | 112.4 | 127.4 | 166.1 |
| 9744 | ok | 0.09 | 0.1 | 1.79e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -52.6 | -49.4 | -22.8 | 82.2 | 8.1 | 161.3 |
| 9745 | ok | 0.09 | 0.1 | 1.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -59.2 | -44.0 | -32.5 | 83.0 | 11.2 | 152.2 |
| 9746 | ok | 0.09 | 0.1 | 2.23e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -60.4 | -28.2 | -38.4 | -111.1 | 21.6 | -164.3 |
| 9747 | ok | 0.09 | 0.2 | 3.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.8 | -63.3 | -91.2 | 101.7 | 134.7 | 164.4 |
| 9748 | ok | 0.09 | 0.1 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.9 | -42.8 | -22.7 | 73.5 | 29.2 | 159.9 |
| 9749 | ok | 0.09 | 0.1 | 1.90e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.5 | -37.8 | -29.0 | 75.4 | 26.3 | 153.5 |
| 9750 | ok | 0.09 | 0.1 | 2.20e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.6 | -30.1 | -49.7 | 75.3 | 21.3 | 140.9 |
| 9751 | ok | 0.09 | 0.2 | 3.53e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.3 | -63.0 | -91.7 | 90.9 | 140.9 | 161.1 |
| 9752 | ok | 0.09 | 0.1 | 1.64e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -47.7 | -36.5 | -22.4 | 66.6 | 58.2 | 154.9 |
| 9753 | ok | 0.09 | 0.1 | 1.85e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.0 | -27.7 | -35.6 | -96.4 | 18.8 | -189.5 |
| 9754 | ok | 0.09 | 0.1 | 2.17e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.1 | -26.6 | -50.0 | 65.7 | 25.9 | 142.8 |
| 9755 | ok | 0.09 | 0.2 | 3.54e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -75.6 | -62.6 | -92.5 | 80.2 | 145.9 | 156.2 |
| 9756 | ok | 0.09 | 0.1 | 1.57e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -46.1 | -30.5 | -21.7 | 61.5 | 98.7 | 145.1 |
| 9757 | ok | 0.09 | 0.1 | 1.80e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.6 | -28.0 | -27.6 | 68.0 | 82.6 | 138.5 |
| 9758 | ok | 0.09 | 0.1 | 2.15e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -65.4 | -22.8 | -50.0 | 57.4 | 31.6 | 142.9 |
| 9759 | ok | 0.09 | 0.2 | 3.58e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -77.0 | -62.0 | -93.7 | 69.8 | 150.0 | 149.5 |
| 9760 | ok | 0.09 | 0.1 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.2 | -25.0 | -20.6 | 58.3 | 156.4 | 128.7 |
| 9761 | ok | 0.09 | 0.1 | 1.75e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -50.0 | -23.0 | -26.4 | 68.7 | 129.8 | 120.7 |
| 9762 | ok | 0.09 | 0.1 | 2.13e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.2 | -18.3 | -49.7 | 50.7 | 39.4 | 140.6 |
| 9763 | ok | 0.09 | 0.2 | 3.63e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -79.2 | -60.9 | -95.4 | 60.2 | 153.0 | 140.4 |
| 9764 | ok | 0.09 | 0.2 | 1.46e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -45.0 | -20.0 | -19.0 | 56.8 | 239.2 | 103.4 |
| 9765 | ok | 0.09 | 0.1 | 1.71e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -49.8 | -17.8 | -25.1 | 72.8 | 197.0 | 92.3 |
| 9766 | ok | 0.09 | 0.1 | 2.08e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -66.1 | -13.4 | -48.8 | 46.1 | 51.1 | 135.2 |
| 9767 | ok | 0.09 | 0.2 | 3.65e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -81.2 | -58.3 | -96.6 | 52.3 | 155.3 | 128.1 |
| 9768 | ok | 0.09 | 0.2 | 1.55e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -53.1 | 19.7 | -23.1 | 4.6 | -54.6 | 129.9 |
| 9769 | ok | 0.09 | 0.2 | 1.65e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -57.8 | 6.6 | -33.1 | 42.8 | 62.6 | 128.2 |
| 9770 | ok | 0.09 | 0.1 | 1.96e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -62.7 | -8.5 | -46.6 | 43.7 | 69.9 | 125.6 |
| 9771 | ok | 0.09 | 0.2 | 3.52e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -78.7 | -51.9 | -94.5 | 48.5 | 157.1 | 112.9 |
| 9772 | ok | 0.09 | 0.2 | 1.41e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -43.1 | 32.7 | -35.6 | 27.3 | -82.7 | 117.5 |
| 9773 | ok | 0.09 | 0.2 | 1.51e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -44.4 | 15.4 | -37.5 | 20.6 | -49.8 | 141.3 |
| 9774 | ok | 0.09 | 0.1 | 1.72e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -54.2 | -8.1 | -38.1 | -44.0 | -114.4 | -168.4 |
| 9775 | ok | 0.09 | 0.1 | 2.87e-02 | 4.5 | 4.5 | 4.0 | 4.0 | -58.9 | -40.5 | -71.9 | 16.1 | 168.3 | -56.9 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | | | | | | | | -237.48 | -228.61 | -142.26 | -269.73 | -464.80 | -189.45 |
| | | 0.09 | 0.61 | 0.07 | 4.52 | 4.52 | 4.00 | 4.00 | 94.23 | 179.81 | 158.85 | 346.03 | 422.70 | 440.96 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 40 | ok | 1.14 | | | | | | |
| 43 | ok | 1.16 | | | | | | |
| 5886 | ok | 1.07 | | | | | | |
| 5887 | ok | 0.71 | | | | | | |
| 5888 | ok | 0.41 | | | | | | |
| 5894 | ok | 0.34 | | | | | | |
| 6002 | ok | 0.55 | | | | | | |
| 6004 | ok | 0.38 | | | | | | |
| 6005 | ok | 0.56 | | | | | | |
| 6006 | ok | 0.68 | | | | | | |
| 6007 | ok | 0.78 | | | | | | |
| 6008 | ok | 0.84 | | | | | | |
| 6009 | ok | 0.89 | | | | | | |
| 6010 | ok | 0.92 | | | | | | |
| 6011 | ok | 0.93 | | | | | | |
| 6012 | ok | 0.93 | | | | | | |
| 6013 | ok | 1.14 | | | | | | |
| 6014 | ok | 0.96 | | | | | | |
| 6015 | ok | 0.47 | | | | | | |
| 6017 | ok | 0.29 | | | | | | |
| 6019 | ok | 0.40 | | | | | | |
| 6021 | ok | 0.49 | | | | | | |
| 6023 | ok | 0.57 | | | | | | |
| 6025 | ok | 0.63 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 6027 | ok | 0.68 | | | | | | |
| 6029 | ok | 0.73 | | | | | | |
| 6031 | ok | 0.76 | | | | | | |
| 6033 | ok | 0.79 | | | | | | |
| 6035 | ok | 0.82 | | | | | | |
| 6037 | ok | 0.85 | | | | | | |
| 6039 | ok | 0.87 | | | | | | |
| 6041 | ok | 0.89 | | | | | | |
| 6043 | ok | 0.91 | | | | | | |
| 6045 | ok | 0.92 | | | | | | |
| 6047 | ok | 0.92 | | | | | | |
| 6049 | ok | 0.93 | | | | | | |
| 6051 | ok | 1.16 | | | | | | |
| 7341 | ok | 0.42 | | | | | | |
| 7342 | ok | 0.52 | | | | | | |
| 7599 | ok | 0.12 | | | | | | |
| 7600 | ok | 0.17 | | | | | | |
| 7601 | ok | 0.18 | | | | | | |
| 7602 | ok | 0.12 | | | | | | |
| 7603 | ok | 0.20 | | | | | | |
| 7604 | ok | 0.24 | | | | | | |
| 7605 | ok | 0.29 | | | | | | |
| 7606 | ok | 0.33 | | | | | | |
| 7607 | ok | 0.37 | | | | | | |
| 7608 | ok | 0.40 | | | | | | |
| 7609 | ok | 0.42 | | | | | | |
| 7610 | ok | 0.42 | | | | | | |
| 7611 | ok | 0.42 | | | | | | |
| 7612 | ok | 0.42 | | | | | | |
| 7613 | ok | 0.42 | | | | | | |
| 7614 | ok | 0.10 | | | | | | |
| 7615 | ok | 0.09 | | | | | | |
| 7616 | ok | 0.12 | | | | | | |
| 7617 | ok | 0.16 | | | | | | |
| 7618 | ok | 0.20 | | | | | | |
| 7619 | ok | 0.25 | | | | | | |
| 7620 | ok | 0.30 | | | | | | |
| 7621 | ok | 0.35 | | | | | | |
| 7622 | ok | 0.39 | | | | | | |
| 7623 | ok | 0.42 | | | | | | |
| 7624 | ok | 0.46 | | | | | | |
| 7625 | ok | 0.48 | | | | | | |
| 7626 | ok | 0.50 | | | | | | |
| 7627 | ok | 0.52 | | | | | | |
| 7628 | ok | 0.52 | | | | | | |
| 7629 | ok | 0.52 | | | | | | |
| 7630 | ok | 0.52 | | | | | | |
| 7631 | ok | 0.51 | | | | | | |
| 7632 | ok | 0.50 | | | | | | |
| 7633 | ok | 0.52 | | | | | | |
| 8261 | ok | 0.47 | | | | | | |
| 8262 | ok | 1.03 | | | | | | |
| 8263 | ok | 0.63 | | | | | | |
| 8264 | ok | 0.53 | | | | | | |
| 8688 | ok | 0.56 | | | | | | |
| 8689 | ok | 1.16 | | | | | | |
| 8690 | ok | 0.73 | | | | | | |
| 8691 | ok | 0.62 | | | | | | |
| 9492 | ok | 1.03 | | | | | | |
| 9493 | ok | 0.63 | | | | | | |
| 9494 | ok | 0.53 | | | | | | |
| 9495 | ok | 0.47 | | | | | | |
| 9496 | ok | 0.82 | | | | | | |
| 9497 | ok | 0.38 | | | | | | |
| 9498 | ok | 0.30 | | | | | | |
| 9499 | ok | 0.28 | | | | | | |
| 9500 | ok | 0.73 | | | | | | |
| 9501 | ok | 0.27 | | | | | | |
| 9502 | ok | 0.19 | | | | | | |
| 9503 | ok | 0.20 | | | | | | |
| 9504 | ok | 0.68 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 9505 | ok | 0.20 | | | | | | |
| 9506 | ok | 0.12 | | | | | | |
| 9507 | ok | 0.14 | | | | | | |
| 9508 | ok | 0.63 | | | | | | |
| 9509 | ok | 0.15 | | | | | | |
| 9510 | ok | 0.07 | | | | | | |
| 9511 | ok | 0.10 | | | | | | |
| 9512 | ok | 0.58 | | | | | | |
| 9513 | ok | 0.12 | | | | | | |
| 9514 | ok | 0.04 | | | | | | |
| 9515 | ok | 0.07 | | | | | | |
| 9516 | ok | 0.53 | | | | | | |
| 9517 | ok | 0.10 | | | | | | |
| 9518 | ok | 0.03 | | | | | | |
| 9519 | ok | 0.05 | | | | | | |
| 9520 | ok | 0.48 | | | | | | |
| 9521 | ok | 0.08 | | | | | | |
| 9522 | ok | 0.04 | | | | | | |
| 9523 | ok | 0.05 | | | | | | |
| 9524 | ok | 0.41 | | | | | | |
| 9525 | ok | 0.07 | | | | | | |
| 9526 | ok | 0.04 | | | | | | |
| 9527 | ok | 0.05 | | | | | | |
| 9528 | ok | 0.33 | | | | | | |
| 9529 | ok | 0.06 | | | | | | |
| 9530 | ok | 0.05 | | | | | | |
| 9531 | ok | 0.05 | | | | | | |
| 9532 | ok | 0.21 | | | | | | |
| 9533 | ok | 0.07 | | | | | | |
| 9534 | ok | 0.06 | | | | | | |
| 9535 | ok | 0.06 | | | | | | |
| 9536 | ok | 0.21 | | | | | | |
| 9537 | ok | 0.11 | | | | | | |
| 9538 | ok | 0.09 | | | | | | |
| 9539 | ok | 0.08 | | | | | | |
| 9540 | ok | 0.21 | | | | | | |
| 9541 | ok | 0.71 | | | | | | |
| 9542 | ok | 0.11 | | | | | | |
| 9543 | ok | 0.09 | | | | | | |
| 9544 | ok | 0.08 | | | | | | |
| 9545 | ok | 0.15 | | | | | | |
| 9546 | ok | 0.14 | | | | | | |
| 9547 | ok | 0.47 | | | | | | |
| 9548 | ok | 0.11 | | | | | | |
| 9549 | ok | 0.09 | | | | | | |
| 9550 | ok | 0.09 | | | | | | |
| 9551 | ok | 0.13 | | | | | | |
| 9552 | ok | 0.10 | | | | | | |
| 9553 | ok | 0.32 | | | | | | |
| 9554 | ok | 0.10 | | | | | | |
| 9555 | ok | 0.09 | | | | | | |
| 9556 | ok | 0.09 | | | | | | |
| 9557 | ok | 0.12 | | | | | | |
| 9558 | ok | 0.09 | | | | | | |
| 9559 | ok | 0.24 | | | | | | |
| 9560 | ok | 0.09 | | | | | | |
| 9561 | ok | 0.09 | | | | | | |
| 9562 | ok | 0.08 | | | | | | |
| 9563 | ok | 0.11 | | | | | | |
| 9564 | ok | 0.14 | | | | | | |
| 9565 | ok | 0.19 | | | | | | |
| 9566 | ok | 0.08 | | | | | | |
| 9567 | ok | 0.08 | | | | | | |
| 9568 | ok | 0.08 | | | | | | |
| 9569 | ok | 0.11 | | | | | | |
| 9570 | ok | 0.19 | | | | | | |
| 9571 | ok | 0.19 | | | | | | |
| 9572 | ok | 0.08 | | | | | | |
| 9573 | ok | 0.08 | | | | | | |
| 9574 | ok | 0.08 | | | | | | |
| 9575 | ok | 0.11 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 9576 | ok | 0.25 | | | | | | |
| 9577 | ok | 0.25 | | | | | | |
| 9578 | ok | 0.10 | | | | | | |
| 9579 | ok | 0.09 | | | | | | |
| 9580 | ok | 0.08 | | | | | | |
| 9581 | ok | 0.11 | | | | | | |
| 9582 | ok | 0.32 | | | | | | |
| 9583 | ok | 0.32 | | | | | | |
| 9584 | ok | 0.10 | | | | | | |
| 9585 | ok | 0.09 | | | | | | |
| 9586 | ok | 0.08 | | | | | | |
| 9587 | ok | 0.12 | | | | | | |
| 9588 | ok | 0.32 | | | | | | |
| 9589 | ok | 0.34 | | | | | | |
| 9590 | ok | 0.10 | | | | | | |
| 9591 | ok | 0.09 | | | | | | |
| 9592 | ok | 0.08 | | | | | | |
| 9593 | ok | 0.12 | | | | | | |
| 9594 | ok | 0.26 | | | | | | |
| 9595 | ok | 0.08 | | | | | | |
| 9596 | ok | 0.08 | | | | | | |
| 9597 | ok | 0.08 | | | | | | |
| 9598 | ok | 0.15 | | | | | | |
| 9599 | ok | 0.30 | | | | | | |
| 9600 | ok | 0.09 | | | | | | |
| 9601 | ok | 0.08 | | | | | | |
| 9602 | ok | 0.08 | | | | | | |
| 9603 | ok | 0.13 | | | | | | |
| 9604 | ok | 0.12 | | | | | | |
| 9605 | ok | 0.20 | | | | | | |
| 9606 | ok | 0.09 | | | | | | |
| 9607 | ok | 0.08 | | | | | | |
| 9608 | ok | 0.08 | | | | | | |
| 9609 | ok | 0.13 | | | | | | |
| 9610 | ok | 0.08 | | | | | | |
| 9611 | ok | 0.16 | | | | | | |
| 9612 | ok | 0.08 | | | | | | |
| 9613 | ok | 0.08 | | | | | | |
| 9614 | ok | 0.08 | | | | | | |
| 9615 | ok | 0.14 | | | | | | |
| 9616 | ok | 0.12 | | | | | | |
| 9617 | ok | 0.20 | | | | | | |
| 9618 | ok | 0.08 | | | | | | |
| 9619 | ok | 0.08 | | | | | | |
| 9620 | ok | 0.08 | | | | | | |
| 9621 | ok | 0.15 | | | | | | |
| 9622 | ok | 0.19 | | | | | | |
| 9623 | ok | 0.24 | | | | | | |
| 9624 | ok | 0.09 | | | | | | |
| 9625 | ok | 0.09 | | | | | | |
| 9626 | ok | 0.08 | | | | | | |
| 9627 | ok | 0.15 | | | | | | |
| 9628 | ok | 0.27 | | | | | | |
| 9629 | ok | 0.33 | | | | | | |
| 9630 | ok | 0.10 | | | | | | |
| 9631 | ok | 0.09 | | | | | | |
| 9632 | ok | 0.09 | | | | | | |
| 9633 | ok | 0.16 | | | | | | |
| 9634 | ok | 0.27 | | | | | | |
| 9635 | ok | 0.41 | | | | | | |
| 9636 | ok | 0.10 | | | | | | |
| 9637 | ok | 0.09 | | | | | | |
| 9638 | ok | 0.09 | | | | | | |
| 9639 | ok | 0.17 | | | | | | |
| 9640 | ok | 0.27 | | | | | | |
| 9641 | ok | 0.09 | | | | | | |
| 9642 | ok | 0.09 | | | | | | |
| 9643 | ok | 0.09 | | | | | | |
| 9644 | ok | 0.19 | | | | | | |
| 9645 | ok | 0.20 | | | | | | |
| 9646 | ok | 0.10 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 9647 | ok | 0.10 | | | | | | |
| 9648 | ok | 0.09 | | | | | | |
| 9649 | ok | 0.18 | | | | | | |
| 9650 | ok | 0.15 | | | | | | |
| 9651 | ok | 0.27 | | | | | | |
| 9652 | ok | 0.10 | | | | | | |
| 9653 | ok | 0.10 | | | | | | |
| 9654 | ok | 0.09 | | | | | | |
| 9655 | ok | 0.19 | | | | | | |
| 9656 | ok | 0.12 | | | | | | |
| 9657 | ok | 0.40 | | | | | | |
| 9658 | ok | 0.10 | | | | | | |
| 9659 | ok | 0.10 | | | | | | |
| 9660 | ok | 0.10 | | | | | | |
| 9661 | ok | 0.19 | | | | | | |
| 9662 | ok | 0.10 | | | | | | |
| 9663 | ok | 0.33 | | | | | | |
| 9664 | ok | 0.10 | | | | | | |
| 9665 | ok | 0.10 | | | | | | |
| 9666 | ok | 0.09 | | | | | | |
| 9667 | ok | 0.19 | | | | | | |
| 9668 | ok | 0.19 | | | | | | |
| 9669 | ok | 0.48 | | | | | | |
| 9670 | ok | 0.11 | | | | | | |
| 9671 | ok | 0.11 | | | | | | |
| 9672 | ok | 0.10 | | | | | | |
| 9673 | ok | 0.18 | | | | | | |
| 9674 | ok | 0.27 | | | | | | |
| 9675 | ok | 0.59 | | | | | | |
| 9676 | ok | 0.13 | | | | | | |
| 9677 | ok | 0.12 | | | | | | |
| 9678 | ok | 0.11 | | | | | | |
| 9679 | ok | 0.18 | | | | | | |
| 9680 | ok | 0.39 | | | | | | |
| 9681 | ok | 0.78 | | | | | | |
| 9682 | ok | 0.15 | | | | | | |
| 9683 | ok | 0.12 | | | | | | |
| 9684 | ok | 0.11 | | | | | | |
| 9685 | ok | 0.16 | | | | | | |
| 9686 | ok | 0.46 | | | | | | |
| 9687 | ok | 1.07 | | | | | | |
| 9688 | ok | 0.15 | | | | | | |
| 9689 | ok | 0.12 | | | | | | |
| 9690 | ok | 0.11 | | | | | | |
| 9691 | ok | 0.15 | | | | | | |
| 9692 | ok | 0.46 | | | | | | |
| 9693 | ok | 0.14 | | | | | | |
| 9694 | ok | 0.12 | | | | | | |
| 9695 | ok | 0.11 | | | | | | |
| 9696 | ok | 0.27 | | | | | | |
| 9697 | ok | 0.10 | | | | | | |
| 9698 | ok | 0.10 | | | | | | |
| 9699 | ok | 0.10 | | | | | | |
| 9700 | ok | 0.15 | | | | | | |
| 9701 | ok | 0.07 | | | | | | |
| 9702 | ok | 0.09 | | | | | | |
| 9703 | ok | 0.09 | | | | | | |
| 9704 | ok | 0.20 | | | | | | |
| 9705 | ok | 0.07 | | | | | | |
| 9706 | ok | 0.08 | | | | | | |
| 9707 | ok | 0.08 | | | | | | |
| 9708 | ok | 0.26 | | | | | | |
| 9709 | ok | 0.08 | | | | | | |
| 9710 | ok | 0.08 | | | | | | |
| 9711 | ok | 0.08 | | | | | | |
| 9712 | ok | 0.32 | | | | | | |
| 9713 | ok | 0.08 | | | | | | |
| 9714 | ok | 0.08 | | | | | | |
| 9715 | ok | 0.08 | | | | | | |
| 9716 | ok | 0.37 | | | | | | |
| 9717 | ok | 0.09 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------------|-------|----------------|-----------------|------------------|----------------|-----------------|-------------|--------------|
| 9718 | ok | 0.08 | | | | | | |
| 9719 | ok | 0.08 | | | | | | |
| 9720 | ok | 0.41 | | | | | | |
| 9721 | ok | 0.09 | | | | | | |
| 9722 | ok | 0.08 | | | | | | |
| 9723 | ok | 0.08 | | | | | | |
| 9724 | ok | 0.44 | | | | | | |
| 9725 | ok | 0.09 | | | | | | |
| 9726 | ok | 0.08 | | | | | | |
| 9727 | ok | 0.08 | | | | | | |
| 9728 | ok | 0.47 | | | | | | |
| 9729 | ok | 0.09 | | | | | | |
| 9730 | ok | 0.08 | | | | | | |
| 9731 | ok | 0.08 | | | | | | |
| 9732 | ok | 0.51 | | | | | | |
| 9733 | ok | 0.09 | | | | | | |
| 9734 | ok | 0.07 | | | | | | |
| 9735 | ok | 0.07 | | | | | | |
| 9736 | ok | 0.54 | | | | | | |
| 9737 | ok | 0.09 | | | | | | |
| 9738 | ok | 0.06 | | | | | | |
| 9739 | ok | 0.06 | | | | | | |
| 9740 | ok | 0.57 | | | | | | |
| 9741 | ok | 0.09 | | | | | | |
| 9742 | ok | 0.05 | | | | | | |
| 9743 | ok | 0.07 | | | | | | |
| 9744 | ok | 0.61 | | | | | | |
| 9745 | ok | 0.10 | | | | | | |
| 9746 | ok | 0.04 | | | | | | |
| 9747 | ok | 0.07 | | | | | | |
| 9748 | ok | 0.64 | | | | | | |
| 9749 | ok | 0.12 | | | | | | |
| 9750 | ok | 0.03 | | | | | | |
| 9751 | ok | 0.09 | | | | | | |
| 9752 | ok | 0.68 | | | | | | |
| 9753 | ok | 0.15 | | | | | | |
| 9754 | ok | 0.05 | | | | | | |
| 9755 | ok | 0.11 | | | | | | |
| 9756 | ok | 0.73 | | | | | | |
| 9757 | ok | 0.19 | | | | | | |
| 9758 | ok | 0.10 | | | | | | |
| 9759 | ok | 0.14 | | | | | | |
| 9760 | ok | 0.78 | | | | | | |
| 9761 | ok | 0.24 | | | | | | |
| 9762 | ok | 0.16 | | | | | | |
| 9763 | ok | 0.19 | | | | | | |
| 9764 | ok | 0.84 | | | | | | |
| 9765 | ok | 0.33 | | | | | | |
| 9766 | ok | 0.24 | | | | | | |
| 9767 | ok | 0.27 | | | | | | |
| 9768 | ok | 0.93 | | | | | | |
| 9769 | ok | 0.46 | | | | | | |
| 9770 | ok | 0.36 | | | | | | |
| 9771 | ok | 0.36 | | | | | | |
| 9772 | ok | 1.16 | | | | | | |
| 9773 | ok | 0.73 | | | | | | |
| 9774 | ok | 0.62 | | | | | | |
| 9775 | ok | 0.56 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 1.16 | | | | | | |

1.1.1.1.7 Verifica Macrosetti sp. 25 cm

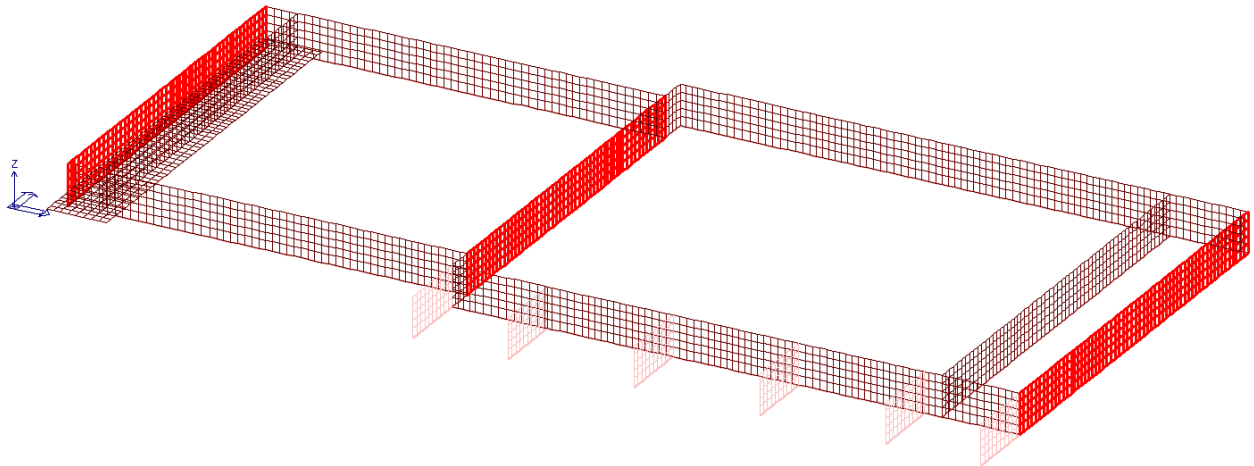


Fig 174. Individuazione del Macrosetto/i oggetto di Verifica (Selezione in rosso).

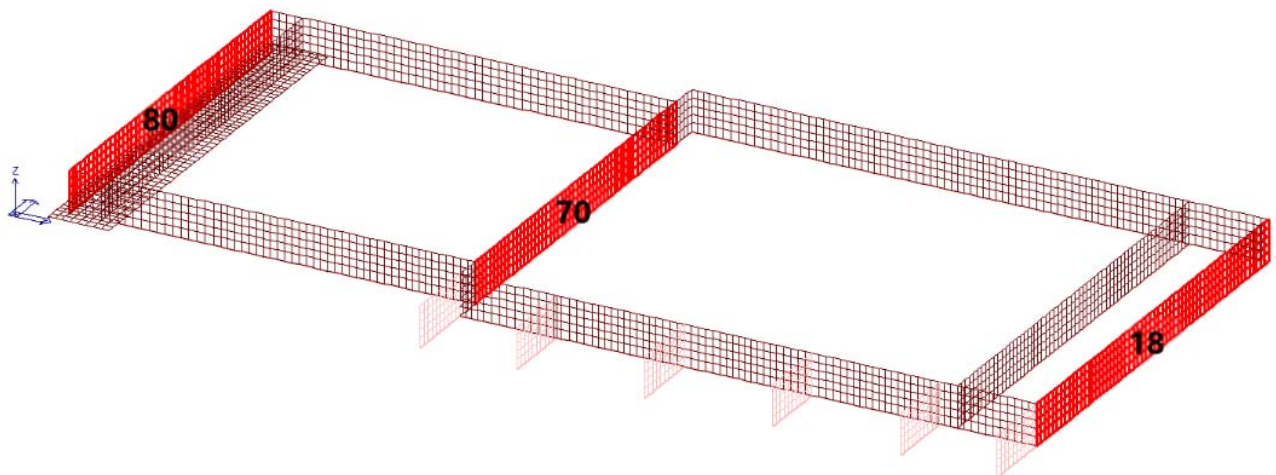


Fig 175. Numerazione Macrosetto oggetto di verifica.

Si riporta il tabulato di verifica completo.

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 18 | 25.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|-------|-------|-------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 2766 | ok | 0.16 | 0.1 | 3.56e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -38.5 | -21.5 | -74.6 | 0.2 | -1.7 | 3.2 |
| 6852 | ok | 0.18 | 1.0 | 0.2 | 5.0 | 5.1 | 4.7 | 4.7 | -441.9 | 331.3 | -118.3 | 122.3 | -10.1 | 44.0 |
| 6943 | ok | 0.16 | 0.2 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -184.0 | -291.5 | 166.0 | -11.6 | 10.0 | 18.6 |
| 7043 | ok | 0.16 | 0.2 | 6.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -112.0 | 2.4 | 112.1 | 14.7 | 266.1 | -19.3 |
| 7236 | ok | 0.16 | 0.4 | 2.21e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 86.8 | -23.8 | -38.0 | 3.3 | 7.1 | -1.2 |
| 7245 | ok | 0.16 | 0.1 | 5.98e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -69.9 | -82.0 | 99.9 | -7.2 | -12.5 | 9.8 |
| 7247 | ok | 0.16 | 0.1 | 5.35e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 7.9 | -1.5 | -3.1 | 0.3 | -8.6 | 3.0 |
| 7248 | ok | 0.16 | 9.02e-02 | 1.53e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -13.7 | -20.9 | 27.3 | -2.5 | -8.7 | 10.2 |
| 7249 | ok | 0.16 | 0.1 | 8.55e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 21.7 | 3.1 | 3.7 | 22.1 | 18.8 |
| 7250 | ok | 0.16 | 9.51e-02 | 7.48e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.0 | -5.2 | 12.2 | -3.2 | -11.6 | -11.9 |
| 7251 | ok | 0.16 | 0.2 | 3.43e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.4 | 33.8 | 3.2 | 3.5 | 17.3 | 24.3 |
| 7252 | ok | 0.16 | 0.1 | 4.13e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.6 | 17.9 | 12.9 | 9.3 | 15.2 | 33.3 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|----------|----------|--------|
| 7260 | ok | 0.16 | 0.2 | 5.98e-04 | 4.5 | 4.5 | 3.1 | 3.1 | 0.4 | 47.4 | 4.3 | 4.4 | 15.6 | 29.2 |
| 7261 | ok | 0.16 | 0.1 | 2.72e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 22.0 | 10.4 | 12.9 | 17.2 | 35.5 |
| 7270 | ok | 0.16 | 0.3 | 2.18e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 2.8 | 67.9 | 9.1 | -7.4 | -15.8 | -29.3 |
| 7271 | ok | 0.16 | 0.2 | 3.31e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 7.3 | 32.9 | 16.0 | 17.6 | 13.1 | 45.7 |
| 7272 | ok | 0.16 | 0.5 | 8.75e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 13.4 | 111.1 | 20.7 | -11.0 | -21.8 | -40.7 |
| 7273 | ok | 0.16 | 0.2 | 6.01e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 6.4 | 32.2 | 13.1 | 28.9 | 16.0 | 49.6 |
| 7274 | ok | 0.16 | 1.0 | 3.11e-02 | 4.7 | 4.5 | 3.3 | 3.1 | -0.4 | 125.0 | 19.0 | -30.2 | -25.1 | -46.7 |
| 7275 | ok | 0.16 | 0.2 | 2.18e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -56.0 | 33.8 | -56.8 | 30.3 | 11.6 | 60.1 |
| 7276 | ok | 0.20 | 1.0 | 5.31e-02 | 6.6 | 6.3 | 5.2 | 5.0 | 206.5 | 244.7 | 191.8 | -61.7 | -14.6 | -16.3 |
| 7277 | ok | 0.16 | 0.3 | 5.25e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -92.1 | -62.9 | -52.8 | -103.2 | -2.7 | -33.2 |
| 7278 | ok | 0.16 | 0.2 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -357.5 | -308.6 | -11.3 | 16.3 | 11.6 | -1.2 |
| 7281 | ok | 0.16 | 0.1 | 2.59e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -52.6 | -0.6 | 40.8 | -7.2 | -12.5 | 8.0 |
| 7282 | ok | 0.16 | 9.73e-02 | 2.20e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -49.5 | 5.4 | 27.3 | -7.9 | -13.9 | 8.0 |
| 7284 | ok | 0.16 | 7.91e-02 | 2.82e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -50.1 | 14.2 | -13.4 | -22.7 | -17.9 | -8.3 |
| 7289 | ok | 0.16 | 0.1 | 1.95e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.4 | -9.3 | 37.0 | -5.8 | -8.9 | 8.6 |
| 7290 | ok | 0.16 | 9.13e-02 | 1.31e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -15.9 | -5.1 | 24.3 | -4.5 | -7.2 | 7.9 |
| 7291 | ok | 0.16 | 9.05e-02 | 9.24e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.1 | -1.6 | 18.0 | -3.3 | -5.4 | 7.0 |
| 7292 | ok | 0.16 | 9.35e-02 | 6.75e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.8 | 6.7 | 12.0 | 11.1 | 10.2 | 33.9 |
| 7293 | ok | 0.16 | 9.12e-02 | 5.01e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.8 | -5.2 | -4.5 | -17.0 | -11.0 | -33.5 |
| 7294 | ok | 0.16 | 9.15e-02 | 8.98e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -26.5 | 8.8 | -18.4 | 30.8 | 4.7 | 40.9 |
| 7296 | ok | 0.16 | 6.88e-02 | 1.62e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.8 | 0.7 | -27.5 | 48.3 | 6.0 | 42.3 |
| 7301 | ok | 0.16 | 0.1 | 4.66e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -129.3 | 1.9 | -79.4 | -106.1 | -3.1 | -31.0 |
| 7302 | ok | 0.16 | 0.3 | 5.07e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -138.9 | -12.3 | -32.7 | -118.1 | -4.9 | -30.8 |
| 7303 | ok | 0.16 | 8.42e-02 | 1.95e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.4 | -0.6 | 29.6 | -8.4 | -9.6 | 8.1 |
| 7355 | ok | 0.16 | 7.98e-02 | 1.62e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -24.6 | -2.4 | 22.0 | -7.8 | -7.4 | 6.5 |
| 7415 | ok | 0.16 | 6.99e-02 | 1.31e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -18.0 | -4.3 | 16.6 | -5.7 | -5.2 | 5.4 |
| 7419 | ok | 0.16 | 6.04e-02 | 1.04e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -15.3 | -6.6 | 9.9 | -3.4 | -3.5 | 4.6 |
| 7467 | ok | 0.16 | 4.15e-02 | 8.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -17.1 | -12.1 | 9.3 | -0.9 | -1.4 | 4.1 |
| 7468 | ok | 0.16 | 2.37e-02 | 1.03e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -23.4 | -14.6 | -10.2 | 0.8 | -1.2 | 3.5 |
| 7530 | ok | 0.16 | 3.48e-02 | 1.89e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -42.6 | -15.4 | -23.7 | 2.5 | -0.3 | 3.0 |
| 7532 | ok | 0.16 | 4.27e-02 | 2.90e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -84.3 | -5.0 | -26.8 | -72.8 | -4.4 | -16.4 |
| 7533 | ok | 0.16 | 7.21e-02 | 3.52e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -97.2 | -5.5 | -15.1 | -64.9 | -3.2 | -15.4 |
| 7534 | ok | 0.16 | 6.91e-02 | 2.85e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -35.6 | 17.8 | -3.1 | -21.7 | -11.4 | -6.4 |
| 7535 | ok | 0.16 | 8.04e-02 | 2.68e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -27.5 | 15.8 | -2.1 | -15.7 | -8.7 | -3.5 |
| 7536 | ok | 0.16 | 8.28e-02 | 2.38e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -30.8 | -23.1 | 43.0 | -4.9 | 0.3 | 7.4 |
| 7537 | ok | 0.16 | 7.82e-02 | 2.07e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.5 | -17.6 | 37.2 | -2.2 | 0.4 | 4.2 |
| 7538 | ok | 0.16 | 7.19e-02 | 1.88e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -32.7 | -12.3 | 31.7 | 6.77e-02 | 0.5 | 1.9 |
| 7574 | ok | 0.16 | 7.67e-02 | 2.14e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -33.9 | -15.8 | -37.2 | -0.3 | -1.5 | 2.9 |
| 7639 | ok | 0.16 | 0.2 | 3.76e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -60.5 | -1.5 | 74.8 | 6.9 | 1.7 | -7.2 |
| 7643 | ok | 0.16 | 0.2 | 3.10e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -67.7 | 14.1 | 44.0 | -83.8 | -45.2 | 81.6 |
| 7648 | ok | 0.16 | 0.2 | 3.14e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -87.0 | 48.9 | -31.8 | -149.7 | -118.9 | -144.5 |
| 7915 | ok | 0.16 | 0.3 | 4.14e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -93.9 | -2.9 | -33.7 | -16.5 | -43.4 | 13.1 |
| 7916 | ok | 0.16 | 0.2 | 2.80e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -70.1 | 10.2 | -32.1 | 7.5 | 55.3 | 0.8 |
| 7917 | ok | 0.16 | 0.1 | 2.46e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -56.1 | 9.3 | -29.7 | 10.5 | 52.8 | 6.0 |
| 7918 | ok | 0.16 | 0.1 | 3.13e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -49.3 | -7.4 | -60.4 | 10.4 | 43.7 | -22.3 |
| 8323 | ok | 0.16 | 8.16e-02 | 2.90e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -48.6 | -18.1 | -50.1 | 1.9 | -0.3 | 3.8 |
| 8324 | ok | 0.16 | 8.26e-02 | 3.44e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -68.2 | -14.8 | -54.6 | 3.2 | 0.6 | 4.4 |
| 8325 | ok | 0.16 | 5.37e-02 | 3.23e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -83.3 | -13.6 | -32.8 | 3.9 | 7.95e-02 | 3.3 |
| 8346 | ok | 0.16 | 0.2 | 4.41e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -49.5 | -25.7 | -91.7 | 3.0 | 0.4 | 6.0 |
| 8369 | ok | 0.16 | 0.2 | 5.53e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -155.1 | 8.6 | 42.5 | -16.5 | -34.8 | -44.2 |
| 8370 | ok | 0.16 | 0.1 | 5.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -126.1 | 3.0 | 62.8 | -14.7 | 17.3 | -23.7 |
| 8371 | ok | 0.16 | 0.1 | 4.63e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -104.3 | -7.0 | 66.2 | -11.9 | 36.6 | -18.7 |
| 8372 | ok | 0.16 | 0.1 | 5.50e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -83.2 | -37.8 | 99.7 | 13.0 | 96.8 | 39.9 |
| 8452 | ok | 0.16 | 0.2 | 4.98e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -64.5 | -26.5 | -100.1 | 5.2 | 1.4 | 7.7 |
| 8457 | ok | 0.16 | 0.1 | 3.69e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.2 | 25.5 | -33.4 | -55.7 | -7.7 | -34.1 |
| 8462 | ok | 0.16 | 0.1 | 3.92e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.2 | 33.0 | -26.2 | -33.5 | -8.6 | -23.3 |
| 8467 | ok | 0.16 | 0.1 | 3.84e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -28.7 | 29.5 | -26.6 | -20.6 | -8.3 | -15.3 |
| 8472 | ok | 0.16 | 0.1 | 3.52e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -41.9 | -35.6 | 64.9 | -0.5 | 3.2 | 9.2 |
| 8477 | ok | 0.16 | 0.1 | 3.14e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -42.5 | -25.6 | 58.2 | 1.7 | 2.6 | 3.9 |
| 8627 | ok | 0.16 | 0.1 | 2.90e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -46.2 | -14.1 | 53.4 | 3.7 | 2.0 | 0.2 |
| 9940 | ok | 0.16 | 0.2 | 3.69e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 50.5 | -0.9 | 9.45e-02 | -3.6 | 1.7 |
| 9941 | ok | 0.16 | 0.2 | 3.50e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 47.1 | 1.0 | 1.28e-02 | -0.2 | 0.7 |
| 9942 | ok | 0.16 | 9.02e-02 | 3.69e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 24.5 | 1.0 | 3.52e-02 | -1.6 | 0.6 |
| 9943 | ok | 0.16 | 9.30e-02 | 3.78e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 27.6 | -0.9 | 2.28e-02 | -0.8 | 0.3 |
| 9966 | ok | 0.16 | 0.2 | 3.41e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 49.0 | 1.0 | 2.30e-02 | -0.6 | 0.6 |
| 9967 | ok | 0.16 | 0.2 | 3.36e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 50.4 | 1.0 | 3.66e-02 | -1.2 | 0.5 |
| 9968 | ok | 0.16 | 0.2 | 3.35e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 51.7 | 1.6 | -1.0 | -3.0 | -0.4 |
| 9969 | ok | 0.16 | 0.2 | 4.43e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.7 | 52.9 | 1.6 | -1.1 | -2.2 | -0.8 |
| 9970 | ok | 0.16 | 0.2 | 1.25e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.4 | 54.0 | 2.5 | 0.2 | -7.4 | 7.8 |
| 9971 | ok | 0.16 | 0.2 | 2.85e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 1.3 | 56.4 | 4.2 | 7.97e-02 | -14.4 | 1.3 |
| 9972 | ok | 0.16 | 0.3 | 8.05e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 1.2 | 69.6 | 10.7 | 0.1 | -26.4 | 1.8 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|--------|--------|--------|
| 9973 | ok | 0.16 | 0.7 | 4.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -88.5 | -106.3 | -56.5 | 11.9 | 108.6 | -0.1 |
| 9974 | ok | 0.17 | 0.9 | 3.25e-02 | 4.8 | 4.7 | 3.4 | 3.4 | 145.0 | 187.0 | 110.2 | -37.8 | -9.5 | -26.4 |
| 9975 | ok | 0.16 | 0.3 | 3.01e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -32.6 | -23.0 | -16.7 | -128.5 | -12.7 | 62.4 |
| 9976 | ok | 0.16 | 0.3 | 4.83e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 1.4 | 28.2 | 67.1 | -105.3 | -109.2 | 106.9 |
| 9977 | ok | 0.16 | 0.2 | 3.61e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 54.8 | -1.0 | 0.1 | -4.2 | 1.9 |
| 9978 | ok | 0.16 | 0.2 | 3.58e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 59.9 | -1.0 | 0.1 | -4.9 | 2.2 |
| 9979 | ok | 0.16 | 0.2 | 3.53e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 65.3 | -1.0 | 0.2 | -5.7 | 2.5 |
| 9980 | ok | 0.16 | 0.2 | 3.51e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 71.0 | -1.0 | 0.2 | -6.7 | 2.9 |
| 9981 | ok | 0.16 | 0.3 | 3.48e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 77.0 | -1.0 | 0.2 | -7.7 | 3.3 |
| 9982 | ok | 0.16 | 0.3 | 3.45e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 83.2 | -1.1 | 0.3 | -8.7 | 3.8 |
| 9983 | ok | 0.16 | 0.3 | 3.41e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 89.4 | -1.1 | 0.3 | -9.7 | 4.4 |
| 9984 | ok | 0.16 | 0.3 | 3.36e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 95.6 | -1.0 | 0.4 | -10.5 | 5.1 |
| 9985 | ok | 0.16 | 0.4 | 3.32e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 101.5 | -1.0 | 0.4 | -10.8 | 5.8 |
| 9986 | ok | 0.16 | 0.4 | 3.29e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 106.9 | -1.0 | 0.5 | -10.3 | 6.6 |
| 9987 | ok | 0.16 | 0.4 | 3.28e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 111.7 | -1.0 | 0.5 | -8.3 | 7.4 |
| 9988 | ok | 0.16 | 0.4 | 3.35e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 115.7 | 0.9 | 0.6 | -3.9 | 8.1 |
| 9989 | ok | 0.16 | 0.4 | 3.66e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 119.2 | 1.0 | 0.7 | 4.1 | 8.8 |
| 9990 | ok | 0.16 | 0.4 | 5.79e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.2 | 122.8 | 1.2 | 0.8 | 17.9 | 9.2 |
| 9991 | ok | 0.16 | 0.5 | 2.12e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.5 | 128.4 | 1.4 | 1.1 | 41.0 | 9.3 |
| 9992 | ok | 0.16 | 0.6 | 1.11e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 142.8 | 1.0 | 2.2 | 81.6 | 8.2 |
| 9993 | ok | 0.16 | 1.0 | 5.46e-02 | 4.5 | 4.7 | 3.1 | 3.9 | -148.1 | 171.0 | 45.0 | -48.9 | 128.1 | 41.2 |
| 9995 | ok | 0.26 | 0.6 | 1.36e-02 | 7.8 | 10.0 | 8.5 | 12.8 | 342.5 | 503.1 | -282.2 | 143.1 | 523.0 | -177.8 |
| 9997 | ok | 0.16 | 0.4 | 3.29e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 31.9 | 69.0 | 26.9 | -24.1 | 60.9 | -163.9 |
| 9999 | ok | 0.16 | 0.4 | 5.01e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 4.6 | 113.6 | -75.4 | -41.3 | -81.5 | -110.1 |
| 10090 | ok | 0.16 | 6.30e-02 | 1.16e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -1.2 | 25.6 | -6.3 | -6.2 | -8.2 | 10.7 |
| 10091 | ok | 0.16 | 6.50e-02 | 1.10e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -8.8 | 10.2 | -12.4 | 2.5 | 7.6 | 4.6 |
| 10092 | ok | 0.16 | 3.54e-02 | 6.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.5 | 8.9 | 6.4 | -1.2 | -2.8 | 2.4 |
| 10093 | ok | 0.16 | 3.64e-02 | 6.73e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.0 | 9.1 | -6.0 | 1.3 | 4.8 | 3.4 |
| 10094 | ok | 0.16 | 7.14e-02 | 1.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -10.3 | 8.6 | -14.9 | 2.5 | 7.9 | 4.3 |
| 10095 | ok | 0.16 | 7.86e-02 | 1.16e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -12.8 | -4.5 | -27.5 | -12.3 | 0.2 | -5.5 |
| 10096 | ok | 0.16 | 8.70e-02 | 1.33e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -14.4 | -8.1 | -30.5 | -15.7 | -0.3 | -6.5 |
| 10097 | ok | 0.16 | 9.86e-02 | 1.54e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -17.0 | -11.9 | -33.4 | -19.8 | -0.8 | -7.7 |
| 10098 | ok | 0.16 | 0.1 | 1.77e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -21.2 | -16.6 | -35.6 | -24.3 | -1.2 | -7.3 |
| 10099 | ok | 0.16 | 0.1 | 2.03e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -16.0 | 18.2 | 13.5 | -43.3 | -14.6 | 48.1 |
| 10100 | ok | 0.16 | 0.1 | 2.35e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -16.8 | 22.4 | 12.2 | -19.4 | -10.7 | 20.4 |
| 10101 | ok | 0.16 | 0.1 | 2.73e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -24.6 | -39.1 | -47.9 | -36.8 | 18.3 | -37.7 |
| 10102 | ok | 0.16 | 0.1 | 3.31e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -8.3 | 46.4 | -9.3 | -31.3 | -19.9 | 29.2 |
| 10103 | ok | 0.16 | 0.2 | 3.79e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -12.9 | 52.5 | -9.6 | -45.1 | -21.4 | 39.9 |
| 10104 | ok | 0.16 | 0.1 | 3.95e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -14.5 | -55.1 | -78.3 | -29.0 | 31.5 | -52.2 |
| 10105 | ok | 0.16 | 7.05e-02 | 1.23e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 29.6 | -5.8 | -6.1 | -9.3 | 11.7 |
| 10106 | ok | 0.16 | 7.34e-02 | 1.30e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -0.7 | 31.0 | -6.2 | -7.2 | -10.0 | 13.6 |
| 10107 | ok | 0.16 | 7.55e-02 | 1.38e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 32.2 | -6.3 | -8.5 | -10.9 | 15.8 |
| 10108 | ok | 0.16 | 7.66e-02 | 1.46e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 33.2 | -6.1 | -10.0 | -11.8 | 18.6 |
| 10109 | ok | 0.16 | 7.66e-02 | 1.53e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -1.4 | 33.9 | -5.6 | -11.9 | -12.8 | 22.0 |
| 10110 | ok | 0.16 | 7.53e-02 | 1.60e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -2.0 | 34.3 | -4.7 | -14.3 | -13.9 | 26.2 |
| 10111 | ok | 0.16 | 7.51e-02 | 1.67e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -2.8 | 34.4 | -3.4 | -17.2 | -15.0 | 31.3 |
| 10112 | ok | 0.16 | 8.02e-02 | 1.74e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -3.9 | 34.0 | -1.5 | -20.9 | -16.2 | 37.6 |
| 10113 | ok | 0.16 | 8.55e-02 | 1.80e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -5.3 | 33.2 | 0.8 | -25.5 | -17.2 | 45.1 |
| 10114 | ok | 0.16 | 9.10e-02 | 1.84e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -7.3 | 31.7 | 3.5 | -31.1 | -18.0 | 54.1 |
| 10115 | ok | 0.16 | 9.63e-02 | 1.83e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -9.8 | 29.3 | 6.6 | -38.0 | -18.2 | 64.4 |
| 10116 | ok | 0.16 | 0.1 | 1.74e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -12.6 | 25.1 | 9.9 | -46.4 | -17.4 | 75.8 |
| 10117 | ok | 0.16 | 0.1 | 1.50e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -19.5 | -7.3 | -30.2 | -75.3 | -6.5 | -68.4 |
| 10118 | ok | 0.16 | 0.1 | 1.67e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -24.9 | -14.0 | 33.7 | 13.1 | 1.8 | 47.7 |
| 10119 | ok | 0.16 | 0.1 | 2.10e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -23.9 | -20.7 | 39.4 | -65.1 | -6.7 | 85.5 |
| 10120 | ok | 0.16 | 0.1 | 2.64e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -15.8 | 29.6 | -6.6 | -82.6 | -23.5 | -94.4 |
| 10121 | ok | 0.16 | 0.2 | 3.37e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -16.4 | 40.8 | 0.4 | -80.4 | -36.0 | -104.4 |
| 10122 | ok | 0.16 | 0.2 | 4.86e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -11.0 | 51.6 | 23.3 | -114.4 | -56.7 | -142.6 |
| 10123 | ok | 0.16 | 0.3 | 6.44e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -14.3 | 104.5 | 41.0 | -90.2 | -84.1 | -147.6 |
| 10124 | ok | 0.16 | 0.2 | 7.19e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.5 | 89.1 | 24.2 | -98.6 | -97.0 | -151.8 |
| 10125 | ok | 0.16 | 0.2 | 3.44e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -51.8 | -5.1 | -45.7 | -45.2 | -24.9 | 39.9 |
| 10126 | ok | 0.16 | 0.2 | 2.30e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -38.5 | 10.0 | -43.7 | -17.1 | -8.0 | 23.9 |
| 10127 | ok | 0.16 | 0.1 | 2.14e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -39.4 | 6.1 | -30.9 | -5.7 | -1.4 | 19.6 |
| 10128 | ok | 0.16 | 0.1 | 2.85e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -44.2 | 21.3 | 0.8 | -23.3 | -24.1 | 35.1 |
| 10129 | ok | 0.16 | 0.3 | 2.95e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -56.9 | -17.2 | -29.6 | -125.0 | -27.2 | 60.9 |
| 10130 | ok | 0.16 | 0.2 | 2.04e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -46.2 | -7.5 | -21.2 | -43.7 | 20.6 | 35.0 |
| 10131 | ok | 0.16 | 0.1 | 1.61e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -47.3 | -4.5 | -19.0 | -45.1 | -1.4 | 30.8 |
| 10132 | ok | 0.16 | 0.1 | 2.61e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -18.1 | 28.0 | -13.7 | -30.0 | -22.4 | 32.6 |
| 10133 | ok | 0.16 | 0.3 | 3.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 109.5 | 22.8 | -11.0 | -9.2 | -27.6 | -35.5 |
| 10134 | ok | 0.16 | 0.2 | 2.05e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -35.0 | -5.7 | -14.7 | -49.6 | -2.8 | 28.9 |
| 10135 | ok | 0.16 | 0.1 | 1.52e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -40.1 | -6.3 | -16.8 | -51.5 | -4.9 | 24.7 |
| 10136 | ok | 0.16 | 0.1 | 2.13e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | 28.0 | -13.8 | -30.9 | -18.6 | 29.3 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | Nz | No | Nzo | Mz | Mo | Mzo |
|-------|-------|------|----------|----------|--------|--------|---------|---------|----------|-------|-------|-----------|-----------|-----------|
| 10137 | ok | 0.16 | 0.4 | 2.29e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -67.3 | 8.5 | -44.1 | -2.9 | 37.0 | -4.3 |
| 10138 | ok | 0.16 | 0.2 | 1.77e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -57.2 | -6.0 | -25.7 | -5.3 | 23.7 | 6.0 |
| 10139 | ok | 0.16 | 9.98e-02 | 1.36e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -33.8 | -12.7 | -24.8 | -6.8 | 8.4 | -0.6 |
| 10140 | ok | 0.16 | 8.65e-02 | 1.73e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -7.4 | 23.1 | -5.4 | -38.2 | -13.7 | 33.4 |
| 10141 | ok | 0.16 | 0.3 | 1.50e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 3.5 | 64.1 | 9.7 | -1.9 | -30.5 | 0.2 |
| 10142 | ok | 0.16 | 0.2 | 1.23e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -31.2 | -11.8 | -17.5 | -4.3 | 18.0 | -3.6 |
| 10143 | ok | 0.16 | 9.69e-02 | 1.17e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -33.0 | -7.3 | -20.9 | -5.8 | 9.1 | -1.2 |
| 10144 | ok | 0.16 | 8.49e-02 | 1.47e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -25.2 | 6.2 | -3.5 | -33.4 | -3.9 | 3.2 |
| 10145 | ok | 0.16 | 0.2 | 7.77e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 4.5 | 55.0 | 10.6 | 9.23e-03 | -13.9 | 9.2 |
| 10146 | ok | 0.16 | 0.2 | 8.89e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 4.2 | 38.0 | 8.7 | -1.3 | -13.0 | 7.2 |
| 10147 | ok | 0.16 | 0.1 | 8.84e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -21.0 | -8.8 | -14.4 | -21.2 | 4.3 | -4.0 |
| 10148 | ok | 0.16 | 0.1 | 1.26e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -20.3 | 1.7 | -5.6 | -30.5 | -4.5 | 1.3 |
| 10149 | ok | 0.16 | 0.2 | 4.52e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 8.67e-02 | 49.1 | 6.1 | 3.48e-02 | -6.6 | 8.7 |
| 10150 | ok | 0.16 | 0.2 | 6.32e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.5 | 38.4 | 4.6 | -1.1 | -6.6 | 7.9 |
| 10151 | ok | 0.16 | 0.1 | 7.17e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -14.4 | -10.0 | -13.3 | -18.1 | 0.9 | -5.7 |
| 10152 | ok | 0.16 | 0.1 | 1.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -15.2 | -14.2 | -26.4 | -24.3 | -0.9 | -7.8 |
| 10153 | ok | 0.16 | 0.2 | 2.77e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.7 | 45.8 | 4.6 | -4.26e-02 | -2.7 | 8.4 |
| 10154 | ok | 0.16 | 0.2 | 4.59e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.5 | 37.1 | 6.8 | 7.0 | -2.0 | 7.2 |
| 10155 | ok | 0.16 | 0.1 | 5.90e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.8 | 24.4 | 4.6 | 11.0 | 1.4 | 5.6 |
| 10156 | ok | 0.16 | 0.1 | 9.42e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -13.6 | -2.8 | -5.6 | -21.9 | -5.0 | -2.8 |
| 10157 | ok | 0.16 | 0.2 | 1.45e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.4 | 43.4 | 3.0 | -0.8 | -1.5 | -0.7 |
| 10158 | ok | 0.16 | 0.1 | 3.42e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.8 | 34.9 | 6.5 | 6.1 | 0.3 | 7.0 |
| 10159 | ok | 0.16 | 0.1 | 4.92e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.1 | 23.2 | 5.1 | 9.3 | 2.0 | 5.6 |
| 10160 | ok | 0.16 | 0.1 | 8.14e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -12.3 | -2.9 | -4.3 | -17.8 | -4.9 | -3.5 |
| 10161 | ok | 0.16 | 0.2 | 1.20e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.6 | 41.2 | 3.2 | -0.6 | -1.2 | -0.2 |
| 10162 | ok | 0.16 | 0.1 | 2.44e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 32.8 | 4.7 | -1.2 | -0.9 | 2.63e-02 |
| 10163 | ok | 0.16 | 0.1 | 3.89e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.9 | 24.3 | 9.1 | 7.5 | 1.2 | 5.8 |
| 10164 | ok | 0.16 | 9.96e-02 | 6.83e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.7 | -2.6 | -2.8 | -14.3 | -4.6 | -3.7 |
| 10165 | ok | 0.16 | 0.2 | 1.13e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.4 | 39.0 | 3.5 | -0.5 | -0.9 | 0.1 |
| 10166 | ok | 0.16 | 0.1 | 2.11e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.3 | 30.8 | 5.1 | -1.0 | -0.7 | 0.3 |
| 10167 | ok | 0.16 | 9.60e-02 | 3.38e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.2 | 22.5 | 6.9 | -1.4 | -0.7 | 0.6 |
| 10168 | ok | 0.16 | 8.52e-02 | 6.86e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.5 | 11.8 | 6.5 | 5.5 | 1.7 | 4.5 |
| 10169 | ok | 0.16 | 0.2 | 1.12e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.2 | 37.6 | 2.9 | -0.2 | -0.2 | 2.1 |
| 10170 | ok | 0.16 | 0.1 | 2.06e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.7 | 28.6 | 4.2 | -0.3 | -9.48e-02 | 2.3 |
| 10171 | ok | 0.16 | 8.93e-02 | 3.22e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.8 | 20.7 | 7.1 | -1.1 | -0.5 | 0.8 |
| 10172 | ok | 0.16 | 7.81e-02 | 6.74e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.7 | 17.0 | -5.0 | 0.9 | 4.3 | 2.9 |
| 10173 | ok | 0.16 | 0.1 | 1.12e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.1 | 36.1 | 3.0 | -0.1 | 9.46e-02 | 2.2 |
| 10174 | ok | 0.16 | 0.2 | 3.49e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 45.0 | 1.0 | 5.76e-03 | 5.41e-02 | 0.7 |
| 10175 | ok | 0.16 | 0.1 | 2.03e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.5 | 27.5 | 4.6 | -0.2 | 0.1 | 2.4 |
| 10176 | ok | 0.16 | 8.37e-02 | 3.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.0 | 18.4 | 6.5 | -0.2 | -0.3 | 2.5 |
| 10177 | ok | 0.16 | 7.30e-02 | 6.72e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.1 | 16.8 | -4.0 | 1.1 | 4.2 | 3.0 |
| 10178 | ok | 0.16 | 5.98e-02 | 1.05e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -8.1 | 10.8 | -10.3 | 2.5 | 7.2 | 4.9 |
| 10179 | ok | 0.16 | 0.1 | 1.12e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.1 | 34.6 | 3.1 | -5.16e-02 | 0.3 | 2.3 |
| 10180 | ok | 0.16 | 0.2 | 3.42e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 42.9 | 0.9 | 8.65e-04 | 0.3 | 0.7 |
| 10181 | ok | 0.16 | 0.1 | 2.01e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.3 | 26.4 | 4.8 | -4.69e-02 | 0.3 | 2.4 |
| 10182 | ok | 0.16 | 7.93e-02 | 3.18e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.8 | 17.7 | 6.8 | -7.18e-03 | -0.2 | 2.5 |
| 10183 | ok | 0.16 | 6.92e-02 | 6.66e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.7 | 16.4 | -2.8 | 1.2 | 4.1 | 3.1 |
| 10184 | ok | 0.16 | 5.57e-02 | 9.99e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.8 | 10.9 | -8.5 | 2.5 | 6.8 | 5.0 |
| 10185 | ok | 0.16 | 0.1 | 1.12e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.1 | 33.0 | 3.2 | -8.93e-03 | 0.4 | 2.3 |
| 10186 | ok | 0.16 | 0.1 | 3.43e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 40.8 | 0.9 | 6.76e-02 | -2.1 | -0.3 |
| 10187 | ok | 0.16 | 9.90e-02 | 2.00e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.2 | 25.3 | 4.9 | 4.28e-02 | 0.4 | 2.5 |
| 10188 | ok | 0.16 | 7.49e-02 | 3.14e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.6 | 17.0 | 6.9 | 0.1 | -8.11e-02 | 2.5 |
| 10189 | ok | 0.16 | 6.48e-02 | 6.44e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.3 | 16.1 | -2.2 | 1.2 | 3.9 | 3.0 |
| 10190 | ok | 0.16 | 5.23e-02 | 9.59e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.3 | 11.2 | -7.4 | 2.4 | 6.5 | 4.9 |
| 10191 | ok | 0.16 | 0.1 | 1.11e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.0 | 31.4 | 3.2 | 2.11e-02 | 0.5 | 2.4 |
| 10192 | ok | 0.16 | 0.1 | 3.46e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 38.7 | 0.9 | 5.63e-02 | -1.8 | -0.2 |
| 10193 | ok | 0.16 | 9.31e-02 | 1.97e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | 24.2 | 4.9 | 0.1 | 0.4 | 2.5 |
| 10194 | ok | 0.16 | 7.06e-02 | 3.07e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.3 | 16.3 | 6.9 | 0.2 | -3.14e-02 | 2.5 |
| 10195 | ok | 0.16 | 6.08e-02 | 6.24e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.9 | 15.7 | -1.8 | 1.2 | 3.8 | 3.0 |
| 10196 | ok | 0.16 | 4.92e-02 | 9.23e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.8 | 11.4 | -6.6 | 2.3 | 6.2 | 4.7 |
| 10197 | ok | 0.16 | 0.1 | 1.11e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.0 | 30.0 | 3.0 | -0.5 | -1.4 | -0.2 |
| 10198 | ok | 0.16 | 0.1 | 3.48e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 36.6 | 0.9 | 4.69e-02 | -1.5 | -6.34e-02 |
| 10199 | ok | 0.16 | 8.75e-02 | 1.94e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.0 | 23.1 | 4.9 | 0.1 | 0.4 | 2.5 |
| 10200 | ok | 0.16 | 6.64e-02 | 3.00e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.1 | 15.6 | 6.8 | 0.2 | -1.40e-02 | 2.4 |
| 10201 | ok | 0.16 | 5.70e-02 | 6.04e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.6 | 15.2 | -1.6 | 1.2 | 3.6 | 2.9 |
| 10202 | ok | 0.16 | 4.63e-02 | 8.86e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.4 | 11.4 | -6.0 | 2.1 | 5.9 | 4.5 |
| 10203 | ok | 0.16 | 0.1 | 1.10e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.0 | 28.5 | 3.0 | -0.4 | -1.2 | 9.02e-02 |
| 10204 | ok | 0.16 | 0.1 | 3.50e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 34.5 | 0.9 | 3.94e-02 | -1.3 | 2.94e-02 |
| 10205 | ok | 0.16 | 8.21e-02 | 1.91e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.9 | 22.1 | 4.6 | -1.0 | -0.9 | 0.2 |
| 10206 | ok | 0.16 | 6.27e-02 | 2.92e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.9 | 14.9 | 6.6 | 0.2 | -2.18e-02 | 2.4 |
| 10207 | ok | 0.16 | 5.34e-02 | 5.83e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.4 | 14.7 | -1.5 | 1.1 | 3.4 | 2.8 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------|-------|------|----------|----------|--------|--------|---------|---------|------|------|------|----------|------|------|
| 10208 | ok | 0.16 | 4.37e-02 | 8.47e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.1 | 11.3 | -5.6 | 1.9 | 5.7 | 4.3 |
| 10209 | ok | 0.16 | 9.53e-02 | 1.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.0 | 27.0 | 2.9 | -0.4 | -1.0 | 0.3 |
| 10210 | ok | 0.16 | 0.1 | 3.51e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 32.6 | 0.9 | 3.34e-02 | -1.1 | 0.1 |
| 10211 | ok | 0.16 | 7.72e-02 | 1.88e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.9 | 21.1 | 4.4 | -0.8 | -0.8 | 0.4 |
| 10212 | ok | 0.16 | 5.91e-02 | 2.84e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.8 | 14.5 | 6.1 | -1.3 | -0.8 | 0.6 |
| 10213 | ok | 0.16 | 5.01e-02 | 5.61e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.3 | 14.0 | -1.6 | 1.0 | 3.3 | 2.6 |
| 10214 | ok | 0.16 | 4.14e-02 | 8.06e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.9 | 10.9 | -5.4 | 1.8 | 5.4 | 4.0 |
| 10215 | ok | 0.16 | 8.92e-02 | 1.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.0 | 25.6 | 2.8 | -0.3 | -0.9 | 0.6 |
| 10216 | ok | 0.16 | 0.1 | 3.53e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 30.7 | 0.9 | 2.87e-02 | -1.0 | 0.2 |
| 10217 | ok | 0.16 | 7.29e-02 | 1.84e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.8 | 20.2 | 4.2 | -0.7 | -0.7 | 0.6 |
| 10218 | ok | 0.16 | 5.68e-02 | 2.76e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.7 | 13.9 | 5.7 | -1.1 | -0.7 | 0.8 |
| 10219 | ok | 0.16 | 4.70e-02 | 5.38e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.2 | 13.3 | -1.8 | 1.0 | 3.1 | 2.5 |
| 10220 | ok | 0.16 | 3.93e-02 | 7.65e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.8 | 10.4 | -5.4 | 1.6 | 5.2 | 3.8 |
| 10221 | ok | 0.16 | 8.59e-02 | 1.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.0 | 24.4 | 2.6 | -0.3 | -0.8 | 0.7 |
| 10222 | ok | 0.16 | 9.76e-02 | 3.56e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 29.0 | 0.9 | 2.52e-02 | -0.9 | 0.2 |
| 10223 | ok | 0.16 | 6.86e-02 | 1.81e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.8 | 19.3 | 3.9 | -0.6 | -0.7 | 0.8 |
| 10224 | ok | 0.16 | 5.34e-02 | 2.68e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.6 | 13.5 | 5.4 | -1.0 | -0.7 | 0.9 |
| 10225 | ok | 0.16 | 4.44e-02 | 5.15e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.1 | 12.6 | -2.1 | 0.9 | 3.0 | 2.4 |
| 10226 | ok | 0.16 | 3.79e-02 | 7.26e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.8 | 9.8 | -5.6 | 1.5 | 5.0 | 3.6 |
| 10227 | ok | 0.16 | 7.92e-02 | 1.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.0 | 23.2 | 2.4 | -0.3 | -0.8 | 0.9 |
| 10228 | ok | 0.16 | 6.47e-02 | 1.78e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.7 | 18.5 | 3.6 | -0.6 | -0.7 | 1.0 |
| 10229 | ok | 0.16 | 5.03e-02 | 2.61e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.6 | 13.0 | 4.9 | -0.9 | -0.7 | 1.1 |
| 10230 | ok | 0.16 | 4.27e-02 | 5.03e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.9 | 11.9 | -1.8 | 0.6 | 2.9 | 2.4 |
| 10231 | ok | 0.16 | 7.58e-02 | 1.06e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 22.1 | 2.3 | -0.2 | -0.7 | 1.1 |
| 10232 | ok | 0.16 | 8.90e-02 | 3.69e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 25.9 | 1.0 | 2.07e-02 | -0.8 | 0.3 |
| 10233 | ok | 0.16 | 6.12e-02 | 1.72e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.6 | 17.7 | 3.3 | -0.5 | -0.6 | 1.1 |
| 10234 | ok | 0.16 | 4.73e-02 | 2.45e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.2 | 12.6 | 4.3 | -0.8 | -0.7 | 1.2 |
| 10235 | ok | 0.16 | 3.84e-02 | 4.49e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.3 | 4.3 | 9.4 | -0.3 | -2.6 | 1.9 |
| 10236 | ok | 0.16 | 3.70e-02 | 6.48e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.4 | 9.1 | -6.8 | 1.0 | 4.9 | 2.9 |
| 10237 | ok | 0.16 | 7.33e-02 | 1.04e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 21.1 | 2.0 | -0.2 | -0.7 | 1.2 |
| 10238 | ok | 0.16 | 8.57e-02 | 3.63e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 24.6 | 1.0 | 1.98e-02 | -0.8 | 0.4 |
| 10239 | ok | 0.16 | 5.92e-02 | 1.67e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.5 | 17.1 | 2.8 | -0.5 | -0.6 | 1.3 |
| 10240 | ok | 0.16 | 4.46e-02 | 2.33e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.0 | 12.3 | 3.6 | -0.8 | -0.7 | 1.3 |
| 10241 | ok | 0.16 | 3.66e-02 | 4.28e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.3 | 4.6 | 8.7 | -0.4 | -2.3 | 1.7 |
| 10242 | ok | 0.16 | 3.64e-02 | 6.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.9 | 7.1 | -8.1 | 0.8 | 4.1 | 2.3 |
| 10243 | ok | 0.16 | 7.15e-02 | 1.02e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 20.4 | 1.7 | -0.2 | -0.8 | 1.4 |
| 10244 | ok | 0.16 | 8.35e-02 | 3.63e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 23.6 | 1.0 | 3.12e-02 | -1.3 | 0.2 |
| 10245 | ok | 0.16 | 5.75e-02 | 1.63e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.5 | 16.7 | 2.2 | -0.5 | -0.7 | 1.5 |
| 10246 | ok | 0.16 | 4.32e-02 | 2.26e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.9 | 12.2 | 2.9 | -0.8 | -0.8 | 1.5 |
| 10247 | ok | 0.16 | 3.51e-02 | 4.04e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.4 | 5.0 | 7.9 | -0.4 | -1.8 | 1.5 |
| 10248 | ok | 0.16 | 3.52e-02 | 5.63e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.5 | 4.9 | -9.5 | 0.4 | 3.2 | 1.6 |
| 10249 | ok | 0.16 | 7.09e-02 | 1.01e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 20.0 | 1.4 | -0.2 | -0.8 | 1.6 |
| 10250 | ok | 0.16 | 8.27e-02 | 3.63e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 23.1 | 1.0 | 3.03e-02 | -1.3 | 0.3 |
| 10251 | ok | 0.16 | 5.71e-02 | 1.60e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.5 | 16.4 | 1.6 | -0.5 | -0.7 | 1.6 |
| 10252 | ok | 0.16 | 4.25e-02 | 2.18e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.8 | 12.3 | 2.1 | -0.8 | -0.8 | 1.6 |
| 10253 | ok | 0.16 | 3.45e-02 | 3.77e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.0 | 6.7 | 6.7 | -1.6 | -1.3 | 1.4 |
| 10254 | ok | 0.16 | 3.39e-02 | 5.15e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.1 | 3.3 | 10.2 | -0.8 | -2.2 | 1.7 |
| 10255 | ok | 0.16 | 7.16e-02 | 1.00e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 19.9 | 1.0 | -0.2 | -0.9 | 1.7 |
| 10256 | ok | 0.16 | 8.31e-02 | 3.64e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 22.9 | 1.0 | 3.03e-02 | -1.3 | 0.3 |
| 10257 | ok | 0.16 | 5.79e-02 | 1.58e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 16.4 | -1.1 | -0.5 | -0.7 | 1.8 |
| 10258 | ok | 0.16 | 4.36e-02 | 2.15e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.7 | 12.4 | -1.6 | -0.8 | -0.3 | 1.7 |
| 10259 | ok | 0.16 | 3.35e-02 | 3.69e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.7 | 7.5 | 5.9 | -1.6 | -1.5 | 1.6 |
| 10260 | ok | 0.16 | 3.31e-02 | 5.13e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.7 | 4.6 | 9.3 | -0.9 | -2.3 | 1.8 |
| 10261 | ok | 0.16 | 7.31e-02 | 1.01e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 20.1 | -1.4 | -0.3 | -1.0 | 1.9 |
| 10262 | ok | 0.16 | 8.44e-02 | 3.64e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 23.1 | 1.0 | 3.11e-02 | -1.4 | 0.4 |
| 10263 | ok | 0.16 | 5.95e-02 | 1.60e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 16.6 | -1.8 | -0.6 | -0.8 | 1.9 |
| 10264 | ok | 0.16 | 4.53e-02 | 2.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.7 | 12.4 | -2.5 | -0.8 | -0.4 | 1.8 |
| 10265 | ok | 0.16 | 3.43e-02 | 3.89e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.5 | 8.4 | 5.1 | -1.7 | -1.7 | 1.8 |
| 10266 | ok | 0.16 | 3.34e-02 | 5.46e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.2 | 6.0 | 8.3 | -1.0 | -2.5 | 2.0 |
| 10267 | ok | 0.16 | 7.54e-02 | 1.02e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 20.6 | -1.8 | -0.3 | -1.1 | 2.1 |
| 10268 | ok | 0.16 | 8.68e-02 | 3.66e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 23.6 | -1.0 | 3.29e-02 | -1.5 | 0.5 |
| 10269 | ok | 0.16 | 6.18e-02 | 1.62e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 17.0 | -2.4 | -0.7 | -0.9 | 2.1 |
| 10270 | ok | 0.16 | 4.76e-02 | 2.26e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.7 | 12.5 | -3.4 | -0.9 | -0.4 | 2.0 |
| 10271 | ok | 0.16 | 3.51e-02 | 4.11e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.0 | 4.4 | -8.4 | -0.3 | 1.1 | 0.7 |
| 10272 | ok | 0.16 | 3.44e-02 | 5.82e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.8 | 7.5 | 7.4 | -1.1 | -2.6 | 2.2 |
| 10273 | ok | 0.16 | 7.86e-02 | 1.04e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 21.5 | -2.1 | -0.3 | -1.2 | 2.3 |
| 10274 | ok | 0.16 | 6.48e-02 | 1.66e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 17.7 | -3.1 | -0.7 | -1.0 | 2.3 |
| 10275 | ok | 0.16 | 5.05e-02 | 2.35e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.7 | 12.9 | -4.3 | -1.1 | -0.5 | 2.2 |
| 10276 | ok | 0.16 | 3.81e-02 | 4.36e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.1 | 4.0 | -9.1 | -0.4 | 1.2 | 0.7 |
| 10277 | ok | 0.16 | 8.26e-02 | 1.05e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 22.6 | -2.5 | -0.4 | -1.4 | 2.5 |
| 10278 | ok | 0.16 | 9.45e-02 | 3.70e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 25.9 | 1.0 | 3.38e-02 | -1.5 | 0.8 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------|-------|------|----------|----------|--------|--------|---------|---------|------|------|-------|----------|------|------|
| 10279 | ok | 0.16 | 6.84e-02 | 1.70e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 18.6 | -3.7 | -0.8 | -1.1 | 2.6 |
| 10280 | ok | 0.16 | 5.40e-02 | 2.45e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.8 | 13.2 | -5.4 | -0.8 | -0.2 | 2.3 |
| 10281 | ok | 0.16 | 4.16e-02 | 4.70e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.2 | 3.8 | -10.1 | -0.5 | 1.6 | 1.0 |
| 10282 | ok | 0.16 | 3.60e-02 | 6.55e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.3 | 10.0 | 5.3 | -1.4 | -2.9 | 2.7 |
| 10283 | ok | 0.16 | 8.71e-02 | 1.07e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 24.0 | -2.8 | -0.4 | -1.6 | 2.8 |
| 10284 | ok | 0.16 | 9.98e-02 | 3.62e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 27.5 | -1.0 | 3.88e-02 | -1.7 | 0.9 |
| 10285 | ok | 0.16 | 7.25e-02 | 1.75e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 19.5 | -4.6 | -0.7 | -0.8 | 2.7 |
| 10286 | ok | 0.16 | 5.77e-02 | 2.55e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.7 | 13.9 | -6.2 | -0.9 | -0.3 | 2.5 |
| 10287 | ok | 0.16 | 4.58e-02 | 4.94e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.0 | 14.5 | 0.4 | -1.4 | -2.6 | 2.4 |
| 10288 | ok | 0.16 | 3.77e-02 | 7.04e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.9 | 11.5 | 4.4 | -1.5 | -3.2 | 3.0 |
| 10289 | ok | 0.16 | 0.1 | 1.10e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 27.7 | -3.7 | -0.4 | -1.5 | 3.1 |
| 10290 | ok | 0.16 | 0.1 | 3.60e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 32.0 | -1.0 | 5.14e-02 | -2.2 | 1.1 |
| 10291 | ok | 0.16 | 8.35e-02 | 1.87e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.3 | 22.5 | -5.9 | -0.9 | -1.2 | 3.1 |
| 10292 | ok | 0.16 | 6.76e-02 | 2.82e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.8 | 15.7 | -8.0 | -1.3 | -0.5 | 2.9 |
| 10293 | ok | 0.16 | 5.56e-02 | 5.68e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | 19.2 | -2.6 | -2.3 | -3.8 | 3.7 |
| 10294 | ok | 0.16 | 4.56e-02 | 8.25e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.4 | 18.9 | -0.8 | -2.9 | -6.0 | 5.7 |
| 10295 | ok | 0.16 | 9.26e-02 | 1.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 25.7 | -3.2 | -0.5 | -1.8 | 3.1 |
| 10296 | ok | 0.16 | 0.1 | 3.61e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 29.6 | -1.0 | 4.45e-02 | -1.9 | 1.0 |
| 10297 | ok | 0.16 | 7.73e-02 | 1.80e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.3 | 20.9 | -5.2 | -0.8 | -1.0 | 2.9 |
| 10298 | ok | 0.16 | 6.22e-02 | 2.67e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.7 | 14.7 | -7.1 | -1.1 | -0.4 | 2.7 |
| 10299 | ok | 0.16 | 5.05e-02 | 5.28e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.8 | 16.1 | -0.5 | -1.6 | -2.8 | 2.7 |
| 10300 | ok | 0.16 | 4.11e-02 | 7.58e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.5 | 12.9 | 3.6 | -1.7 | -3.4 | 3.3 |
| 10301 | ok | 0.16 | 0.1 | 1.12e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 30.1 | -4.1 | -0.5 | -1.7 | 3.4 |
| 10302 | ok | 0.16 | 0.1 | 3.60e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 34.8 | -1.0 | 4.58e-02 | -1.9 | 1.1 |
| 10303 | ok | 0.16 | 9.04e-02 | 1.93e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.3 | 24.4 | -6.6 | -1.1 | -1.4 | 3.4 |
| 10304 | ok | 0.16 | 7.34e-02 | 2.97e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.8 | 16.9 | -8.9 | -1.6 | -0.7 | 3.1 |
| 10305 | ok | 0.16 | 6.12e-02 | 6.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.8 | 21.2 | -3.6 | -2.6 | -4.1 | 4.1 |
| 10306 | ok | 0.16 | 5.01e-02 | 8.96e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.9 | 21.0 | -1.8 | -3.2 | -6.4 | 6.4 |
| 10307 | ok | 0.16 | 0.1 | 1.14e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 32.8 | -4.5 | -0.6 | -2.0 | 3.7 |
| 10308 | ok | 0.16 | 0.1 | 3.59e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 38.2 | -1.0 | 5.48e-02 | -2.2 | 1.2 |
| 10309 | ok | 0.16 | 9.81e-02 | 2.00e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.3 | 26.4 | -7.3 | -1.4 | -1.6 | 3.8 |
| 10310 | ok | 0.16 | 7.96e-02 | 3.13e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | 21.9 | -7.0 | -2.1 | -1.8 | 3.7 |
| 10311 | ok | 0.16 | 6.70e-02 | 6.49e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.6 | 23.2 | -4.6 | -3.0 | -4.4 | 4.6 |
| 10312 | ok | 0.16 | 5.48e-02 | 9.68e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.6 | 23.0 | -2.9 | -3.7 | -6.9 | 7.1 |
| 10313 | ok | 0.16 | 0.1 | 1.16e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 35.8 | -4.9 | -0.7 | -2.4 | 4.2 |
| 10314 | ok | 0.16 | 0.1 | 3.59e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 41.9 | -1.0 | 6.56e-02 | -2.6 | 1.3 |
| 10315 | ok | 0.16 | 0.1 | 2.07e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 28.8 | -8.0 | -1.6 | -1.9 | 4.2 |
| 10316 | ok | 0.16 | 8.63e-02 | 3.28e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | 23.8 | -7.9 | -2.5 | -2.1 | 4.1 |
| 10317 | ok | 0.16 | 7.30e-02 | 6.87e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 25.2 | -5.6 | -3.5 | -4.8 | 5.2 |
| 10318 | ok | 0.16 | 5.93e-02 | 1.04e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -1.3 | 24.9 | -3.8 | -4.2 | -7.4 | 8.0 |
| 10319 | ok | 0.16 | 0.1 | 1.18e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 39.2 | -5.3 | -0.9 | -2.8 | 4.7 |
| 10320 | ok | 0.16 | 0.2 | 3.65e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 46.1 | -1.0 | 7.87e-02 | -3.1 | 1.5 |
| 10321 | ok | 0.16 | 0.1 | 2.14e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 31.3 | -8.7 | -2.0 | -2.3 | 4.7 |
| 10322 | ok | 0.16 | 9.34e-02 | 3.43e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | 25.8 | -8.8 | -3.0 | -2.4 | 4.5 |
| 10323 | ok | 0.16 | 7.90e-02 | 7.18e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.3 | 27.1 | -6.6 | -4.1 | -5.2 | 5.8 |
| 10324 | ok | 0.16 | 6.34e-02 | 1.11e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -1.3 | 26.6 | -4.6 | -4.7 | -8.0 | 9.1 |
| 10325 | ok | 0.16 | 0.2 | 1.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 42.8 | -5.5 | -1.0 | -3.3 | 5.3 |
| 10326 | ok | 0.16 | 0.1 | 2.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.5 | 34.0 | -9.2 | -2.4 | -2.7 | 5.3 |
| 10327 | ok | 0.16 | 0.1 | 3.63e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | 27.8 | -9.6 | -3.6 | -2.7 | 5.1 |
| 10328 | ok | 0.16 | 8.52e-02 | 7.66e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.7 | 28.9 | -8.1 | -4.8 | -5.7 | 6.6 |
| 10329 | ok | 0.16 | 0.2 | 1.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 46.1 | -5.9 | -1.2 | -3.8 | 6.0 |
| 10330 | ok | 0.16 | 0.1 | 2.22e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 36.6 | -9.8 | -2.8 | -3.1 | 5.9 |
| 10331 | ok | 0.16 | 0.1 | 3.66e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | 29.9 | -10.1 | -4.2 | -3.1 | 5.7 |
| 10332 | ok | 0.16 | 8.88e-02 | 7.86e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.8 | 30.1 | -7.2 | -5.8 | -6.1 | 7.7 |
| 10333 | ok | 0.16 | 0.2 | 1.21e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 50.2 | -6.3 | -1.5 | -4.5 | 6.8 |
| 10334 | ok | 0.16 | 0.1 | 2.28e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 40.4 | -8.4 | -3.3 | -3.8 | 6.8 |
| 10335 | ok | 0.16 | 0.1 | 3.80e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.3 | 32.0 | -10.8 | -5.0 | -3.5 | 6.4 |
| 10336 | ok | 0.16 | 9.70e-02 | 8.31e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 33.1 | -8.6 | -6.6 | -6.8 | 8.7 |
| 10337 | ok | 0.16 | 0.2 | 1.22e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 55.0 | -6.6 | -1.6 | -5.4 | 9.0 |
| 10338 | ok | 0.16 | 0.2 | 2.33e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 43.7 | -8.9 | -4.0 | -4.4 | 7.8 |
| 10339 | ok | 0.16 | 0.1 | 3.93e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.4 | 34.5 | -11.5 | -6.0 | -4.0 | 7.4 |
| 10340 | ok | 0.16 | 0.1 | 8.68e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.2 | 35.1 | -9.1 | -7.8 | -7.4 | 10.1 |
| 10341 | ok | 0.16 | 0.2 | 1.23e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 59.5 | -6.8 | -1.9 | -6.3 | 10.4 |
| 10342 | ok | 0.16 | 0.2 | 2.38e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.5 | 47.1 | -9.4 | -4.8 | -5.1 | 8.9 |
| 10343 | ok | 0.16 | 0.1 | 4.05e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.5 | 36.9 | -12.0 | -7.2 | -4.6 | 8.5 |
| 10344 | ok | 0.16 | 0.1 | 9.03e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | 37.0 | -9.3 | -9.3 | -8.1 | 11.8 |
| 10345 | ok | 0.16 | 0.2 | 1.24e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 64.1 | -7.0 | -2.2 | -7.3 | 12.0 |
| 10346 | ok | 0.16 | 0.2 | 2.43e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.7 | 50.6 | -9.7 | -5.7 | -5.8 | 10.3 |
| 10347 | ok | 0.16 | 0.1 | 4.17e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.8 | 39.4 | -12.3 | -8.7 | -5.2 | 9.8 |
| 10348 | ok | 0.16 | 0.1 | 9.37e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.7 | 38.8 | -9.4 | -11.1 | -8.9 | 14.0 |
| 10349 | ok | 0.16 | 0.2 | 1.25e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 68.9 | -7.2 | -2.6 | -8.3 | 13.8 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------------|-------|------------|--------------|-----------------|---------------|---------------|----------------|----------------|------------|------------|-------------|------------|------------|-------------|
| 10350 | ok | 0.16 | 0.2 | 2.47e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.9 | 54.1 | -9.9 | -6.7 | -6.6 | 11.9 |
| 10351 | ok | 0.16 | 0.2 | 4.28e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.2 | 41.9 | -12.5 | -10.4 | -5.9 | 11.3 |
| 10352 | ok | 0.16 | 0.1 | 9.70e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | 40.4 | -9.1 | -13.3 | -9.7 | 16.6 |
| 10353 | ok | 0.16 | 0.3 | 1.26e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 73.7 | -7.1 | -3.0 | -9.3 | 15.9 |
| 10354 | ok | 0.16 | 0.2 | 2.51e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.2 | 57.8 | -11.8 | -7.8 | -7.4 | 13.8 |
| 10355 | ok | 0.16 | 0.2 | 4.38e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.7 | 44.4 | -12.5 | -12.4 | -6.6 | 13.0 |
| 10356 | ok | 0.16 | 0.1 | 1.00e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -5.7 | 42.0 | -8.6 | -16.0 | -10.6 | 19.7 |
| 10357 | ok | 0.16 | 0.3 | 1.26e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 78.4 | -7.0 | -3.4 | -10.0 | 18.2 |
| 10358 | ok | 0.16 | 0.2 | 2.55e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.5 | 61.3 | -11.5 | -9.1 | -8.1 | 15.8 |
| 10359 | ok | 0.16 | 0.2 | 4.47e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.2 | 46.9 | -12.2 | -14.7 | -7.2 | 15.0 |
| 10360 | ok | 0.16 | 0.1 | 1.03e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -6.5 | 43.4 | -7.7 | -19.1 | -11.4 | 23.5 |
| 10361 | ok | 0.16 | 0.3 | 1.27e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.2 | 83.0 | -6.7 | -3.8 | -10.4 | 20.8 |
| 10362 | ok | 0.16 | 0.2 | 2.57e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.8 | 64.8 | -11.1 | -10.5 | -8.4 | 17.9 |
| 10363 | ok | 0.16 | 0.2 | 4.51e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.9 | 49.3 | -11.6 | -17.3 | -7.6 | 17.1 |
| 10364 | ok | 0.16 | 0.1 | 1.05e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -7.5 | 44.6 | -6.3 | -22.8 | -12.0 | 27.9 |
| 10365 | ok | 0.16 | 0.3 | 1.26e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.3 | 87.4 | -6.2 | -4.2 | -9.9 | 23.4 |
| 10366 | ok | 0.16 | 0.2 | 2.56e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.1 | 68.3 | -10.4 | -11.9 | -8.2 | 20.1 |
| 10367 | ok | 0.16 | 0.2 | 4.48e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.4 | 51.7 | -10.7 | -20.2 | -7.6 | 19.3 |
| 10368 | ok | 0.16 | 0.1 | 1.04e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -8.5 | 45.4 | -4.5 | -27.1 | -12.3 | 33.1 |
| 10369 | ok | 0.16 | 0.3 | 1.24e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.3 | 91.4 | -5.6 | -4.5 | -8.1 | 26.0 |
| 10370 | ok | 0.16 | 0.3 | 2.48e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.1 | 71.5 | -9.6 | -13.4 | -6.8 | 22.2 |
| 10371 | ok | 0.16 | 0.2 | 4.29e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.6 | 53.7 | -9.5 | -23.4 | -6.8 | 21.4 |
| 10372 | ok | 0.16 | 0.1 | 9.98e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.4 | 45.6 | -2.2 | -31.9 | -12.0 | 38.9 |
| 10373 | ok | 0.16 | 0.3 | 1.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.2 | 95.3 | -5.1 | -4.7 | -4.1 | 28.3 |
| 10374 | ok | 0.16 | 0.3 | 2.48e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.7 | 74.5 | -8.9 | -14.8 | -3.7 | 23.9 |
| 10375 | ok | 0.16 | 0.2 | 3.79e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.0 | 55.1 | -8.3 | -26.8 | -4.8 | 23.1 |
| 10376 | ok | 0.16 | 0.2 | 8.86e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.8 | 44.5 | 0.5 | -37.3 | -10.6 | 45.1 |
| 10377 | ok | 0.16 | 0.4 | 1.71e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 99.4 | -3.3 | -4.8 | 3.5 | 30.0 |
| 10378 | ok | 0.16 | 0.3 | 3.58e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.0 | 76.8 | -7.2 | -16.4 | 2.4 | 24.7 |
| 10379 | ok | 0.16 | 0.2 | 4.67e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.9 | 55.1 | -7.3 | -30.5 | -0.7 | 23.8 |
| 10380 | ok | 0.16 | 0.2 | 7.69e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.2 | 41.1 | 3.5 | -43.1 | -7.6 | 50.9 |
| 10381 | ok | 0.16 | 0.4 | 3.39e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 2.16e-02 | 104.4 | -4.6 | -4.8 | 16.4 | 30.7 |
| 10382 | ok | 0.16 | 0.3 | 5.40e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.08e-02 | 78.2 | -8.9 | -18.1 | 12.5 | 23.9 |
| 10383 | ok | 0.16 | 0.2 | 5.97e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 52.5 | -6.5 | -34.4 | 6.2 | 22.5 |
| 10384 | ok | 0.16 | 0.1 | 9.67e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.0 | 29.2 | -6.0 | -55.1 | -4.0 | 4.8 |
| 10385 | ok | 0.16 | 0.4 | 7.22e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 2.4 | 112.5 | -9.5 | -4.6 | 37.8 | 29.1 |
| 10386 | ok | 0.16 | 0.3 | 8.07e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 10.3 | 79.8 | -16.3 | -19.8 | 28.7 | 20.6 |
| 10387 | ok | 0.16 | 0.2 | 8.82e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 19.7 | 34.8 | -13.9 | -46.6 | 19.9 | 14.1 |
| 10388 | ok | 0.16 | 0.1 | 1.11e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -9.2 | 27.7 | -4.5 | -52.6 | -3.0 | -34.2 |
| 10389 | ok | 0.16 | 0.5 | 1.48e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 10.1 | 127.5 | -24.4 | -4.5 | 73.4 | 22.4 |
| 10390 | ok | 0.16 | 0.3 | 1.25e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 29.0 | 68.4 | -21.9 | -24.9 | 50.9 | 10.2 |
| 10391 | ok | 0.16 | 0.2 | 1.18e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 19.2 | 31.2 | 14.7 | -63.4 | 23.0 | 3.1 |
| 10392 | ok | 0.16 | 0.1 | 1.38e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -7.3 | 30.3 | 1.4 | -55.6 | -4.9 | -44.2 |
| 10393 | ok | 0.18 | 0.6 | 1.82e-02 | 4.6 | 5.7 | 3.2 | 4.3 | 137.2 | 191.1 | -143.1 | 33.8 | 177.0 | -34.9 |
| 10394 | ok | 0.16 | 0.3 | 1.71e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 70.1 | 52.6 | -20.1 | -28.7 | 82.7 | -16.6 |
| 10395 | ok | 0.16 | 0.2 | 1.35e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 51.5 | 10.3 | 15.3 | -69.0 | 28.7 | -20.0 |
| 10396 | ok | 0.16 | 0.2 | 1.90e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 7.2 | 33.7 | 10.1 | -71.7 | -10.6 | -76.5 |
| 10397 | ok | 0.16 | 0.5 | 3.88e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 146.8 | 52.6 | 8.2 | -60.9 | 129.1 | -64.9 |
| 10398 | ok | 0.16 | 0.3 | 2.04e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 81.6 | 18.0 | 23.9 | -73.9 | 49.9 | -37.4 |
| 10399 | ok | 0.16 | 0.2 | 1.40e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 49.3 | 8.9 | 22.0 | -68.0 | 29.3 | -36.8 |
| 10400 | ok | 0.16 | 0.2 | 2.64e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 13.9 | 53.0 | 39.8 | -66.4 | -24.9 | -76.1 |
| 10401 | ok | 0.16 | 0.5 | 2.93e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 95.5 | 73.0 | 89.7 | -7.8 | 95.3 | -90.2 |
| 10402 | ok | 0.16 | 0.3 | 1.99e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 65.0 | 8.8 | 36.9 | -66.7 | 46.1 | -75.2 |
| 10403 | ok | 0.16 | 0.2 | 2.31e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 31.1 | -0.8 | 41.1 | -57.0 | 10.5 | -61.1 |
| 10404 | ok | 0.16 | 0.2 | 4.19e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -6.5 | 55.3 | 38.5 | -59.0 | -35.9 | -96.7 |
| 10405 | ok | 0.16 | 0.3 | 3.36e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -69.5 | 11.5 | 46.0 | -95.8 | -44.4 | -102.6 |
| 10406 | ok | 0.16 | 0.2 | 3.27e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -62.2 | 10.8 | 56.3 | -62.2 | -34.5 | -78.7 |
| 10407 | ok | 0.16 | 0.2 | 3.59e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -44.1 | -4.4 | 71.9 | -16.5 | 23.7 | -81.2 |
| 10408 | ok | 0.16 | 0.2 | 5.04e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -54.1 | 47.9 | 25.1 | -49.6 | -49.2 | -109.0 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | | | | | | | | -441.91 | -308.58 | -282.17 | -149.69 | -118.90 | -177.77 |
| | | 0.26 | 0.99 | 0.15 | 7.84 | 9.99 | 8.54 | 12.82 | 342.45 | 503.11 | 191.84 | 143.14 | 523.00 | 106.86 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 2766 | ok | 0.19 | | | | | | |
| 6852 | ok | 3.24 | | | | | | |
| 6943 | ok | 0.62 | | | | | | |
| 7043 | ok | 0.50 | | | | | | |
| 7236 | ok | 0.33 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 7245 | ok | 0.18 | | | | | | |
| 7247 | ok | 0.39 | | | | | | |
| 7248 | ok | 0.07 | | | | | | |
| 7249 | ok | 0.45 | | | | | | |
| 7250 | ok | 0.03 | | | | | | |
| 7251 | ok | 0.52 | | | | | | |
| 7252 | ok | 0.05 | | | | | | |
| 7260 | ok | 0.62 | | | | | | |
| 7261 | ok | 0.08 | | | | | | |
| 7270 | ok | 0.76 | | | | | | |
| 7271 | ok | 0.11 | | | | | | |
| 7272 | ok | 0.95 | | | | | | |
| 7273 | ok | 0.15 | | | | | | |
| 7274 | ok | 1.85 | | | | | | |
| 7275 | ok | 0.75 | | | | | | |
| 7276 | ok | 3.24 | | | | | | |
| 7277 | ok | 1.74 | | | | | | |
| 7278 | ok | 1.74 | | | | | | |
| 7281 | ok | 0.13 | | | | | | |
| 7282 | ok | 0.10 | | | | | | |
| 7284 | ok | 0.14 | | | | | | |
| 7289 | ok | 0.09 | | | | | | |
| 7290 | ok | 0.05 | | | | | | |
| 7291 | ok | 0.03 | | | | | | |
| 7292 | ok | 0.05 | | | | | | |
| 7293 | ok | 0.08 | | | | | | |
| 7294 | ok | 0.16 | | | | | | |
| 7296 | ok | 0.22 | | | | | | |
| 7301 | ok | 0.32 | | | | | | |
| 7302 | ok | 0.32 | | | | | | |
| 7303 | ok | 0.09 | | | | | | |
| 7355 | ok | 0.06 | | | | | | |
| 7415 | ok | 0.04 | | | | | | |
| 7419 | ok | 0.05 | | | | | | |
| 7467 | ok | 0.08 | | | | | | |
| 7468 | ok | 0.09 | | | | | | |
| 7530 | ok | 0.11 | | | | | | |
| 7532 | ok | 0.21 | | | | | | |
| 7533 | ok | 0.21 | | | | | | |
| 7534 | ok | 0.11 | | | | | | |
| 7535 | ok | 0.09 | | | | | | |
| 7536 | ok | 0.09 | | | | | | |
| 7537 | ok | 0.10 | | | | | | |
| 7538 | ok | 0.11 | | | | | | |
| 7574 | ok | 0.11 | | | | | | |
| 7639 | ok | 0.21 | | | | | | |
| 7643 | ok | 0.21 | | | | | | |
| 7648 | ok | 0.15 | | | | | | |
| 7915 | ok | 0.25 | | | | | | |
| 7916 | ok | 0.18 | | | | | | |
| 7917 | ok | 0.12 | | | | | | |
| 7918 | ok | 0.15 | | | | | | |
| 8323 | ok | 0.11 | | | | | | |
| 8324 | ok | 0.21 | | | | | | |
| 8325 | ok | 0.21 | | | | | | |
| 8346 | ok | 0.16 | | | | | | |
| 8369 | ok | 0.24 | | | | | | |
| 8370 | ok | 0.22 | | | | | | |
| 8371 | ok | 0.17 | | | | | | |
| 8372 | ok | 0.16 | | | | | | |
| 8452 | ok | 0.21 | | | | | | |
| 8457 | ok | 0.22 | | | | | | |
| 8462 | ok | 0.22 | | | | | | |
| 8467 | ok | 0.22 | | | | | | |
| 8472 | ok | 0.22 | | | | | | |
| 8477 | ok | 0.22 | | | | | | |
| 8627 | ok | 0.21 | | | | | | |
| 9940 | ok | 0.02 | | | | | | |
| 9941 | ok | 0.05 | | | | | | |
| 9942 | ok | 0.01 | | | | | | |
| 9943 | ok | 0.02 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------|-------|---------|----------|-----------|---------|----------|------|-------|
| 9966 | ok | 0.06 | | | | | | |
| 9967 | ok | 0.07 | | | | | | |
| 9968 | ok | 0.09 | | | | | | |
| 9969 | ok | 0.11 | | | | | | |
| 9970 | ok | 0.13 | | | | | | |
| 9971 | ok | 0.17 | | | | | | |
| 9972 | ok | 0.25 | | | | | | |
| 9973 | ok | 0.63 | | | | | | |
| 9974 | ok | 0.63 | | | | | | |
| 9975 | ok | 0.20 | | | | | | |
| 9976 | ok | 0.62 | | | | | | |
| 9977 | ok | 0.03 | | | | | | |
| 9978 | ok | 0.03 | | | | | | |
| 9979 | ok | 0.03 | | | | | | |
| 9980 | ok | 0.04 | | | | | | |
| 9981 | ok | 0.04 | | | | | | |
| 9982 | ok | 0.05 | | | | | | |
| 9983 | ok | 0.06 | | | | | | |
| 9984 | ok | 0.07 | | | | | | |
| 9985 | ok | 0.08 | | | | | | |
| 9986 | ok | 0.10 | | | | | | |
| 9987 | ok | 0.11 | | | | | | |
| 9988 | ok | 0.13 | | | | | | |
| 9989 | ok | 0.16 | | | | | | |
| 9990 | ok | 0.19 | | | | | | |
| 9991 | ok | 0.24 | | | | | | |
| 9992 | ok | 0.38 | | | | | | |
| 9993 | ok | 0.84 | | | | | | |
| 9995 | ok | 0.84 | | | | | | |
| 9997 | ok | 0.24 | | | | | | |
| 9999 | ok | 0.50 | | | | | | |
| 10090 | ok | 0.02 | | | | | | |
| 10091 | ok | 0.03 | | | | | | |
| 10092 | ok | 0.01 | | | | | | |
| 10093 | ok | 0.02 | | | | | | |
| 10094 | ok | 0.03 | | | | | | |
| 10095 | ok | 0.03 | | | | | | |
| 10096 | ok | 0.03 | | | | | | |
| 10097 | ok | 0.03 | | | | | | |
| 10098 | ok | 0.03 | | | | | | |
| 10099 | ok | 0.04 | | | | | | |
| 10100 | ok | 0.04 | | | | | | |
| 10101 | ok | 0.06 | | | | | | |
| 10102 | ok | 0.07 | | | | | | |
| 10103 | ok | 0.10 | | | | | | |
| 10104 | ok | 0.15 | | | | | | |
| 10105 | ok | 0.02 | | | | | | |
| 10106 | ok | 0.03 | | | | | | |
| 10107 | ok | 0.03 | | | | | | |
| 10108 | ok | 0.03 | | | | | | |
| 10109 | ok | 0.03 | | | | | | |
| 10110 | ok | 0.03 | | | | | | |
| 10111 | ok | 0.04 | | | | | | |
| 10112 | ok | 0.04 | | | | | | |
| 10113 | ok | 0.04 | | | | | | |
| 10114 | ok | 0.04 | | | | | | |
| 10115 | ok | 0.04 | | | | | | |
| 10116 | ok | 0.04 | | | | | | |
| 10117 | ok | 0.04 | | | | | | |
| 10118 | ok | 0.05 | | | | | | |
| 10119 | ok | 0.07 | | | | | | |
| 10120 | ok | 0.08 | | | | | | |
| 10121 | ok | 0.09 | | | | | | |
| 10122 | ok | 0.10 | | | | | | |
| 10123 | ok | 0.13 | | | | | | |
| 10124 | ok | 0.15 | | | | | | |
| 10125 | ok | 0.25 | | | | | | |
| 10126 | ok | 0.18 | | | | | | |
| 10127 | ok | 0.12 | | | | | | |
| 10128 | ok | 0.15 | | | | | | |
| 10129 | ok | 0.21 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------|-------|----------|----------|-----------|---------|----------|------|-------|
| 10130 | ok | 0.14 | | | | | | |
| 10131 | ok | 0.09 | | | | | | |
| 10132 | ok | 0.07 | | | | | | |
| 10133 | ok | 0.20 | | | | | | |
| 10134 | ok | 0.10 | | | | | | |
| 10135 | ok | 0.06 | | | | | | |
| 10136 | ok | 0.05 | | | | | | |
| 10137 | ok | 0.20 | | | | | | |
| 10138 | ok | 0.07 | | | | | | |
| 10139 | ok | 0.04 | | | | | | |
| 10140 | ok | 0.03 | | | | | | |
| 10141 | ok | 0.08 | | | | | | |
| 10142 | ok | 0.07 | | | | | | |
| 10143 | ok | 0.04 | | | | | | |
| 10144 | ok | 0.03 | | | | | | |
| 10145 | ok | 0.05 | | | | | | |
| 10146 | ok | 0.04 | | | | | | |
| 10147 | ok | 0.03 | | | | | | |
| 10148 | ok | 0.03 | | | | | | |
| 10149 | ok | 0.04 | | | | | | |
| 10150 | ok | 0.03 | | | | | | |
| 10151 | ok | 0.03 | | | | | | |
| 10152 | ok | 0.03 | | | | | | |
| 10153 | ok | 0.03 | | | | | | |
| 10154 | ok | 0.02 | | | | | | |
| 10155 | ok | 0.02 | | | | | | |
| 10156 | ok | 0.02 | | | | | | |
| 10157 | ok | 0.02 | | | | | | |
| 10158 | ok | 0.01 | | | | | | |
| 10159 | ok | 0.02 | | | | | | |
| 10160 | ok | 0.02 | | | | | | |
| 10161 | ok | 0.02 | | | | | | |
| 10162 | ok | 0.01 | | | | | | |
| 10163 | ok | 0.01 | | | | | | |
| 10164 | ok | 0.02 | | | | | | |
| 10165 | ok | 0.01 | | | | | | |
| 10166 | ok | 8.19e-03 | | | | | | |
| 10167 | ok | 8.93e-03 | | | | | | |
| 10168 | ok | 0.02 | | | | | | |
| 10169 | ok | 0.01 | | | | | | |
| 10170 | ok | 6.31e-03 | | | | | | |
| 10171 | ok | 7.28e-03 | | | | | | |
| 10172 | ok | 0.01 | | | | | | |
| 10173 | ok | 0.01 | | | | | | |
| 10174 | ok | 0.05 | | | | | | |
| 10175 | ok | 5.26e-03 | | | | | | |
| 10176 | ok | 5.91e-03 | | | | | | |
| 10177 | ok | 0.01 | | | | | | |
| 10178 | ok | 0.03 | | | | | | |
| 10179 | ok | 9.37e-03 | | | | | | |
| 10180 | ok | 0.04 | | | | | | |
| 10181 | ok | 4.52e-03 | | | | | | |
| 10182 | ok | 4.82e-03 | | | | | | |
| 10183 | ok | 9.72e-03 | | | | | | |
| 10184 | ok | 0.03 | | | | | | |
| 10185 | ok | 8.30e-03 | | | | | | |
| 10186 | ok | 0.04 | | | | | | |
| 10187 | ok | 3.86e-03 | | | | | | |
| 10188 | ok | 3.96e-03 | | | | | | |
| 10189 | ok | 8.56e-03 | | | | | | |
| 10190 | ok | 0.03 | | | | | | |
| 10191 | ok | 7.39e-03 | | | | | | |
| 10192 | ok | 0.03 | | | | | | |
| 10193 | ok | 3.28e-03 | | | | | | |
| 10194 | ok | 3.26e-03 | | | | | | |
| 10195 | ok | 7.53e-03 | | | | | | |
| 10196 | ok | 0.03 | | | | | | |
| 10197 | ok | 6.62e-03 | | | | | | |
| 10198 | ok | 0.03 | | | | | | |
| 10199 | ok | 2.79e-03 | | | | | | |
| 10200 | ok | 2.68e-03 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------|-------|----------|----------|-----------|---------|----------|------|-------|
| 10201 | ok | 6.65e-03 | | | | | | |
| 10202 | ok | 0.03 | | | | | | |
| 10203 | ok | 5.97e-03 | | | | | | |
| 10204 | ok | 0.02 | | | | | | |
| 10205 | ok | 2.38e-03 | | | | | | |
| 10206 | ok | 2.21e-03 | | | | | | |
| 10207 | ok | 5.89e-03 | | | | | | |
| 10208 | ok | 0.02 | | | | | | |
| 10209 | ok | 5.41e-03 | | | | | | |
| 10210 | ok | 0.02 | | | | | | |
| 10211 | ok | 2.03e-03 | | | | | | |
| 10212 | ok | 1.84e-03 | | | | | | |
| 10213 | ok | 5.24e-03 | | | | | | |
| 10214 | ok | 0.02 | | | | | | |
| 10215 | ok | 4.94e-03 | | | | | | |
| 10216 | ok | 0.02 | | | | | | |
| 10217 | ok | 1.75e-03 | | | | | | |
| 10218 | ok | 1.55e-03 | | | | | | |
| 10219 | ok | 4.69e-03 | | | | | | |
| 10220 | ok | 0.02 | | | | | | |
| 10221 | ok | 4.54e-03 | | | | | | |
| 10222 | ok | 0.02 | | | | | | |
| 10223 | ok | 1.52e-03 | | | | | | |
| 10224 | ok | 1.35e-03 | | | | | | |
| 10225 | ok | 4.22e-03 | | | | | | |
| 10226 | ok | 0.02 | | | | | | |
| 10227 | ok | 4.19e-03 | | | | | | |
| 10228 | ok | 1.34e-03 | | | | | | |
| 10229 | ok | 1.20e-03 | | | | | | |
| 10230 | ok | 3.78e-03 | | | | | | |
| 10231 | ok | 3.88e-03 | | | | | | |
| 10232 | ok | 0.02 | | | | | | |
| 10233 | ok | 1.19e-03 | | | | | | |
| 10234 | ok | 1.06e-03 | | | | | | |
| 10235 | ok | 3.42e-03 | | | | | | |
| 10236 | ok | 0.02 | | | | | | |
| 10237 | ok | 3.59e-03 | | | | | | |
| 10238 | ok | 0.01 | | | | | | |
| 10239 | ok | 1.07e-03 | | | | | | |
| 10240 | ok | 9.57e-04 | | | | | | |
| 10241 | ok | 3.05e-03 | | | | | | |
| 10242 | ok | 0.02 | | | | | | |
| 10243 | ok | 3.36e-03 | | | | | | |
| 10244 | ok | 0.01 | | | | | | |
| 10245 | ok | 1.02e-03 | | | | | | |
| 10246 | ok | 9.12e-04 | | | | | | |
| 10247 | ok | 2.78e-03 | | | | | | |
| 10248 | ok | 0.02 | | | | | | |
| 10249 | ok | 3.21e-03 | | | | | | |
| 10250 | ok | 0.01 | | | | | | |
| 10251 | ok | 9.97e-04 | | | | | | |
| 10252 | ok | 9.11e-04 | | | | | | |
| 10253 | ok | 2.56e-03 | | | | | | |
| 10254 | ok | 0.01 | | | | | | |
| 10255 | ok | 3.13e-03 | | | | | | |
| 10256 | ok | 0.01 | | | | | | |
| 10257 | ok | 1.00e-03 | | | | | | |
| 10258 | ok | 9.52e-04 | | | | | | |
| 10259 | ok | 2.41e-03 | | | | | | |
| 10260 | ok | 0.01 | | | | | | |
| 10261 | ok | 3.08e-03 | | | | | | |
| 10262 | ok | 0.01 | | | | | | |
| 10263 | ok | 1.04e-03 | | | | | | |
| 10264 | ok | 9.83e-04 | | | | | | |
| 10265 | ok | 2.31e-03 | | | | | | |
| 10266 | ok | 0.01 | | | | | | |
| 10267 | ok | 3.08e-03 | | | | | | |
| 10268 | ok | 0.01 | | | | | | |
| 10269 | ok | 1.08e-03 | | | | | | |
| 10270 | ok | 1.03e-03 | | | | | | |
| 10271 | ok | 2.25e-03 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------|-------|----------|----------|-----------|---------|----------|------|-------|
| 10272 | ok | 0.01 | | | | | | |
| 10273 | ok | 3.19e-03 | | | | | | |
| 10274 | ok | 1.14e-03 | | | | | | |
| 10275 | ok | 1.09e-03 | | | | | | |
| 10276 | ok | 2.29e-03 | | | | | | |
| 10277 | ok | 3.37e-03 | | | | | | |
| 10278 | ok | 0.01 | | | | | | |
| 10279 | ok | 1.21e-03 | | | | | | |
| 10280 | ok | 1.16e-03 | | | | | | |
| 10281 | ok | 2.37e-03 | | | | | | |
| 10282 | ok | 0.01 | | | | | | |
| 10283 | ok | 3.57e-03 | | | | | | |
| 10284 | ok | 0.01 | | | | | | |
| 10285 | ok | 1.32e-03 | | | | | | |
| 10286 | ok | 1.26e-03 | | | | | | |
| 10287 | ok | 2.48e-03 | | | | | | |
| 10288 | ok | 0.01 | | | | | | |
| 10289 | ok | 4.20e-03 | | | | | | |
| 10290 | ok | 0.01 | | | | | | |
| 10291 | ok | 1.58e-03 | | | | | | |
| 10292 | ok | 1.50e-03 | | | | | | |
| 10293 | ok | 3.03e-03 | | | | | | |
| 10294 | ok | 0.01 | | | | | | |
| 10295 | ok | 3.82e-03 | | | | | | |
| 10296 | ok | 0.01 | | | | | | |
| 10297 | ok | 1.44e-03 | | | | | | |
| 10298 | ok | 1.37e-03 | | | | | | |
| 10299 | ok | 2.71e-03 | | | | | | |
| 10300 | ok | 0.01 | | | | | | |
| 10301 | ok | 4.65e-03 | | | | | | |
| 10302 | ok | 0.01 | | | | | | |
| 10303 | ok | 1.75e-03 | | | | | | |
| 10304 | ok | 1.67e-03 | | | | | | |
| 10305 | ok | 3.40e-03 | | | | | | |
| 10306 | ok | 0.02 | | | | | | |
| 10307 | ok | 5.17e-03 | | | | | | |
| 10308 | ok | 0.02 | | | | | | |
| 10309 | ok | 1.96e-03 | | | | | | |
| 10310 | ok | 1.87e-03 | | | | | | |
| 10311 | ok | 3.83e-03 | | | | | | |
| 10312 | ok | 0.02 | | | | | | |
| 10313 | ok | 5.80e-03 | | | | | | |
| 10314 | ok | 0.02 | | | | | | |
| 10315 | ok | 2.22e-03 | | | | | | |
| 10316 | ok | 2.14e-03 | | | | | | |
| 10317 | ok | 4.34e-03 | | | | | | |
| 10318 | ok | 0.02 | | | | | | |
| 10319 | ok | 6.54e-03 | | | | | | |
| 10320 | ok | 0.02 | | | | | | |
| 10321 | ok | 2.55e-03 | | | | | | |
| 10322 | ok | 2.48e-03 | | | | | | |
| 10323 | ok | 4.95e-03 | | | | | | |
| 10324 | ok | 0.02 | | | | | | |
| 10325 | ok | 7.35e-03 | | | | | | |
| 10326 | ok | 2.91e-03 | | | | | | |
| 10327 | ok | 2.86e-03 | | | | | | |
| 10328 | ok | 5.58e-03 | | | | | | |
| 10329 | ok | 8.31e-03 | | | | | | |
| 10330 | ok | 3.34e-03 | | | | | | |
| 10331 | ok | 3.32e-03 | | | | | | |
| 10332 | ok | 6.29e-03 | | | | | | |
| 10333 | ok | 9.54e-03 | | | | | | |
| 10334 | ok | 3.88e-03 | | | | | | |
| 10335 | ok | 3.92e-03 | | | | | | |
| 10336 | ok | 7.20e-03 | | | | | | |
| 10337 | ok | 0.01 | | | | | | |
| 10338 | ok | 4.54e-03 | | | | | | |
| 10339 | ok | 4.56e-03 | | | | | | |
| 10340 | ok | 8.31e-03 | | | | | | |
| 10341 | ok | 0.01 | | | | | | |
| 10342 | ok | 5.19e-03 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------------|-------|----------------|-----------------|------------------|----------------|-----------------|-------------|--------------|
| 10343 | ok | 5.47e-03 | | | | | | |
| 10344 | ok | 9.62e-03 | | | | | | |
| 10345 | ok | 0.02 | | | | | | |
| 10346 | ok | 6.17e-03 | | | | | | |
| 10347 | ok | 6.57e-03 | | | | | | |
| 10348 | ok | 0.01 | | | | | | |
| 10349 | ok | 0.02 | | | | | | |
| 10350 | ok | 7.40e-03 | | | | | | |
| 10351 | ok | 8.05e-03 | | | | | | |
| 10352 | ok | 0.01 | | | | | | |
| 10353 | ok | 0.02 | | | | | | |
| 10354 | ok | 8.97e-03 | | | | | | |
| 10355 | ok | 9.90e-03 | | | | | | |
| 10356 | ok | 0.02 | | | | | | |
| 10357 | ok | 0.03 | | | | | | |
| 10358 | ok | 0.01 | | | | | | |
| 10359 | ok | 0.01 | | | | | | |
| 10360 | ok | 0.02 | | | | | | |
| 10361 | ok | 0.03 | | | | | | |
| 10362 | ok | 0.01 | | | | | | |
| 10363 | ok | 0.02 | | | | | | |
| 10364 | ok | 0.02 | | | | | | |
| 10365 | ok | 0.04 | | | | | | |
| 10366 | ok | 0.02 | | | | | | |
| 10367 | ok | 0.02 | | | | | | |
| 10368 | ok | 0.03 | | | | | | |
| 10369 | ok | 0.05 | | | | | | |
| 10370 | ok | 0.02 | | | | | | |
| 10371 | ok | 0.03 | | | | | | |
| 10372 | ok | 0.03 | | | | | | |
| 10373 | ok | 0.06 | | | | | | |
| 10374 | ok | 0.03 | | | | | | |
| 10375 | ok | 0.04 | | | | | | |
| 10376 | ok | 0.04 | | | | | | |
| 10377 | ok | 0.08 | | | | | | |
| 10378 | ok | 0.04 | | | | | | |
| 10379 | ok | 0.05 | | | | | | |
| 10380 | ok | 0.05 | | | | | | |
| 10381 | ok | 0.10 | | | | | | |
| 10382 | ok | 0.06 | | | | | | |
| 10383 | ok | 0.06 | | | | | | |
| 10384 | ok | 0.06 | | | | | | |
| 10385 | ok | 0.14 | | | | | | |
| 10386 | ok | 0.09 | | | | | | |
| 10387 | ok | 0.08 | | | | | | |
| 10388 | ok | 0.07 | | | | | | |
| 10389 | ok | 0.22 | | | | | | |
| 10390 | ok | 0.13 | | | | | | |
| 10391 | ok | 0.10 | | | | | | |
| 10392 | ok | 0.09 | | | | | | |
| 10393 | ok | 0.42 | | | | | | |
| 10394 | ok | 0.17 | | | | | | |
| 10395 | ok | 0.11 | | | | | | |
| 10396 | ok | 0.09 | | | | | | |
| 10397 | ok | 0.42 | | | | | | |
| 10398 | ok | 0.17 | | | | | | |
| 10399 | ok | 0.11 | | | | | | |
| 10400 | ok | 0.09 | | | | | | |
| 10401 | ok | 0.29 | | | | | | |
| 10402 | ok | 0.15 | | | | | | |
| 10403 | ok | 0.09 | | | | | | |
| 10404 | ok | 0.09 | | | | | | |
| 10405 | ok | 0.24 | | | | | | |
| 10406 | ok | 0.22 | | | | | | |
| 10407 | ok | 0.17 | | | | | | |
| 10408 | ok | 0.16 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 3.24 | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 70 | 20.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|---------|--------|---------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 21 | ok | 0.21 | 0.6 | 4.49e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -78.5 | 71.9 | -58.3 | -353.6 | -808.1 | -269.7 |
| 30 | ok | 0.21 | 0.4 | 3.84e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -68.9 | -24.8 | 34.3 | -281.4 | -723.2 | 267.1 |
| 53 | ok | 0.22 | 1.0 | 4.09e-02 | 4.5 | 4.9 | 3.1 | 4.3 | 33.5 | 247.4 | -36.8 | 300.8 | 277.7 | -197.7 |
| 54 | ok | 0.21 | 0.5 | 0.2 | 4.5 | 4.5 | 3.1 | 3.1 | -193.0 | -250.8 | -152.6 | -1135.7 | -412.2 | -1050.8 |
| 55 | ok | 0.21 | 0.5 | 0.2 | 4.5 | 4.5 | 3.1 | 3.1 | -191.2 | -273.9 | 152.3 | -1111.9 | -462.3 | 1037.1 |
| 58 | ok | 0.21 | 0.9 | 5.65e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -129.1 | -109.6 | -27.2 | -733.8 | 138.3 | -137.9 |
| 2883 | ok | 0.21 | 0.4 | 4.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -82.3 | 47.7 | -36.1 | -372.7 | -322.0 | -238.2 |
| 2885 | ok | 0.21 | 0.4 | 4.27e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -88.2 | 46.9 | -33.3 | -392.2 | -166.5 | -210.0 |
| 2887 | ok | 0.21 | 0.4 | 4.41e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -92.7 | 52.2 | -31.3 | -402.6 | -89.9 | -181.0 |
| 2889 | ok | 0.21 | 0.5 | 4.39e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -91.5 | 64.2 | -30.8 | -391.7 | -42.7 | -142.5 |
| 2891 | ok | 0.21 | 0.7 | 4.60e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -132.4 | -109.7 | 7.0 | -502.9 | 118.1 | -98.6 |
| 3268 | ok | 0.21 | 0.2 | 3.23e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -64.6 | -22.1 | 25.8 | -311.2 | -289.1 | 213.8 |
| 3285 | ok | 0.21 | 0.2 | 3.30e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -67.9 | -22.3 | 24.3 | -320.3 | -136.2 | 184.7 |
| 3302 | ok | 0.21 | 0.2 | 3.41e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -70.9 | -27.2 | 16.8 | -320.8 | -64.7 | 173.0 |
| 3319 | ok | 0.21 | 0.2 | 3.54e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -77.0 | -25.8 | 15.1 | -347.8 | -24.3 | 159.6 |
| 3336 | ok | 0.21 | 0.2 | 3.68e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -83.2 | -24.2 | 15.3 | -379.1 | 4.1 | 139.5 |
| 3353 | ok | 0.21 | 0.2 | 3.78e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -75.1 | -60.5 | -8.5 | -343.1 | 41.8 | 135.5 |
| 3370 | ok | 0.21 | 0.3 | 3.90e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -89.4 | -72.7 | -8.8 | -403.2 | 70.3 | 121.7 |
| 3387 | ok | 0.21 | 0.4 | 4.07e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -113.4 | -94.2 | -7.4 | -477.8 | 118.4 | 111.9 |
| 3404 | ok | 0.21 | 0.5 | 4.85e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -145.3 | -122.5 | -13.4 | -650.3 | 178.9 | 41.1 |
| 3461 | ok | 0.21 | 0.4 | 9.38e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -206.0 | -174.6 | 35.2 | -1108.8 | 120.6 | 211.1 |
| 3478 | ok | 0.21 | 0.3 | 8.18e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -184.5 | -144.8 | 27.0 | -938.1 | 100.1 | 133.3 |
| 3495 | ok | 0.21 | 0.3 | 7.51e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -175.9 | -131.2 | 19.5 | -865.7 | 86.6 | 90.7 |
| 3512 | ok | 0.21 | 0.3 | 7.18e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -173.1 | -124.5 | 12.3 | -839.6 | 82.2 | 55.0 |
| 3529 | ok | 0.21 | 0.3 | 7.14e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -176.3 | -124.4 | -1.4 | -855.2 | 85.7 | 21.3 |
| 3546 | ok | 0.21 | 0.3 | 7.56e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -184.8 | -130.5 | -7.3 | -906.3 | 97.3 | -24.8 |
| 3563 | ok | 0.21 | 0.3 | 8.31e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -197.9 | -142.6 | -16.4 | -999.1 | 117.5 | -78.9 |
| 3580 | ok | 0.21 | 0.4 | 9.47e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -220.9 | -168.7 | -27.2 | -1181.5 | 143.5 | -174.6 |
| 7323 | ok | 0.21 | 0.1 | 4.57e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -44.2 | -18.2 | -78.5 | 28.9 | -95.3 | -44.5 |
| 7332 | ok | 0.21 | 0.1 | 4.14e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -28.8 | -32.3 | 69.4 | 23.5 | -75.4 | 31.9 |
| 7351 | ok | 0.21 | 0.3 | 5.73e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -52.5 | 16.0 | -61.4 | -116.8 | -120.8 | -227.4 |
| 7352 | ok | 0.21 | 0.5 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -105.5 | -131.7 | -207.6 | -473.8 | -144.6 | -614.6 |
| 7353 | ok | 0.21 | 0.5 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -108.5 | -138.3 | 211.8 | -426.0 | -159.0 | 585.8 |
| 7354 | ok | 0.21 | 0.3 | 6.26e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -74.4 | -27.6 | -98.2 | -315.8 | -137.7 | -379.7 |
| 7356 | ok | 0.21 | 0.3 | 6.53e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -63.1 | 16.1 | 62.2 | -232.0 | -123.1 | 308.3 |
| 7472 | ok | 0.21 | 0.2 | 4.93e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -44.6 | -6.6 | -74.4 | -12.3 | -85.1 | -64.2 |
| 7473 | ok | 0.21 | 0.2 | 5.29e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -46.0 | 6.4 | -67.1 | -27.5 | -88.0 | -87.1 |
| 7474 | ok | 0.21 | 0.2 | 5.66e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -53.8 | 12.2 | -68.7 | -44.1 | -99.8 | -120.1 |
| 7475 | ok | 0.21 | 0.2 | 5.84e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -58.0 | 15.6 | -66.7 | -69.0 | -109.8 | -158.6 |
| 7476 | ok | 0.21 | 0.3 | 5.83e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -59.0 | 15.9 | -62.8 | -105.0 | -116.1 | -199.1 |
| 7477 | ok | 0.21 | 0.1 | 5.06e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -55.4 | 7.4 | -46.9 | -13.4 | 75.2 | 36.1 |
| 7478 | ok | 0.21 | 0.1 | 5.68e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -56.6 | -29.5 | 93.6 | 6.6 | -77.8 | 47.9 |
| 7479 | ok | 0.21 | 0.2 | 5.92e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -63.0 | -26.8 | 97.1 | -9.6 | -94.4 | 88.5 |
| 7480 | ok | 0.21 | 0.2 | 5.89e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -66.3 | -21.4 | 96.7 | -38.9 | -107.3 | 132.8 |
| 7481 | ok | 0.21 | 0.2 | 5.67e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -67.6 | -14.0 | 93.3 | -74.5 | -116.3 | 175.1 |
| 7482 | ok | 0.21 | 0.2 | 6.06e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -67.7 | -5.8 | 87.8 | -111.3 | -122.1 | 212.9 |
| 7483 | ok | 0.21 | 0.3 | 6.48e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -68.1 | 6.5 | 83.3 | -160.8 | -123.7 | 254.8 |
| 7484 | ok | 0.21 | 0.3 | 6.74e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -67.4 | 13.8 | 76.1 | -187.6 | -124.4 | 277.0 |
| 7485 | ok | 0.21 | 0.3 | 6.77e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -65.0 | 18.2 | 68.6 | -206.3 | -124.3 | 292.6 |
| 7486 | ok | 0.21 | 0.5 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -119.2 | -116.0 | 210.7 | -474.6 | -159.3 | 628.8 |
| 7487 | ok | 0.21 | 0.5 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -121.8 | -90.3 | 199.3 | -511.8 | -154.6 | 660.0 |
| 7488 | ok | 0.21 | 0.5 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -117.8 | -66.6 | 184.0 | -550.8 | -142.6 | 682.4 |
| 7489 | ok | 0.21 | 0.5 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -115.5 | -38.5 | 168.7 | -575.0 | -127.1 | 684.7 |
| 7490 | ok | 0.21 | 0.5 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -112.2 | -8.2 | 151.1 | -586.6 | -109.1 | 671.0 |
| 7491 | ok | 0.21 | 0.5 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -119.5 | -59.6 | -182.2 | -559.0 | -118.0 | -671.9 |
| 7492 | ok | 0.21 | 0.5 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -121.7 | -85.5 | -198.5 | -536.9 | -132.6 | -668.6 |
| 7493 | ok | 0.21 | 0.5 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -116.7 | -111.4 | -208.4 | -506.0 | -140.4 | -646.1 |
| 7691 | ok | 0.21 | 0.2 | 3.02e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -41.0 | -22.1 | 36.0 | -105.5 | -334.2 | 145.6 |
| 7745 | ok | 0.21 | 0.1 | 2.66e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -43.5 | -18.3 | 30.4 | -39.5 | -141.1 | 71.6 |
| 7799 | ok | 0.21 | 6.41e-02 | 2.40e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -42.6 | -17.9 | 25.4 | -14.9 | -51.1 | 49.5 |
| 7853 | ok | 0.21 | 6.15e-02 | 2.42e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -46.1 | -8.5 | -12.5 | -3.0 | 35.7 | 75.8 |
| 8762 | ok | 0.21 | 0.4 | 3.18e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -48.4 | 44.1 | -50.0 | -114.9 | -324.4 | -124.6 |
| 8763 | ok | 0.21 | 0.2 | 2.63e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -46.1 | 32.4 | -34.4 | -39.8 | -122.6 | -72.9 |
| 8764 | ok | 0.21 | 0.2 | 2.29e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -47.6 | 22.0 | -18.1 | -13.7 | -40.8 | -56.1 |
| 8765 | ok | 0.21 | 0.1 | 2.84e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -57.0 | 5.4 | 28.7 | -8.5 | 43.0 | -94.3 |
| 8766 | ok | 0.21 | 0.4 | 3.86e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -76.0 | 59.0 | -42.0 | -235.0 | -277.0 | -164.0 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|-------|----------|--------|--------|---------|---------|--------|-------|--------|--------|--------|--------|
| 8767 | ok | 0.21 | 0.3 | 3.21e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -62.8 | 43.5 | -30.4 | -94.5 | -164.7 | -95.9 |
| 8768 | ok | 0.21 | 0.2 | 2.86e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -62.6 | 25.4 | -21.2 | -47.6 | -85.4 | -67.7 |
| 8769 | ok | 0.21 | 0.2 | 3.49e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -57.5 | 2.0 | -48.2 | -28.4 | -67.1 | -25.7 |
| 8770 | ok | 0.21 | 0.4 | 3.96e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -82.8 | 57.9 | -30.0 | -267.8 | -160.5 | -179.0 |
| 8771 | ok | 0.21 | 0.3 | 3.48e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -80.6 | 45.1 | -21.7 | -159.0 | -138.2 | -146.3 |
| 8772 | ok | 0.21 | 0.2 | 3.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -73.1 | 32.0 | -20.5 | -91.5 | -98.7 | -98.5 |
| 8773 | ok | 0.21 | 0.2 | 3.71e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -62.5 | 6.2 | -41.5 | -58.7 | -82.8 | -77.3 |
| 8774 | ok | 0.21 | 0.4 | 3.99e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -87.9 | 64.5 | -20.6 | -277.0 | -102.5 | -154.6 |
| 8775 | ok | 0.21 | 0.3 | 3.51e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -83.7 | 52.3 | -12.4 | -193.9 | -99.2 | -152.9 |
| 8776 | ok | 0.21 | 0.2 | 3.15e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -75.8 | 36.6 | -13.0 | -127.3 | -82.6 | -120.6 |
| 8777 | ok | 0.21 | 0.2 | 4.02e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -60.8 | 9.3 | -31.8 | -81.7 | -77.9 | -95.0 |
| 8778 | ok | 0.21 | 0.4 | 3.87e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -93.1 | 68.7 | -9.1 | -297.8 | -57.8 | -146.4 |
| 8779 | ok | 0.21 | 0.3 | 3.37e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -78.6 | 56.3 | -2.0 | -207.7 | -63.6 | -146.7 |
| 8780 | ok | 0.21 | 0.2 | 3.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -70.6 | 38.2 | -5.7 | -153.1 | -61.3 | -130.6 |
| 8781 | ok | 0.21 | 0.2 | 4.16e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -62.6 | 12.8 | -29.0 | -107.8 | -80.2 | -116.0 |
| 8782 | ok | 0.21 | 0.5 | 3.93e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -114.4 | -33.1 | 27.5 | -404.0 | -25.3 | -26.4 |
| 8783 | ok | 0.21 | 0.3 | 3.09e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -87.5 | -24.9 | 25.5 | -254.4 | -58.5 | -78.4 |
| 8784 | ok | 0.21 | 0.2 | 2.86e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -58.2 | 36.1 | -1.3 | -170.8 | -40.5 | -132.3 |
| 8785 | ok | 0.21 | 0.2 | 4.17e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -60.0 | 13.8 | -25.6 | -131.3 | -79.8 | -135.0 |
| 8786 | ok | 0.21 | 0.6 | 3.80e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -88.0 | -38.8 | 34.5 | -462.6 | -28.0 | 38.7 |
| 8787 | ok | 0.21 | 0.4 | 3.00e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -64.5 | -33.1 | 41.5 | -230.2 | -50.2 | -66.9 |
| 8788 | ok | 0.21 | 0.2 | 2.54e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -60.3 | -22.8 | 32.4 | -163.2 | -32.7 | -69.4 |
| 8789 | ok | 0.21 | 0.2 | 3.64e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -54.5 | 13.1 | -27.9 | -152.7 | -76.5 | -154.2 |
| 8790 | ok | 0.21 | 0.6 | 2.54e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 0.6 | 119.7 | -9.9 | -67.7 | 28.5 | -75.3 |
| 8791 | ok | 0.23 | 1.0 | 3.24e-02 | 4.5 | 5.0 | 3.1 | 3.7 | 49.3 | 240.3 | -43.9 | 53.6 | 99.0 | -189.7 |
| 8792 | ok | 0.21 | 0.4 | 2.47e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -44.6 | -30.4 | 29.2 | -164.5 | -31.1 | -67.2 |
| 8793 | ok | 0.21 | 0.3 | 2.21e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -40.9 | -27.0 | 32.5 | -170.0 | -24.6 | -66.9 |
| 8794 | ok | 0.21 | 0.2 | 3.27e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -45.4 | 7.4 | -23.6 | -171.2 | -72.3 | -157.2 |
| 8795 | ok | 0.21 | 0.3 | 5.19e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -55.2 | -24.2 | -80.1 | -177.5 | -140.0 | -303.8 |
| 8796 | ok | 0.21 | 0.6 | 1.98e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 1.3 | 123.8 | -14.9 | -34.5 | 20.6 | -108.1 |
| 8797 | ok | 0.21 | 0.7 | 9.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 1.3 | 149.0 | -6.2 | 18.1 | -11.4 | -72.5 |
| 8798 | ok | 0.21 | 0.4 | 1.84e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -3.1 | 70.6 | -22.6 | -80.7 | 12.4 | -71.2 |
| 8799 | ok | 0.21 | 0.3 | 1.85e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.7 | -25.4 | 25.1 | -176.9 | -21.2 | -59.8 |
| 8800 | ok | 0.21 | 0.2 | 3.24e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -42.5 | -5.8 | -51.5 | -222.0 | -78.0 | -192.1 |
| 8801 | ok | 0.21 | 0.3 | 5.62e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -53.7 | -37.9 | -90.0 | -218.4 | -134.9 | -328.1 |
| 8802 | ok | 0.21 | 0.5 | 1.27e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 75.4 | -12.7 | -133.1 | -19.5 | -191.6 |
| 8803 | ok | 0.21 | 0.6 | 3.48e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 4.2 | 137.0 | 2.4 | 25.0 | -59.6 | -87.1 |
| 8804 | ok | 0.21 | 0.4 | 1.46e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -18.4 | 39.2 | -28.7 | -251.7 | -2.3 | -142.4 |
| 8805 | ok | 0.21 | 0.3 | 2.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.8 | 23.4 | -30.9 | -266.9 | -15.7 | -89.4 |
| 8806 | ok | 0.21 | 0.2 | 3.90e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -48.9 | -11.2 | -62.0 | -254.7 | -80.3 | -190.2 |
| 8807 | ok | 0.21 | 0.3 | 6.40e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -56.8 | -47.1 | -102.8 | -246.5 | -129.3 | -338.9 |
| 8808 | ok | 0.21 | 0.4 | 1.62e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -25.1 | 11.2 | -26.2 | -313.9 | -33.5 | -367.5 |
| 8809 | ok | 0.21 | 0.6 | 2.41e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 38.6 | 136.0 | 13.6 | 196.0 | -41.3 | -102.7 |
| 8810 | ok | 0.21 | 0.3 | 3.54e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -59.1 | 33.4 | -57.7 | -393.6 | -30.4 | -146.6 |
| 8811 | ok | 0.21 | 0.3 | 3.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -59.3 | 28.8 | -39.8 | -313.7 | -44.2 | -75.4 |
| 8812 | ok | 0.21 | 0.2 | 4.50e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -61.6 | -11.2 | -68.8 | -286.2 | -90.1 | -183.5 |
| 8813 | ok | 0.21 | 0.3 | 6.98e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -66.1 | -46.9 | -112.2 | -269.4 | -126.6 | -344.8 |
| 8816 | ok | 0.21 | 0.3 | 5.63e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -117.4 | 26.8 | -58.9 | -445.9 | -249.4 | -158.2 |
| 8817 | ok | 0.21 | 0.3 | 3.85e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -83.9 | 36.0 | -32.6 | -335.1 | -89.6 | -63.3 |
| 8818 | ok | 0.21 | 0.2 | 4.74e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -75.3 | -5.9 | -66.6 | -315.1 | -108.0 | -179.8 |
| 8819 | ok | 0.21 | 0.3 | 7.15e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -83.0 | -35.0 | -112.1 | -335.5 | -126.9 | -365.1 |
| 8822 | ok | 0.21 | 0.4 | 5.39e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -131.5 | 59.9 | -17.3 | -465.8 | -107.9 | -61.2 |
| 8823 | ok | 0.21 | 0.3 | 4.03e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -94.6 | 38.4 | -26.2 | -356.9 | -86.4 | -72.1 |
| 8824 | ok | 0.21 | 0.2 | 5.03e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -86.5 | 5.1 | -68.4 | -330.9 | -111.5 | -209.4 |
| 8825 | ok | 0.21 | 0.3 | 6.69e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -79.0 | -31.3 | -104.7 | -331.6 | -134.2 | -370.6 |
| 8827 | ok | 0.21 | 0.3 | 5.09e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -115.9 | 21.2 | 35.1 | -448.5 | -235.6 | 26.6 |
| 8828 | ok | 0.21 | 0.2 | 3.66e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -89.3 | 34.7 | -11.5 | -362.8 | -75.3 | -67.7 |
| 8829 | ok | 0.21 | 0.2 | 4.69e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -82.6 | 4.9 | -62.0 | -335.2 | -110.3 | -217.0 |
| 8830 | ok | 0.21 | 0.2 | 2.30e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -38.4 | 7.0 | 28.8 | -394.7 | -33.4 | 274.8 |
| 8831 | ok | 0.21 | 0.4 | 1.79e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 41.8 | 107.0 | -14.1 | 193.7 | -23.1 | 86.5 |
| 8832 | ok | 0.21 | 0.2 | 3.56e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -73.2 | 23.9 | 34.9 | -433.4 | -52.6 | 21.6 |
| 8833 | ok | 0.21 | 0.2 | 2.85e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -68.1 | 22.1 | -4.2 | -347.7 | -63.3 | -57.7 |
| 8834 | ok | 0.21 | 0.2 | 4.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -71.6 | -1.2 | -54.0 | -337.0 | -106.8 | -215.5 |
| 8835 | ok | 0.21 | 0.3 | 5.93e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -73.6 | -25.5 | -91.5 | -329.7 | -137.1 | -395.0 |
| 8836 | ok | 0.21 | 0.2 | 5.38e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.3 | 36.9 | 2.2 | -178.0 | -71.0 | 147.5 |
| 8837 | ok | 0.21 | 0.4 | 1.99e-04 | 4.5 | 4.5 | 3.1 | 3.1 | 4.9 | 97.9 | -3.6 | 25.0 | -95.8 | 66.6 |
| 8838 | ok | 0.21 | 0.2 | 1.51e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -30.0 | 16.9 | 10.8 | -314.8 | -38.6 | 22.8 |
| 8839 | ok | 0.21 | 0.1 | 2.04e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -47.8 | 10.4 | -7.6 | -325.6 | -59.4 | -49.0 |
| 8840 | ok | 0.21 | 0.2 | 3.83e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -60.9 | -8.0 | -52.8 | -336.2 | -102.7 | -220.9 |
| 8841 | ok | 0.21 | 0.3 | 5.72e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -69.7 | -28.9 | -87.2 | -343.6 | -137.0 | -408.6 |
| 8842 | ok | 0.21 | 0.2 | 3.11e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.2 | 41.9 | -8.4 | -98.8 | -122.8 | 13.9 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|-------|----------|--------|--------|---------|---------|--------|--------|--------|--------|--------|--------|
| 8843 | ok | 0.21 | 0.4 | 2.75e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.4 | 81.4 | -1.3 | 8.1 | -143.4 | 8.9 |
| 8844 | ok | 0.21 | 0.2 | 8.31e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -12.9 | 15.7 | -11.7 | -218.7 | -79.0 | -14.7 |
| 8845 | ok | 0.21 | 0.2 | 1.77e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -27.7 | -3.2 | -24.9 | -288.6 | -71.9 | -55.0 |
| 8846 | ok | 0.21 | 0.2 | 4.09e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -46.1 | -26.5 | -62.0 | -331.6 | -102.9 | -236.8 |
| 8847 | ok | 0.21 | 0.3 | 6.22e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -62.9 | -50.1 | -93.9 | -361.8 | -136.8 | -434.2 |
| 8848 | ok | 0.21 | 0.2 | 4.45e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.8 | 36.1 | -12.4 | -89.6 | -137.8 | -41.9 |
| 8849 | ok | 0.21 | 0.3 | 2.98e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.6 | 71.3 | -1.0 | 7.6 | -157.4 | -12.7 |
| 8850 | ok | 0.21 | 0.1 | 1.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -11.3 | 8.6 | -21.6 | -206.6 | -94.0 | -45.8 |
| 8851 | ok | 0.21 | 0.2 | 2.14e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -24.9 | -9.9 | -33.7 | -284.5 | -79.1 | -67.9 |
| 8852 | ok | 0.21 | 0.2 | 4.65e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -44.4 | -38.9 | -70.7 | -332.3 | -103.9 | -249.2 |
| 8853 | ok | 0.21 | 0.3 | 7.03e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -60.5 | -70.9 | -103.9 | -349.0 | -136.8 | -444.7 |
| 8854 | ok | 0.21 | 0.3 | 2.58e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.1 | 43.1 | -4.3 | -122.0 | -101.9 | 73.8 |
| 8855 | ok | 0.21 | 0.4 | 2.33e-04 | 4.5 | 4.5 | 3.1 | 3.1 | 0.3 | 90.2 | -1.9 | 10.3 | -124.9 | 33.9 |
| 8856 | ok | 0.21 | 0.2 | 7.72e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -18.2 | 16.6 | -5.0 | -248.5 | -61.8 | 5.4 |
| 8857 | ok | 0.21 | 0.2 | 1.65e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.7 | 2.7 | -15.8 | -303.6 | -63.9 | -47.8 |
| 8858 | ok | 0.21 | 0.2 | 3.80e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -51.7 | -16.6 | -55.6 | -333.7 | -101.9 | -226.9 |
| 8859 | ok | 0.21 | 0.3 | 5.79e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -65.8 | -37.0 | -87.9 | -357.1 | -136.7 | -421.5 |
| 8860 | ok | 0.21 | 0.2 | 6.87e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.8 | 25.6 | -15.1 | -90.9 | -148.9 | -102.2 |
| 8861 | ok | 0.21 | 0.3 | 3.64e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.6 | 59.2 | -0.7 | 7.7 | -169.2 | -35.6 |
| 8862 | ok | 0.21 | 0.1 | 1.46e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -11.3 | -0.3 | -29.0 | -210.5 | -102.7 | -80.9 |
| 8863 | ok | 0.21 | 0.2 | 2.69e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -24.6 | -18.5 | -43.3 | -291.2 | -84.6 | -84.6 |
| 8864 | ok | 0.21 | 0.2 | 5.42e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -43.7 | -56.2 | -80.6 | -340.8 | -107.3 | -254.2 |
| 8865 | ok | 0.21 | 0.3 | 8.28e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -65.3 | -90.8 | -120.8 | -367.5 | -137.3 | -467.9 |
| 8866 | ok | 0.21 | 0.2 | 1.13e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -2.3 | 12.7 | -16.6 | -100.2 | -152.4 | -163.5 |
| 8867 | ok | 0.21 | 0.3 | 7.30e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.4 | 47.6 | -0.4 | 8.3 | -174.3 | -58.9 |
| 8868 | ok | 0.21 | 0.1 | 2.11e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -11.7 | -12.1 | -35.4 | -231.7 | -104.9 | -119.5 |
| 8869 | ok | 0.21 | 0.2 | 3.45e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.0 | -28.8 | -54.5 | -313.1 | -87.2 | -105.5 |
| 8870 | ok | 0.21 | 0.2 | 6.49e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -50.0 | -72.1 | -94.7 | -360.8 | -110.1 | -274.3 |
| 8871 | ok | 0.21 | 0.4 | 9.63e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -70.4 | -110.7 | -140.0 | -386.9 | -140.1 | -493.7 |
| 8872 | ok | 0.21 | 0.2 | 1.85e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -6.2 | -10.6 | -25.1 | -146.4 | -143.4 | -201.1 |
| 8873 | ok | 0.21 | 0.3 | 3.92e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 0.2 | 42.9 | 4.6 | 7.4 | -108.7 | -61.1 |
| 8874 | ok | 0.21 | 0.2 | 3.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -18.7 | -28.6 | -47.2 | -277.7 | -100.4 | -158.6 |
| 8875 | ok | 0.21 | 0.2 | 4.40e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -39.5 | -39.0 | -67.1 | -350.8 | -87.4 | -123.7 |
| 8876 | ok | 0.21 | 0.2 | 7.63e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -60.4 | -86.5 | -109.8 | -389.8 | -112.7 | -294.0 |
| 8877 | ok | 0.21 | 0.4 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -77.0 | -127.4 | -160.8 | -409.4 | -142.7 | -522.6 |
| 8878 | ok | 0.21 | 0.2 | 3.15e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -12.8 | -42.5 | -35.3 | -207.9 | -154.9 | -350.4 |
| 8879 | ok | 0.21 | 0.4 | 1.30e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 9.2 | 14.1 | 5.0 | 50.6 | -180.8 | -122.3 |
| 8880 | ok | 0.21 | 0.2 | 4.54e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -38.0 | -46.7 | -67.2 | -361.0 | -95.0 | -194.2 |
| 8881 | ok | 0.21 | 0.2 | 5.48e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -58.7 | -46.2 | -79.9 | -403.1 | -87.9 | -136.2 |
| 8882 | ok | 0.21 | 0.2 | 8.73e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -75.9 | -96.2 | -124.1 | -425.8 | -115.6 | -312.5 |
| 8883 | ok | 0.21 | 0.4 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -85.9 | -137.5 | -181.3 | -434.5 | -144.8 | -553.6 |
| 8884 | ok | 0.21 | 0.4 | 8.89e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -59.0 | -132.7 | -111.6 | -496.9 | -290.1 | -635.3 |
| 8885 | ok | 0.21 | 0.9 | 3.47e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 98.5 | 5.2 | 47.1 | 503.7 | -21.9 | 5.0 |
| 8886 | ok | 0.21 | 0.2 | 6.28e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -81.5 | -52.9 | -83.9 | -462.4 | -107.3 | -203.5 |
| 8887 | ok | 0.21 | 0.2 | 6.51e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -88.3 | -47.6 | -87.9 | -465.4 | -91.1 | -140.8 |
| 8888 | ok | 0.21 | 0.3 | 9.61e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -96.2 | -98.9 | -134.6 | -465.7 | -119.0 | -329.4 |
| 8889 | ok | 0.21 | 0.5 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -96.8 | -138.4 | -198.4 | -461.4 | -146.0 | -586.3 |
| 8890 | ok | 0.21 | 0.3 | 9.01e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -143.8 | -52.0 | -91.3 | -881.0 | 28.9 | -317.1 |
| 8891 | ok | 0.21 | 0.2 | 7.51e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -138.5 | -42.0 | -76.5 | -578.8 | -86.0 | -194.7 |
| 8892 | ok | 0.21 | 0.2 | 7.22e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -122.6 | -44.5 | -83.9 | -531.0 | -93.4 | -137.9 |
| 8893 | ok | 0.21 | 0.3 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -118.4 | -94.6 | -138.1 | -505.0 | -120.1 | -346.2 |
| 8894 | ok | 0.21 | 0.3 | 9.47e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -231.1 | -74.5 | -20.6 | -982.7 | 8.0 | -233.2 |
| 8895 | ok | 0.21 | 0.3 | 7.87e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -174.9 | -46.5 | -52.2 | -678.2 | -63.0 | -163.1 |
| 8896 | ok | 0.21 | 0.2 | 7.36e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -148.6 | -42.8 | -66.2 | -590.4 | -87.8 | -124.4 |
| 8897 | ok | 0.21 | 0.3 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -133.9 | -87.6 | -130.3 | -542.1 | -118.2 | -348.5 |
| 8898 | ok | 0.21 | 0.3 | 7.84e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -188.3 | -98.2 | -11.4 | -872.0 | 42.0 | -102.2 |
| 8899 | ok | 0.21 | 0.3 | 7.44e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -177.8 | -55.5 | -23.7 | -726.1 | -34.2 | -111.1 |
| 8900 | ok | 0.21 | 0.2 | 7.09e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -158.3 | -46.3 | -45.3 | -631.9 | -74.2 | -100.2 |
| 8901 | ok | 0.21 | 0.3 | 9.55e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -143.4 | -76.1 | -117.7 | -573.9 | -110.6 | -351.6 |
| 8902 | ok | 0.21 | 0.3 | 7.26e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -179.0 | -98.3 | -3.3 | -828.4 | 40.2 | -39.2 |
| 8903 | ok | 0.21 | 0.3 | 6.98e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -169.4 | -66.6 | -9.0 | -735.9 | -15.8 | -51.0 |
| 8904 | ok | 0.21 | 0.2 | 6.68e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -158.0 | -50.3 | -27.5 | -653.8 | -61.5 | -66.4 |
| 8905 | ok | 0.21 | 0.3 | 8.77e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -144.9 | -62.9 | -101.9 | -595.8 | -99.6 | -344.1 |
| 8906 | ok | 0.21 | 0.3 | 6.93e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -168.9 | -99.3 | 1.7 | -800.1 | 38.2 | 20.4 |
| 8907 | ok | 0.21 | 0.3 | 6.67e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -164.6 | -71.2 | 2.9 | -727.7 | -10.8 | 2.3 |
| 8908 | ok | 0.21 | 0.2 | 6.32e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -154.4 | -51.7 | -13.1 | -659.1 | -54.2 | -28.7 |
| 8909 | ok | 0.21 | 0.3 | 7.93e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -138.8 | -36.1 | 76.5 | -609.0 | -92.2 | 322.9 |
| 8910 | ok | 0.21 | 0.3 | 6.87e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -168.3 | -99.6 | 8.1 | -789.6 | 37.6 | 35.7 |
| 8911 | ok | 0.21 | 0.3 | 6.62e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -162.0 | -72.2 | 10.2 | -716.2 | -11.2 | 42.7 |
| 8912 | ok | 0.21 | 0.2 | 6.35e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -151.3 | -53.3 | 22.3 | -651.6 | -55.4 | 61.6 |
| 8913 | ok | 0.21 | 0.3 | 8.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -139.5 | -54.3 | 91.7 | -600.4 | -101.0 | 344.5 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|-------|----------|--------|--------|---------|---------|--------|--------|-------|--------|--------|--------|
| 8914 | ok | 0.21 | 0.3 | 7.09e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -171.9 | -101.8 | 13.2 | -803.2 | 35.8 | 84.4 |
| 8915 | ok | 0.21 | 0.3 | 6.87e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -164.4 | -70.3 | 15.9 | -718.7 | -16.2 | 86.4 |
| 8916 | ok | 0.21 | 0.2 | 6.68e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -155.1 | -53.4 | 32.1 | -638.9 | -62.2 | 94.4 |
| 8917 | ok | 0.21 | 0.3 | 8.89e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -143.6 | -66.8 | 104.5 | -580.8 | -112.3 | 355.4 |
| 8918 | ok | 0.21 | 0.3 | 7.55e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -182.0 | -102.9 | 18.4 | -834.5 | 28.2 | 147.1 |
| 8919 | ok | 0.21 | 0.3 | 7.31e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -171.7 | -61.5 | 27.7 | -703.0 | -35.3 | 143.3 |
| 8920 | ok | 0.21 | 0.2 | 7.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -155.0 | -50.6 | 48.2 | -609.9 | -74.9 | 126.7 |
| 8921 | ok | 0.21 | 0.3 | 9.69e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -142.8 | -80.5 | 119.9 | -551.4 | -122.2 | 358.1 |
| 8922 | ok | 0.21 | 0.3 | 9.15e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -222.7 | -87.0 | 20.7 | -949.9 | -6.0 | 251.7 |
| 8923 | ok | 0.21 | 0.3 | 7.81e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -171.3 | -52.9 | 53.3 | -652.0 | -66.6 | 191.8 |
| 8924 | ok | 0.21 | 0.2 | 7.37e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -146.1 | -47.7 | 67.4 | -562.3 | -88.6 | 147.8 |
| 8925 | ok | 0.21 | 0.3 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -133.4 | -93.6 | 131.2 | -510.8 | -128.4 | 344.9 |
| 8926 | ok | 0.21 | 0.3 | 9.17e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -165.6 | -26.5 | 91.3 | -697.2 | 147.1 | 383.6 |
| 8927 | ok | 0.21 | 0.2 | 7.62e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -137.9 | -47.7 | 77.9 | -550.2 | -90.5 | 220.1 |
| 8928 | ok | 0.21 | 0.2 | 7.27e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -121.4 | -49.0 | 84.7 | -497.6 | -93.4 | 156.0 |
| 8929 | ok | 0.21 | 0.3 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -115.3 | -103.8 | 137.1 | -463.0 | -127.4 | 326.8 |
| 8930 | ok | 0.21 | 0.4 | 8.96e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -50.4 | -142.3 | 109.1 | -442.9 | -301.8 | 638.2 |
| 8931 | ok | 0.21 | 0.9 | 3.20e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 100.1 | -0.3 | -50.7 | 513.2 | -20.5 | -24.8 |
| 8932 | ok | 0.21 | 0.2 | 6.35e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -78.0 | -58.5 | 85.1 | -423.9 | -107.4 | 224.2 |
| 8933 | ok | 0.21 | 0.2 | 6.62e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -86.7 | -52.3 | 89.4 | -424.2 | -89.0 | 158.4 |
| 8934 | ok | 0.21 | 0.3 | 9.85e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -97.4 | -104.0 | 137.2 | -417.2 | -122.4 | 321.0 |
| 8935 | ok | 0.21 | 0.5 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -92.4 | -151.3 | 199.5 | -382.5 | -157.6 | 539.2 |
| 8936 | ok | 0.21 | 0.2 | 3.06e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -8.0 | -47.3 | 36.3 | -168.9 | -144.9 | 352.6 |
| 8937 | ok | 0.21 | 0.3 | 1.13e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 9.6 | 2.4 | -4.7 | 52.7 | -172.8 | 123.9 |
| 8938 | ok | 0.21 | 0.2 | 4.65e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -36.8 | -51.6 | 67.5 | -323.2 | -93.5 | 213.7 |
| 8939 | ok | 0.21 | 0.2 | 5.60e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -58.3 | -49.6 | 81.3 | -358.0 | -84.8 | 152.1 |
| 8940 | ok | 0.21 | 0.2 | 8.92e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -76.2 | -100.7 | 126.1 | -374.3 | -119.1 | 296.3 |
| 8941 | ok | 0.21 | 0.4 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -86.7 | -143.5 | 184.0 | -377.3 | -154.8 | 506.2 |
| 8942 | ok | 0.21 | 0.2 | 1.80e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -4.0 | -16.7 | 24.1 | -114.1 | -144.2 | 266.3 |
| 8943 | ok | 0.21 | 0.3 | 2.86e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 1.0 | 21.0 | -1.8 | 12.0 | -168.7 | 97.1 |
| 8944 | ok | 0.21 | 0.2 | 3.19e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -19.1 | -32.4 | 47.8 | -241.1 | -94.1 | 180.0 |
| 8945 | ok | 0.21 | 0.2 | 4.52e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -39.8 | -41.6 | 68.4 | -302.5 | -82.7 | 139.6 |
| 8946 | ok | 0.21 | 0.3 | 7.83e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -61.0 | -90.6 | 111.8 | -334.3 | -114.6 | 273.4 |
| 8947 | ok | 0.21 | 0.4 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -77.7 | -133.2 | 163.3 | -347.0 | -150.2 | 466.7 |
| 8948 | ok | 0.21 | 0.2 | 1.06e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -4.3 | 3.3 | 18.8 | -94.7 | -130.2 | 168.2 |
| 8949 | ok | 0.21 | 0.3 | 6.84e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.2 | 36.0 | -1.1 | 7.3 | -157.7 | 71.8 |
| 8950 | ok | 0.21 | 0.1 | 2.21e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -12.2 | -15.4 | 35.9 | -191.6 | -95.8 | 145.8 |
| 8951 | ok | 0.21 | 0.2 | 3.56e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.5 | -30.8 | 55.8 | -259.1 | -81.2 | 122.5 |
| 8952 | ok | 0.21 | 0.2 | 6.68e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -50.7 | -75.8 | 96.9 | -300.0 | -110.2 | 250.3 |
| 8953 | ok | 0.21 | 0.4 | 9.91e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -71.0 | -116.8 | 142.8 | -320.8 | -144.5 | 430.5 |
| 8954 | ok | 0.21 | 0.2 | 6.47e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.5 | 19.0 | 13.4 | -76.5 | -122.7 | 124.8 |
| 8955 | ok | 0.21 | 0.3 | 5.41e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.5 | 48.6 | 0.6 | 5.9 | -145.2 | 52.2 |
| 8956 | ok | 0.21 | 0.2 | 1.53e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -11.4 | -3.0 | 29.6 | -162.5 | -93.0 | 112.9 |
| 8957 | ok | 0.21 | 0.2 | 2.76e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -24.1 | -19.9 | 44.8 | -227.8 | -78.4 | 103.4 |
| 8958 | ok | 0.21 | 0.2 | 5.59e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -44.0 | -59.2 | 82.8 | -273.0 | -105.6 | 228.1 |
| 8959 | ok | 0.21 | 0.3 | 8.55e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -65.7 | -97.0 | 123.8 | -299.4 | -138.5 | 398.4 |
| 8960 | ok | 0.21 | 0.2 | 5.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.7 | 31.1 | 12.1 | -55.2 | -105.2 | 95.0 |
| 8961 | ok | 0.21 | 0.3 | 7.30e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.6 | 59.7 | -0.7 | 5.3 | -131.2 | 35.7 |
| 8962 | ok | 0.21 | 0.2 | 1.07e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -9.7 | 9.3 | 20.7 | -144.7 | -84.2 | 82.9 |
| 8963 | ok | 0.21 | 0.2 | 2.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -21.5 | -10.5 | 34.9 | -206.9 | -73.0 | 84.7 |
| 8964 | ok | 0.21 | 0.2 | 4.60e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -39.8 | -42.9 | 69.8 | -253.3 | -100.4 | 208.5 |
| 8965 | ok | 0.21 | 0.3 | 7.28e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -61.2 | -76.1 | 106.8 | -283.3 | -132.7 | 371.7 |
| 8966 | ok | 0.21 | 0.3 | 8.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.6 | 39.5 | 8.8 | -52.1 | -90.9 | 59.1 |
| 8967 | ok | 0.21 | 0.3 | 1.22e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.6 | 69.2 | -0.5 | 5.0 | -114.8 | 20.8 |
| 8968 | ok | 0.21 | 0.2 | 1.36e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -14.1 | -20.6 | -24.2 | -127.2 | -62.9 | 30.4 |
| 8969 | ok | 0.21 | 0.2 | 1.61e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -19.0 | 5.9 | 16.5 | -193.9 | -53.2 | 42.8 |
| 8970 | ok | 0.21 | 0.2 | 3.76e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.4 | -28.0 | 58.1 | -240.0 | -94.7 | 192.6 |
| 8971 | ok | 0.21 | 0.3 | 6.14e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -57.5 | -55.6 | 91.8 | -271.7 | -127.8 | 351.0 |
| 8972 | ok | 0.21 | 0.3 | 1.38e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 52.7 | 7.2 | -35.7 | -52.8 | 50.6 |
| 8973 | ok | 0.21 | 0.4 | 3.16e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 0.1 | 73.0 | 6.0 | 9.4 | -56.3 | 46.1 |
| 8974 | ok | 0.21 | 0.2 | 1.84e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -22.3 | -27.4 | -31.9 | -142.1 | -52.9 | -21.6 |
| 8975 | ok | 0.21 | 0.2 | 1.95e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -31.0 | -22.4 | -31.9 | -172.4 | -46.6 | 36.1 |
| 8976 | ok | 0.21 | 0.2 | 3.09e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.4 | -3.2 | 28.6 | -218.7 | -82.7 | 163.8 |
| 8977 | ok | 0.21 | 0.3 | 5.19e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -55.1 | -36.6 | 79.3 | -262.9 | -124.5 | 336.3 |
| 8978 | ok | 0.21 | 0.4 | 2.33e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 20.3 | 82.0 | 34.1 | 7.6 | 11.3 | 62.8 |
| 8979 | ok | 0.21 | 0.5 | 1.00e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 5.7 | 112.4 | 16.9 | 43.2 | 3.6 | 57.6 |
| 8980 | ok | 0.21 | 0.2 | 2.31e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -17.7 | -27.7 | -30.3 | -163.8 | -41.2 | -44.7 |
| 8981 | ok | 0.21 | 0.2 | 2.39e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -43.6 | -21.7 | -39.9 | -198.5 | -42.5 | 20.4 |
| 8982 | ok | 0.21 | 0.2 | 3.40e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -42.5 | 4.3 | 22.5 | -217.4 | -79.5 | 157.4 |
| 8983 | ok | 0.21 | 0.3 | 5.34e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -54.5 | -19.9 | 69.8 | -254.1 | -123.2 | 325.7 |
| 8984 | ok | 0.21 | 0.4 | 3.43e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -54.4 | -38.0 | -45.1 | -218.2 | 10.0 | -100.8 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------------|-------|------------|--------------|-----------------|---------------|---------------|----------------|----------------|------------|------------|-------------|------------|------------|-------------|
| 8985 | ok | 0.22 | 1.0 | 3.46e-02 | 4.5 | 4.6 | 3.1 | 3.2 | 65.3 | 185.5 | 53.4 | 117.2 | 80.8 | 246.4 |
| 8986 | ok | 0.21 | 0.3 | 3.09e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -64.3 | -27.1 | -46.6 | -257.6 | -40.0 | -48.0 |
| 8987 | ok | 0.21 | 0.2 | 2.81e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -50.4 | -23.1 | -44.7 | -221.2 | -41.2 | 25.4 |
| 8988 | ok | 0.21 | 0.2 | 4.04e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -50.3 | 9.7 | 19.7 | -217.4 | -77.9 | 154.1 |
| 8989 | ok | 0.21 | 0.3 | 6.05e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -59.0 | 9.6 | 59.7 | -244.9 | -122.9 | 317.7 |
| 8990 | ok | 0.21 | 0.4 | 4.28e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -82.5 | -50.3 | -64.2 | -614.1 | -29.8 | -145.9 |
| 8991 | ok | 0.21 | 0.3 | 3.54e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -77.9 | -30.7 | -50.6 | -311.8 | -50.7 | -28.0 |
| 8992 | ok | 0.21 | 0.2 | 3.07e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -71.2 | -20.6 | -42.9 | -237.4 | -40.1 | 25.7 |
| 8993 | ok | 0.21 | 0.2 | 4.55e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -58.9 | 12.4 | 19.1 | -215.4 | -77.7 | 148.8 |
| 8994 | ok | 0.21 | 0.3 | 4.55e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -135.5 | -38.4 | -27.1 | -563.4 | 11.3 | -56.0 |
| 8995 | ok | 0.21 | 0.2 | 3.68e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -103.7 | -25.1 | -32.0 | -363.3 | -49.2 | 23.9 |
| 8996 | ok | 0.21 | 0.1 | 3.34e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -86.0 | -18.2 | -32.1 | -256.8 | -39.6 | 32.1 |
| 8997 | ok | 0.21 | 0.2 | 4.73e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -66.9 | 12.0 | 25.4 | -211.7 | -77.0 | 149.2 |
| 8998 | ok | 0.21 | 0.3 | 3.87e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -87.5 | -50.2 | -14.4 | -428.2 | 36.9 | 69.5 |
| 8999 | ok | 0.21 | 0.2 | 3.59e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -101.3 | -26.1 | -13.7 | -347.3 | -13.3 | 59.3 |
| 9000 | ok | 0.21 | 0.1 | 3.45e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -88.4 | -18.0 | -18.3 | -262.6 | -34.5 | 44.3 |
| 9001 | ok | 0.21 | 0.1 | 4.79e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -74.0 | 8.9 | 34.1 | -214.2 | -83.3 | 160.4 |
| 9002 | ok | 0.21 | 0.2 | 3.76e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -90.1 | -53.8 | -2.8 | -345.7 | 43.8 | 114.9 |
| 9003 | ok | 0.21 | 0.2 | 3.58e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -73.9 | -32.3 | -7.5 | -305.0 | 1.6 | 98.2 |
| 9004 | ok | 0.21 | 0.1 | 3.46e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -79.3 | -4.7 | -0.6 | -229.7 | -27.6 | 80.8 |
| 9005 | ok | 0.21 | 0.1 | 4.68e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -76.4 | 2.9 | 39.9 | -198.3 | -82.3 | 154.9 |
| 9006 | ok | 0.21 | 0.2 | 3.61e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -75.7 | -49.2 | -1.8 | -304.3 | 26.5 | 141.3 |
| 9007 | ok | 0.21 | 0.1 | 3.47e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -82.7 | 8.0 | 9.4 | -267.8 | -18.6 | 112.7 |
| 9008 | ok | 0.21 | 0.1 | 3.35e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -81.4 | -4.5 | 6.3 | -225.4 | -31.3 | 103.0 |
| 9009 | ok | 0.21 | 0.1 | 4.44e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -76.1 | -4.0 | 44.8 | -177.0 | -81.3 | 146.5 |
| 9010 | ok | 0.21 | 0.2 | 3.52e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -80.8 | -16.1 | 12.2 | -323.5 | -9.3 | 176.2 |
| 9011 | ok | 0.21 | 0.1 | 3.35e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -80.7 | -10.7 | 9.0 | -259.4 | -24.6 | 134.9 |
| 9012 | ok | 0.21 | 0.1 | 3.24e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -77.9 | -3.9 | 12.4 | -198.5 | -38.0 | 111.7 |
| 9013 | ok | 0.21 | 0.1 | 4.16e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -74.1 | -7.3 | 51.2 | -137.8 | -81.6 | 125.6 |
| 9014 | ok | 0.21 | 0.2 | 3.41e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -74.8 | -18.9 | 14.5 | -295.2 | -33.4 | 196.6 |
| 9015 | ok | 0.21 | 0.1 | 3.26e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -73.6 | -13.7 | 11.5 | -231.5 | -41.3 | 149.8 |
| 9016 | ok | 0.21 | 0.1 | 3.18e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -72.9 | -11.7 | 14.1 | -173.3 | -46.1 | 118.1 |
| 9017 | ok | 0.21 | 0.1 | 4.25e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -71.6 | -13.1 | 54.0 | -111.0 | -81.9 | 105.7 |
| 9018 | ok | 0.21 | 0.2 | 3.28e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -68.6 | -21.0 | 16.7 | -266.0 | -69.0 | 212.6 |
| 9019 | ok | 0.21 | 0.1 | 3.13e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -67.4 | -16.3 | 14.4 | -196.3 | -68.3 | 158.3 |
| 9020 | ok | 0.21 | 0.1 | 3.07e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -66.7 | -14.4 | 16.9 | -137.2 | -60.5 | 116.0 |
| 9021 | ok | 0.21 | 0.1 | 4.19e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -66.6 | -17.5 | 54.9 | -83.8 | -82.4 | 80.9 |
| 9022 | ok | 0.21 | 0.2 | 3.18e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -62.8 | -22.4 | 19.4 | -234.9 | -124.8 | 224.6 |
| 9023 | ok | 0.21 | 0.1 | 2.99e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -60.7 | -18.4 | 17.6 | -150.0 | -105.8 | 155.2 |
| 9024 | ok | 0.21 | 9.78e-02 | 2.89e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -61.0 | -13.7 | 21.9 | -96.3 | -82.4 | 96.5 |
| 9025 | ok | 0.21 | 9.41e-02 | 3.94e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -58.5 | -20.5 | 53.2 | -58.0 | -80.3 | 51.8 |
| 9026 | ok | 0.21 | 0.2 | 3.19e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -62.1 | -16.0 | 27.8 | -214.5 | -257.2 | 194.4 |
| 9027 | ok | 0.21 | 0.1 | 2.87e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -54.0 | -16.8 | 23.7 | -97.2 | -149.3 | 116.6 |
| 9028 | ok | 0.21 | 7.99e-02 | 2.72e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -51.5 | -15.8 | 20.3 | -50.4 | -76.6 | 68.8 |
| 9029 | ok | 0.21 | 7.30e-02 | 3.47e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -46.1 | -26.0 | 45.3 | -28.6 | -61.2 | 29.4 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | 0.44 | 1.03 | 0.41 | 10.09 | 21.82 | 8.42 | 19.87 | -1016.45 | -360.38 | -537.70 | -6743.97 | -815.42 | -3704.10 |
| | | | | | | | | | 474.06 | 341.46 | 266.30 | 2741.37 | 1063.04 | 1300.61 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 21 | ok | 1.55 | | | | | | |
| 30 | ok | 1.50 | | | | | | |
| 53 | ok | 1.53 | | | | | | |
| 54 | ok | 2.89 | | | | | | |
| 55 | ok | 2.70 | | | | | | |
| 56 | ok | 4.73 | | | | | | |
| 58 | ok | 1.33 | | | | | | |
| 2883 | ok | 1.55 | | | | | | |
| 2885 | ok | 1.35 | | | | | | |
| 2887 | ok | 1.37 | | | | | | |
| 2889 | ok | 1.55 | | | | | | |
| 2891 | ok | 1.55 | | | | | | |
| 3268 | ok | 1.50 | | | | | | |
| 3285 | ok | 1.33 | | | | | | |
| 3302 | ok | 1.29 | | | | | | |
| 3319 | ok | 1.30 | | | | | | |
| 3336 | ok | 1.32 | | | | | | |
| 3353 | ok | 1.34 | | | | | | |
| 3370 | ok | 1.36 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 3387 | ok | 1.44 | | | | | | |
| 3404 | ok | 1.44 | | | | | | |
| 3461 | ok | 2.00 | | | | | | |
| 3478 | ok | 1.76 | | | | | | |
| 3495 | ok | 1.53 | | | | | | |
| 3512 | ok | 1.46 | | | | | | |
| 3529 | ok | 1.43 | | | | | | |
| 3546 | ok | 1.50 | | | | | | |
| 3563 | ok | 1.74 | | | | | | |
| 3580 | ok | 2.01 | | | | | | |
| 7323 | ok | 0.33 | | | | | | |
| 7332 | ok | 0.28 | | | | | | |
| 7351 | ok | 0.43 | | | | | | |
| 7352 | ok | 0.56 | | | | | | |
| 7353 | ok | 0.61 | | | | | | |
| 7354 | ok | 0.45 | | | | | | |
| 7356 | ok | 0.44 | | | | | | |
| 7472 | ok | 0.35 | | | | | | |
| 7473 | ok | 0.36 | | | | | | |
| 7474 | ok | 0.38 | | | | | | |
| 7475 | ok | 0.40 | | | | | | |
| 7476 | ok | 0.42 | | | | | | |
| 7477 | ok | 0.32 | | | | | | |
| 7478 | ok | 0.35 | | | | | | |
| 7479 | ok | 0.38 | | | | | | |
| 7480 | ok | 0.41 | | | | | | |
| 7481 | ok | 0.42 | | | | | | |
| 7482 | ok | 0.43 | | | | | | |
| 7483 | ok | 0.43 | | | | | | |
| 7484 | ok | 0.44 | | | | | | |
| 7485 | ok | 0.44 | | | | | | |
| 7486 | ok | 0.59 | | | | | | |
| 7487 | ok | 0.57 | | | | | | |
| 7488 | ok | 0.55 | | | | | | |
| 7489 | ok | 0.53 | | | | | | |
| 7490 | ok | 0.52 | | | | | | |
| 7491 | ok | 0.54 | | | | | | |
| 7492 | ok | 0.55 | | | | | | |
| 7493 | ok | 0.56 | | | | | | |
| 7691 | ok | 0.95 | | | | | | |
| 7745 | ok | 0.46 | | | | | | |
| 7799 | ok | 0.29 | | | | | | |
| 7853 | ok | 0.22 | | | | | | |
| 8762 | ok | 0.97 | | | | | | |
| 8763 | ok | 0.52 | | | | | | |
| 8764 | ok | 0.33 | | | | | | |
| 8765 | ok | 0.25 | | | | | | |
| 8766 | ok | 0.97 | | | | | | |
| 8767 | ok | 0.52 | | | | | | |
| 8768 | ok | 0.33 | | | | | | |
| 8769 | ok | 0.25 | | | | | | |
| 8770 | ok | 0.52 | | | | | | |
| 8771 | ok | 0.44 | | | | | | |
| 8772 | ok | 0.32 | | | | | | |
| 8773 | ok | 0.22 | | | | | | |
| 8774 | ok | 0.41 | | | | | | |
| 8775 | ok | 0.32 | | | | | | |
| 8776 | ok | 0.25 | | | | | | |
| 8777 | ok | 0.21 | | | | | | |
| 8778 | ok | 0.54 | | | | | | |
| 8779 | ok | 0.26 | | | | | | |
| 8780 | ok | 0.19 | | | | | | |
| 8781 | ok | 0.21 | | | | | | |
| 8782 | ok | 0.66 | | | | | | |
| 8783 | ok | 0.29 | | | | | | |
| 8784 | ok | 0.17 | | | | | | |
| 8785 | ok | 0.20 | | | | | | |
| 8786 | ok | 0.66 | | | | | | |
| 8787 | ok | 0.29 | | | | | | |
| 8788 | ok | 0.13 | | | | | | |
| 8789 | ok | 0.20 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 8790 | ok | 0.60 | | | | | | |
| 8791 | ok | 0.84 | | | | | | |
| 8792 | ok | 0.26 | | | | | | |
| 8793 | ok | 0.14 | | | | | | |
| 8794 | ok | 0.21 | | | | | | |
| 8795 | ok | 0.44 | | | | | | |
| 8796 | ok | 0.36 | | | | | | |
| 8797 | ok | 0.72 | | | | | | |
| 8798 | ok | 0.21 | | | | | | |
| 8799 | ok | 0.15 | | | | | | |
| 8800 | ok | 0.23 | | | | | | |
| 8801 | ok | 0.44 | | | | | | |
| 8802 | ok | 0.41 | | | | | | |
| 8803 | ok | 0.95 | | | | | | |
| 8804 | ok | 0.33 | | | | | | |
| 8805 | ok | 0.21 | | | | | | |
| 8806 | ok | 0.27 | | | | | | |
| 8807 | ok | 0.45 | | | | | | |
| 8808 | ok | 0.83 | | | | | | |
| 8809 | ok | 1.58 | | | | | | |
| 8810 | ok | 0.56 | | | | | | |
| 8811 | ok | 0.26 | | | | | | |
| 8812 | ok | 0.31 | | | | | | |
| 8813 | ok | 0.47 | | | | | | |
| 8814 | ok | 3.70 | | | | | | |
| 8815 | ok | 3.87 | | | | | | |
| 8816 | ok | 0.86 | | | | | | |
| 8817 | ok | 0.29 | | | | | | |
| 8818 | ok | 0.31 | | | | | | |
| 8819 | ok | 0.47 | | | | | | |
| 8820 | ok | 3.77 | | | | | | |
| 8821 | ok | 4.73 | | | | | | |
| 8822 | ok | 0.86 | | | | | | |
| 8823 | ok | 0.29 | | | | | | |
| 8824 | ok | 0.20 | | | | | | |
| 8825 | ok | 0.45 | | | | | | |
| 8826 | ok | 3.77 | | | | | | |
| 8827 | ok | 0.81 | | | | | | |
| 8828 | ok | 0.26 | | | | | | |
| 8829 | ok | 0.24 | | | | | | |
| 8830 | ok | 1.10 | | | | | | |
| 8831 | ok | 1.74 | | | | | | |
| 8832 | ok | 0.52 | | | | | | |
| 8833 | ok | 0.18 | | | | | | |
| 8834 | ok | 0.24 | | | | | | |
| 8835 | ok | 0.45 | | | | | | |
| 8836 | ok | 0.49 | | | | | | |
| 8837 | ok | 0.84 | | | | | | |
| 8838 | ok | 0.35 | | | | | | |
| 8839 | ok | 0.17 | | | | | | |
| 8840 | ok | 0.22 | | | | | | |
| 8841 | ok | 0.46 | | | | | | |
| 8842 | ok | 0.22 | | | | | | |
| 8843 | ok | 0.57 | | | | | | |
| 8844 | ok | 0.20 | | | | | | |
| 8845 | ok | 0.17 | | | | | | |
| 8846 | ok | 0.21 | | | | | | |
| 8847 | ok | 0.47 | | | | | | |
| 8848 | ok | 0.23 | | | | | | |
| 8849 | ok | 0.69 | | | | | | |
| 8850 | ok | 0.19 | | | | | | |
| 8851 | ok | 0.18 | | | | | | |
| 8852 | ok | 0.25 | | | | | | |
| 8853 | ok | 0.50 | | | | | | |
| 8854 | ok | 0.31 | | | | | | |
| 8855 | ok | 0.65 | | | | | | |
| 8856 | ok | 0.24 | | | | | | |
| 8857 | ok | 0.17 | | | | | | |
| 8858 | ok | 0.20 | | | | | | |
| 8859 | ok | 0.46 | | | | | | |
| 8860 | ok | 0.26 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 8861 | ok | 0.88 | | | | | | |
| 8862 | ok | 0.21 | | | | | | |
| 8863 | ok | 0.20 | | | | | | |
| 8864 | ok | 0.26 | | | | | | |
| 8865 | ok | 0.52 | | | | | | |
| 8866 | ok | 0.31 | | | | | | |
| 8867 | ok | 1.13 | | | | | | |
| 8868 | ok | 0.25 | | | | | | |
| 8869 | ok | 0.23 | | | | | | |
| 8870 | ok | 0.29 | | | | | | |
| 8871 | ok | 0.53 | | | | | | |
| 8872 | ok | 0.39 | | | | | | |
| 8873 | ok | 1.44 | | | | | | |
| 8874 | ok | 0.32 | | | | | | |
| 8875 | ok | 0.26 | | | | | | |
| 8876 | ok | 0.32 | | | | | | |
| 8877 | ok | 0.54 | | | | | | |
| 8878 | ok | 0.55 | | | | | | |
| 8879 | ok | 1.98 | | | | | | |
| 8880 | ok | 0.39 | | | | | | |
| 8881 | ok | 0.28 | | | | | | |
| 8882 | ok | 0.37 | | | | | | |
| 8883 | ok | 0.55 | | | | | | |
| 8884 | ok | 1.05 | | | | | | |
| 8885 | ok | 2.89 | | | | | | |
| 8886 | ok | 0.44 | | | | | | |
| 8887 | ok | 0.28 | | | | | | |
| 8888 | ok | 0.41 | | | | | | |
| 8889 | ok | 0.55 | | | | | | |
| 8890 | ok | 1.20 | | | | | | |
| 8891 | ok | 0.50 | | | | | | |
| 8892 | ok | 0.25 | | | | | | |
| 8893 | ok | 0.49 | | | | | | |
| 8894 | ok | 1.20 | | | | | | |
| 8895 | ok | 0.50 | | | | | | |
| 8896 | ok | 0.25 | | | | | | |
| 8897 | ok | 0.51 | | | | | | |
| 8898 | ok | 0.65 | | | | | | |
| 8899 | ok | 0.32 | | | | | | |
| 8900 | ok | 0.25 | | | | | | |
| 8901 | ok | 0.52 | | | | | | |
| 8902 | ok | 0.42 | | | | | | |
| 8903 | ok | 0.22 | | | | | | |
| 8904 | ok | 0.23 | | | | | | |
| 8905 | ok | 0.52 | | | | | | |
| 8906 | ok | 0.36 | | | | | | |
| 8907 | ok | 0.21 | | | | | | |
| 8908 | ok | 0.23 | | | | | | |
| 8909 | ok | 0.52 | | | | | | |
| 8910 | ok | 0.34 | | | | | | |
| 8911 | ok | 0.20 | | | | | | |
| 8912 | ok | 0.22 | | | | | | |
| 8913 | ok | 0.52 | | | | | | |
| 8914 | ok | 0.41 | | | | | | |
| 8915 | ok | 0.22 | | | | | | |
| 8916 | ok | 0.23 | | | | | | |
| 8917 | ok | 0.52 | | | | | | |
| 8918 | ok | 0.64 | | | | | | |
| 8919 | ok | 0.31 | | | | | | |
| 8920 | ok | 0.24 | | | | | | |
| 8921 | ok | 0.51 | | | | | | |
| 8922 | ok | 1.16 | | | | | | |
| 8923 | ok | 0.50 | | | | | | |
| 8924 | ok | 0.24 | | | | | | |
| 8925 | ok | 0.50 | | | | | | |
| 8926 | ok | 1.16 | | | | | | |
| 8927 | ok | 0.50 | | | | | | |
| 8928 | ok | 0.25 | | | | | | |
| 8929 | ok | 0.50 | | | | | | |
| 8930 | ok | 1.03 | | | | | | |
| 8931 | ok | 2.70 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| 8932 | ok | 0.44 | | | | | | |
| 8933 | ok | 0.26 | | | | | | |
| 8934 | ok | 0.46 | | | | | | |
| 8935 | ok | 0.61 | | | | | | |
| 8936 | ok | 0.53 | | | | | | |
| 8937 | ok | 1.92 | | | | | | |
| 8938 | ok | 0.37 | | | | | | |
| 8939 | ok | 0.26 | | | | | | |
| 8940 | ok | 0.34 | | | | | | |
| 8941 | ok | 0.58 | | | | | | |
| 8942 | ok | 0.37 | | | | | | |
| 8943 | ok | 1.44 | | | | | | |
| 8944 | ok | 0.28 | | | | | | |
| 8945 | ok | 0.24 | | | | | | |
| 8946 | ok | 0.30 | | | | | | |
| 8947 | ok | 0.58 | | | | | | |
| 8948 | ok | 0.30 | | | | | | |
| 8949 | ok | 1.17 | | | | | | |
| 8950 | ok | 0.22 | | | | | | |
| 8951 | ok | 0.21 | | | | | | |
| 8952 | ok | 0.28 | | | | | | |
| 8953 | ok | 0.56 | | | | | | |
| 8954 | ok | 0.24 | | | | | | |
| 8955 | ok | 0.96 | | | | | | |
| 8956 | ok | 0.18 | | | | | | |
| 8957 | ok | 0.17 | | | | | | |
| 8958 | ok | 0.26 | | | | | | |
| 8959 | ok | 0.54 | | | | | | |
| 8960 | ok | 0.21 | | | | | | |
| 8961 | ok | 0.80 | | | | | | |
| 8962 | ok | 0.15 | | | | | | |
| 8963 | ok | 0.15 | | | | | | |
| 8964 | ok | 0.23 | | | | | | |
| 8965 | ok | 0.52 | | | | | | |
| 8966 | ok | 0.19 | | | | | | |
| 8967 | ok | 0.68 | | | | | | |
| 8968 | ok | 0.14 | | | | | | |
| 8969 | ok | 0.14 | | | | | | |
| 8970 | ok | 0.21 | | | | | | |
| 8971 | ok | 0.50 | | | | | | |
| 8972 | ok | 0.20 | | | | | | |
| 8973 | ok | 0.66 | | | | | | |
| 8974 | ok | 0.14 | | | | | | |
| 8975 | ok | 0.12 | | | | | | |
| 8976 | ok | 0.19 | | | | | | |
| 8977 | ok | 0.47 | | | | | | |
| 8978 | ok | 0.40 | | | | | | |
| 8979 | ok | 0.93 | | | | | | |
| 8980 | ok | 0.17 | | | | | | |
| 8981 | ok | 0.14 | | | | | | |
| 8982 | ok | 0.19 | | | | | | |
| 8983 | ok | 0.45 | | | | | | |
| 8984 | ok | 0.77 | | | | | | |
| 8985 | ok | 1.33 | | | | | | |
| 8986 | ok | 0.25 | | | | | | |
| 8987 | ok | 0.14 | | | | | | |
| 8988 | ok | 0.19 | | | | | | |
| 8989 | ok | 0.44 | | | | | | |
| 8990 | ok | 0.77 | | | | | | |
| 8991 | ok | 0.32 | | | | | | |
| 8992 | ok | 0.13 | | | | | | |
| 8993 | ok | 0.21 | | | | | | |
| 8994 | ok | 0.74 | | | | | | |
| 8995 | ok | 0.32 | | | | | | |
| 8996 | ok | 0.16 | | | | | | |
| 8997 | ok | 0.21 | | | | | | |
| 8998 | ok | 0.48 | | | | | | |
| 8999 | ok | 0.22 | | | | | | |
| 9000 | ok | 0.16 | | | | | | |
| 9001 | ok | 0.21 | | | | | | |
| 9002 | ok | 0.34 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------------|-------|----------------|-----------------|------------------|----------------|-----------------|-------------|--------------|
| 9003 | ok | 0.14 | | | | | | |
| 9004 | ok | 0.14 | | | | | | |
| 9005 | ok | 0.21 | | | | | | |
| 9006 | ok | 0.30 | | | | | | |
| 9007 | ok | 0.13 | | | | | | |
| 9008 | ok | 0.13 | | | | | | |
| 9009 | ok | 0.21 | | | | | | |
| 9010 | ok | 0.28 | | | | | | |
| 9011 | ok | 0.15 | | | | | | |
| 9012 | ok | 0.16 | | | | | | |
| 9013 | ok | 0.21 | | | | | | |
| 9014 | ok | 0.28 | | | | | | |
| 9015 | ok | 0.18 | | | | | | |
| 9016 | ok | 0.18 | | | | | | |
| 9017 | ok | 0.22 | | | | | | |
| 9018 | ok | 0.31 | | | | | | |
| 9019 | ok | 0.24 | | | | | | |
| 9020 | ok | 0.23 | | | | | | |
| 9021 | ok | 0.22 | | | | | | |
| 9022 | ok | 0.48 | | | | | | |
| 9023 | ok | 0.36 | | | | | | |
| 9024 | ok | 0.29 | | | | | | |
| 9025 | ok | 0.23 | | | | | | |
| 9026 | ok | 0.95 | | | | | | |
| 9027 | ok | 0.46 | | | | | | |
| 9028 | ok | 0.29 | | | | | | |
| 9029 | ok | 0.23 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 4.73 | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 80 | 25.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|----------|-----------|--------|-------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 1 | ok | 0.16 | 0.2 | 3.31e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -39.7 | -70.6 | -38.7 | -11.6 | -619.1 | -14.2 |
| 5 | ok | 0.16 | 0.2 | 3.68e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -45.8 | -75.8 | 44.5 | -11.2 | -577.7 | 17.4 |
| 7078 | ok | 0.16 | 0.1 | 1.79e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -31.8 | -10.7 | -29.5 | 363.4 | 65.7 | 39.9 |
| 7304 | ok | 0.16 | 0.1 | 3.34e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -100.0 | -12.9 | -4.2 | 323.3 | -120.3 | 16.1 |
| 7307 | ok | 0.16 | 0.1 | 3.60e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -107.4 | -12.3 | 8.1 | 356.8 | -104.9 | -20.3 |
| 7369 | ok | 0.16 | 5.81e-02 | 1.70e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -33.6 | -12.4 | -24.9 | 90.9 | -23.7 | 91.3 |
| 7683 | ok | 0.16 | 0.2 | 2.15e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -41.8 | -19.8 | -31.0 | -93.0 | -536.4 | -12.0 |
| 7685 | ok | 0.16 | 0.2 | 2.16e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -48.0 | -9.2 | -33.0 | -61.0 | -354.2 | -15.0 |
| 7687 | ok | 0.16 | 0.1 | 2.34e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -51.4 | -11.0 | -32.5 | -70.1 | -365.3 | -12.3 |
| 7689 | ok | 0.16 | 0.1 | 2.68e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -57.8 | -3.3 | -40.9 | -40.1 | -276.1 | -17.8 |
| 9284 | ok | 0.16 | 0.2 | 2.45e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -48.9 | 1.7 | 37.5 | -96.1 | -510.3 | 25.2 |
| 9285 | ok | 0.16 | 0.2 | 2.45e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -47.3 | -8.9 | 37.9 | -93.0 | -412.9 | 15.3 |
| 9286 | ok | 0.16 | 0.1 | 2.66e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -56.7 | -9.2 | 39.4 | -66.3 | -340.0 | 15.1 |
| 9287 | ok | 0.16 | 0.1 | 3.04e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -64.6 | -3.9 | 47.4 | -41.5 | -264.5 | 19.1 |
| 10428 | ok | 0.16 | 0.2 | 3.75e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 41.1 | 0.2 | 0.3 | -22.6 | -26.3 |
| 10429 | ok | 0.16 | 0.2 | 3.67e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 52.1 | -0.3 | 3.96e-03 | 37.0 | -24.9 |
| 10430 | ok | 0.16 | 0.2 | 3.69e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 53.9 | 0.5 | -0.8 | 31.7 | -21.5 |
| 10431 | ok | 0.16 | 0.2 | 3.54e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 52.5 | -1.2 | -0.5 | 22.6 | -14.7 |
| 10432 | ok | 0.16 | 0.2 | 3.40e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 48.2 | -0.2 | -0.4 | 19.1 | -12.1 |
| 10433 | ok | 0.16 | 0.2 | 3.55e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 38.7 | 0.2 | 7.10e-02 | 18.6 | -4.0 |
| 10434 | ok | 0.16 | 0.1 | 3.88e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 33.0 | -0.5 | -4.65e-02 | 15.6 | -0.4 |
| 10435 | ok | 0.16 | 0.1 | 3.56e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 33.7 | 1.1 | -1.95e-02 | 18.5 | 6.2 |
| 10436 | ok | 0.16 | 0.2 | 1.18e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 36.0 | 0.6 | 0.8 | 45.1 | 33.0 |
| 10437 | ok | 0.16 | 0.2 | 2.64e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 1.1 | 5.4 | 1.8 | 1.3 | -282.2 | 17.4 |
| 10438 | ok | 0.16 | 0.2 | 3.29e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 44.7 | 1.79e-02 | -4.67e-02 | 9.5 | -27.9 |
| 10439 | ok | 0.16 | 0.2 | 3.34e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 47.6 | -0.1 | 1.88e-02 | 25.7 | -27.8 |
| 10440 | ok | 0.16 | 0.2 | 3.48e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 50.1 | -0.2 | 4.18e-02 | 34.0 | -26.6 |
| 10441 | ok | 0.16 | 0.2 | 3.52e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 54.3 | -0.9 | -0.7 | 30.2 | -19.9 |
| 10442 | ok | 0.16 | 0.2 | 3.41e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 54.2 | -1.0 | -0.6 | 27.9 | -18.0 |
| 10443 | ok | 0.16 | 0.2 | 3.46e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 53.6 | -1.1 | -0.6 | 25.2 | -16.3 |
| 10444 | ok | 0.16 | 0.2 | 3.35e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.7 | -3.2 | 2.8 | 2.3 | -390.9 | -4.8 |
| 10445 | ok | 0.16 | 0.2 | 1.16e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 1.5 | 16.4 | -1.9 | 1.0 | -226.1 | -18.5 |
| 10446 | ok | 0.16 | 0.2 | 4.96e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 36.2 | 0.6 | -5.83e-02 | -71.4 | -22.3 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------|-------|------|----------|----------|--------|--------|---------|---------|-------|-------|-------|-----------|--------|-------|
| 10447 | ok | 0.16 | 0.2 | 3.21e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 53.3 | -0.6 | -4.75e-02 | 36.9 | -23.4 |
| 10448 | ok | 0.16 | 0.2 | 3.41e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 51.1 | -1.3 | -0.5 | 20.6 | -13.4 |
| 10449 | ok | 0.16 | 0.2 | 3.50e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 37.4 | 0.2 | 7.70e-02 | 18.4 | -3.6 |
| 10450 | ok | 0.16 | 0.2 | 3.50e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 36.2 | 0.2 | 8.98e-02 | 18.2 | -3.2 |
| 10451 | ok | 0.16 | 0.2 | 3.51e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 35.0 | 0.2 | 0.1 | 17.9 | -2.7 |
| 10452 | ok | 0.16 | 0.2 | 3.51e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 34.5 | -0.9 | 0.1 | 17.6 | -2.2 |
| 10453 | ok | 0.16 | 0.1 | 3.55e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 33.6 | -0.9 | 0.1 | 17.2 | -1.5 |
| 10454 | ok | 0.16 | 0.1 | 3.59e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 33.5 | 1.1 | 1.72e-03 | 21.0 | 7.6 |
| 10455 | ok | 0.16 | 0.2 | 3.78e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 33.4 | 1.1 | -1.26e-04 | 23.9 | 9.2 |
| 10456 | ok | 0.16 | 0.2 | 5.03e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 33.4 | 1.2 | 0.1 | 27.0 | 11.0 |
| 10457 | ok | 0.16 | 0.2 | 6.89e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 33.4 | 1.1 | 0.2 | 30.9 | 12.9 |
| 10458 | ok | 0.16 | 0.2 | 9.08e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 33.7 | 1.1 | 0.3 | 34.4 | 15.1 |
| 10459 | ok | 0.16 | 0.2 | 1.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 34.1 | 1.1 | 0.4 | 37.9 | 17.4 |
| 10460 | ok | 0.16 | 0.2 | 1.18e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 34.6 | 1.0 | 0.5 | 41.2 | 19.8 |
| 10461 | ok | 0.16 | 0.2 | 1.23e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 35.2 | 1.0 | 0.6 | 44.1 | 22.3 |
| 10462 | ok | 0.16 | 0.2 | 1.23e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 35.7 | 1.1 | 0.7 | 46.2 | 26.5 |
| 10463 | ok | 0.16 | 0.2 | 1.22e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 36.0 | 1.1 | 0.8 | 47.1 | 29.7 |
| 10464 | ok | 0.16 | 0.2 | 4.72e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.1 | -11.6 | -2.9 | 2.6 | -442.8 | 2.8 |
| 10465 | ok | 0.16 | 9.04e-02 | 1.67e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -27.2 | -13.9 | 20.4 | 233.2 | 54.2 | -28.4 |
| 10466 | ok | 0.16 | 4.42e-02 | 9.29e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -20.4 | -10.3 | 6.5 | 109.0 | 29.0 | -26.6 |
| 10467 | ok | 0.16 | 3.58e-02 | 7.51e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -17.5 | -9.5 | 3.1 | 84.7 | 23.7 | -24.3 |
| 10468 | ok | 0.16 | 2.77e-02 | 5.25e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -12.2 | 3.0 | 5.5 | 52.1 | 13.6 | -17.6 |
| 10469 | ok | 0.16 | 2.50e-02 | 5.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.6 | 3.5 | 3.4 | 41.8 | 9.9 | -15.5 |
| 10470 | ok | 0.16 | 2.81e-02 | 4.56e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.5 | -1.7 | -6.9 | 36.4 | 10.0 | -11.5 |
| 10471 | ok | 0.16 | 2.78e-02 | 3.88e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.9 | 3.4 | 2.4 | 32.7 | 8.1 | 0.2 |
| 10472 | ok | 0.16 | 3.39e-02 | 4.05e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.7 | 4.9 | -6.4 | 39.0 | 8.9 | 2.4 |
| 10473 | ok | 0.16 | 4.31e-02 | 6.54e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -15.3 | -7.9 | -3.5 | 120.5 | 32.9 | 33.4 |
| 10474 | ok | 0.16 | 7.43e-02 | 1.46e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -25.0 | -13.0 | 16.5 | 191.2 | 46.6 | -28.8 |
| 10475 | ok | 0.16 | 5.90e-02 | 1.26e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -23.1 | -12.2 | 12.7 | 157.9 | 40.2 | -28.6 |
| 10476 | ok | 0.16 | 5.08e-02 | 1.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -21.5 | -11.4 | 9.4 | 131.3 | 34.6 | -27.8 |
| 10477 | ok | 0.16 | 3.15e-02 | 6.49e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -14.3 | 1.2 | 9.9 | 79.6 | 21.6 | -22.5 |
| 10478 | ok | 0.16 | 2.78e-02 | 5.70e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -13.3 | 2.0 | 8.3 | 68.7 | 18.6 | -20.6 |
| 10479 | ok | 0.16 | 2.88e-02 | 5.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -12.7 | 2.6 | 6.9 | 59.7 | 16.0 | -19.0 |
| 10480 | ok | 0.16 | 0.1 | 2.06e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.6 | -21.1 | 32.3 | 438.6 | 102.2 | -37.1 |
| 10481 | ok | 0.16 | 0.1 | 2.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -35.1 | -17.9 | 24.7 | 366.1 | 75.8 | -28.2 |
| 10482 | ok | 0.16 | 0.1 | 1.89e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -30.1 | -15.3 | 23.8 | 286.8 | 63.8 | -27.3 |
| 10483 | ok | 0.16 | 3.97e-02 | 8.32e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -18.8 | -9.6 | 4.8 | 95.6 | 25.9 | -25.4 |
| 10484 | ok | 0.16 | 2.62e-02 | 5.18e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.9 | 3.2 | 4.4 | 46.2 | 11.4 | -16.5 |
| 10485 | ok | 0.16 | 2.90e-02 | 4.33e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.0 | -1.2 | -6.7 | 38.0 | 10.9 | -10.3 |
| 10486 | ok | 0.16 | 2.99e-02 | 4.15e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.6 | -0.8 | -6.5 | 38.6 | 11.3 | -9.0 |
| 10487 | ok | 0.16 | 2.98e-02 | 4.01e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.5 | -0.4 | -6.3 | 38.1 | 11.1 | -7.7 |
| 10488 | ok | 0.16 | 2.92e-02 | 3.94e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.9 | 3.6 | 1.9 | 38.8 | 11.2 | -2.2 |
| 10489 | ok | 0.16 | 2.90e-02 | 3.93e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.3 | 3.5 | 2.1 | 36.3 | 10.0 | -1.1 |
| 10490 | ok | 0.16 | 3.53e-02 | 3.88e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.1 | 5.7 | -6.6 | 45.9 | 11.5 | 3.6 |
| 10491 | ok | 0.16 | 3.52e-02 | 3.70e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.4 | 6.5 | -6.7 | 53.2 | 14.2 | 5.1 |
| 10492 | ok | 0.16 | 3.50e-02 | 3.56e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.9 | 7.2 | -6.8 | 60.5 | 16.7 | 7.0 |
| 10493 | ok | 0.16 | 3.62e-02 | 3.48e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.6 | 7.7 | -6.9 | 67.5 | 19.1 | 9.3 |
| 10494 | ok | 0.16 | 3.88e-02 | 3.47e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.5 | 8.1 | -7.0 | 74.1 | 21.2 | 11.9 |
| 10495 | ok | 0.16 | 4.05e-02 | 3.56e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.6 | 8.2 | -7.1 | 80.5 | 23.1 | 14.8 |
| 10496 | ok | 0.16 | 4.24e-02 | 3.76e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.0 | 8.1 | -7.4 | 86.9 | 25.0 | 17.9 |
| 10497 | ok | 0.16 | 4.30e-02 | 4.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.8 | 7.6 | -7.9 | 93.5 | 26.7 | 21.3 |
| 10498 | ok | 0.16 | 4.15e-02 | 4.59e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.8 | 6.9 | -8.7 | 100.9 | 28.4 | 24.7 |
| 10499 | ok | 0.16 | 4.06e-02 | 5.28e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.1 | 6.2 | -9.9 | 109.9 | 30.2 | 28.4 |
| 10500 | ok | 0.16 | 0.1 | 1.78e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -36.9 | -17.4 | -22.8 | 412.0 | 65.9 | 36.5 |
| 10501 | ok | 0.16 | 0.2 | 2.01e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -12.8 | -22.6 | -24.5 | -54.7 | -405.0 | -6.5 |
| 10502 | ok | 0.16 | 0.1 | 1.74e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.9 | -12.4 | -27.2 | -71.3 | -304.9 | -2.2 |
| 10503 | ok | 0.16 | 9.98e-02 | 1.92e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -40.8 | -12.9 | -24.9 | -39.7 | -223.2 | -8.0 |
| 10504 | ok | 0.16 | 5.75e-02 | 2.09e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -47.1 | -12.5 | -23.3 | 53.9 | -108.3 | 17.4 |
| 10505 | ok | 0.16 | 0.1 | 3.68e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.3 | -1.8 | -4.5 | -17.1 | -132.3 | 89.3 |
| 10506 | ok | 0.16 | 0.2 | 1.78e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.3 | 28.3 | -0.5 | -3.4 | -123.5 | 28.6 |
| 10507 | ok | 0.16 | 8.18e-02 | 7.93e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.3 | -8.3 | -13.1 | -14.8 | -91.4 | 81.3 |
| 10508 | ok | 0.16 | 6.19e-02 | 1.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -18.8 | -10.1 | -18.1 | 30.7 | -37.1 | 93.7 |
| 10509 | ok | 0.16 | 7.04e-02 | 1.41e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -24.7 | -16.2 | -16.2 | 125.7 | 15.1 | 117.6 |
| 10510 | ok | 0.16 | 8.75e-02 | 1.61e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -26.1 | -6.0 | -29.3 | 292.3 | 55.2 | 39.9 |
| 10511 | ok | 0.16 | 0.1 | 2.02e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.6 | 3.6 | -2.3 | -7.4 | -49.0 | 97.6 |
| 10512 | ok | 0.16 | 0.2 | 1.40e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 31.6 | 0.4 | 1.0 | -47.0 | 34.8 |
| 10513 | ok | 0.16 | 7.71e-02 | 5.18e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.9 | -3.3 | -7.0 | 7.5 | -27.0 | 105.9 |
| 10514 | ok | 0.16 | 6.00e-02 | 8.35e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -13.9 | -7.6 | -11.7 | 53.2 | 3.1 | 113.0 |
| 10515 | ok | 0.16 | 7.24e-02 | 1.16e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -20.4 | -12.8 | -13.0 | 128.9 | 27.6 | 127.9 |
| 10516 | ok | 0.16 | 7.87e-02 | 1.39e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -23.0 | -3.2 | -25.7 | 234.4 | 46.9 | 39.8 |
| 10517 | ok | 0.16 | 0.1 | 1.50e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 20.6 | -2.6 | 3.4 | 7.9 | 94.0 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------|-------|------|----------|----------|--------|--------|---------|---------|-------|----------|-----------|-----------|------|-------|
| 10518 | ok | 0.16 | 0.1 | 1.23e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 34.0 | -1.0 | 0.9 | 5.8 | 37.2 |
| 10519 | ok | 0.16 | 7.66e-02 | 3.69e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.0 | 2.4 | -4.6 | 22.8 | 12.2 | 112.7 |
| 10520 | ok | 0.16 | 5.81e-02 | 6.30e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.8 | -3.6 | -8.3 | 63.5 | 22.8 | 117.8 |
| 10521 | ok | 0.16 | 7.05e-02 | 9.42e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -18.1 | -9.1 | -9.5 | 116.2 | 31.7 | 121.2 |
| 10522 | ok | 0.16 | 6.38e-02 | 1.17e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -23.4 | -12.7 | -11.0 | 184.8 | 42.4 | 33.9 |
| 10523 | ok | 0.16 | 0.1 | 1.29e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 23.4 | -2.0 | 6.8 | 28.0 | 94.6 |
| 10524 | ok | 0.16 | 0.2 | 1.16e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 35.2 | -1.0 | 0.9 | 28.0 | 36.8 |
| 10525 | ok | 0.16 | 7.73e-02 | 2.87e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.3 | 3.8 | -3.0 | 30.8 | 29.5 | 116.1 |
| 10526 | ok | 0.16 | 5.59e-02 | 4.92e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.0 | 6.20e-02 | -6.0 | 66.2 | 32.0 | 117.4 |
| 10527 | ok | 0.16 | 6.63e-02 | 7.64e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -16.4 | -6.3 | -6.0 | 107.0 | 33.5 | 116.8 |
| 10528 | ok | 0.16 | 5.52e-02 | 9.71e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -21.1 | -11.2 | -7.3 | 154.8 | 38.2 | 34.4 |
| 10529 | ok | 0.16 | 0.1 | 1.18e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 24.6 | -4.65e-02 | 8.5 | 37.8 | 91.5 |
| 10530 | ok | 0.16 | 0.2 | 1.14e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 35.9 | -1.0 | 0.9 | 39.7 | 34.8 |
| 10531 | ok | 0.16 | 9.26e-02 | 2.42e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.6 | 14.7 | -3.2 | 34.8 | 36.1 | 88.1 |
| 10532 | ok | 0.16 | 5.33e-02 | 4.04e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.8 | 2.5 | -3.4 | 66.2 | 38.2 | 108.1 |
| 10533 | ok | 0.16 | 6.12e-02 | 6.23e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -15.0 | -4.0 | -3.2 | 98.2 | 33.9 | 109.8 |
| 10534 | ok | 0.16 | 4.83e-02 | 7.98e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -18.7 | -9.7 | -4.2 | 133.5 | 35.1 | 33.9 |
| 10535 | ok | 0.16 | 0.1 | 1.13e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 26.0 | 0.3 | 9.4 | 43.2 | 85.4 |
| 10536 | ok | 0.16 | 0.1 | 2.17e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.2 | 16.7 | -1.9 | 34.5 | 39.1 | 81.5 |
| 10537 | ok | 0.16 | 6.39e-02 | 3.49e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.9 | 3.1 | -2.8 | 61.1 | 37.9 | 99.6 |
| 10538 | ok | 0.16 | 5.60e-02 | 5.17e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.6 | 4.5 | -8.5 | 94.1 | 33.5 | 109.9 |
| 10539 | ok | 0.16 | 0.1 | 1.14e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 26.9 | 1.1 | 9.6 | 44.9 | 77.2 |
| 10540 | ok | 0.16 | 0.1 | 1.97e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.9 | 18.3 | -0.7 | 32.7 | 39.5 | 73.2 |
| 10541 | ok | 0.16 | 7.29e-02 | 3.04e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.6 | 10.5 | -1.9 | 52.7 | 34.0 | 71.8 |
| 10542 | ok | 0.16 | 5.03e-02 | 4.52e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.7 | -1.3 | -0.5 | 87.1 | 33.5 | 101.3 |
| 10543 | ok | 0.16 | 0.1 | 1.07e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 27.4 | 1.1 | 9.4 | 43.9 | 69.3 |
| 10544 | ok | 0.16 | 0.1 | 1.86e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.6 | 19.2 | 1.1 | 30.5 | 38.2 | 65.5 |
| 10545 | ok | 0.16 | 7.94e-02 | 2.77e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.9 | 11.6 | -1.1 | 48.3 | 32.4 | 62.5 |
| 10546 | ok | 0.16 | 4.73e-02 | 4.02e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.1 | 0.2 | 0.4 | 80.6 | 31.8 | 91.4 |
| 10547 | ok | 0.16 | 0.1 | 1.05e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 27.5 | 1.1 | 8.9 | 41.9 | 61.7 |
| 10548 | ok | 0.16 | 0.1 | 1.78e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.3 | 19.8 | 1.2 | 28.2 | 36.1 | 56.7 |
| 10549 | ok | 0.16 | 8.07e-02 | 2.59e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.4 | 12.5 | 1.0 | 44.1 | 30.4 | 55.6 |
| 10550 | ok | 0.16 | 5.06e-02 | 3.70e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.2 | 1.4 | 0.7 | 74.8 | 30.1 | 81.4 |
| 10551 | ok | 0.16 | 0.1 | 1.04e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 27.5 | 1.0 | 8.3 | 39.1 | 53.4 |
| 10552 | ok | 0.16 | 0.1 | 1.74e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.1 | 20.2 | 1.3 | 25.7 | 33.5 | 50.1 |
| 10553 | ok | 0.16 | 8.10e-02 | 2.48e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.9 | 13.1 | 1.1 | 40.0 | 28.1 | 48.9 |
| 10554 | ok | 0.16 | 5.18e-02 | 3.49e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.6 | 2.5 | 0.8 | 69.4 | 28.1 | 71.6 |
| 10555 | ok | 0.16 | 0.1 | 1.04e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.7 | 27.4 | 1.0 | 7.7 | 36.0 | 46.7 |
| 10556 | ok | 0.16 | 0.1 | 1.71e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.9 | 20.4 | 1.3 | 23.3 | 30.7 | 43.8 |
| 10557 | ok | 0.16 | 7.97e-02 | 2.42e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.6 | 13.5 | 1.2 | 36.1 | 25.6 | 42.5 |
| 10558 | ok | 0.16 | 5.20e-02 | 3.38e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.2 | 3.5 | 0.7 | 64.1 | 25.9 | 62.1 |
| 10559 | ok | 0.16 | 0.1 | 1.04e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.7 | 27.4 | 0.8 | 7.0 | 32.6 | 40.4 |
| 10560 | ok | 0.16 | 0.1 | 1.72e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.9 | 20.6 | 1.2 | 21.0 | 27.7 | 37.8 |
| 10561 | ok | 0.16 | 7.76e-02 | 2.41e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.5 | 13.9 | 1.1 | 32.5 | 23.0 | 36.6 |
| 10562 | ok | 0.16 | 5.13e-02 | 3.35e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.0 | 4.4 | 0.5 | 58.8 | 23.6 | 53.1 |
| 10563 | ok | 0.16 | 0.1 | 1.05e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.7 | 27.3 | 0.7 | 6.4 | 29.3 | 34.6 |
| 10564 | ok | 0.16 | 0.1 | 1.74e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.7 | 20.7 | 1.1 | 18.9 | 24.8 | 32.4 |
| 10565 | ok | 0.16 | 7.50e-02 | 2.44e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.6 | 11.0 | -3.6 | 36.9 | 26.3 | 40.4 |
| 10566 | ok | 0.16 | 4.99e-02 | 3.39e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.0 | 5.2 | 0.3 | 53.5 | 21.1 | 44.6 |
| 10567 | ok | 0.16 | 0.1 | 1.06e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.7 | 27.3 | 0.7 | 5.8 | 25.7 | 29.2 |
| 10568 | ok | 0.16 | 9.91e-02 | 1.77e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.7 | 20.8 | 0.9 | 16.6 | 21.5 | 27.4 |
| 10569 | ok | 0.16 | 7.26e-02 | 2.49e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.7 | 11.5 | -3.8 | 33.6 | 23.5 | 33.9 |
| 10570 | ok | 0.16 | 4.76e-02 | 3.47e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.1 | 5.8 | 3.89e-02 | 48.2 | 18.5 | 36.9 |
| 10571 | ok | 0.16 | 0.1 | 1.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 27.4 | 0.5 | 5.2 | 22.6 | 24.3 |
| 10572 | ok | 0.16 | 9.78e-02 | 1.81e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.8 | 21.0 | 1.0 | 14.9 | 18.7 | 22.8 |
| 10573 | ok | 0.16 | 7.08e-02 | 2.56e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.9 | 12.1 | -3.7 | 31.5 | 21.5 | 28.3 |
| 10574 | ok | 0.16 | 4.57e-02 | 3.58e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.4 | 6.5 | -0.1 | 42.9 | 15.9 | 29.9 |
| 10575 | ok | 0.16 | 0.1 | 1.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 27.5 | 0.5 | 4.7 | 19.8 | 19.8 |
| 10576 | ok | 0.16 | 9.65e-02 | 1.85e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.9 | 21.1 | 0.9 | 13.4 | 16.1 | 18.6 |
| 10577 | ok | 0.16 | 6.97e-02 | 2.63e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | 12.7 | -3.8 | 28.4 | 18.5 | 22.7 |
| 10578 | ok | 0.16 | 4.35e-02 | 3.70e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.7 | 7.0 | -0.2 | 38.0 | 13.2 | 23.6 |
| 10579 | ok | 0.16 | 0.1 | 1.10e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.4 | 27.4 | 1.0 | 5.6 | 17.1 | 14.7 |
| 10580 | ok | 0.16 | 9.55e-02 | 1.88e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.0 | 21.2 | 0.9 | 12.1 | 13.9 | 14.8 |
| 10581 | ok | 0.16 | 6.87e-02 | 2.69e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.4 | 12.7 | -1.5 | 25.7 | 15.7 | 17.7 |
| 10582 | ok | 0.16 | 4.25e-02 | 3.81e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.0 | 7.6 | -6.40e-02 | 33.6 | 10.8 | 18.0 |
| 10583 | ok | 0.16 | 0.1 | 1.10e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.4 | 27.5 | 1.1 | 5.1 | 15.3 | 11.1 |
| 10584 | ok | 0.16 | 0.1 | 3.54e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 33.8 | 1.1 | -3.78e-02 | 16.6 | 4.8 |
| 10585 | ok | 0.16 | 9.47e-02 | 1.89e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.3 | 18.3 | -2.9 | 15.6 | 18.0 | 13.6 |
| 10586 | ok | 0.16 | 6.80e-02 | 2.72e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.6 | 13.2 | -1.3 | 23.6 | 13.5 | 12.8 |
| 10587 | ok | 0.16 | 4.16e-02 | 3.89e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.2 | 8.1 | 0.2 | 30.1 | 8.8 | 13.0 |
| 10588 | ok | 0.16 | 3.27e-02 | 4.21e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.2 | 4.1 | -6.1 | 33.3 | 6.7 | 1.4 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------|-------|------|----------|----------|--------|--------|---------|---------|-------|------|------|-----------|------|-------|
| 10589 | ok | 0.16 | 0.1 | 1.10e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.4 | 27.5 | 1.1 | 4.8 | 14.1 | 7.8 |
| 10590 | ok | 0.16 | 0.1 | 3.52e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 33.8 | 1.1 | -5.11e-02 | 15.3 | 3.6 |
| 10591 | ok | 0.16 | 9.42e-02 | 1.89e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.3 | 18.9 | -2.7 | 14.7 | 16.4 | 8.6 |
| 10592 | ok | 0.16 | 6.75e-02 | 2.72e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.6 | 13.6 | -1.0 | 22.0 | 12.1 | 8.1 |
| 10593 | ok | 0.16 | 4.21e-02 | 3.93e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.2 | 8.7 | -5.3 | 28.1 | 7.9 | 6.8 |
| 10594 | ok | 0.16 | 3.10e-02 | 4.29e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.2 | 3.1 | -6.4 | 28.1 | 5.0 | -0.8 |
| 10595 | ok | 0.16 | 0.1 | 1.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.3 | 27.4 | 1.2 | 4.4 | 13.5 | 1.7 |
| 10596 | ok | 0.16 | 0.1 | 3.53e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 33.6 | 1.1 | -6.36e-02 | 14.6 | 1.4 |
| 10597 | ok | 0.16 | 9.38e-02 | 1.85e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.2 | 19.6 | -2.3 | 13.7 | 15.9 | -0.7 |
| 10598 | ok | 0.16 | 6.72e-02 | 2.64e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.4 | 14.2 | -2.8 | 20.8 | 12.1 | -1.0 |
| 10599 | ok | 0.16 | 4.26e-02 | 3.83e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.9 | 8.3 | -4.6 | 27.0 | 8.1 | -1.5 |
| 10600 | ok | 0.16 | 2.84e-02 | 4.21e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.1 | 1.7 | -5.8 | 27.1 | 5.0 | -2.3 |
| 10601 | ok | 0.16 | 0.1 | 1.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.3 | 27.5 | 1.2 | 4.6 | 13.5 | 4.7 |
| 10602 | ok | 0.16 | 0.1 | 3.51e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 33.7 | 1.1 | -5.96e-02 | 14.7 | 2.4 |
| 10603 | ok | 0.16 | 9.39e-02 | 1.87e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.3 | 19.5 | -2.5 | 14.0 | 15.8 | 3.9 |
| 10604 | ok | 0.16 | 6.73e-02 | 2.69e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.6 | 14.0 | -0.7 | 21.1 | 11.7 | 3.6 |
| 10605 | ok | 0.16 | 4.20e-02 | 3.90e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.9 | 9.3 | -2.8 | 26.4 | 7.9 | 3.1 |
| 10606 | ok | 0.16 | 2.98e-02 | 4.28e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.3 | 2.4 | -6.1 | 26.3 | 4.4 | -1.5 |
| 10607 | ok | 0.16 | 0.1 | 1.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.3 | 27.2 | -1.9 | 5.1 | 15.8 | -3.7 |
| 10608 | ok | 0.16 | 9.57e-02 | 1.79e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 20.9 | -2.0 | 13.6 | 17.7 | -9.0 |
| 10609 | ok | 0.16 | 7.05e-02 | 2.55e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.1 | 14.5 | -2.6 | 21.5 | 14.5 | -9.1 |
| 10610 | ok | 0.16 | 4.59e-02 | 3.73e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.4 | 7.5 | -5.3 | 27.9 | 10.3 | -10.7 |
| 10611 | ok | 0.16 | 0.1 | 1.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 27.6 | 0.7 | 3.4 | 14.1 | -1.8 |
| 10612 | ok | 0.16 | 0.1 | 3.67e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 32.9 | -0.5 | -4.87e-02 | 15.0 | 0.5 |
| 10613 | ok | 0.16 | 9.39e-02 | 1.82e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.0 | 20.5 | -2.2 | 13.6 | 16.7 | -4.9 |
| 10614 | ok | 0.16 | 6.84e-02 | 2.59e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.3 | 14.3 | -2.7 | 21.0 | 13.2 | -5.1 |
| 10615 | ok | 0.16 | 4.36e-02 | 3.71e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.2 | 9.1 | -1.0 | 27.5 | 9.9 | -4.7 |
| 10616 | ok | 0.16 | 2.78e-02 | 4.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.6 | 1.1 | -5.6 | 30.1 | 6.6 | -3.3 |
| 10617 | ok | 0.16 | 0.1 | 1.05e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.2 | 27.7 | -2.0 | 5.0 | 16.1 | -5.9 |
| 10618 | ok | 0.16 | 9.78e-02 | 1.75e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 21.2 | -0.6 | 13.8 | 18.5 | -12.1 |
| 10619 | ok | 0.16 | 7.21e-02 | 2.48e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.8 | 14.7 | -2.7 | 22.0 | 15.4 | -12.1 |
| 10620 | ok | 0.16 | 4.68e-02 | 3.61e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.6 | 9.9 | 0.9 | 30.9 | 11.9 | -11.8 |
| 10621 | ok | 0.16 | 0.1 | 1.05e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.7 | 28.6 | -1.5 | 3.5 | 16.6 | -9.3 |
| 10622 | ok | 0.16 | 0.1 | 1.74e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.5 | 22.0 | -2.9 | 10.9 | 14.1 | -8.2 |
| 10623 | ok | 0.16 | 7.39e-02 | 2.46e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.7 | 15.5 | -1.1 | 22.4 | 16.3 | -14.8 |
| 10624 | ok | 0.16 | 4.87e-02 | 3.60e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.4 | 10.0 | 0.7 | 31.9 | 12.9 | -15.3 |
| 10625 | ok | 0.16 | 0.1 | 1.05e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.7 | 29.0 | -0.4 | 3.6 | 17.0 | -11.4 |
| 10626 | ok | 0.16 | 0.1 | 1.74e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.5 | 22.5 | -3.0 | 11.0 | 14.5 | -9.9 |
| 10627 | ok | 0.16 | 7.58e-02 | 2.46e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.6 | 14.6 | -3.8 | 21.3 | 15.8 | -17.6 |
| 10628 | ok | 0.16 | 5.07e-02 | 3.63e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.3 | 10.2 | 0.4 | 32.6 | 13.4 | -18.9 |
| 10629 | ok | 0.16 | 0.1 | 1.05e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.7 | 29.8 | -0.5 | 3.6 | 17.2 | -13.3 |
| 10630 | ok | 0.16 | 0.1 | 1.75e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.5 | 22.9 | -1.9 | 11.1 | 14.7 | -11.5 |
| 10631 | ok | 0.16 | 7.77e-02 | 2.50e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.6 | 14.9 | -4.0 | 21.6 | 16.0 | -20.3 |
| 10632 | ok | 0.16 | 5.27e-02 | 3.71e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.8 | 7.2 | -6.1 | 30.9 | 12.8 | -24.0 |
| 10633 | ok | 0.16 | 0.1 | 1.05e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.7 | 30.7 | -0.6 | 3.7 | 17.4 | -15.3 |
| 10634 | ok | 0.16 | 0.1 | 1.77e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.6 | 23.5 | -2.1 | 11.3 | 14.8 | -13.2 |
| 10635 | ok | 0.16 | 7.95e-02 | 2.55e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.7 | 15.2 | -4.2 | 21.8 | 15.9 | -23.1 |
| 10636 | ok | 0.16 | 5.44e-02 | 3.82e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.0 | 7.2 | -6.3 | 30.9 | 12.5 | -27.4 |
| 10637 | ok | 0.16 | 0.1 | 1.06e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.7 | 31.6 | -0.7 | 3.8 | 17.6 | -17.3 |
| 10638 | ok | 0.16 | 0.1 | 1.81e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.6 | 24.1 | -2.2 | 11.6 | 14.8 | -14.8 |
| 10639 | ok | 0.16 | 8.13e-02 | 2.61e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.9 | 15.5 | -4.4 | 22.0 | 15.5 | -26.0 |
| 10640 | ok | 0.16 | 5.56e-02 | 3.93e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.3 | 7.1 | -6.4 | 30.6 | 11.9 | -30.8 |
| 10641 | ok | 0.16 | 0.1 | 1.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 33.1 | -2.0 | 4.0 | 17.8 | -23.1 |
| 10642 | ok | 0.16 | 0.2 | 3.50e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 40.8 | -1.1 | 5.20e-02 | 18.8 | -8.0 |
| 10643 | ok | 0.16 | 0.1 | 1.85e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.3 | 25.2 | -3.2 | 10.5 | 14.6 | -21.5 |
| 10644 | ok | 0.16 | 8.29e-02 | 2.70e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.0 | 16.6 | -2.6 | 22.2 | 15.1 | -28.9 |
| 10645 | ok | 0.16 | 5.61e-02 | 4.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.8 | 7.1 | -6.5 | 30.4 | 11.3 | -34.4 |
| 10646 | ok | 0.16 | 2.60e-02 | 4.75e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.1 | -2.2 | -6.9 | 34.6 | 9.1 | -12.5 |
| 10647 | ok | 0.16 | 0.2 | 1.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 34.2 | -2.0 | 4.1 | 17.8 | -26.0 |
| 10648 | ok | 0.16 | 0.2 | 3.46e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 42.4 | -1.1 | 6.89e-02 | 18.9 | -9.0 |
| 10649 | ok | 0.16 | 0.1 | 1.89e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.3 | 25.5 | -1.9 | 10.9 | 14.6 | -24.1 |
| 10650 | ok | 0.16 | 8.56e-02 | 2.77e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.3 | 16.6 | -2.8 | 21.1 | 13.7 | -30.3 |
| 10651 | ok | 0.16 | 5.61e-02 | 4.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.2 | 6.7 | -6.7 | 28.2 | 9.9 | -35.7 |
| 10652 | ok | 0.16 | 2.29e-02 | 4.93e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.6 | 4.5 | 0.8 | 37.6 | 9.0 | -11.5 |
| 10653 | ok | 0.16 | 0.2 | 1.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 35.2 | -1.9 | 4.4 | 18.4 | -29.2 |
| 10654 | ok | 0.16 | 0.2 | 3.44e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 43.9 | -1.1 | 8.84e-02 | 19.6 | -10.2 |
| 10655 | ok | 0.16 | 0.1 | 1.92e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.4 | 26.1 | -1.9 | 11.4 | 14.6 | -27.1 |
| 10656 | ok | 0.16 | 8.71e-02 | 2.83e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.6 | 16.9 | -2.6 | 21.6 | 13.5 | -33.6 |
| 10657 | ok | 0.16 | 5.58e-02 | 4.29e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.9 | 11.2 | 0.6 | 32.8 | 10.9 | -41.8 |
| 10658 | ok | 0.16 | 2.20e-02 | 5.07e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.2 | 4.4 | 1.3 | 36.7 | 8.3 | -12.6 |
| 10659 | ok | 0.16 | 0.2 | 1.10e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 36.3 | -0.9 | 4.5 | 17.0 | -34.4 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------|-------|------|----------|----------|--------|--------|---------|---------|-------|-------|------|----------|--------|--------|
| 10660 | ok | 0.16 | 0.2 | 3.41e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 46.2 | -0.2 | -0.4 | 18.0 | -11.0 |
| 10661 | ok | 0.16 | 0.1 | 1.95e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.8 | 26.7 | -2.6 | 11.4 | 13.5 | -31.8 |
| 10662 | ok | 0.16 | 8.95e-02 | 2.91e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.6 | 17.6 | -3.8 | 17.1 | 10.3 | -30.8 |
| 10663 | ok | 0.16 | 5.49e-02 | 4.38e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.6 | 6.4 | -4.0 | 35.2 | 11.6 | -51.5 |
| 10664 | ok | 0.16 | 2.34e-02 | 5.19e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.2 | 3.9 | 2.6 | 38.7 | 8.8 | -14.6 |
| 10665 | ok | 0.16 | 0.2 | 1.10e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 35.6 | -0.6 | 4.6 | 19.0 | -32.3 |
| 10666 | ok | 0.16 | 0.2 | 3.42e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 44.6 | 0.2 | 6.02e-02 | 20.3 | -11.1 |
| 10667 | ok | 0.16 | 0.1 | 1.94e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.6 | 25.8 | -2.8 | 10.8 | 13.0 | -28.7 |
| 10668 | ok | 0.16 | 8.83e-02 | 2.88e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.6 | 17.1 | -5.7 | 16.4 | 9.7 | -28.4 |
| 10669 | ok | 0.16 | 5.51e-02 | 4.35e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.3 | 11.1 | 1.1 | 33.6 | 11.0 | -45.8 |
| 10670 | ok | 0.16 | 2.26e-02 | 5.15e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.8 | 4.1 | 1.9 | 37.0 | 8.2 | -13.6 |
| 10671 | ok | 0.16 | 0.2 | 1.10e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 37.6 | -0.7 | 4.8 | 18.1 | -37.9 |
| 10672 | ok | 0.16 | 0.1 | 1.96e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 27.5 | -2.2 | 12.2 | 14.3 | -34.9 |
| 10673 | ok | 0.16 | 9.04e-02 | 2.94e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | 17.8 | -3.0 | 18.4 | 10.9 | -33.6 |
| 10674 | ok | 0.16 | 5.44e-02 | 4.39e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.9 | 6.0 | -3.3 | 37.6 | 12.6 | -55.7 |
| 10675 | ok | 0.16 | 0.2 | 1.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 39.5 | -1.7 | 5.2 | 19.5 | -41.8 |
| 10676 | ok | 0.16 | 0.1 | 1.96e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.0 | 28.7 | -2.7 | 13.2 | 15.5 | -38.5 |
| 10677 | ok | 0.16 | 9.10e-02 | 2.94e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.3 | 18.0 | -2.4 | 20.0 | 11.9 | -36.8 |
| 10678 | ok | 0.16 | 5.39e-02 | 4.41e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -12.2 | 5.5 | -2.7 | 40.9 | 14.1 | -60.2 |
| 10679 | ok | 0.16 | 0.2 | 1.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 40.3 | -1.5 | 5.6 | 21.5 | -45.9 |
| 10680 | ok | 0.16 | 0.1 | 1.96e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.1 | 29.0 | -2.3 | 14.3 | 17.2 | -42.2 |
| 10681 | ok | 0.16 | 9.16e-02 | 2.95e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.6 | 18.4 | -2.5 | 21.9 | 13.4 | -40.2 |
| 10682 | ok | 0.16 | 5.33e-02 | 4.36e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -12.3 | 4.8 | -1.8 | 44.9 | 16.0 | -65.0 |
| 10683 | ok | 0.16 | 0.2 | 1.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 40.9 | -1.2 | 6.1 | 24.0 | -50.8 |
| 10684 | ok | 0.16 | 0.1 | 2.00e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.2 | 29.1 | -1.5 | 15.8 | 19.6 | -46.7 |
| 10685 | ok | 0.16 | 9.16e-02 | 3.03e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.0 | 15.7 | -0.5 | 36.0 | 23.4 | -62.9 |
| 10686 | ok | 0.16 | 5.16e-02 | 4.42e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -12.8 | 4.1 | -0.9 | 50.7 | 18.6 | -70.8 |
| 10687 | ok | 0.16 | 0.2 | 1.11e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 41.0 | -0.8 | 6.6 | 26.7 | -56.1 |
| 10688 | ok | 0.16 | 0.1 | 2.06e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.3 | 28.9 | -0.8 | 17.5 | 22.1 | -51.6 |
| 10689 | ok | 0.16 | 9.09e-02 | 3.18e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.2 | 15.0 | 0.6 | 40.4 | 26.4 | -69.0 |
| 10690 | ok | 0.16 | 4.75e-02 | 4.67e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -13.2 | 3.3 | 0.3 | 57.6 | 21.4 | -77.1 |
| 10691 | ok | 0.16 | 0.2 | 1.12e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 40.7 | -0.4 | 7.0 | 29.1 | -61.7 |
| 10692 | ok | 0.16 | 0.1 | 2.15e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.3 | 28.3 | 0.1 | 19.1 | 24.5 | -56.8 |
| 10693 | ok | 0.16 | 8.66e-02 | 3.41e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.3 | 15.1 | 4.1 | 45.3 | 29.5 | -75.2 |
| 10694 | ok | 0.16 | 4.48e-02 | 5.13e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -12.4 | 8.1 | 8.1 | 65.4 | 24.3 | -81.9 |
| 10695 | ok | 0.16 | 0.2 | 1.14e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 40.0 | 0.3 | 8.0 | 30.5 | -67.3 |
| 10696 | ok | 0.16 | 0.1 | 2.27e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.4 | 27.3 | 1.3 | 20.6 | 26.3 | -62.3 |
| 10697 | ok | 0.16 | 8.08e-02 | 3.71e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.7 | 13.9 | 5.4 | 47.5 | 30.5 | -77.0 |
| 10698 | ok | 0.16 | 4.65e-02 | 5.67e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.7 | 3.8 | 6.9 | 73.4 | 28.2 | -78.3 |
| 10699 | ok | 0.16 | 0.2 | 1.17e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 38.9 | 0.5 | 8.1 | 35.6 | -71.8 |
| 10700 | ok | 0.16 | 0.1 | 2.39e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -3.6 | 26.1 | 2.6 | 23.7 | 30.9 | -66.7 |
| 10701 | ok | 0.16 | 7.55e-02 | 4.03e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.2 | 12.5 | 6.2 | 51.2 | 32.6 | -82.2 |
| 10702 | ok | 0.16 | 5.08e-02 | 6.38e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -15.4 | 1.1 | 3.9 | 75.0 | 27.3 | -86.1 |
| 10703 | ok | 0.16 | 0.2 | 1.24e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 37.4 | 1.0 | 8.1 | 35.9 | -76.1 |
| 10704 | ok | 0.16 | 0.1 | 2.60e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.9 | 24.2 | 4.2 | 27.2 | 32.4 | -70.2 |
| 10705 | ok | 0.16 | 7.19e-02 | 4.52e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.4 | 11.0 | 7.7 | 55.0 | 34.1 | -87.6 |
| 10706 | ok | 0.16 | 5.53e-02 | 7.22e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -15.7 | -0.3 | 5.8 | 83.1 | 29.8 | -91.5 |
| 10707 | ok | 0.16 | 0.2 | 1.30e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 35.1 | 1.5 | 7.4 | 33.5 | -80.4 |
| 10708 | ok | 0.16 | 0.1 | 2.93e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.1 | 21.6 | 5.9 | 27.8 | 32.1 | -75.1 |
| 10709 | ok | 0.16 | 6.83e-02 | 5.22e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.0 | 7.9 | 8.2 | 59.7 | 34.9 | -94.8 |
| 10710 | ok | 0.16 | 6.08e-02 | 8.32e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -16.7 | -2.2 | 8.4 | 94.9 | 32.9 | -98.4 |
| 10711 | ok | 0.16 | 0.2 | 1.38e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 31.9 | 2.1 | 5.7 | 26.4 | -82.8 |
| 10712 | ok | 0.16 | 9.58e-02 | 3.42e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.4 | 18.1 | 7.9 | 26.7 | 28.6 | -78.3 |
| 10713 | ok | 0.16 | 7.05e-02 | 6.25e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.6 | 4.7 | 10.7 | 62.4 | 33.2 | -100.1 |
| 10714 | ok | 0.16 | 6.63e-02 | 9.84e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -17.8 | -4.4 | 11.6 | 107.2 | 35.1 | -104.5 |
| 10715 | ok | 0.16 | 0.1 | 1.58e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 27.7 | 2.8 | 2.6 | 11.9 | -81.7 |
| 10716 | ok | 0.16 | 9.56e-02 | 4.27e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -7.4 | 9.8 | 8.8 | 22.9 | 17.1 | -104.5 |
| 10717 | ok | 0.16 | 7.21e-02 | 7.77e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -12.6 | 0.9 | 13.7 | 61.7 | 27.4 | -102.6 |
| 10718 | ok | 0.16 | 7.12e-02 | 1.17e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -19.2 | -7.1 | 15.1 | 119.2 | 36.0 | -109.0 |
| 10719 | ok | 0.16 | 0.1 | 2.07e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.4 | 22.1 | 3.8 | -2.1 | -17.1 | -74.9 |
| 10720 | ok | 0.16 | 9.56e-02 | 5.79e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.8 | 4.7 | 13.5 | 10.6 | -10.9 | -96.5 |
| 10721 | ok | 0.16 | 7.35e-02 | 9.86e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -12.6 | -2.9 | 17.4 | 56.8 | 13.0 | -104.2 |
| 10722 | ok | 0.16 | 7.42e-02 | 1.39e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -21.5 | -10.2 | 18.7 | 129.1 | 34.7 | -110.3 |
| 10723 | ok | 0.16 | 0.1 | 3.42e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.5 | 9.4 | 7.4 | -16.6 | -92.6 | -71.1 |
| 10724 | ok | 0.16 | 9.62e-02 | 8.54e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.6 | -2.9 | 16.9 | -8.6 | -67.1 | -79.8 |
| 10725 | ok | 0.16 | 7.51e-02 | 1.27e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -17.5 | -7.2 | 23.0 | 40.1 | -17.0 | -88.9 |
| 10726 | ok | 0.16 | 7.42e-02 | 1.64e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -25.7 | -13.5 | 21.8 | 131.4 | 29.2 | -105.5 |
| 10727 | ok | 0.16 | 0.1 | 7.01e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.4 | -5.2 | 13.7 | -27.2 | -204.9 | -49.2 |
| 10728 | ok | 0.16 | 0.1 | 1.30e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -19.6 | -6.8 | 24.4 | -32.7 | -137.6 | -44.4 |
| 10729 | ok | 0.16 | 7.69e-02 | 1.63e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -26.6 | -9.8 | 27.5 | 12.0 | -72.6 | -56.8 |
| 10730 | ok | 0.16 | 6.72e-02 | 1.92e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.4 | -16.4 | 22.8 | 116.2 | 9.8 | -91.7 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------|-------|------|----------|----------|--------|--------|---------|---------|-------|-------|-------|--------|--------|--------|
| 10731 | ok | 0.16 | 0.2 | 2.09e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -11.0 | -18.4 | 26.3 | -48.5 | -357.7 | 2.5 |
| 10732 | ok | 0.16 | 0.1 | 1.90e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -33.7 | -9.5 | 31.1 | -62.5 | -257.8 | 9.4 |
| 10733 | ok | 0.16 | 9.74e-02 | 2.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -43.0 | -10.5 | 30.5 | -30.0 | -176.9 | 4.4 |
| 10734 | ok | 0.16 | 5.21e-02 | 2.30e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -48.3 | -12.6 | 28.9 | 72.4 | -69.2 | -27.7 |
| 11065 | ok | 0.16 | 0.1 | 7.89e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | -11.9 | -12.9 | -33.3 | -260.8 | 45.4 |
| 11066 | ok | 0.16 | 0.1 | 1.26e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -20.2 | -11.8 | -19.1 | -43.8 | -186.2 | 37.7 |
| 11067 | ok | 0.16 | 7.47e-02 | 1.51e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -28.7 | -12.1 | -22.8 | -5.4 | -112.2 | 51.0 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | 0.16 | 0.24 | 0.04 | 4.52 | 4.52 | 3.14 | 3.14 | 1.47 | 54.31 | 47.38 | 438.57 | 102.24 | 127.90 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 1 | ok | 0.47 | | | | | | |
| 5 | ok | 0.45 | | | | | | |
| 7078 | ok | 0.64 | | | | | | |
| 7304 | ok | 0.98 | | | | | | |
| 7307 | ok | 1.01 | | | | | | |
| 7369 | ok | 0.64 | | | | | | |
| 7683 | ok | 0.47 | | | | | | |
| 7685 | ok | 0.44 | | | | | | |
| 7687 | ok | 0.52 | | | | | | |
| 7689 | ok | 0.98 | | | | | | |
| 9284 | ok | 0.45 | | | | | | |
| 9285 | ok | 0.42 | | | | | | |
| 9286 | ok | 0.52 | | | | | | |
| 9287 | ok | 1.01 | | | | | | |
| 10428 | ok | 0.27 | | | | | | |
| 10429 | ok | 0.16 | | | | | | |
| 10430 | ok | 0.13 | | | | | | |
| 10431 | ok | 0.08 | | | | | | |
| 10432 | ok | 0.07 | | | | | | |
| 10433 | ok | 0.04 | | | | | | |
| 10434 | ok | 0.01 | | | | | | |
| 10435 | ok | 0.04 | | | | | | |
| 10436 | ok | 0.19 | | | | | | |
| 10437 | ok | 0.41 | | | | | | |
| 10438 | ok | 0.24 | | | | | | |
| 10439 | ok | 0.21 | | | | | | |
| 10440 | ok | 0.19 | | | | | | |
| 10441 | ok | 0.12 | | | | | | |
| 10442 | ok | 0.11 | | | | | | |
| 10443 | ok | 0.09 | | | | | | |
| 10444 | ok | 0.45 | | | | | | |
| 10445 | ok | 0.38 | | | | | | |
| 10446 | ok | 0.32 | | | | | | |
| 10447 | ok | 0.15 | | | | | | |
| 10448 | ok | 0.07 | | | | | | |
| 10449 | ok | 0.03 | | | | | | |
| 10450 | ok | 0.03 | | | | | | |
| 10451 | ok | 0.03 | | | | | | |
| 10452 | ok | 0.02 | | | | | | |
| 10453 | ok | 0.02 | | | | | | |
| 10454 | ok | 0.05 | | | | | | |
| 10455 | ok | 0.06 | | | | | | |
| 10456 | ok | 0.07 | | | | | | |
| 10457 | ok | 0.08 | | | | | | |
| 10458 | ok | 0.09 | | | | | | |
| 10459 | ok | 0.10 | | | | | | |
| 10460 | ok | 0.11 | | | | | | |
| 10461 | ok | 0.12 | | | | | | |
| 10462 | ok | 0.14 | | | | | | |
| 10463 | ok | 0.16 | | | | | | |
| 10464 | ok | 0.47 | | | | | | |
| 10465 | ok | 0.27 | | | | | | |
| 10466 | ok | 0.12 | | | | | | |
| 10467 | ok | 0.10 | | | | | | |
| 10468 | ok | 0.07 | | | | | | |
| 10469 | ok | 0.06 | | | | | | |
| 10470 | ok | 0.03 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------|-------|---------|----------|-----------|---------|----------|------|-------|
| 10471 | ok | 0.02 | | | | | | |
| 10472 | ok | 0.05 | | | | | | |
| 10473 | ok | 0.13 | | | | | | |
| 10474 | ok | 0.21 | | | | | | |
| 10475 | ok | 0.17 | | | | | | |
| 10476 | ok | 0.14 | | | | | | |
| 10477 | ok | 0.09 | | | | | | |
| 10478 | ok | 0.08 | | | | | | |
| 10479 | ok | 0.07 | | | | | | |
| 10480 | ok | 1.01 | | | | | | |
| 10481 | ok | 0.60 | | | | | | |
| 10482 | ok | 0.39 | | | | | | |
| 10483 | ok | 0.11 | | | | | | |
| 10484 | ok | 0.06 | | | | | | |
| 10485 | ok | 0.03 | | | | | | |
| 10486 | ok | 0.03 | | | | | | |
| 10487 | ok | 0.03 | | | | | | |
| 10488 | ok | 0.02 | | | | | | |
| 10489 | ok | 0.02 | | | | | | |
| 10490 | ok | 0.06 | | | | | | |
| 10491 | ok | 0.06 | | | | | | |
| 10492 | ok | 0.07 | | | | | | |
| 10493 | ok | 0.07 | | | | | | |
| 10494 | ok | 0.08 | | | | | | |
| 10495 | ok | 0.08 | | | | | | |
| 10496 | ok | 0.09 | | | | | | |
| 10497 | ok | 0.10 | | | | | | |
| 10498 | ok | 0.10 | | | | | | |
| 10499 | ok | 0.12 | | | | | | |
| 10500 | ok | 0.98 | | | | | | |
| 10501 | ok | 0.47 | | | | | | |
| 10502 | ok | 0.44 | | | | | | |
| 10503 | ok | 0.52 | | | | | | |
| 10504 | ok | 0.98 | | | | | | |
| 10505 | ok | 0.35 | | | | | | |
| 10506 | ok | 0.35 | | | | | | |
| 10507 | ok | 0.29 | | | | | | |
| 10508 | ok | 0.34 | | | | | | |
| 10509 | ok | 0.41 | | | | | | |
| 10510 | ok | 0.41 | | | | | | |
| 10511 | ok | 0.29 | | | | | | |
| 10512 | ok | 0.30 | | | | | | |
| 10513 | ok | 0.20 | | | | | | |
| 10514 | ok | 0.22 | | | | | | |
| 10515 | ok | 0.27 | | | | | | |
| 10516 | ok | 0.27 | | | | | | |
| 10517 | ok | 0.25 | | | | | | |
| 10518 | ok | 0.27 | | | | | | |
| 10519 | ok | 0.13 | | | | | | |
| 10520 | ok | 0.15 | | | | | | |
| 10521 | ok | 0.20 | | | | | | |
| 10522 | ok | 0.20 | | | | | | |
| 10523 | ok | 0.21 | | | | | | |
| 10524 | ok | 0.24 | | | | | | |
| 10525 | ok | 0.09 | | | | | | |
| 10526 | ok | 0.10 | | | | | | |
| 10527 | ok | 0.16 | | | | | | |
| 10528 | ok | 0.17 | | | | | | |
| 10529 | ok | 0.18 | | | | | | |
| 10530 | ok | 0.21 | | | | | | |
| 10531 | ok | 0.06 | | | | | | |
| 10532 | ok | 0.07 | | | | | | |
| 10533 | ok | 0.13 | | | | | | |
| 10534 | ok | 0.15 | | | | | | |
| 10535 | ok | 0.16 | | | | | | |
| 10536 | ok | 0.05 | | | | | | |
| 10537 | ok | 0.05 | | | | | | |
| 10538 | ok | 0.11 | | | | | | |
| 10539 | ok | 0.14 | | | | | | |
| 10540 | ok | 0.04 | | | | | | |
| 10541 | ok | 0.04 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------|-------|----------|----------|-----------|---------|----------|------|-------|
| 10542 | ok | 0.10 | | | | | | |
| 10543 | ok | 0.12 | | | | | | |
| 10544 | ok | 0.03 | | | | | | |
| 10545 | ok | 0.04 | | | | | | |
| 10546 | ok | 0.09 | | | | | | |
| 10547 | ok | 0.10 | | | | | | |
| 10548 | ok | 0.03 | | | | | | |
| 10549 | ok | 0.03 | | | | | | |
| 10550 | ok | 0.08 | | | | | | |
| 10551 | ok | 0.09 | | | | | | |
| 10552 | ok | 0.02 | | | | | | |
| 10553 | ok | 0.03 | | | | | | |
| 10554 | ok | 0.07 | | | | | | |
| 10555 | ok | 0.08 | | | | | | |
| 10556 | ok | 0.02 | | | | | | |
| 10557 | ok | 0.03 | | | | | | |
| 10558 | ok | 0.07 | | | | | | |
| 10559 | ok | 0.06 | | | | | | |
| 10560 | ok | 0.02 | | | | | | |
| 10561 | ok | 0.03 | | | | | | |
| 10562 | ok | 0.06 | | | | | | |
| 10563 | ok | 0.05 | | | | | | |
| 10564 | ok | 0.02 | | | | | | |
| 10565 | ok | 0.02 | | | | | | |
| 10566 | ok | 0.05 | | | | | | |
| 10567 | ok | 0.04 | | | | | | |
| 10568 | ok | 0.02 | | | | | | |
| 10569 | ok | 0.02 | | | | | | |
| 10570 | ok | 0.05 | | | | | | |
| 10571 | ok | 0.04 | | | | | | |
| 10572 | ok | 0.02 | | | | | | |
| 10573 | ok | 0.02 | | | | | | |
| 10574 | ok | 0.04 | | | | | | |
| 10575 | ok | 0.03 | | | | | | |
| 10576 | ok | 0.01 | | | | | | |
| 10577 | ok | 0.02 | | | | | | |
| 10578 | ok | 0.03 | | | | | | |
| 10579 | ok | 0.02 | | | | | | |
| 10580 | ok | 0.01 | | | | | | |
| 10581 | ok | 0.01 | | | | | | |
| 10582 | ok | 0.03 | | | | | | |
| 10583 | ok | 0.02 | | | | | | |
| 10584 | ok | 0.03 | | | | | | |
| 10585 | ok | 9.99e-03 | | | | | | |
| 10586 | ok | 0.01 | | | | | | |
| 10587 | ok | 0.02 | | | | | | |
| 10588 | ok | 0.04 | | | | | | |
| 10589 | ok | 0.01 | | | | | | |
| 10590 | ok | 0.03 | | | | | | |
| 10591 | ok | 8.32e-03 | | | | | | |
| 10592 | ok | 9.06e-03 | | | | | | |
| 10593 | ok | 0.01 | | | | | | |
| 10594 | ok | 0.03 | | | | | | |
| 10595 | ok | 7.47e-03 | | | | | | |
| 10596 | ok | 0.02 | | | | | | |
| 10597 | ok | 7.47e-03 | | | | | | |
| 10598 | ok | 6.63e-03 | | | | | | |
| 10599 | ok | 0.01 | | | | | | |
| 10600 | ok | 0.01 | | | | | | |
| 10601 | ok | 9.31e-03 | | | | | | |
| 10602 | ok | 0.02 | | | | | | |
| 10603 | ok | 7.41e-03 | | | | | | |
| 10604 | ok | 6.99e-03 | | | | | | |
| 10605 | ok | 9.64e-03 | | | | | | |
| 10606 | ok | 0.02 | | | | | | |
| 10607 | ok | 0.01 | | | | | | |
| 10608 | ok | 9.11e-03 | | | | | | |
| 10609 | ok | 0.01 | | | | | | |
| 10610 | ok | 0.02 | | | | | | |
| 10611 | ok | 9.37e-03 | | | | | | |
| 10612 | ok | 0.01 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------|-------|----------|----------|-----------|---------|----------|------|-------|
| 10613 | ok | 8.04e-03 | | | | | | |
| 10614 | ok | 8.81e-03 | | | | | | |
| 10615 | ok | 0.02 | | | | | | |
| 10616 | ok | 0.02 | | | | | | |
| 10617 | ok | 0.02 | | | | | | |
| 10618 | ok | 9.80e-03 | | | | | | |
| 10619 | ok | 0.01 | | | | | | |
| 10620 | ok | 0.02 | | | | | | |
| 10621 | ok | 0.02 | | | | | | |
| 10622 | ok | 0.01 | | | | | | |
| 10623 | ok | 0.01 | | | | | | |
| 10624 | ok | 0.02 | | | | | | |
| 10625 | ok | 0.03 | | | | | | |
| 10626 | ok | 0.01 | | | | | | |
| 10627 | ok | 0.01 | | | | | | |
| 10628 | ok | 0.03 | | | | | | |
| 10629 | ok | 0.03 | | | | | | |
| 10630 | ok | 0.01 | | | | | | |
| 10631 | ok | 0.01 | | | | | | |
| 10632 | ok | 0.03 | | | | | | |
| 10633 | ok | 0.03 | | | | | | |
| 10634 | ok | 0.01 | | | | | | |
| 10635 | ok | 0.01 | | | | | | |
| 10636 | ok | 0.02 | | | | | | |
| 10637 | ok | 0.04 | | | | | | |
| 10638 | ok | 9.69e-03 | | | | | | |
| 10639 | ok | 0.01 | | | | | | |
| 10640 | ok | 0.02 | | | | | | |
| 10641 | ok | 0.04 | | | | | | |
| 10642 | ok | 0.04 | | | | | | |
| 10643 | ok | 9.24e-03 | | | | | | |
| 10644 | ok | 9.43e-03 | | | | | | |
| 10645 | ok | 0.03 | | | | | | |
| 10646 | ok | 0.03 | | | | | | |
| 10647 | ok | 0.05 | | | | | | |
| 10648 | ok | 0.05 | | | | | | |
| 10649 | ok | 9.06e-03 | | | | | | |
| 10650 | ok | 8.37e-03 | | | | | | |
| 10651 | ok | 0.03 | | | | | | |
| 10652 | ok | 0.04 | | | | | | |
| 10653 | ok | 0.05 | | | | | | |
| 10654 | ok | 0.05 | | | | | | |
| 10655 | ok | 8.97e-03 | | | | | | |
| 10656 | ok | 8.00e-03 | | | | | | |
| 10657 | ok | 0.03 | | | | | | |
| 10658 | ok | 0.04 | | | | | | |
| 10659 | ok | 0.06 | | | | | | |
| 10660 | ok | 0.06 | | | | | | |
| 10661 | ok | 0.01 | | | | | | |
| 10662 | ok | 0.01 | | | | | | |
| 10663 | ok | 0.05 | | | | | | |
| 10664 | ok | 0.05 | | | | | | |
| 10665 | ok | 0.06 | | | | | | |
| 10666 | ok | 0.06 | | | | | | |
| 10667 | ok | 9.32e-03 | | | | | | |
| 10668 | ok | 9.38e-03 | | | | | | |
| 10669 | ok | 0.04 | | | | | | |
| 10670 | ok | 0.05 | | | | | | |
| 10671 | ok | 0.07 | | | | | | |
| 10672 | ok | 0.01 | | | | | | |
| 10673 | ok | 0.01 | | | | | | |
| 10674 | ok | 0.05 | | | | | | |
| 10675 | ok | 0.07 | | | | | | |
| 10676 | ok | 0.01 | | | | | | |
| 10677 | ok | 0.02 | | | | | | |
| 10678 | ok | 0.06 | | | | | | |
| 10679 | ok | 0.08 | | | | | | |
| 10680 | ok | 0.02 | | | | | | |
| 10681 | ok | 0.02 | | | | | | |
| 10682 | ok | 0.06 | | | | | | |
| 10683 | ok | 0.09 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------------|-------|----------------|-----------------|------------------|----------------|-----------------|-------------|--------------|
| 10684 | ok | 0.02 | | | | | | |
| 10685 | ok | 0.02 | | | | | | |
| 10686 | ok | 0.07 | | | | | | |
| 10687 | ok | 0.10 | | | | | | |
| 10688 | ok | 0.02 | | | | | | |
| 10689 | ok | 0.03 | | | | | | |
| 10690 | ok | 0.08 | | | | | | |
| 10691 | ok | 0.11 | | | | | | |
| 10692 | ok | 0.03 | | | | | | |
| 10693 | ok | 0.03 | | | | | | |
| 10694 | ok | 0.09 | | | | | | |
| 10695 | ok | 0.12 | | | | | | |
| 10696 | ok | 0.03 | | | | | | |
| 10697 | ok | 0.04 | | | | | | |
| 10698 | ok | 0.10 | | | | | | |
| 10699 | ok | 0.13 | | | | | | |
| 10700 | ok | 0.04 | | | | | | |
| 10701 | ok | 0.05 | | | | | | |
| 10702 | ok | 0.11 | | | | | | |
| 10703 | ok | 0.15 | | | | | | |
| 10704 | ok | 0.05 | | | | | | |
| 10705 | ok | 0.06 | | | | | | |
| 10706 | ok | 0.12 | | | | | | |
| 10707 | ok | 0.17 | | | | | | |
| 10708 | ok | 0.06 | | | | | | |
| 10709 | ok | 0.08 | | | | | | |
| 10710 | ok | 0.14 | | | | | | |
| 10711 | ok | 0.20 | | | | | | |
| 10712 | ok | 0.09 | | | | | | |
| 10713 | ok | 0.11 | | | | | | |
| 10714 | ok | 0.17 | | | | | | |
| 10715 | ok | 0.23 | | | | | | |
| 10716 | ok | 0.13 | | | | | | |
| 10717 | ok | 0.15 | | | | | | |
| 10718 | ok | 0.21 | | | | | | |
| 10719 | ok | 0.27 | | | | | | |
| 10720 | ok | 0.19 | | | | | | |
| 10721 | ok | 0.22 | | | | | | |
| 10722 | ok | 0.27 | | | | | | |
| 10723 | ok | 0.32 | | | | | | |
| 10724 | ok | 0.27 | | | | | | |
| 10725 | ok | 0.32 | | | | | | |
| 10726 | ok | 0.39 | | | | | | |
| 10727 | ok | 0.38 | | | | | | |
| 10728 | ok | 0.36 | | | | | | |
| 10729 | ok | 0.44 | | | | | | |
| 10730 | ok | 0.60 | | | | | | |
| 10731 | ok | 0.45 | | | | | | |
| 10732 | ok | 0.42 | | | | | | |
| 10733 | ok | 0.52 | | | | | | |
| 10734 | ok | 1.01 | | | | | | |
| 11065 | ok | 0.41 | | | | | | |
| 11066 | ok | 0.38 | | | | | | |
| 11067 | ok | 0.46 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 1.01 | | | | | | |

1.1.1.1.8 Verifica Macrosetti fondazioni pilastri porticato

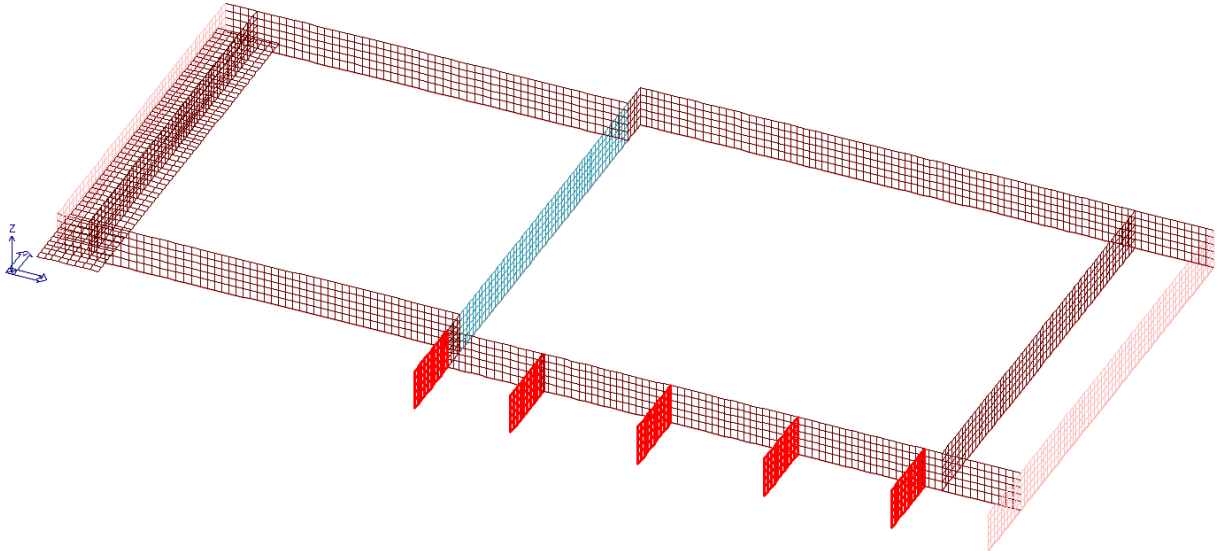


Fig 176. Individuazione del Macrosetto/i oggetto di Verifica (Selezione in rosso).

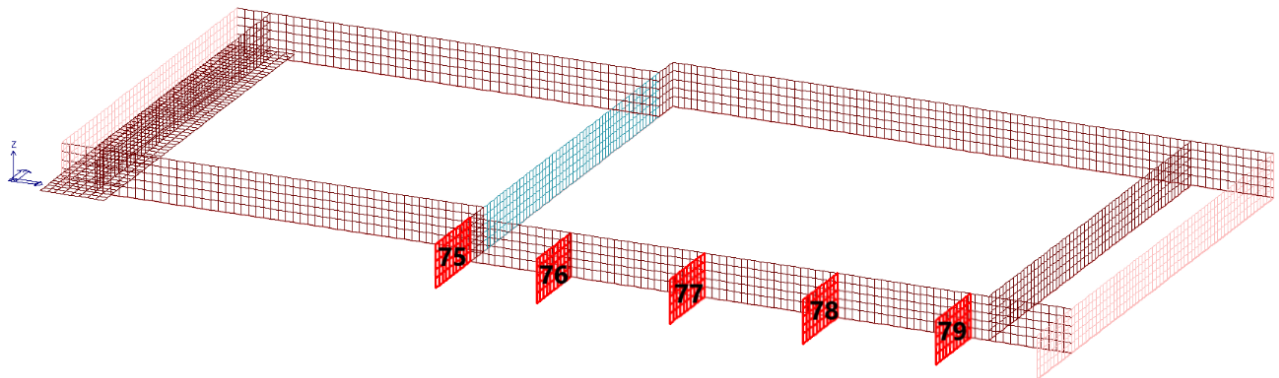


Fig 177. Numerazione Macrosetto oggetto di verifica.

Si riporta il tabulato di verifica completo.

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 75 | 25.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|--------|--------|--------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 31 | ok | 0.16 | 0.2 | 6.65e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -62.4 | -174.1 | 66.2 | -0.9 | -126.9 | 25.0 |
| 6847 | ok | 0.16 | 0.9 | 9.17e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -207.6 | 210.2 | -83.2 | -576.6 | -30.3 | -254.3 |
| 7333 | ok | 0.16 | 0.2 | 2.05e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -45.9 | 31.5 | -37.8 | -35.2 | 67.0 | 77.3 |
| 7634 | ok | 0.16 | 0.2 | 3.40e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -54.0 | -4.5 | 67.0 | 23.1 | 12.0 | -29.6 |
| 7907 | ok | 0.16 | 0.2 | 3.15e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -57.6 | -45.4 | 50.0 | -21.1 | -168.2 | 65.6 |
| 7908 | ok | 0.16 | 9.34e-02 | 2.64e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -54.5 | -21.9 | 46.8 | -17.7 | -115.8 | 70.5 |
| 7909 | ok | 0.16 | 7.06e-02 | 2.61e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -51.0 | -14.3 | 40.9 | -13.2 | -81.0 | 67.7 |
| 7910 | ok | 0.16 | 8.70e-02 | 3.83e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -53.5 | -33.9 | 68.8 | 9.7 | -87.2 | 83.0 |
| 9776 | ok | 0.16 | 0.5 | 2.70e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -5.6 | -51.7 | 14.2 | -3.5 | -115.0 | -4.4 |
| 9777 | ok | 0.16 | 0.1 | 3.34e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -39.2 | -39.8 | 44.8 | -24.2 | -132.5 | 7.3 |
| 9778 | ok | 0.16 | 0.2 | 1.01e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -2.2 | -35.1 | 10.3 | -6.4 | -90.1 | -8.7 |
| 9779 | ok | 0.16 | 0.2 | 1.71e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -17.9 | -40.2 | 33.8 | -16.4 | -83.6 | -6.7 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------------|-------|------------|--------------|-----------------|---------------|---------------|----------------|----------------|------------|------------|-------------|------------|------------|-------------|
| 9780 | ok | 0.16 | 0.2 | 3.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.0 | -8.1 | 5.9 | -5.1 | -57.1 | -18.2 |
| 9781 | ok | 0.16 | 0.1 | 1.05e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -8.7 | -21.9 | 23.5 | -13.7 | -51.8 | -22.6 |
| 9782 | ok | 0.16 | 0.2 | 6.58e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.2 | 32.7 | -5.3 | -3.3 | -25.1 | -17.6 |
| 9783 | ok | 0.16 | 0.1 | 6.22e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | -5.5 | 18.1 | -13.9 | -32.6 | -30.3 |
| 9784 | ok | 0.16 | 0.2 | 5.39e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -3.89e-02 | 35.1 | 6.1 | -3.7 | -23.3 | -31.0 |
| 9785 | ok | 0.16 | 0.1 | 3.89e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 13.9 | 17.0 | -10.6 | -20.3 | -40.3 |
| 9786 | ok | 0.16 | 0.2 | 1.24e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 2.0 | 53.2 | 8.5 | -7.9 | -12.2 | -37.5 |
| 9787 | ok | 0.16 | 0.2 | 3.61e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 14.9 | 14.1 | -14.7 | -17.9 | -43.8 |
| 9788 | ok | 0.16 | 0.4 | 5.52e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 11.8 | 86.1 | 16.8 | -11.6 | -13.6 | -51.3 |
| 9789 | ok | 0.16 | 0.2 | 5.49e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 0.8 | 19.0 | 12.7 | -34.3 | -10.0 | -52.5 |
| 9790 | ok | 0.16 | 0.8 | 2.24e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -4.2 | 88.2 | 13.1 | -33.0 | -24.7 | -58.9 |
| 9791 | ok | 0.16 | 0.2 | 2.32e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -27.7 | -10.8 | -25.1 | 52.3 | 7.3 | 52.9 |
| 9792 | ok | 0.17 | 1.0 | 5.17e-02 | 4.9 | 4.5 | 3.5 | 3.3 | -47.7 | 241.1 | 96.8 | 29.5 | 91.9 | -276.5 |
| 9793 | ok | 0.16 | 0.3 | 3.95e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -74.5 | 22.6 | -21.2 | 124.1 | 31.3 | 80.4 |
| 9794 | ok | 0.16 | 0.3 | 7.07e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -148.3 | -80.8 | -68.0 | -128.9 | -2.2 | -43.4 |
| 9795 | ok | 0.16 | 0.2 | 5.11e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.8 | 45.6 | -21.5 | 35.7 | 35.6 | 75.8 |
| 9796 | ok | 0.16 | 0.2 | 5.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.7 | 45.0 | -21.3 | 51.9 | 23.3 | 69.5 |
| 9797 | ok | 0.16 | 0.2 | 4.71e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -30.6 | 36.9 | -24.9 | 56.1 | 13.9 | 63.1 |
| 9798 | ok | 0.16 | 0.2 | 4.19e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -32.9 | 23.5 | -33.0 | 53.0 | 8.2 | 54.8 |
| 9799 | ok | 0.16 | 0.1 | 3.67e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -47.0 | -34.0 | 67.4 | 39.0 | 9.4 | -56.9 |
| 9800 | ok | 0.16 | 0.1 | 3.29e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -48.1 | -21.0 | 61.3 | 34.3 | 10.3 | -51.4 |
| 9801 | ok | 0.16 | 0.1 | 3.43e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -52.3 | -9.8 | 59.5 | 30.2 | 10.4 | -45.8 |
| 9802 | ok | 0.16 | 0.2 | 4.01e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -58.2 | -1.9 | 63.1 | 26.4 | 10.1 | -40.8 |
| 9803 | ok | 0.16 | 0.2 | 4.36e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -61.4 | 2.5 | 69.8 | 23.0 | 9.1 | -35.7 |
| 9804 | ok | 0.16 | 0.1 | 2.31e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -43.4 | -22.1 | 41.0 | -19.3 | -99.9 | 12.3 |
| 9805 | ok | 0.16 | 8.25e-02 | 2.44e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -45.1 | -15.0 | 41.1 | -13.1 | -68.6 | 14.9 |
| 9806 | ok | 0.16 | 0.1 | 3.75e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -49.3 | -47.2 | 62.1 | 9.6 | -46.2 | 5.1 |
| 9807 | ok | 0.16 | 9.94e-02 | 1.78e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -28.4 | -23.5 | 38.6 | -16.9 | -63.9 | -4.0 |
| 9808 | ok | 0.16 | 9.57e-02 | 1.38e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -12.5 | -20.8 | 28.5 | -11.1 | -37.9 | -21.2 |
| 9809 | ok | 0.16 | 9.56e-02 | 1.04e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -7.7 | -14.4 | 21.3 | -11.1 | -22.0 | -29.3 |
| 9810 | ok | 0.16 | 9.30e-02 | 7.58e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -8.2 | -7.8 | 20.8 | -12.8 | -15.4 | -32.4 |
| 9811 | ok | 0.16 | 8.13e-02 | 5.51e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.2 | -5.5 | 15.1 | -18.5 | -6.6 | -36.7 |
| 9812 | ok | 0.16 | 8.41e-02 | 8.45e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -14.0 | 2.7 | -18.7 | 36.7 | 4.3 | 40.8 |
| 9813 | ok | 0.16 | 8.53e-02 | 1.56e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -31.7 | 6.1 | -26.3 | 54.0 | 4.0 | 45.1 |
| 9814 | ok | 0.16 | 0.1 | 3.50e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -106.6 | 9.5 | -61.6 | -112.9 | -3.5 | -41.1 |
| 9815 | ok | 0.16 | 0.3 | 3.59e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -111.8 | -8.7 | -19.7 | -126.3 | -7.0 | -37.7 |
| 9816 | ok | 0.16 | 8.13e-02 | 2.13e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -32.8 | -17.2 | 40.5 | -11.2 | -42.2 | -3.0 |
| 9817 | ok | 0.16 | 7.52e-02 | 1.77e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -23.0 | -17.5 | 35.1 | -4.3 | -23.9 | -18.6 |
| 9818 | ok | 0.16 | 6.78e-02 | 1.43e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -16.2 | -16.0 | 28.1 | -4.8 | -13.6 | -25.9 |
| 9819 | ok | 0.16 | 6.58e-02 | 1.13e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -12.7 | -14.2 | 21.3 | -7.8 | -5.4 | -30.5 |
| 9820 | ok | 0.16 | 6.12e-02 | 8.97e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.5 | -13.8 | 14.4 | -13.9 | -2.8 | -33.3 |
| 9821 | ok | 0.16 | 6.03e-02 | 1.16e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -28.6 | -11.0 | -1.4 | 14.6 | 2.7 | -6.8 |
| 9822 | ok | 0.16 | 5.92e-02 | 1.75e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -44.0 | -7.8 | -9.8 | 15.1 | 2.6 | -6.3 |
| 9823 | ok | 0.16 | 4.21e-02 | 2.43e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -72.9 | -3.3 | -19.9 | -72.8 | -4.8 | -22.9 |
| 9824 | ok | 0.16 | 5.17e-02 | 2.80e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -83.4 | -4.5 | -10.4 | -64.6 | -4.1 | -17.7 |
| 9825 | ok | 0.16 | 0.1 | 3.55e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -30.4 | 21.6 | 3.7 | 16.0 | -1.3 | 39.4 |
| 9826 | ok | 0.16 | 0.1 | 3.18e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -26.3 | 17.9 | -0.3 | 23.7 | 1.1 | 31.3 |
| 9827 | ok | 0.16 | 0.1 | 2.75e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -33.8 | -30.7 | 48.7 | 22.4 | -0.7 | -30.0 |
| 9828 | ok | 0.16 | 0.1 | 2.35e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -33.0 | -22.3 | 41.4 | 22.9 | 3.5 | -29.4 |
| 9829 | ok | 0.16 | 0.1 | 2.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -35.4 | -15.0 | 34.9 | 22.4 | 5.5 | -27.2 |
| 9830 | ok | 0.16 | 0.1 | 2.14e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -40.1 | -4.4 | 25.6 | 18.5 | 4.7 | -19.7 |
| 9831 | ok | 0.16 | 9.87e-02 | 2.66e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -52.5 | -2.0 | 28.1 | 20.7 | 5.4 | -21.0 |
| 9832 | ok | 0.16 | 8.63e-02 | 3.01e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -53.2 | -4.8 | -4.0 | -33.9 | -4.0 | -22.6 |
| 9833 | ok | 0.16 | 5.18e-02 | 2.74e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -69.7 | -10.8 | -29.4 | 21.1 | -2.2 | 9.4 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | | | | | | | | -207.58 | -174.13 | -83.23 | -576.60 | -168.18 | -276.54 |
| | | 0.17 | 0.99 | 0.09 | 4.87 | 4.55 | 3.49 | 3.30 | 11.78 | 241.14 | 96.82 | 124.07 | 91.88 | 82.96 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 31 | ok | 0.37 | | | | | | |
| 6847 | ok | 3.25 | | | | | | |
| 7333 | ok | 0.26 | | | | | | |
| 7634 | ok | 0.23 | | | | | | |
| 7907 | ok | 0.25 | | | | | | |
| 7908 | ok | 0.20 | | | | | | |
| 7909 | ok | 0.19 | | | | | | |
| 7910 | ok | 0.21 | | | | | | |
| 9776 | ok | 0.40 | | | | | | |
| 9777 | ok | 0.25 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------------|-------|----------------|-----------------|------------------|----------------|-----------------|-------------|--------------|
| 9778 | ok | 0.44 | | | | | | |
| 9779 | ok | 0.12 | | | | | | |
| 9780 | ok | 0.49 | | | | | | |
| 9781 | ok | 0.06 | | | | | | |
| 9782 | ok | 0.55 | | | | | | |
| 9783 | ok | 0.07 | | | | | | |
| 9784 | ok | 0.64 | | | | | | |
| 9785 | ok | 0.09 | | | | | | |
| 9786 | ok | 0.79 | | | | | | |
| 9787 | ok | 0.12 | | | | | | |
| 9788 | ok | 0.96 | | | | | | |
| 9789 | ok | 0.15 | | | | | | |
| 9790 | ok | 1.87 | | | | | | |
| 9791 | ok | 0.76 | | | | | | |
| 9792 | ok | 3.25 | | | | | | |
| 9793 | ok | 1.75 | | | | | | |
| 9794 | ok | 1.75 | | | | | | |
| 9795 | ok | 0.26 | | | | | | |
| 9796 | ok | 0.25 | | | | | | |
| 9797 | ok | 0.23 | | | | | | |
| 9798 | ok | 0.23 | | | | | | |
| 9799 | ok | 0.22 | | | | | | |
| 9800 | ok | 0.21 | | | | | | |
| 9801 | ok | 0.20 | | | | | | |
| 9802 | ok | 0.17 | | | | | | |
| 9803 | ok | 0.23 | | | | | | |
| 9804 | ok | 0.20 | | | | | | |
| 9805 | ok | 0.19 | | | | | | |
| 9806 | ok | 0.21 | | | | | | |
| 9807 | ok | 0.12 | | | | | | |
| 9808 | ok | 0.08 | | | | | | |
| 9809 | ok | 0.05 | | | | | | |
| 9810 | ok | 0.06 | | | | | | |
| 9811 | ok | 0.08 | | | | | | |
| 9812 | ok | 0.16 | | | | | | |
| 9813 | ok | 0.22 | | | | | | |
| 9814 | ok | 0.33 | | | | | | |
| 9815 | ok | 0.33 | | | | | | |
| 9816 | ok | 0.13 | | | | | | |
| 9817 | ok | 0.10 | | | | | | |
| 9818 | ok | 0.07 | | | | | | |
| 9819 | ok | 0.06 | | | | | | |
| 9820 | ok | 0.08 | | | | | | |
| 9821 | ok | 0.09 | | | | | | |
| 9822 | ok | 0.12 | | | | | | |
| 9823 | ok | 0.22 | | | | | | |
| 9824 | ok | 0.22 | | | | | | |
| 9825 | ok | 0.16 | | | | | | |
| 9826 | ok | 0.11 | | | | | | |
| 9827 | ok | 0.10 | | | | | | |
| 9828 | ok | 0.10 | | | | | | |
| 9829 | ok | 0.11 | | | | | | |
| 9830 | ok | 0.11 | | | | | | |
| 9831 | ok | 0.11 | | | | | | |
| 9832 | ok | 0.23 | | | | | | |
| 9833 | ok | 0.23 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 3.25 | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 76 | 25.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|-------|------|-------|
| 57 | ok | 0.16 | 5.85e-02 | 3.85e-03 | 4.5 | 4.5 | 3.1 | 3.1 | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 82 | ok | 0.16 | 6.27e-02 | 7.11e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.7 | 6.1 | -8.1 | 16.8 | 3.2 | 26.6 |
| 822 | ok | 0.16 | 5.80e-02 | 2.15e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -10.1 | -0.9 | -15.1 | -15.7 | -2.9 | -22.6 |
| 823 | ok | 0.16 | 0.1 | 5.71e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -28.8 | -35.4 | -30.4 | 7.0 | 1.5 | 1.3 |
| | | | | | | | | | -135.9 | -11.2 | -73.7 | 8.6 | 1.0 | 0.3 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|-------------|-------|------------|--------------|-----------------|---------------|---------------|----------------|----------------|------------|------------|-------------|------------|------------|-------------|
| 835 | ok | 0.16 | 0.2 | 6.09e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -159.1 | 43.1 | 25.0 | 9.6 | 1.2 | 0.9 |
| 1780 | ok | 0.16 | 7.70e-02 | 1.52e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -23.0 | 4.9 | 22.6 | -2.6 | -13.6 | 6.8 |
| 1803 | ok | 0.16 | 6.66e-02 | 1.29e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -20.0 | -4.2 | 25.0 | 0.6 | -7.0 | 1.1 |
| 1805 | ok | 0.16 | 5.16e-02 | 1.06e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -17.4 | -4.2 | 19.5 | 3.0 | -2.7 | -1.0 |
| 1875 | ok | 0.16 | 3.29e-02 | 8.47e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -16.8 | -5.4 | 12.8 | 4.7 | -0.2 | -2.0 |
| 1975 | ok | 0.16 | 3.57e-02 | 9.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -19.0 | -7.3 | 1.4 | 5.9 | 1.3 | -1.0 |
| 1976 | ok | 0.16 | 3.72e-02 | 1.56e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -26.4 | -13.2 | -25.5 | 4.9 | 1.2 | 1.9 |
| 1984 | ok | 0.16 | 4.32e-02 | 2.47e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -53.3 | -16.5 | -33.8 | 8.0 | 1.3 | 5.75e-02 |
| 1985 | ok | 0.16 | 4.61e-02 | 3.59e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -94.3 | -9.3 | -35.4 | 9.0 | 0.7 | -1.43e-02 |
| 2608 | ok | 0.16 | 5.27e-02 | 4.32e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -129.5 | -10.1 | -4.4 | 9.6 | 0.5 | -5.51e-02 |
| 2756 | ok | 0.16 | 6.77e-02 | 2.54e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.3 | -23.7 | 45.8 | 4.3 | -7.0 | -7.1 |
| 2757 | ok | 0.16 | 7.42e-02 | 2.35e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -31.4 | -19.3 | 43.7 | 6.9 | -1.6 | -10.5 |
| 2758 | ok | 0.16 | 7.35e-02 | 2.07e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.5 | -13.8 | 38.8 | 8.6 | 1.3 | -11.6 |
| 2759 | ok | 0.16 | 6.74e-02 | 1.82e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -24.8 | -3.0 | -20.5 | 10.0 | 1.43e-02 | 8.2 |
| 2760 | ok | 0.16 | 6.40e-02 | 2.25e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -28.0 | -23.8 | -40.4 | 3.9 | 1.4 | 3.0 |
| 2761 | ok | 0.16 | 7.16e-02 | 2.96e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.9 | -30.8 | -52.8 | 4.6 | 1.3 | 3.4 |
| 2762 | ok | 0.16 | 8.00e-02 | 3.68e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -54.8 | -30.3 | -63.8 | 5.3 | 1.1 | 3.6 |
| 2763 | ok | 0.16 | 7.27e-02 | 4.21e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -82.0 | -21.2 | -66.7 | 10.2 | 0.5 | 5.3 |
| 2764 | ok | 0.16 | 4.91e-02 | 3.79e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -99.4 | -18.7 | -36.2 | 10.0 | -0.8 | 4.6 |
| 4709 | ok | 0.16 | 0.3 | 5.25e-04 | 4.5 | 4.5 | 3.1 | 3.1 | 0.1 | 75.8 | 2.2 | -0.2 | 3.1 | 1.2 |
| 5792 | ok | 0.16 | 0.8 | 6.04e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 79.5 | 181.5 | 49.6 | 12.9 | 4.3 | 26.7 |
| 5801 | ok | 0.16 | 0.2 | 1.96e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -51.3 | 20.5 | -39.9 | -14.0 | -4.7 | -33.5 |
| 5804 | ok | 0.20 | 0.9 | 5.94e-02 | 6.8 | 6.6 | 5.4 | 5.2 | 188.9 | 236.6 | 237.2 | -48.8 | -10.6 | -13.3 |
| 6577 | ok | 0.16 | 0.1 | 2.25e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.9 | 39.4 | 4.9 | 1.1 | 3.5 | 2.6 |
| 6578 | ok | 0.16 | 0.2 | 6.39e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 20.0 | -147.4 | -88.8 | 18.7 | 11.3 | 16.3 |
| 6848 | ok | 0.19 | 0.9 | 0.2 | 5.5 | 5.5 | 4.6 | 4.5 | -484.8 | 317.9 | -166.8 | 96.2 | -8.1 | 34.8 |
| 7098 | ok | 0.16 | 0.2 | 1.62e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 4.0 | 30.2 | 15.0 | 12.2 | 10.9 | 23.9 |
| 7101 | ok | 0.16 | 0.4 | 1.03e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 11.0 | 93.3 | 14.4 | 5.8 | 11.5 | 26.4 |
| 7105 | ok | 0.16 | 0.2 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -397.1 | -321.6 | 12.1 | 14.3 | 9.1 | -1.3 |
| 7108 | ok | 0.16 | 0.2 | 2.99e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 3.1 | 26.6 | 12.6 | 20.0 | 13.0 | 26.5 |
| 7264 | ok | 0.16 | 9.82e-02 | 1.61e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -25.4 | 3.3 | 28.8 | -6.7 | -22.1 | 10.3 |
| 7511 | ok | 0.16 | 0.1 | 3.10e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.5 | 38.3 | 4.5 | 0.8 | 4.4 | 2.0 |
| 7524 | ok | 0.16 | 0.2 | 3.72e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 67.8 | 1.4 | -9.44e-02 | 3.8 | 0.9 |
| 7531 | ok | 0.16 | 0.1 | 4.81e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.1 | 18.4 | 10.9 | -1.4 | -9.3 | 3.3 |
| 7635 | ok | 0.16 | 0.2 | 3.91e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -61.7 | 2.2 | 80.1 | 11.8 | 5.7 | -14.7 |
| 7650 | ok | 0.16 | 0.1 | 1.39e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -20.3 | 20.4 | -25.9 | 15.2 | 6.7 | 21.0 |
| 8326 | ok | 0.16 | 0.2 | 4.79e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -39.1 | -116.7 | 47.7 | -2.7 | -50.0 | 1.4 |
| 8328 | ok | 0.16 | 8.17e-02 | 1.66e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.7 | -1.5 | 30.7 | -6.3 | -24.8 | 9.8 |
| 8329 | ok | 0.16 | 0.1 | 2.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.8 | -11.8 | 35.8 | -13.1 | -61.4 | 5.7 |
| 8330 | ok | 0.16 | 9.70e-02 | 1.80e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -38.1 | 8.6 | 29.6 | -9.6 | -35.2 | 3.8 |
| 8331 | ok | 0.16 | 9.62e-02 | 1.73e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.1 | 7.9 | 25.3 | -7.6 | -28.4 | 3.6 |
| 8332 | ok | 0.16 | 8.10e-02 | 2.40e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -42.4 | -10.5 | 41.9 | -6.7 | -30.4 | -5.0 |
| 8333 | ok | 0.16 | 7.23e-02 | 2.58e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -38.7 | -24.0 | 44.4 | 7.29e-02 | -11.6 | -2.6 |
| 8335 | ok | 0.16 | 9.30e-02 | 1.28e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -15.4 | -0.5 | 26.8 | -5.3 | -20.3 | 7.2 |
| 8336 | ok | 0.16 | 8.88e-02 | 9.49e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -11.6 | 3.3 | 19.9 | -2.5 | -11.4 | 3.3 |
| 8337 | ok | 0.16 | 8.62e-02 | 7.04e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.1 | 5.1 | 17.5 | -0.3 | -5.6 | 0.9 |
| 8338 | ok | 0.16 | 7.73e-02 | 5.26e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.1 | 15.4 | 2.7 | 2.3 | 2.9 | 2.1 |
| 8360 | ok | 0.16 | 0.2 | 3.71e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 63.0 | 1.0 | -5.82e-02 | 7.3 | 0.6 |
| 8482 | ok | 0.16 | 0.1 | 3.50e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -17.1 | 34.4 | -19.2 | 12.6 | 4.6 | 20.0 |
| 8487 | ok | 0.16 | 0.1 | 3.70e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -19.9 | 34.2 | -21.1 | 18.0 | 3.7 | 23.9 |
| 8548 | ok | 0.16 | 0.1 | 3.52e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -44.7 | -35.9 | 63.2 | 19.9 | 2.9 | -23.7 |
| 8553 | ok | 0.16 | 0.1 | 3.19e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -43.5 | -26.2 | 58.8 | 18.3 | 4.9 | -24.3 |
| 8558 | ok | 0.16 | 9.98e-02 | 3.00e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -44.0 | -14.8 | 53.2 | 16.9 | 5.6 | -23.3 |
| 8563 | ok | 0.16 | 0.1 | 3.78e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -48.4 | -3.2 | 49.8 | 15.6 | 5.7 | -21.8 |
| 8568 | ok | 0.16 | 0.1 | 4.60e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -41.4 | -48.7 | -89.6 | 4.2 | 1.4 | 6.0 |
| 8617 | ok | 0.16 | 0.2 | 5.44e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -58.1 | -40.7 | -110.8 | 12.6 | 0.9 | 13.3 |
| 8622 | ok | 0.16 | 0.2 | 5.90e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -77.5 | -35.7 | -116.0 | 11.1 | 1.0 | 11.9 |
| 9836 | ok | 0.16 | 0.4 | 1.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 17.4 | -13.0 | -9.1 | 1.9 | -50.3 | 4.5 |
| 9837 | ok | 0.16 | 0.1 | 2.23e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -20.2 | -9.1 | 30.5 | -6.2 | -40.9 | 14.8 |
| 9838 | ok | 0.16 | 0.3 | 3.05e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.2 | 65.2 | -1.9 | -7.35e-02 | 15.7 | -0.1 |
| 9839 | ok | 0.16 | 0.1 | 8.67e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.4 | -0.9 | 18.3 | -3.9 | -25.7 | 7.2 |
| 9840 | ok | 0.16 | 0.2 | 6.66e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 62.9 | -1.2 | -5.36e-02 | 10.6 | 0.3 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | 0.20 | 0.94 | 0.17 | 6.81 | 6.56 | 5.43 | 5.17 | 188.88 | 317.85 | 237.17 | 96.25 | 15.72 | 34.78 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 57 | ok | 0.06 | | | | | | |
| 82 | ok | 0.12 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------------|-------|----------------|-----------------|------------------|----------------|-----------------|-------------|--------------|
| 822 | ok | 0.16 | | | | | | |
| 823 | ok | 0.19 | | | | | | |
| 835 | ok | 0.19 | | | | | | |
| 1780 | ok | 0.07 | | | | | | |
| 1803 | ok | 0.05 | | | | | | |
| 1805 | ok | 0.03 | | | | | | |
| 1875 | ok | 0.04 | | | | | | |
| 1975 | ok | 0.05 | | | | | | |
| 1976 | ok | 0.06 | | | | | | |
| 1984 | ok | 0.08 | | | | | | |
| 1985 | ok | 0.08 | | | | | | |
| 2608 | ok | 0.05 | | | | | | |
| 2756 | ok | 0.09 | | | | | | |
| 2757 | ok | 0.07 | | | | | | |
| 2758 | ok | 0.06 | | | | | | |
| 2759 | ok | 0.06 | | | | | | |
| 2760 | ok | 0.07 | | | | | | |
| 2761 | ok | 0.07 | | | | | | |
| 2762 | ok | 0.06 | | | | | | |
| 2763 | ok | 0.06 | | | | | | |
| 2764 | ok | 0.06 | | | | | | |
| 4709 | ok | 0.54 | | | | | | |
| 5792 | ok | 1.39 | | | | | | |
| 5801 | ok | 0.57 | | | | | | |
| 5804 | ok | 2.43 | | | | | | |
| 6577 | ok | 0.06 | | | | | | |
| 6578 | ok | 1.31 | | | | | | |
| 6848 | ok | 2.43 | | | | | | |
| 7098 | ok | 0.08 | | | | | | |
| 7101 | ok | 0.68 | | | | | | |
| 7105 | ok | 1.31 | | | | | | |
| 7108 | ok | 0.11 | | | | | | |
| 7264 | ok | 0.10 | | | | | | |
| 7511 | ok | 0.04 | | | | | | |
| 7524 | ok | 0.44 | | | | | | |
| 7531 | ok | 0.03 | | | | | | |
| 7635 | ok | 0.06 | | | | | | |
| 7650 | ok | 0.14 | | | | | | |
| 8326 | ok | 0.20 | | | | | | |
| 8328 | ok | 0.08 | | | | | | |
| 8329 | ok | 0.14 | | | | | | |
| 8330 | ok | 0.10 | | | | | | |
| 8331 | ok | 0.08 | | | | | | |
| 8332 | ok | 0.11 | | | | | | |
| 8333 | ok | 0.11 | | | | | | |
| 8335 | ok | 0.07 | | | | | | |
| 8336 | ok | 0.04 | | | | | | |
| 8337 | ok | 0.02 | | | | | | |
| 8338 | ok | 0.04 | | | | | | |
| 8360 | ok | 0.36 | | | | | | |
| 8482 | ok | 0.15 | | | | | | |
| 8487 | ok | 0.15 | | | | | | |
| 8548 | ok | 0.14 | | | | | | |
| 8553 | ok | 0.13 | | | | | | |
| 8558 | ok | 0.13 | | | | | | |
| 8563 | ok | 0.12 | | | | | | |
| 8568 | ok | 0.10 | | | | | | |
| 8617 | ok | 0.08 | | | | | | |
| 8622 | ok | 0.06 | | | | | | |
| 9836 | ok | 0.23 | | | | | | |
| 9837 | ok | 0.14 | | | | | | |
| 9838 | ok | 0.27 | | | | | | |
| 9839 | ok | 0.05 | | | | | | |
| 9840 | ok | 0.31 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 2.43 | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 77 | 25.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|-----------|-----------|-------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 2765 | ok | 0.16 | 0.2 | 6.53e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -84.9 | -39.1 | -128.9 | 6.6 | 1.7 | 8.7 |
| 2767 | ok | 0.16 | 0.5 | 1.89e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -1.5 | 79.7 | -0.7 | -1.17e-02 | -0.1 | 0.5 |
| 2768 | ok | 0.16 | 0.2 | 2.33e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -20.7 | -29.1 | 43.5 | 0.5 | -5.2 | 3.1 |
| 2769 | ok | 0.16 | 0.3 | 7.48e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 2.6 | 78.2 | -11.5 | -0.9 | -1.7 | -10.8 |
| 2770 | ok | 0.16 | 0.2 | 9.52e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.6 | 44.0 | -2.1 | 0.4 | 8.12e-02 | 2.4 |
| 2771 | ok | 0.16 | 0.3 | 1.70e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 71.0 | -1.2 | -3.98e-02 | 0.5 | 0.7 |
| 2772 | ok | 0.16 | 0.2 | 5.87e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 1.6 | 39.0 | -9.0 | -4.8 | -3.5 | -15.2 |
| 2773 | ok | 0.16 | 0.2 | 5.75e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 70.6 | 1.0 | -5.50e-02 | 0.9 | 0.8 |
| 2869 | ok | 0.16 | 0.2 | 3.80e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.4 | 43.3 | 4.5 | 0.7 | 0.8 | 3.1 |
| 2876 | ok | 0.16 | 0.2 | 3.83e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 75.0 | 1.5 | -9.80e-02 | 1.3 | 1.2 |
| 2877 | ok | 0.16 | 0.2 | 2.68e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.7 | 44.2 | 5.1 | 1.0 | 1.0 | 3.6 |
| 2907 | ok | 0.16 | 0.3 | 5.53e-04 | 4.5 | 4.5 | 3.1 | 3.1 | 0.2 | 83.8 | 2.3 | -0.2 | 1.4 | 1.5 |
| 3071 | ok | 0.16 | 0.2 | 1.86e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 4.3 | 32.2 | 17.2 | 12.4 | 10.4 | 25.3 |
| 3601 | ok | 0.16 | 0.4 | 1.11e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 12.1 | 101.4 | 15.7 | 5.9 | 11.6 | 27.7 |
| 3650 | ok | 0.16 | 0.2 | 3.41e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 3.3 | 28.2 | 14.7 | 20.1 | 8.6 | 28.1 |
| 3655 | ok | 0.16 | 0.9 | 6.69e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 87.6 | 197.1 | 53.9 | 12.2 | 3.2 | 27.8 |
| 3676 | ok | 0.16 | 0.2 | 2.19e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -56.4 | 21.7 | -43.6 | -13.3 | -5.2 | -32.3 |
| 3690 | ok | 0.21 | 0.9 | 6.61e-02 | 7.5 | 7.1 | 6.1 | 5.7 | 206.1 | 258.8 | 262.4 | -71.5 | -16.2 | -19.2 |
| 4263 | ok | 0.16 | 0.3 | 5.05e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -39.2 | -125.9 | 47.6 | -0.2 | -6.1 | -0.2 |
| 4455 | ok | 0.16 | 0.3 | 7.07e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 20.8 | -162.6 | -98.8 | 26.3 | 15.9 | 25.4 |
| 4456 | ok | 0.16 | 0.2 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -437.4 | -353.1 | 14.7 | 19.8 | 13.3 | -1.6 |
| 4457 | ok | 0.16 | 9.97e-02 | 1.64e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -23.4 | 6.4 | 30.9 | 0.4 | -3.4 | 3.1 |
| 4458 | ok | 0.16 | 9.19e-02 | 1.67e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -26.6 | 6.5 | 28.0 | 0.3 | -2.8 | 3.1 |
| 4459 | ok | 0.16 | 8.18e-02 | 2.58e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.2 | -23.1 | 45.5 | 0.5 | -3.7 | 0.4 |
| 4460 | ok | 0.16 | 9.46e-02 | 1.34e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -17.3 | -0.2 | 29.7 | 0.3 | -2.6 | 2.5 |
| 4461 | ok | 0.16 | 9.26e-02 | 1.02e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -12.2 | 2.5 | 24.4 | 0.7 | -1.1 | 2.2 |
| 4708 | ok | 0.16 | 9.08e-02 | 7.75e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -9.3 | 5.1 | 19.6 | 1.2 | -0.2 | 2.0 |
| 4710 | ok | 0.16 | 8.46e-02 | 5.89e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.0 | 10.0 | 12.1 | 2.2 | 0.6 | 2.9 |
| 4711 | ok | 0.16 | 6.26e-02 | 4.40e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.7 | 8.9 | -9.6 | -12.7 | -5.4 | -20.3 |
| 4712 | ok | 0.16 | 6.94e-02 | 7.74e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.7 | -0.4 | -17.2 | -15.5 | -3.1 | -21.4 |
| 4713 | ok | 0.16 | 6.40e-02 | 2.39e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -32.3 | -39.1 | -33.4 | 7.5 | 1.1 | 4.0 |
| 4714 | ok | 0.16 | 0.1 | 6.31e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -150.6 | -11.9 | -81.2 | 9.4 | 1.0 | 2.3 |
| 4716 | ok | 0.16 | 0.3 | 6.73e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -176.2 | 47.5 | 28.0 | 10.7 | 1.8 | 1.7 |
| 4717 | ok | 0.16 | 8.21e-02 | 1.56e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -24.2 | -3.3 | 30.8 | 0.7 | -1.9 | 2.1 |
| 4718 | ok | 0.16 | 7.14e-02 | 1.36e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -20.3 | -4.1 | 26.8 | 1.4 | -0.7 | 1.6 |
| 4728 | ok | 0.16 | 5.48e-02 | 1.13e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -17.9 | -4.6 | 21.3 | 2.1 | 8.55e-02 | 1.4 |
| 4729 | ok | 0.16 | 4.54e-02 | 9.24e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -17.5 | -6.3 | 14.4 | 2.8 | 0.5 | 1.3 |
| 4730 | ok | 0.16 | 4.69e-02 | 9.95e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -20.0 | -10.0 | -3.4 | 3.6 | 0.8 | 1.7 |
| 4731 | ok | 0.16 | 4.52e-02 | 1.71e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -28.2 | -14.4 | -28.4 | 5.2 | 0.7 | 2.6 |
| 4732 | ok | 0.16 | 5.53e-02 | 2.72e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -58.7 | -18.1 | -36.7 | 6.6 | 0.8 | 2.1 |
| 4733 | ok | 0.16 | 4.97e-02 | 3.96e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -104.4 | -10.1 | -38.6 | 7.8 | 0.6 | 1.8 |
| 4734 | ok | 0.16 | 5.67e-02 | 4.79e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -143.6 | -11.1 | -4.8 | 8.3 | 0.4 | 0.4 |
| 4735 | ok | 0.16 | 7.85e-02 | 2.58e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.3 | -23.7 | 46.7 | 1.7 | -1.9 | -0.9 |
| 4736 | ok | 0.16 | 7.71e-02 | 2.42e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -32.1 | -20.0 | 45.1 | 2.6 | -0.7 | -1.5 |
| 4737 | ok | 0.16 | 7.44e-02 | 2.17e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -30.8 | -14.9 | 40.7 | 3.3 | -8.43e-02 | -1.9 |
| 4738 | ok | 0.16 | 7.32e-02 | 1.95e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -27.7 | -11.2 | 12.0 | 3.9 | 0.7 | 0.4 |
| 4739 | ok | 0.16 | 7.85e-02 | 2.44e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.2 | -26.9 | -43.9 | 4.5 | 1.9 | 4.3 |
| 4740 | ok | 0.16 | 8.69e-02 | 3.22e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -40.3 | -34.4 | -57.5 | 5.3 | 1.7 | 4.5 |
| 4741 | ok | 0.16 | 9.60e-02 | 4.01e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -59.4 | -33.8 | -69.8 | 6.0 | 1.6 | 4.6 |
| 4742 | ok | 0.16 | 8.73e-02 | 4.62e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -90.3 | -23.0 | -73.2 | 6.9 | 1.2 | 4.6 |
| 4743 | ok | 0.16 | 5.25e-02 | 4.22e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -110.6 | -20.4 | -40.2 | 7.1 | 0.1 | 3.4 |
| 6849 | ok | 0.19 | 0.9 | 0.2 | 5.7 | 5.6 | 5.1 | 4.9 | -533.7 | 347.4 | -185.6 | 141.5 | -11.8 | 51.0 |
| 7636 | ok | 0.16 | 0.2 | 4.47e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -71.5 | 1.3 | 90.5 | 6.2 | 1.8 | -7.1 |
| 7651 | ok | 0.16 | 9.24e-02 | 1.52e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -24.1 | 24.8 | -23.5 | 4.4 | 1.8 | 6.1 |
| 8065 | ok | 0.16 | 8.22e-02 | 2.40e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -35.9 | -11.6 | 45.6 | -1.8 | -8.8 | -1.4 |
| 8066 | ok | 0.16 | 0.2 | 2.10e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -36.0 | 14.8 | 36.2 | -0.2 | -7.7 | 1.1 |
| 8067 | ok | 0.16 | 0.1 | 1.73e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -33.3 | 9.9 | 30.1 | 0.2 | -5.0 | 1.0 |
| 8068 | ok | 0.16 | 9.71e-02 | 1.70e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.4 | 4.0 | 29.9 | -0.5 | -5.9 | 0.8 |
| 8632 | ok | 0.16 | 0.1 | 3.52e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -36.7 | -43.9 | 63.2 | 2.1 | -3.3 | -1.7 |
| 8637 | ok | 0.16 | 0.2 | 3.70e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -44.8 | -42.2 | 65.6 | 4.0 | -2.3 | -3.0 |
| 8642 | ok | 0.16 | 0.1 | 3.57e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -45.7 | -37.3 | 63.7 | 4.8 | -0.9 | -4.7 |
| 8643 | ok | 0.16 | 0.1 | 3.30e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -45.5 | -28.0 | 60.2 | 5.0 | -0.2 | -5.3 |
| 8648 | ok | 0.16 | 0.1 | 3.24e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.5 | -32.2 | -62.0 | 4.2 | 3.1 | 6.7 |
| 8653 | ok | 0.16 | 0.1 | 4.10e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.2 | -46.7 | -78.6 | 4.7 | 2.8 | 7.2 |
| 9834 | ok | 0.16 | 0.1 | 4.99e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -43.7 | -54.6 | -97.5 | 5.2 | 2.6 | 7.8 |
| 9835 | ok | 0.16 | 0.2 | 5.96e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -62.8 | -44.2 | -121.9 | 6.4 | 2.1 | 8.7 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|-------|----------|--------|--------|---------|---------|---------|---------|---------|--------|--------|--------|
| | | | | | | | | | -533.70 | -353.11 | -185.56 | -71.50 | -16.22 | -32.26 |
| | | 0.21 | 0.93 | 0.19 | 7.48 | 7.08 | 6.10 | 5.70 | 206.07 | 347.40 | 262.43 | 141.50 | 15.86 | 51.03 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------------------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm ² | | | | | daN/cm | daN/cm |
| 2765 | ok | 0.06 | | | | | | |
| 2767 | ok | 0.22 | | | | | | |
| 2768 | ok | 0.11 | | | | | | |
| 2769 | ok | 0.26 | | | | | | |
| 2770 | ok | 0.04 | | | | | | |
| 2771 | ok | 0.31 | | | | | | |
| 2772 | ok | 0.02 | | | | | | |
| 2773 | ok | 0.36 | | | | | | |
| 2869 | ok | 0.04 | | | | | | |
| 2876 | ok | 0.43 | | | | | | |
| 2877 | ok | 0.05 | | | | | | |
| 2907 | ok | 0.54 | | | | | | |
| 3071 | ok | 0.08 | | | | | | |
| 3601 | ok | 0.68 | | | | | | |
| 3650 | ok | 0.11 | | | | | | |
| 3655 | ok | 1.39 | | | | | | |
| 3676 | ok | 0.57 | | | | | | |
| 3690 | ok | 2.43 | | | | | | |
| 4263 | ok | 0.19 | | | | | | |
| 4455 | ok | 1.31 | | | | | | |
| 4456 | ok | 1.31 | | | | | | |
| 4457 | ok | 0.08 | | | | | | |
| 4458 | ok | 0.07 | | | | | | |
| 4459 | ok | 0.10 | | | | | | |
| 4460 | ok | 0.06 | | | | | | |
| 4461 | ok | 0.03 | | | | | | |
| 4708 | ok | 0.02 | | | | | | |
| 4710 | ok | 0.04 | | | | | | |
| 4711 | ok | 0.06 | | | | | | |
| 4712 | ok | 0.12 | | | | | | |
| 4713 | ok | 0.16 | | | | | | |
| 4714 | ok | 0.20 | | | | | | |
| 4716 | ok | 0.20 | | | | | | |
| 4717 | ok | 0.06 | | | | | | |
| 4718 | ok | 0.04 | | | | | | |
| 4728 | ok | 0.02 | | | | | | |
| 4729 | ok | 0.04 | | | | | | |
| 4730 | ok | 0.05 | | | | | | |
| 4731 | ok | 0.06 | | | | | | |
| 4732 | ok | 0.08 | | | | | | |
| 4733 | ok | 0.08 | | | | | | |
| 4734 | ok | 0.05 | | | | | | |
| 4735 | ok | 0.08 | | | | | | |
| 4736 | ok | 0.06 | | | | | | |
| 4737 | ok | 0.06 | | | | | | |
| 4738 | ok | 0.06 | | | | | | |
| 4739 | ok | 0.07 | | | | | | |
| 4740 | ok | 0.07 | | | | | | |
| 4741 | ok | 0.06 | | | | | | |
| 4742 | ok | 0.05 | | | | | | |
| 4743 | ok | 0.05 | | | | | | |
| 6849 | ok | 2.43 | | | | | | |
| 7636 | ok | 0.06 | | | | | | |
| 7651 | ok | 0.13 | | | | | | |
| 8065 | ok | 0.10 | | | | | | |
| 8066 | ok | 0.11 | | | | | | |
| 8067 | ok | 0.08 | | | | | | |
| 8068 | ok | 0.07 | | | | | | |
| 8632 | ok | 0.13 | | | | | | |
| 8637 | ok | 0.13 | | | | | | |
| 8642 | ok | 0.13 | | | | | | |
| 8643 | ok | 0.13 | | | | | | |
| 8648 | ok | 0.12 | | | | | | |
| 8653 | ok | 0.12 | | | | | | |
| 9834 | ok | 0.10 | | | | | | |
| 9835 | ok | 0.08 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|------|-------|
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 2.43 | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 78 | 25.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|-----------|-------|-------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 4565 | ok | 0.16 | 0.4 | 4.91e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -38.5 | -122.0 | 46.7 | 1.3 | 24.7 | -1.0 |
| 4744 | ok | 0.16 | 0.1 | 3.57e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -36.6 | -45.0 | 64.1 | -2.2 | 1.4 | -1.2 |
| 4756 | ok | 0.16 | 0.1 | 3.74e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -45.1 | -42.9 | 66.2 | -3.7 | -0.7 | 3.1 |
| 5521 | ok | 0.16 | 0.5 | 2.00e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 1.2 | 69.4 | -9.5 | -3.7 | -38.1 | -3.0 |
| 5522 | ok | 0.16 | 0.2 | 2.28e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -19.4 | -9.4 | 31.4 | 3.7 | 19.2 | -4.6 |
| 5523 | ok | 0.16 | 0.4 | 7.96e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 2.7 | 79.8 | -12.0 | -5.9 | -40.8 | -5.2 |
| 5524 | ok | 0.16 | 0.2 | 9.26e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.4 | -1.2 | 20.0 | 2.4 | 12.8 | -1.0 |
| 5525 | ok | 0.16 | 0.3 | 1.85e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 69.7 | -1.2 | -3.57e-02 | -0.4 | 0.8 |
| 5526 | ok | 0.16 | 0.2 | 6.15e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 1.9 | 39.7 | -9.5 | -9.3 | -24.6 | -15.1 |
| 5527 | ok | 0.16 | 0.2 | 6.10e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.1 | 69.8 | 1.1 | -5.36e-02 | 0.3 | 0.8 |
| 5755 | ok | 0.16 | 0.2 | 4.01e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.4 | 43.0 | 4.8 | 0.8 | 1.4 | 3.1 |
| 6579 | ok | 0.16 | 0.2 | 4.01e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 74.9 | 1.5 | -9.85e-02 | 1.6 | 1.2 |
| 6592 | ok | 0.16 | 0.2 | 2.81e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.7 | 44.1 | 5.4 | 1.1 | 1.3 | 3.7 |
| 6668 | ok | 0.16 | 0.3 | 5.05e-04 | 4.5 | 4.5 | 3.1 | 3.1 | 0.2 | 84.1 | 2.3 | -0.2 | 1.6 | 1.5 |
| 6678 | ok | 0.16 | 0.2 | 1.80e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 4.0 | 32.0 | 17.1 | 15.7 | 10.2 | 33.4 |
| 6689 | ok | 0.16 | 0.4 | 1.08e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 11.6 | 99.1 | 15.0 | 7.5 | 15.0 | 36.2 |
| 6696 | ok | 0.16 | 0.2 | 3.36e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 3.0 | 27.9 | 14.6 | 25.4 | 11.7 | 37.0 |
| 6734 | ok | 0.16 | 0.8 | 6.65e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 86.0 | 190.5 | 51.8 | 15.8 | 1.7 | 36.3 |
| 6737 | ok | 0.16 | 0.2 | 2.14e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -54.6 | 20.3 | -41.0 | -17.5 | -7.0 | -42.0 |
| 6758 | ok | 0.21 | 0.9 | 6.57e-02 | 7.6 | 7.2 | 6.3 | 5.8 | 211.8 | 264.8 | 264.2 | -84.3 | -19.3 | -22.6 |
| 6773 | ok | 0.16 | 0.2 | 7.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 22.6 | -164.6 | -98.8 | 30.5 | 18.5 | 30.5 |
| 6816 | ok | 0.16 | 0.2 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -443.3 | -359.4 | 13.1 | 22.8 | 15.7 | -1.8 |
| 6846 | ok | 0.16 | 0.1 | 1.62e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -24.2 | 4.5 | 29.8 | 3.9 | 12.0 | -2.2 |
| 6850 | ok | 0.19 | 0.9 | 0.2 | 5.7 | 5.5 | 5.2 | 5.0 | -541.3 | 355.8 | -185.4 | 167.0 | -13.9 | 60.2 |
| 6867 | ok | 0.16 | 9.65e-02 | 1.67e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -28.2 | -0.5 | 32.3 | 3.5 | 11.4 | -2.9 |
| 6868 | ok | 0.16 | 8.51e-02 | 2.61e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.4 | -23.8 | 45.9 | 0.6 | 5.0 | -1.0 |
| 6869 | ok | 0.16 | 0.1 | 1.32e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -14.3 | 2.9 | 27.7 | 11.1 | 33.6 | 6.2 |
| 6870 | ok | 0.16 | 9.17e-02 | 1.01e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -12.1 | 3.0 | 24.1 | 2.6 | 6.5 | 1.0 |
| 6871 | ok | 0.16 | 8.93e-02 | 7.60e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.4 | 10.9 | 16.4 | 2.2 | 3.4 | 2.9 |
| 6872 | ok | 0.16 | 8.37e-02 | 5.76e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -5.0 | 10.3 | 12.1 | 2.4 | 2.1 | 3.8 |
| 6874 | ok | 0.16 | 6.40e-02 | 4.26e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.8 | 9.2 | -9.7 | -12.7 | -5.3 | -23.7 |
| 6875 | ok | 0.16 | 6.62e-02 | 7.58e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.2 | 0.6 | -16.9 | -20.3 | -2.9 | -27.9 |
| 6877 | ok | 0.16 | 6.16e-02 | 2.39e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -31.6 | -39.7 | -33.6 | 7.7 | 1.0 | 5.5 |
| 6879 | ok | 0.16 | 0.1 | 6.35e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -151.3 | -12.8 | -81.9 | 9.8 | 1.0 | 3.4 |
| 6880 | ok | 0.16 | 0.3 | 6.78e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -177.3 | 48.0 | 27.9 | 11.2 | 2.2 | 2.2 |
| 6882 | ok | 0.16 | 8.74e-02 | 1.55e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -24.1 | -3.2 | 30.7 | 2.6 | 7.1 | -0.5 |
| 6888 | ok | 0.16 | 7.48e-02 | 1.35e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -20.2 | -3.8 | 26.7 | 2.0 | 4.3 | 1.3 |
| 6908 | ok | 0.16 | 5.73e-02 | 1.12e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -17.8 | -4.2 | 21.1 | 1.6 | 2.4 | 2.4 |
| 6928 | ok | 0.16 | 4.71e-02 | 9.09e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -17.4 | -6.0 | 14.1 | 1.7 | 1.3 | 3.0 |
| 6948 | ok | 0.16 | 4.92e-02 | 9.82e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -19.8 | -10.0 | -3.7 | 2.2 | 0.9 | 3.1 |
| 6968 | ok | 0.16 | 4.63e-02 | 1.70e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -28.2 | -14.6 | -28.2 | 5.1 | 0.7 | 2.8 |
| 6988 | ok | 0.16 | 5.60e-02 | 2.73e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -58.6 | -18.3 | -37.1 | 5.6 | 0.5 | 3.2 |
| 7008 | ok | 0.16 | 4.99e-02 | 3.97e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -104.6 | -10.3 | -39.0 | 6.8 | 0.5 | 2.7 |
| 7028 | ok | 0.16 | 5.67e-02 | 4.81e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -144.2 | -11.1 | -4.8 | 7.4 | 0.3 | 0.7 |
| 7048 | ok | 0.16 | 7.85e-02 | 2.59e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.4 | -23.9 | 46.9 | 0.3 | 3.2 | 1.8 |
| 7068 | ok | 0.16 | 7.79e-02 | 2.42e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -32.1 | -19.8 | 45.2 | -2.29e-02 | 1.0 | 3.4 |
| 7083 | ok | 0.16 | 7.58e-02 | 2.16e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -30.7 | -14.5 | 40.5 | -1.98e-02 | -0.2 | 3.9 |
| 7086 | ok | 0.16 | 7.63e-02 | 1.93e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -27.6 | -10.9 | 11.7 | 0.2 | 0.4 | 2.8 |
| 7087 | ok | 0.16 | 7.82e-02 | 2.44e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.3 | -26.7 | -43.8 | 4.0 | 1.8 | 4.0 |
| 7088 | ok | 0.16 | 8.70e-02 | 3.22e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -40.4 | -34.4 | -57.5 | 4.9 | 1.7 | 4.3 |
| 7091 | ok | 0.16 | 9.62e-02 | 4.02e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -59.6 | -33.8 | -70.0 | 5.7 | 1.6 | 4.5 |
| 7092 | ok | 0.16 | 8.70e-02 | 4.64e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -90.4 | -23.2 | -73.5 | 4.6 | 1.4 | 3.8 |
| 7093 | ok | 0.16 | 5.21e-02 | 4.22e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -110.7 | -20.6 | -40.1 | 5.0 | 0.6 | 2.4 |
| 7100 | ok | 0.16 | 0.1 | 3.59e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -45.9 | -37.4 | 64.1 | -4.8 | -1.8 | 6.5 |
| 7104 | ok | 0.16 | 0.1 | 3.30e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -45.6 | -27.6 | 60.3 | -3.4 | -2.5 | 6.4 |
| 7234 | ok | 0.16 | 0.1 | 3.23e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.6 | -31.5 | -61.9 | 3.1 | 2.8 | 5.7 |
| 7235 | ok | 0.16 | 0.1 | 4.10e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.4 | -46.3 | -78.7 | 3.8 | 2.7 | 6.4 |
| 7637 | ok | 0.16 | 0.2 | 4.41e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -70.4 | 1.8 | 89.7 | 2.5 | -0.6 | -2.1 |
| 7652 | ok | 0.16 | 9.59e-02 | 1.52e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -25.0 | 24.9 | -23.8 | 0.4 | -1.8 | -3.3 |
| 8157 | ok | 0.16 | 8.53e-02 | 2.43e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -36.0 | -12.0 | 46.4 | 1.1 | 10.3 | -0.3 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|-------|----------|--------|--------|---------|---------|---------|---------|---------|--------|--------|--------|
| 8158 | ok | 0.16 | 0.2 | 2.08e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.6 | -13.5 | 35.9 | 7.1 | 29.1 | -2.0 |
| 8159 | ok | 0.16 | 0.1 | 1.73e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -33.2 | 9.7 | 30.3 | 5.1 | 17.7 | -1.3 |
| 8160 | ok | 0.16 | 0.1 | 1.72e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.4 | 3.7 | 30.3 | 3.1 | 12.4 | -1.1 |
| 8327 | ok | 0.16 | 0.1 | 5.00e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -43.9 | -54.4 | -97.9 | 4.4 | 2.5 | 7.1 |
| 8334 | ok | 0.16 | 0.2 | 5.98e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -63.0 | -44.6 | -122.1 | 2.1 | 2.5 | 5.2 |
| 8340 | ok | 0.16 | 0.2 | 6.54e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -85.1 | -39.3 | -128.9 | 3.4 | 2.0 | 6.1 |
| | | | | | | | | | | | | | | |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | 0.21 | 0.89 | 0.19 | 7.63 | 7.17 | 6.25 | 5.78 | -541.32 | -359.45 | -185.41 | -84.30 | -40.79 | -42.00 |
| | | | | | | | | | 211.84 | 355.82 | 264.19 | 166.98 | 33.62 | 60.17 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 4565 | ok | 0.19 | | | | | | |
| 4744 | ok | 0.13 | | | | | | |
| 4756 | ok | 0.13 | | | | | | |
| 5521 | ok | 0.23 | | | | | | |
| 5522 | ok | 0.12 | | | | | | |
| 5523 | ok | 0.27 | | | | | | |
| 5524 | ok | 0.04 | | | | | | |
| 5525 | ok | 0.31 | | | | | | |
| 5526 | ok | 0.02 | | | | | | |
| 5527 | ok | 0.36 | | | | | | |
| 5755 | ok | 0.04 | | | | | | |
| 6579 | ok | 0.44 | | | | | | |
| 6592 | ok | 0.06 | | | | | | |
| 6668 | ok | 0.55 | | | | | | |
| 6678 | ok | 0.08 | | | | | | |
| 6689 | ok | 0.68 | | | | | | |
| 6696 | ok | 0.11 | | | | | | |
| 6734 | ok | 1.39 | | | | | | |
| 6737 | ok | 0.57 | | | | | | |
| 6758 | ok | 2.44 | | | | | | |
| 6773 | ok | 1.32 | | | | | | |
| 6816 | ok | 1.32 | | | | | | |
| 6846 | ok | 0.08 | | | | | | |
| 6850 | ok | 2.44 | | | | | | |
| 6867 | ok | 0.07 | | | | | | |
| 6868 | ok | 0.09 | | | | | | |
| 6869 | ok | 0.06 | | | | | | |
| 6870 | ok | 0.03 | | | | | | |
| 6871 | ok | 0.02 | | | | | | |
| 6872 | ok | 0.04 | | | | | | |
| 6874 | ok | 0.06 | | | | | | |
| 6875 | ok | 0.12 | | | | | | |
| 6877 | ok | 0.16 | | | | | | |
| 6879 | ok | 0.20 | | | | | | |
| 6880 | ok | 0.20 | | | | | | |
| 6882 | ok | 0.06 | | | | | | |
| 6888 | ok | 0.04 | | | | | | |
| 6908 | ok | 0.02 | | | | | | |
| 6928 | ok | 0.04 | | | | | | |
| 6948 | ok | 0.05 | | | | | | |
| 6968 | ok | 0.06 | | | | | | |
| 6988 | ok | 0.08 | | | | | | |
| 7008 | ok | 0.08 | | | | | | |
| 7028 | ok | 0.05 | | | | | | |
| 7048 | ok | 0.08 | | | | | | |
| 7068 | ok | 0.06 | | | | | | |
| 7083 | ok | 0.06 | | | | | | |
| 7086 | ok | 0.06 | | | | | | |
| 7087 | ok | 0.07 | | | | | | |
| 7088 | ok | 0.07 | | | | | | |
| 7091 | ok | 0.06 | | | | | | |
| 7092 | ok | 0.05 | | | | | | |
| 7093 | ok | 0.05 | | | | | | |
| 7100 | ok | 0.13 | | | | | | |
| 7104 | ok | 0.13 | | | | | | |
| 7234 | ok | 0.12 | | | | | | |
| 7235 | ok | 0.12 | | | | | | |
| 7637 | ok | 0.06 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|---------|----------|-----------|-----------|----------|----------|-------|-------|
| 7652 | ok | 0.13 | | | | | | |
| 8157 | ok | 0.09 | | | | | | |
| 8158 | ok | 0.12 | | | | | | |
| 8159 | ok | 0.08 | | | | | | |
| 8160 | ok | 0.07 | | | | | | |
| 8327 | ok | 0.10 | | | | | | |
| 8334 | ok | 0.08 | | | | | | |
| 8340 | ok | 0.06 | | | | | | |
| Nodo | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec | |
| | 2.44 | | | | | | | |

| Macro Setto | Spessore | Id Materiale | Id Criterio | Progettazione |
|-------------|----------|--------------|-------------|----------------------------------|
| | cm | | | |
| 79 | 25.00 | 1 | 7 | Singolo elemento NON DISSIPATIVO |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|--------|--------|--------|-----------|-------|-------|
| | | | | | | | | | daN/cm | daN/cm | daN/cm | daN | daN | daN |
| 6851 | ok | 0.19 | 0.7 | 0.2 | 5.5 | 5.3 | 4.5 | 4.3 | -475.4 | 307.4 | -167.0 | 160.8 | -13.4 | 58.0 |
| 7107 | ok | 0.16 | 0.3 | 7.51e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 13.2 | 2.5 | -7.7 | -1.7 | 50.0 | -1.1 |
| 7109 | ok | 0.16 | 0.1 | 1.64e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -14.7 | -17.1 | 32.5 | -3.2 | 42.9 | -10.3 |
| 7116 | ok | 0.16 | 0.2 | 1.34e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 44.9 | 0.7 | 0.2 | -40.5 | 3.2 |
| 7119 | ok | 0.16 | 0.1 | 6.30e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.1 | 24.4 | 5.2 | -4.6 | -37.5 | 13.4 |
| 7122 | ok | 0.16 | 0.2 | 4.14e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 49.5 | 0.9 | 0.1 | -24.4 | 1.7 |
| 7125 | ok | 0.16 | 0.1 | 3.59e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.5 | 28.1 | 8.1 | -2.4 | -17.2 | 7.2 |
| 7127 | ok | 0.16 | 0.2 | 3.40e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 55.5 | 1.2 | -9.25e-03 | -10.0 | 1.1 |
| 7130 | ok | 0.16 | 0.1 | 2.39e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -1.0 | 33.3 | 7.3 | -0.9 | -9.2 | 4.4 |
| 7139 | ok | 0.16 | 0.2 | 3.56e-04 | 4.5 | 4.5 | 3.1 | 3.1 | -0.9 | 63.4 | 1.5 | -9.42e-02 | -4.5 | 0.8 |
| 7141 | ok | 0.16 | 0.1 | 1.81e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.1 | 35.4 | 7.3 | 0.1 | -4.0 | 2.7 |
| 7144 | ok | 0.16 | 0.2 | 4.29e-04 | 4.5 | 4.5 | 3.1 | 3.1 | 0.1 | 73.8 | 2.2 | -0.2 | -1.1 | 0.8 |
| 7146 | ok | 0.16 | 0.1 | 1.29e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -0.8 | 36.7 | 8.9 | 1.0 | -0.3 | 4.1 |
| 7147 | ok | 0.16 | 0.3 | 9.92e-04 | 4.5 | 4.5 | 3.1 | 3.1 | 9.2 | 91.0 | 5.2 | -0.6 | 0.7 | 1.4 |
| 7148 | ok | 0.16 | 0.1 | 2.93e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.3 | 31.4 | 10.0 | 2.9 | 2.4 | 6.6 |
| 7149 | ok | 0.16 | 0.5 | 5.98e-03 | 4.5 | 4.5 | 3.1 | 3.1 | 95.4 | 133.7 | 31.3 | -7.2 | 1.2 | 1.0 |
| 7150 | ok | 0.16 | 0.2 | 1.90e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -51.6 | -4.5 | -16.3 | 6.9 | 1.7 | 7.0 |
| 7153 | ok | 0.20 | 0.8 | 5.89e-02 | 6.8 | 6.4 | 5.4 | 5.0 | 181.6 | 229.0 | 235.1 | -81.2 | -18.3 | -21.8 |
| 7157 | ok | 0.16 | 0.2 | 6.33e-02 | 4.5 | 4.5 | 3.1 | 3.1 | 17.7 | -144.9 | -88.9 | 29.7 | 18.1 | 28.9 |
| 7164 | ok | 0.16 | 0.1 | 0.1 | 4.5 | 4.5 | 3.1 | 3.1 | -389.9 | -313.8 | 14.1 | 22.3 | 15.1 | -1.8 |
| 7165 | ok | 0.16 | 9.12e-02 | 1.45e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -22.5 | 1.6 | 27.2 | -3.7 | 9.3 | -5.0 |
| 7166 | ok | 0.16 | 6.89e-02 | 1.64e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.0 | -3.8 | 29.6 | -2.4 | 4.7 | -4.7 |
| 7167 | ok | 0.16 | 7.63e-02 | 2.61e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.6 | -27.9 | 43.9 | -1.4 | 4.1 | -13.6 |
| 7168 | ok | 0.16 | 8.62e-02 | 1.07e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -14.8 | 3.9 | 21.6 | -1.5 | 8.4 | -0.6 |
| 7169 | ok | 0.16 | 8.19e-02 | 7.83e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.4 | 6.2 | 18.7 | 0.2 | 6.5 | 0.7 |
| 7170 | ok | 0.16 | 7.85e-02 | 5.78e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -6.0 | 9.3 | 12.5 | 1.4 | 4.9 | 1.8 |
| 7171 | ok | 0.16 | 7.25e-02 | 4.31e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -4.9 | 9.1 | 8.4 | 2.3 | 3.5 | 2.6 |
| 7172 | ok | 0.16 | 5.38e-02 | 3.12e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -2.9 | 8.1 | -4.7 | -12.4 | -2.2 | -20.0 |
| 7173 | ok | 0.16 | 3.63e-02 | 6.59e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -10.0 | -8.8 | -6.2 | 5.1 | 1.4 | 4.0 |
| 7184 | ok | 0.16 | 3.45e-02 | 2.14e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.5 | -34.6 | -30.5 | 8.0 | 1.5 | 4.5 |
| 7185 | ok | 0.16 | 8.00e-02 | 5.66e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -135.0 | -10.0 | -73.0 | 10.1 | 1.2 | 2.7 |
| 7186 | ok | 0.16 | 0.2 | 6.03e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -157.6 | 42.5 | 25.2 | 11.6 | 2.1 | 2.0 |
| 7190 | ok | 0.16 | 6.73e-02 | 1.41e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -22.6 | -4.5 | 26.8 | -0.5 | 5.7 | -2.8 |
| 7191 | ok | 0.16 | 6.04e-02 | 1.16e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -18.3 | -3.3 | 22.2 | 1.2 | 4.8 | -1.0 |
| 7192 | ok | 0.16 | 4.93e-02 | 9.25e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -13.4 | -1.0 | 13.9 | 1.4 | 6.9 | -0.2 |
| 7193 | ok | 0.16 | 3.36e-02 | 7.34e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -15.4 | -3.0 | 2.2 | 3.2 | 2.9 | 1.6 |
| 7194 | ok | 0.16 | 3.26e-02 | 8.32e-03 | 4.5 | 4.5 | 3.1 | 3.1 | -18.8 | -8.8 | -7.4 | 4.1 | 2.0 | 2.2 |
| 7195 | ok | 0.16 | 3.56e-02 | 1.51e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -27.7 | -13.9 | -22.9 | 8.6 | 1.3 | 0.8 |
| 7196 | ok | 0.16 | 3.85e-02 | 2.47e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -53.3 | -16.2 | -33.8 | 6.4 | 1.0 | 2.3 |
| 7200 | ok | 0.16 | 4.60e-02 | 3.56e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -93.7 | -9.1 | -35.2 | 7.6 | 0.7 | 2.0 |
| 7202 | ok | 0.16 | 5.23e-02 | 4.29e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -128.5 | -10.0 | -4.4 | 8.2 | 0.3 | 0.5 |
| 7203 | ok | 0.16 | 8.37e-02 | 2.54e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -33.4 | -25.5 | 45.3 | 1.5 | 3.7 | -8.6 |
| 7204 | ok | 0.16 | 7.98e-02 | 2.27e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -30.2 | -18.6 | 42.2 | 2.6 | 2.5 | -4.7 |
| 7205 | ok | 0.16 | 7.43e-02 | 1.93e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -28.4 | -11.2 | 36.4 | 3.1 | 1.5 | -2.4 |
| 7206 | ok | 0.16 | 6.94e-02 | 1.67e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -25.7 | 1.0 | 23.0 | 10.1 | -0.6 | -10.5 |
| 7215 | ok | 0.16 | 6.94e-02 | 2.16e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.1 | -20.8 | -38.4 | 12.3 | 2.8 | 9.5 |
| 7219 | ok | 0.16 | 7.55e-02 | 2.91e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -39.3 | -28.4 | -51.8 | 12.4 | 2.5 | 8.6 |
| 7220 | ok | 0.16 | 8.21e-02 | 3.67e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -56.7 | -28.6 | -63.8 | 12.5 | 2.1 | 7.9 |
| 7221 | ok | 0.16 | 7.33e-02 | 4.19e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -81.6 | -21.1 | -66.4 | 5.9 | 1.2 | 3.7 |
| 7222 | ok | 0.16 | 4.81e-02 | 3.76e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -98.6 | -18.6 | -35.9 | 6.1 | 0.3 | 2.5 |
| 7638 | ok | 0.16 | 0.2 | 3.75e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -57.9 | 5.2 | 78.8 | 5.1 | 1.0 | -5.6 |
| 7653 | ok | 0.16 | 0.1 | 1.17e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -17.8 | 19.6 | -23.1 | 26.5 | -0.2 | 19.4 |

| Nodo | Stato | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
|------|-------|------|----------|----------|--------|--------|---------|---------|---------|---------|---------|--------|-----------|--------|
| 8345 | ok | 0.16 | 0.1 | 3.33e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -29.7 | -77.7 | 36.3 | 0.8 | 65.6 | 5.0 |
| 8347 | ok | 0.16 | 0.2 | 1.88e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -38.4 | 14.4 | 33.4 | -8.5 | 23.6 | -2.6 |
| 8348 | ok | 0.16 | 9.40e-02 | 1.75e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -36.0 | 5.1 | 29.1 | -5.3 | 6.6 | -3.0 |
| 8349 | ok | 0.16 | 6.74e-02 | 1.72e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -36.1 | 4.5 | 25.6 | -3.2 | -0.8 | -2.1 |
| 8350 | ok | 0.16 | 5.24e-02 | 2.42e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -41.8 | -13.4 | 41.7 | -6.6 | -2.1 | -12.2 |
| 8351 | ok | 0.16 | 0.1 | 3.52e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.9 | -45.9 | 61.4 | 9.3 | 4.2 | -27.4 |
| 8352 | ok | 0.16 | 0.1 | 3.74e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -45.2 | -44.9 | 65.2 | 3.4 | 2.9 | -15.4 |
| 8353 | ok | 0.16 | 0.1 | 3.52e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -45.1 | -35.7 | 63.1 | 2.3 | 1.0 | -8.4 |
| 8354 | ok | 0.16 | 0.1 | 3.10e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -43.5 | -23.4 | 57.3 | 2.3 | -4.58e-02 | -4.9 |
| 8355 | ok | 0.16 | 0.1 | 2.88e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -34.1 | -21.0 | -57.2 | 20.5 | 5.5 | 22.6 |
| 8356 | ok | 0.16 | 0.1 | 3.72e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -37.1 | -35.7 | -73.1 | 18.5 | 4.5 | 20.4 |
| 8357 | ok | 0.16 | 0.1 | 4.60e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -43.2 | -44.5 | -91.2 | 16.9 | 3.5 | 18.7 |
| 8358 | ok | 0.16 | 0.2 | 5.43e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -58.2 | -40.7 | -110.3 | 4.0 | 2.1 | 6.3 |
| 8359 | ok | 0.16 | 0.2 | 5.87e-02 | 4.5 | 4.5 | 3.1 | 3.1 | -77.2 | -35.5 | -115.1 | 4.5 | 1.6 | 6.6 |
| Nodo | | x/d | V N/M | ver. rid | Af pr- | Af pr+ | Af sec- | Af sec+ | N z | N o | N zo | M z | M o | M zo |
| | | 0.20 | 0.78 | 0.17 | 6.81 | 6.40 | 5.43 | 5.01 | -475.42 | -313.80 | -167.04 | -81.22 | -40.55 | -27.41 |
| | | | | | | | | | 181.63 | 307.37 | 235.08 | 160.81 | 65.64 | 57.98 |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|------|-------|---------|----------|-----------|---------|----------|--------|--------|
| | | daN/cm2 | | | | | daN/cm | daN/cm |
| 6851 | ok | 2.43 | | | | | | |
| 7107 | ok | 0.23 | | | | | | |
| 7109 | ok | 0.13 | | | | | | |
| 7116 | ok | 0.26 | | | | | | |
| 7119 | ok | 0.05 | | | | | | |
| 7122 | ok | 0.31 | | | | | | |
| 7125 | ok | 0.03 | | | | | | |
| 7127 | ok | 0.36 | | | | | | |
| 7130 | ok | 0.04 | | | | | | |
| 7139 | ok | 0.43 | | | | | | |
| 7141 | ok | 0.05 | | | | | | |
| 7144 | ok | 0.54 | | | | | | |
| 7146 | ok | 0.08 | | | | | | |
| 7147 | ok | 0.68 | | | | | | |
| 7148 | ok | 0.11 | | | | | | |
| 7149 | ok | 1.39 | | | | | | |
| 7150 | ok | 0.57 | | | | | | |
| 7153 | ok | 2.43 | | | | | | |
| 7157 | ok | 1.31 | | | | | | |
| 7164 | ok | 1.31 | | | | | | |
| 7165 | ok | 0.09 | | | | | | |
| 7166 | ok | 0.07 | | | | | | |
| 7167 | ok | 0.10 | | | | | | |
| 7168 | ok | 0.06 | | | | | | |
| 7169 | ok | 0.04 | | | | | | |
| 7170 | ok | 0.02 | | | | | | |
| 7171 | ok | 0.04 | | | | | | |
| 7172 | ok | 0.06 | | | | | | |
| 7173 | ok | 0.12 | | | | | | |
| 7184 | ok | 0.16 | | | | | | |
| 7185 | ok | 0.20 | | | | | | |
| 7186 | ok | 0.20 | | | | | | |
| 7190 | ok | 0.07 | | | | | | |
| 7191 | ok | 0.05 | | | | | | |
| 7192 | ok | 0.03 | | | | | | |
| 7193 | ok | 0.04 | | | | | | |
| 7194 | ok | 0.05 | | | | | | |
| 7195 | ok | 0.06 | | | | | | |
| 7196 | ok | 0.08 | | | | | | |
| 7200 | ok | 0.08 | | | | | | |
| 7202 | ok | 0.05 | | | | | | |
| 7203 | ok | 0.08 | | | | | | |
| 7204 | ok | 0.06 | | | | | | |
| 7205 | ok | 0.06 | | | | | | |
| 7206 | ok | 0.06 | | | | | | |
| 7215 | ok | 0.06 | | | | | | |
| 7219 | ok | 0.06 | | | | | | |
| 7220 | ok | 0.06 | | | | | | |
| 7221 | ok | 0.06 | | | | | | |
| 7222 | ok | 0.06 | | | | | | |

| Nodo | Stato | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
|-------------|--------------|----------------|-----------------|------------------|----------------|-----------------|-------------|--------------|
| 7638 | ok | 0.06 | | | | | | |
| 7653 | ok | 0.13 | | | | | | |
| 8345 | ok | 0.20 | | | | | | |
| 8347 | ok | 0.13 | | | | | | |
| 8348 | ok | 0.09 | | | | | | |
| 8349 | ok | 0.07 | | | | | | |
| 8350 | ok | 0.10 | | | | | | |
| 8351 | ok | 0.13 | | | | | | |
| 8352 | ok | 0.13 | | | | | | |
| 8353 | ok | 0.13 | | | | | | |
| 8354 | ok | 0.13 | | | | | | |
| 8355 | ok | 0.12 | | | | | | |
| 8356 | ok | 0.12 | | | | | | |
| 8357 | ok | 0.10 | | | | | | |
| 8358 | ok | 0.08 | | | | | | |
| 8359 | ok | 0.06 | | | | | | |
| Nodo | | Max tau | Ver V pr | Ver V sec | Af V pr | Af V sec | V pr | V sec |
| | | 2.43 | | | | | | |

2.2.4 Verifica Suole di fondazione

Il progetto e la verifica strutturale delle suole in c.a. di fondazione è stato svolto mediante l'ausilio di programma di calcolo Pro-Sap, implementando i risultati delle analisi ottenute dal solutore di calcolo sul modello strutturale per le fondazioni.

Parametri sismici di riferimento e Criteri di Progetto:

- Terreno: Cat. “**B**” – **T1**
- Comportamento Strutturale: **NON DISSIPATIVO**;
- Fattore di Comportamento: **$q_x=q_y= 1.5$**
- Progettazione **Non Dissipativa in Campo Sostanzialmente Elastico**.

Materiali:

- Calcestruzzo **C25/30**;
- Acciaio **B450C**.

2.2.4.1 Legenda Tabella Verifica Travi agli SLU

In tabella vengono riportati per ogni elemento il numero identificativo ed il codice di verifica con le sigle **Ok** o **NV**.

La progettazione degli elementi trave viene eseguita a pressoflessione retta; la progettazione delle staffe è legata alle sollecitazioni di taglio e torsione.

In particolare vengono riportati: il rapporto x/d , le verifiche per sollecitazioni proporzionali e la verifica per compressione media con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori, le quantità di armatura inferiore e superiore oltre che l'armatura trasversale.

| | |
|---------------|--|
| M_T Z P P | Numero della travata (T), quota media (Z), n° pilastrata iniziale (P) e finale (P) (nodo in assenza di pilastrata) |
| Trave | numero identificativo dell'elemento D2 |
| Note | Codici identificativi sezione (s) e materiale (m) trave; sono inoltre presenti le sigle relative all'esito delle verifiche effettuate appresso descritte |
| %Af | Percentuale di area di armatura rispetto a quella di calcestruzzo |
| Af inf. | Area di armatura longitudinale posta all'intradosso |
| Af sup | Area di armatura longitudinale posta all'estradosso |
| Af long. | Area complessiva armatura longitudinale |
| x/d | rapporto tra posizione dell'asse neutro e altezza utile |
| V N/M | Verifica a pressoflessione rapporto E_d/R_d : valore minore o uguale a 1 per verifica positiva |
| Staffe | Dati tratto di staffatura oggetto di verifica, nello specifico: numero delle braccia, diametro, passo, lunghezza L tratto |
| V V/T cls | Verifica a taglio/torsione lato cls con rapporto V_{ed}/V_{rd} : valore minore o uguale a 1 per verifica positiva |
| V V/T acciaio | Verifica a taglio/torsione lato acciaio con rapporto V_{ed}/V_{rd} : valore minore o uguale a 1 per verifica positiva |
| Rif. cmb. | Riferimento combinazioni da cui si generano le verifiche più gravose per la trave |

Avendo progettato a comportamento strutturale non dissipativo le verifiche geotecniche vengono effettuate senza nessun incremento.

2.2.4.2 Suola continua in c.a. - sez. 100x40

Numerazione Travate: 2 - 13 - 14 - 15 - 16 - 17 - 18 - 19 - 20 - 21 - 22

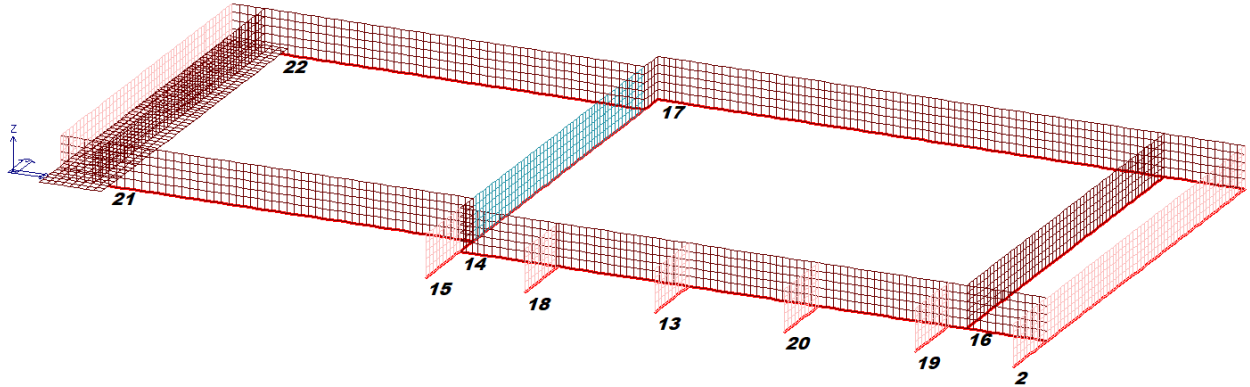


Fig 178. Numerazione Travate oggetto di verifica da modello di calcolo.

Mappe Cromatiche di Verifica

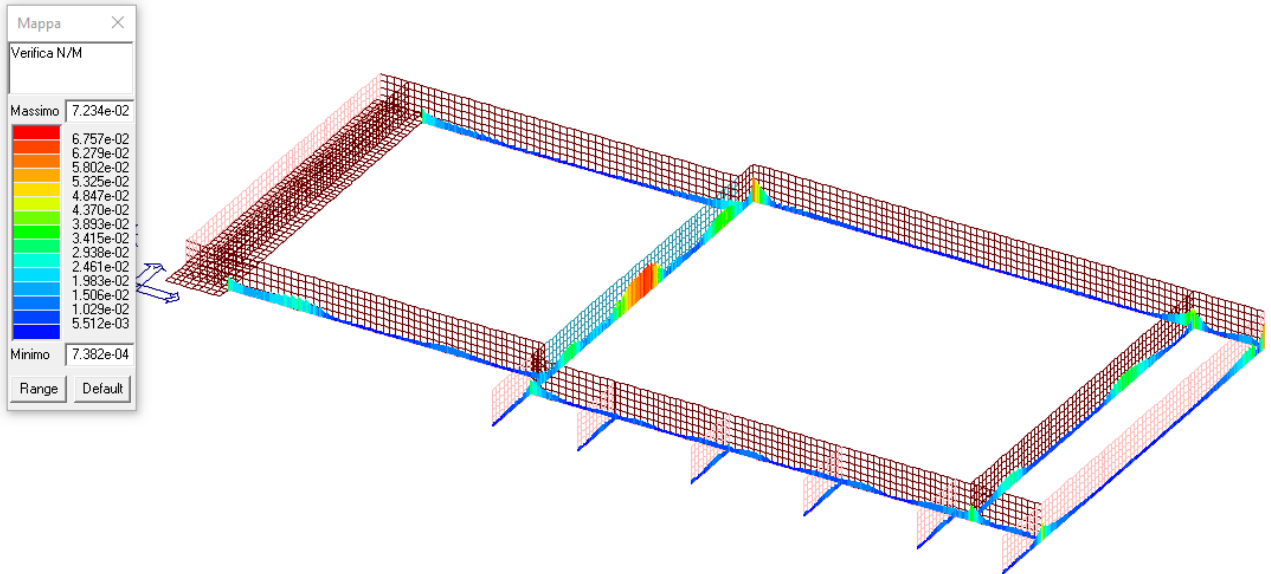


Fig 179. SLU: Mappa di Verifica a Pressoflessione N/M.

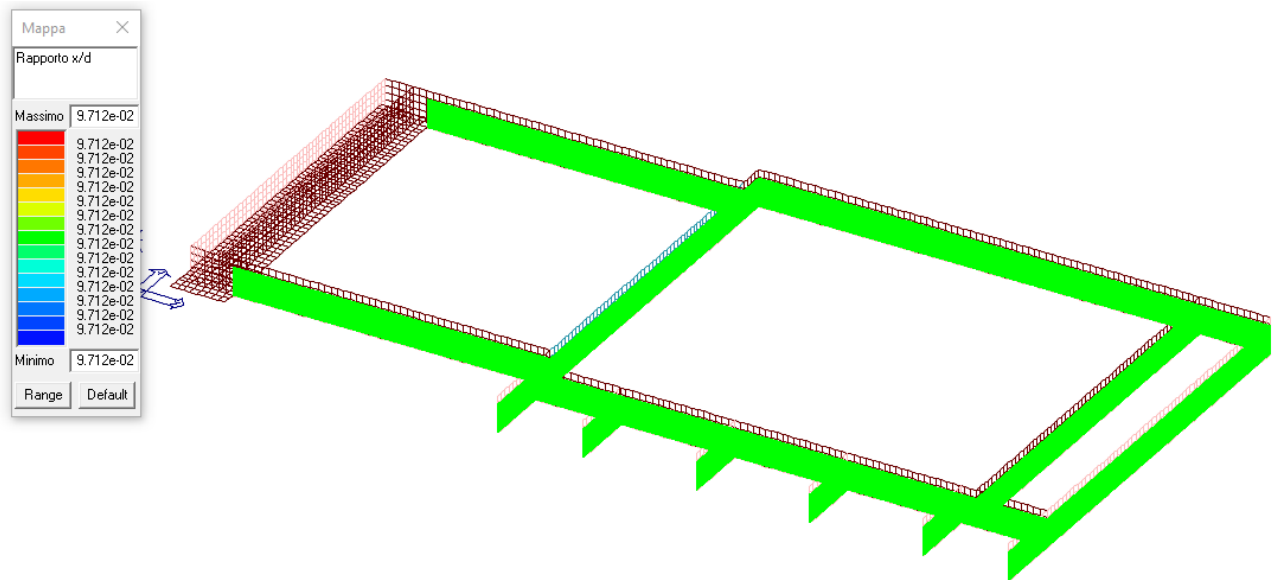


Fig 180. SLU: Mappa Rapporto x/d.

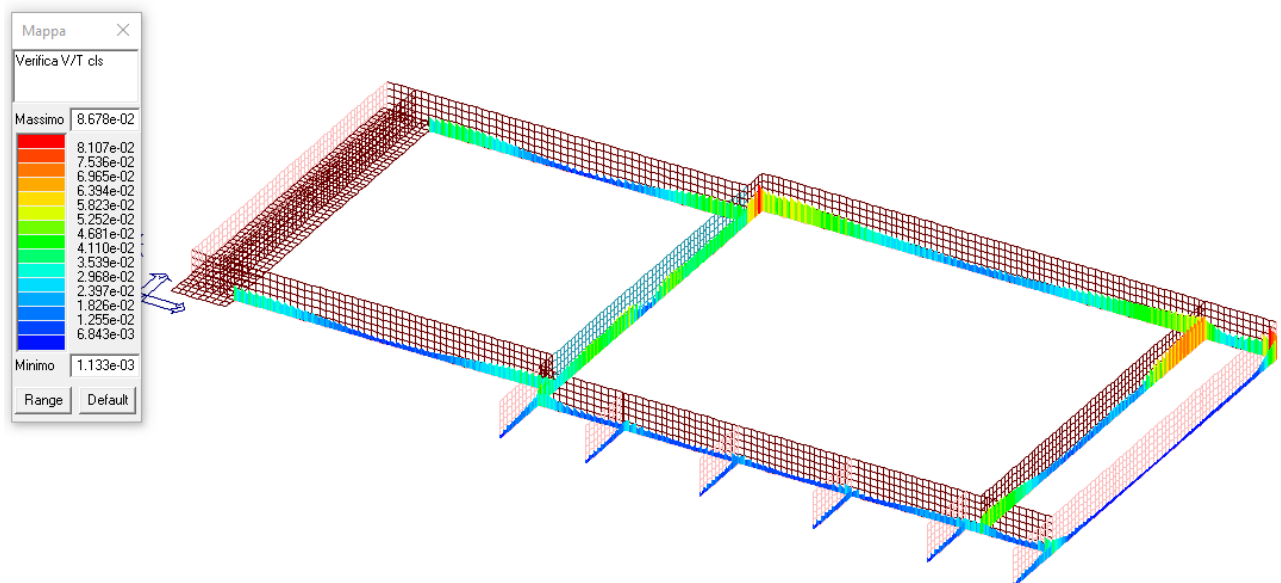


Fig 181. SLU: Mappa Verifica V/T cls.

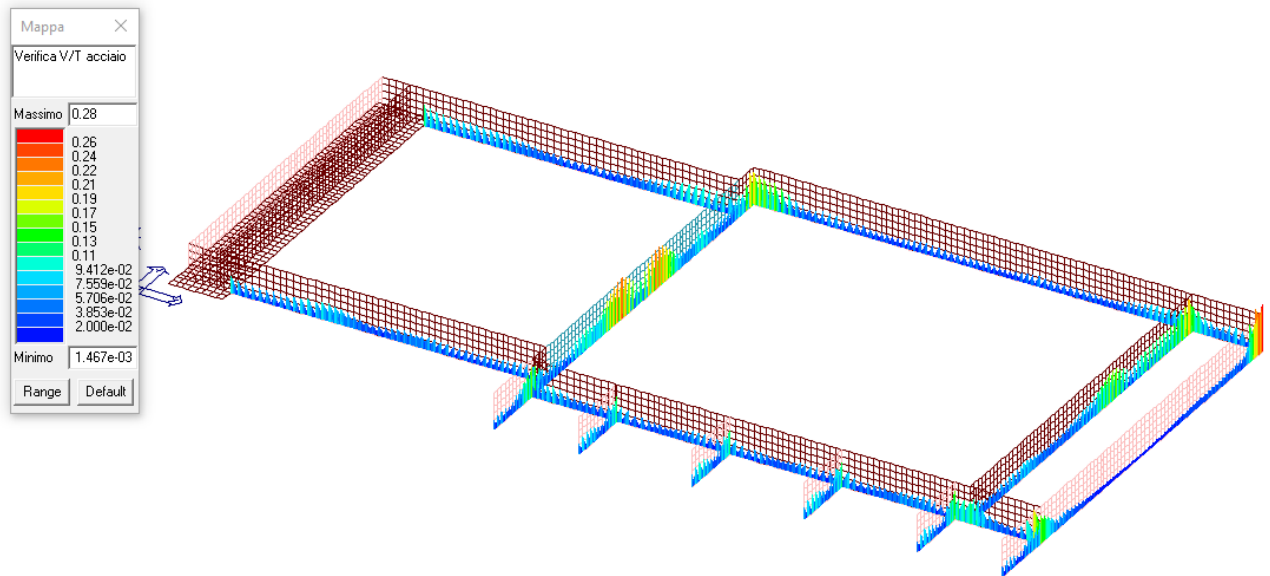


Fig 182. SLU: Mappa Verifica V/T acciaio.

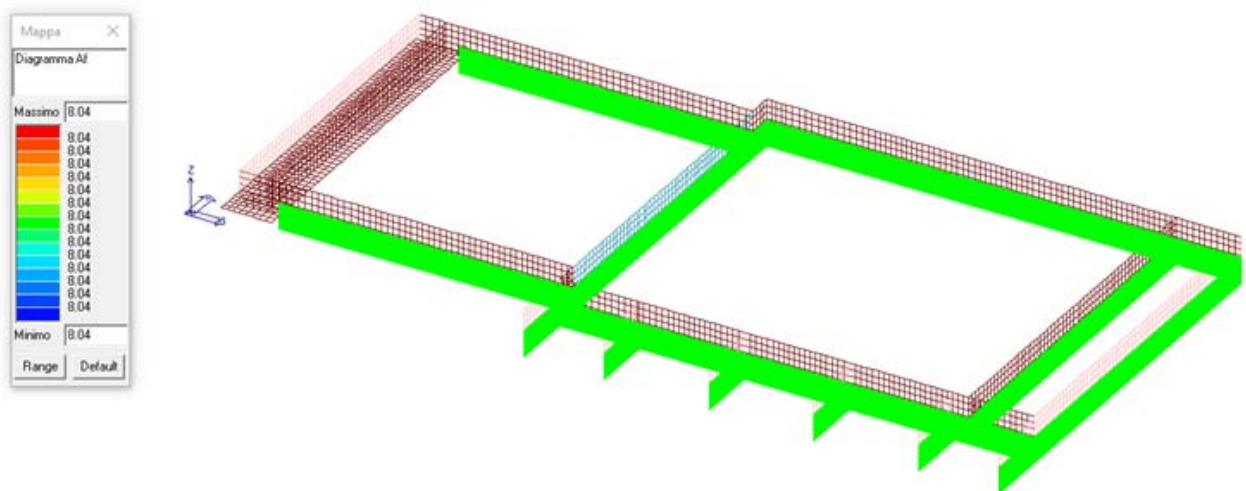


Fig 183. SLU: Mappa Armatura Longitudinale da calcolo [cm²].

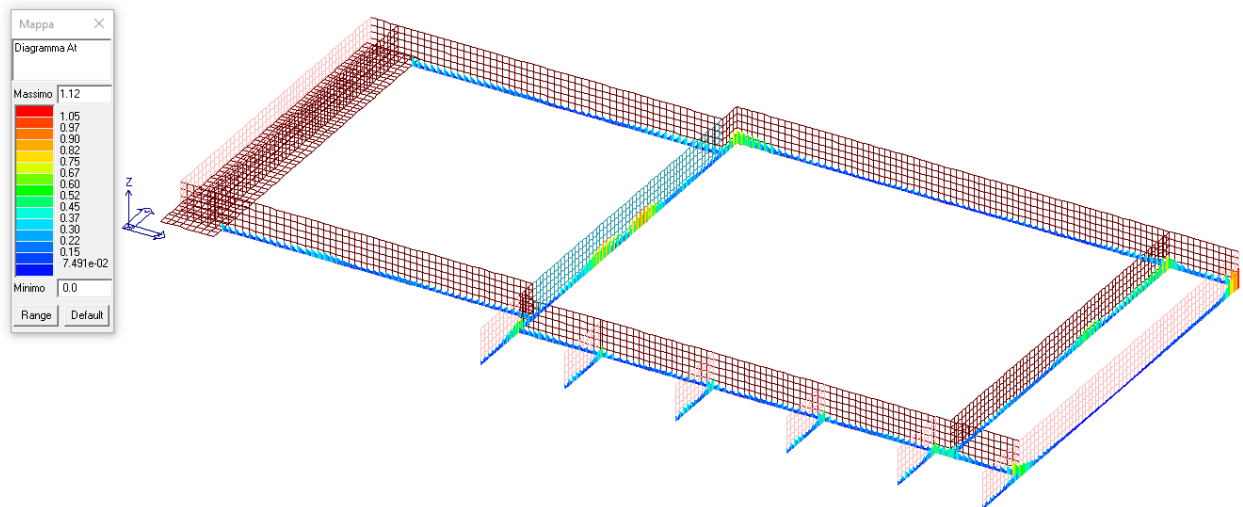


Fig 184. SLU: Mappa Armatura Trasversale da calcolo [cm²/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

2.2.4.3 Suola continua in c.a. - sez. 215x40

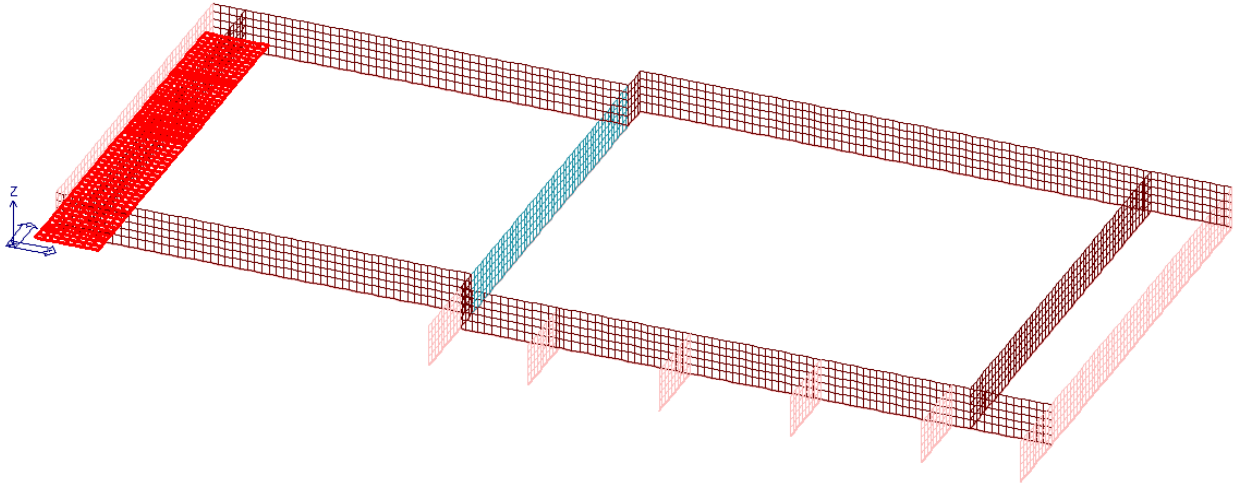


Fig 185. Suola oggetto di verifica da modello di calcolo.

Mappe Cromatiche di Verifica

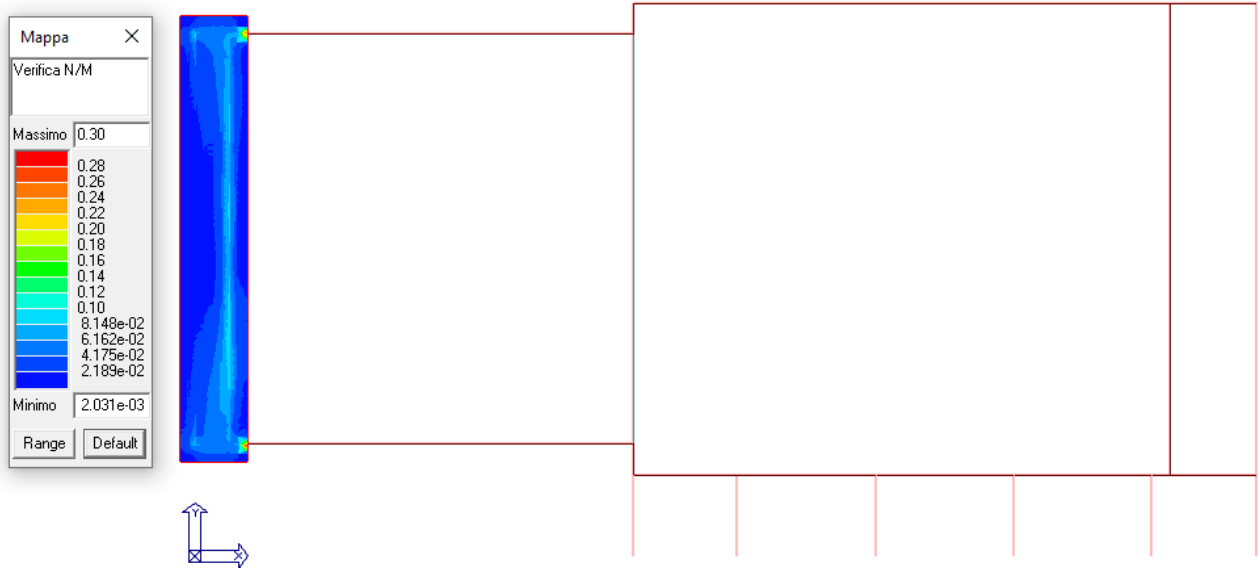


Fig 186. SLU: Mappa di Verifica a Pressoflessione N/M.

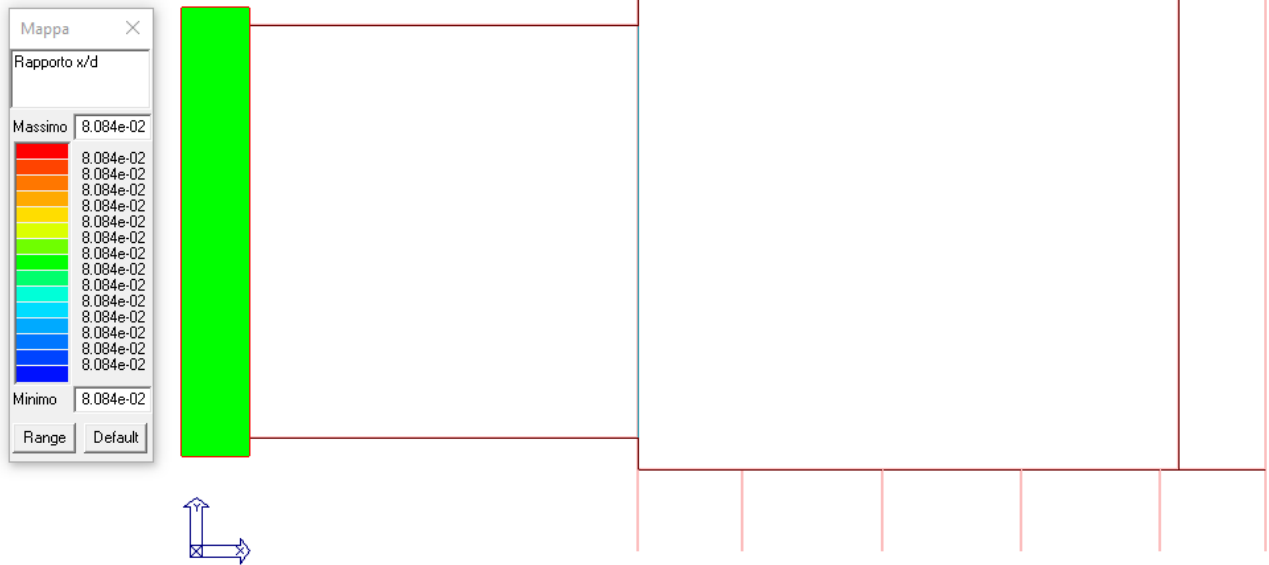


Fig 187. SLU: Mappa Rapporto x/d.

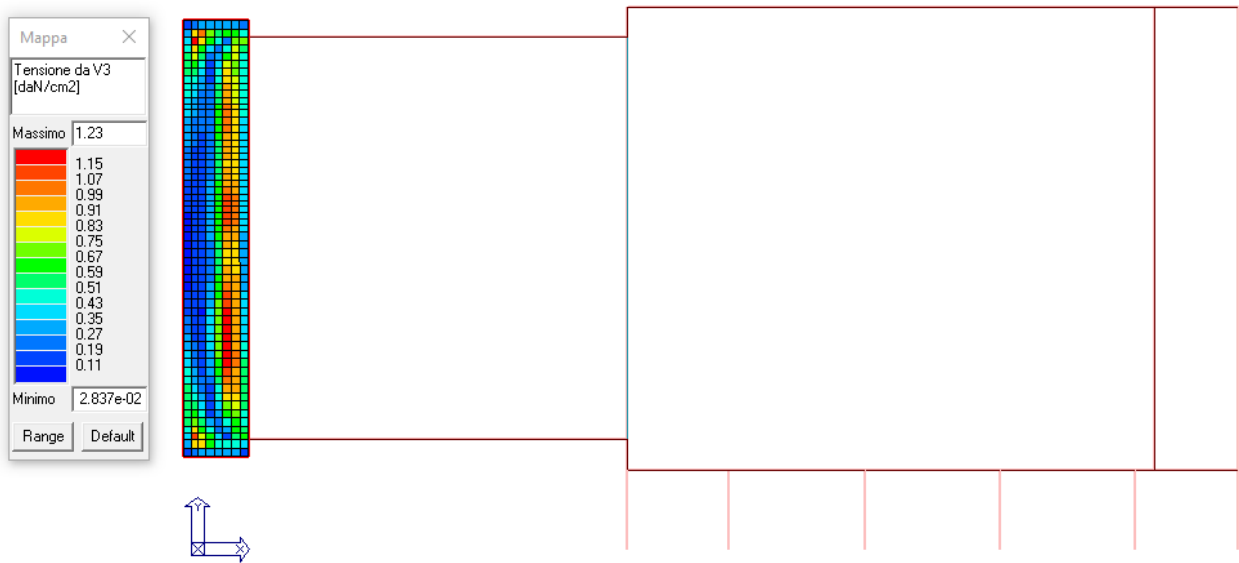


Fig 188. SLU: Mappa Tensione V3 – Massima tensione tangenziale [$\tau < V_{Rd}/H_u \cdot L$ – taglio resistente [4.1.23] per unità di lunghezza diviso per altezza utile = v_{min}]

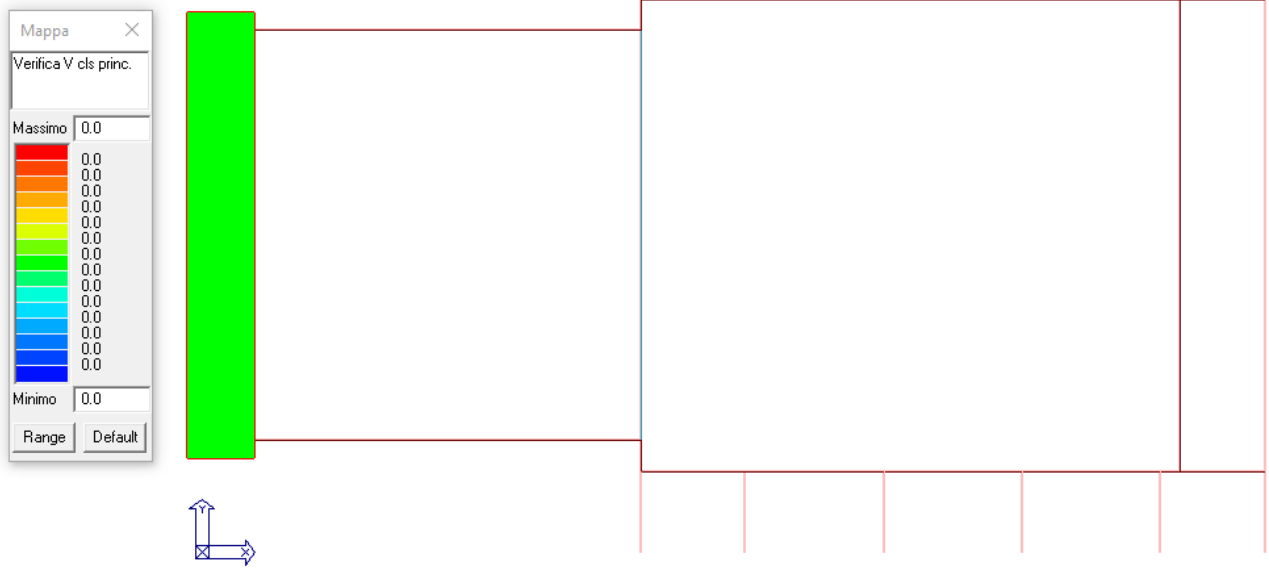


Fig 189. SLU: Mappa di Verifica Vcls direzione principale – Verifica non necessaria in quanto $\tau < v_{min}$ [$\rho_{st} \leq 1.0$ Verifica Soddisfatta].

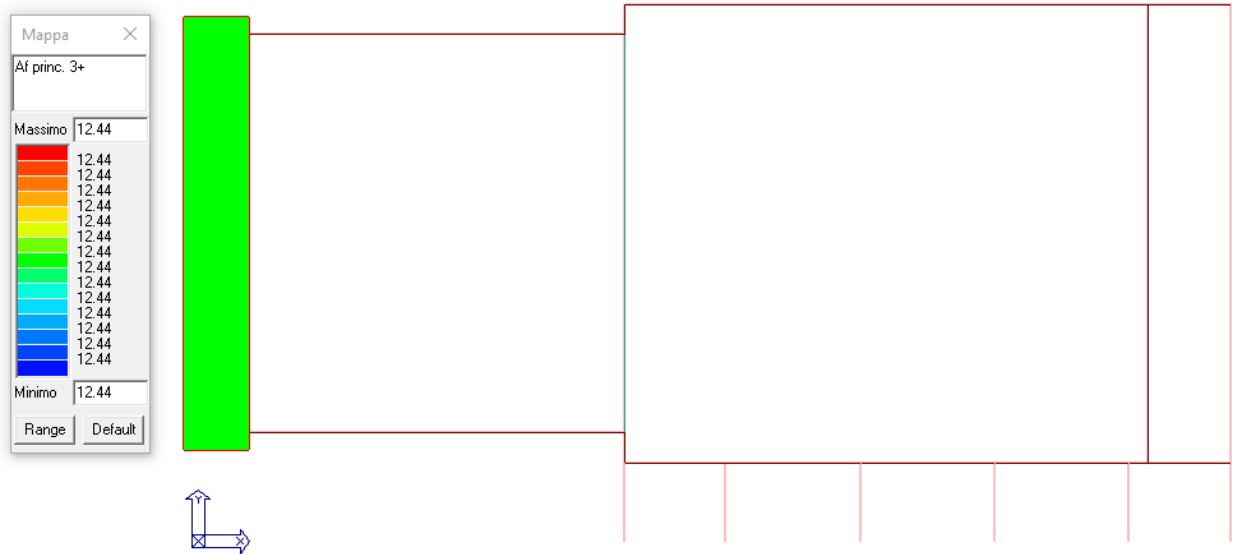


Fig 190. SLU: Mappa Armatura Longitudinale da calcolo [cm²].

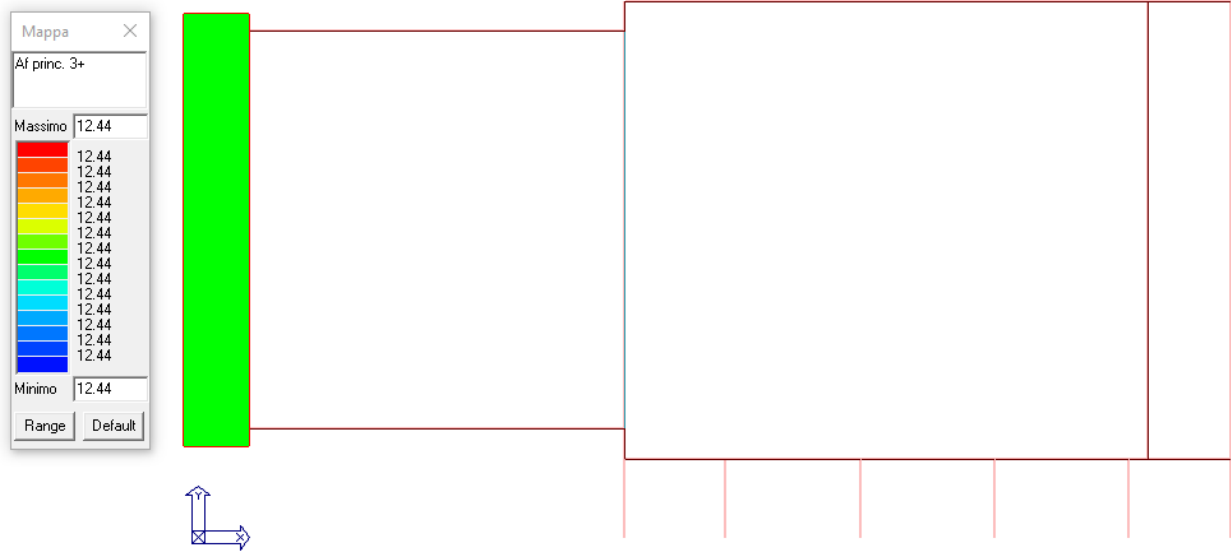


Fig 191. SLU: Mappa Armatura Trasversale da calcolo [cm²/m].

Per l'armatura effettivamente presente si rimanda agli Elaborati Grafici Esecutivi, si sottolinea che essa è sempre maggiore o equivalente a quella considerata nelle verifiche di sicurezza.

2.2.4.4 Verifica Analitica Trave di fondazione in corrispondenza Apertura setto interno

Si riporta la verifica analitica della porzione di trave di fondazione in corrispondenza delle aperture nel setto interno, come evidenziato nella vista assometrica semplificata in figura.

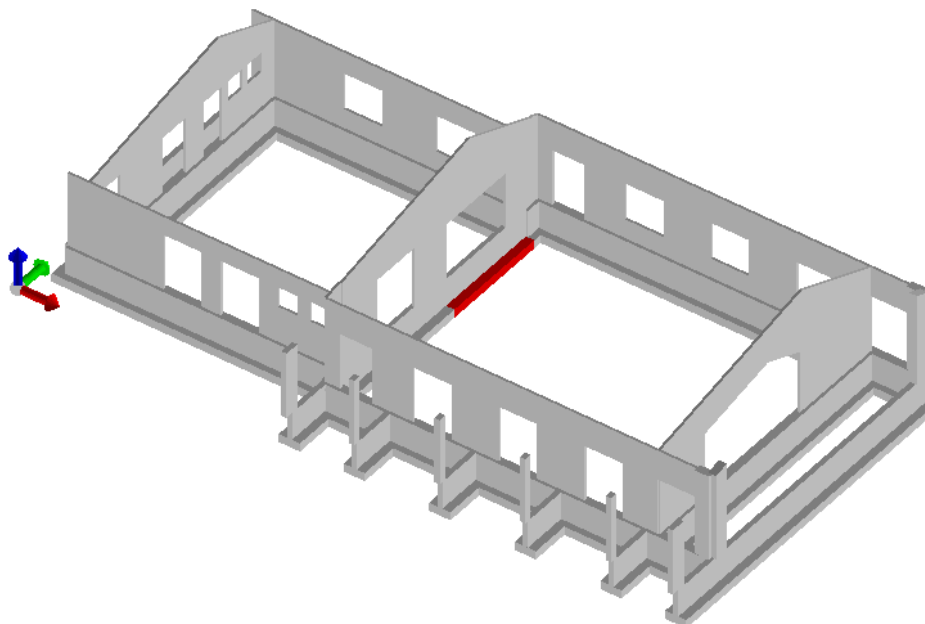
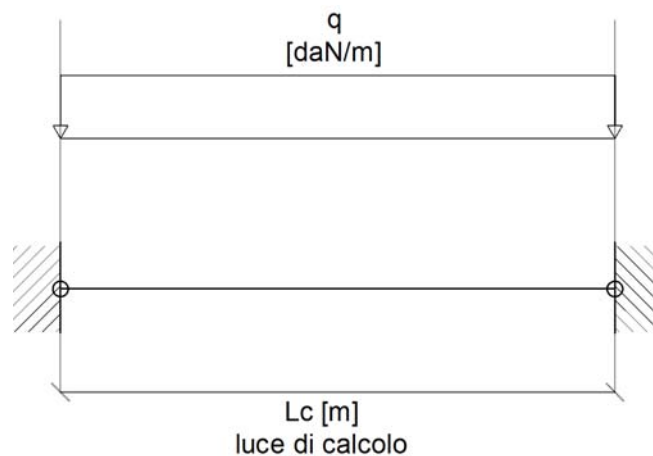


Fig 192. Trave di fondazione oggetto di verifica (Selezione in rosso) – Vista assometrica solida.

CARATTERISTICHE GEOMETRICHE E SCHEMA DI CALCOLO

| | |
|---------------------|---------------------------|
| Sezione | T rovesciata |
| Altezza totale | 170 cm |
| Altezza suola | 40 cm |
| Larghezza anima | 25 cm |
| Larghezza suola B | 100 cm |
| Luce di calcolo Lc: | 5.20 m |
| Carico: | uniformemente distribuito |
| Schema Statico: | semincastro – semincastro |



ANALISI DEI CARICHI

A favore di sicurezza si considerano le pressioni massime agenti sulla suola di fondazione con riferimento alle combinazioni involuppo SLU. Da cui si ottengono le pressioni di calcolo, e il corrispondente carico uniformemente distribuito.

- **Combinazione SLU**

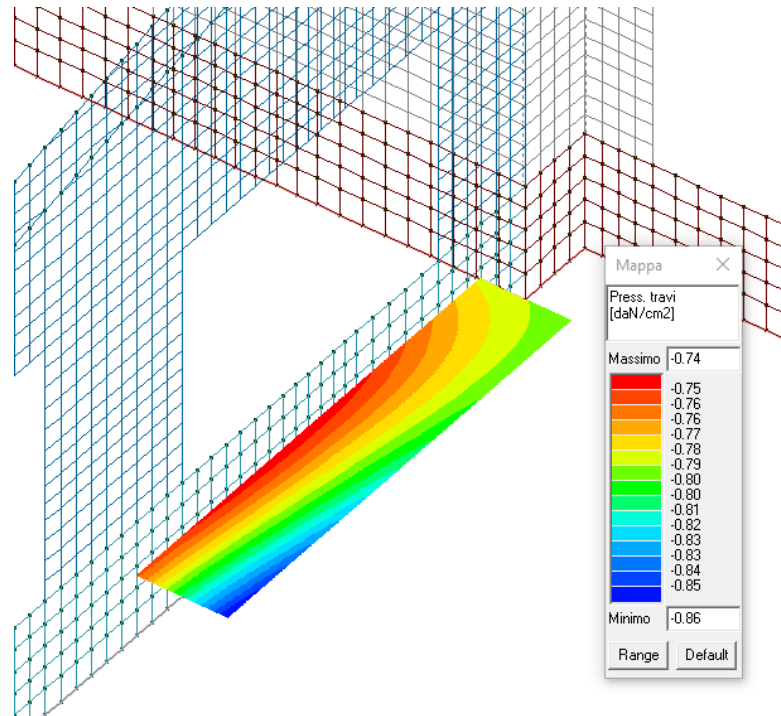


Fig 193. Pressioni massime agenti sul terreno – Condizione Involuppo SLU.

| | |
|------------------------------------|---|
| Pressione massima | $\sigma_{t,max} = 0.86 \text{ daN/cm}^2$ |
| Pressione minima | $\sigma_{t,min} = 0.74 \text{ daN/cm}^2$ |
| Pressione di calcolo | $\sigma_d = (3\sigma_{t,max} + \sigma_{t,min}) / 4 = 0.83 \text{ daN/cm}^2$ (media di Meyerhof) |
| Carico uniforme di progetto | $q_d = B \sigma_d 100 = 8300 \text{ daN/m}$ |

SOLLECITAZIONI DI VERIFICA

| <u>COMBINAZIONE</u> | <u>SOLLECITAZIONI</u> | | | |
|---------------------|-----------------------|-------|------|------------------------------|
| SLU FONDAMENTALE | $M_{Ed,SLU} =$ | 22445 | daNm | $V_{Ed} = 21580 \text{ daN}$ |

ARMATURE LONGITUDINALI

| | | |
|---|----------------|---------------|
| Armatura longitudinale intradosso (suola) | 4+4 Ø16 | Acciaio B450C |
| Armatura longitudinale estradosso | 2 Ø16 | Acciaio B450C |

VERIFICA A PRESSOFLESSIONE – SLU

Titolo : Trave di fondazione

N° figure elementari Zoom N° strati barre Zoom

| N° | b [cm] | h [cm] |
|----|--------|--------|
| 1 | 40 | 130 |
| 2 | 100 | 40 |

| N° | As [cm²] | d [cm] |
|----|----------|--------|
| 1 | 8,04 | 5 |
| 2 | 8,04 | 135 |
| 3 | 4,02 | 165 |

Tipo Sezione
 Rettan.re Trapezi
 a T Circolare
 Rettangoli Coord.

Sollecitazioni
 S.L.U. Metodo n

N_{Ed} kN
 M_{xEd} kNm
 M_{yEd} kNm

P.to applicazione N
 Centro Baricentro cls
 Coord.[cm] xN yN

Tipo rottura
 Lato acciaio - Acciaio snervato

Materiali

 ε_{su} ‰ ε_{c2} ‰
 f_{yd} N/mm² ε_{cu} ‰
 E_s N/mm² f_{cd} N/mm²
 E_s/E_c f_{cc}/f_{cd} ?
 ε_{syd} ‰ σ_{c,adm} N/mm²
 σ_{s,adm} N/mm² τ_{co} τ_{c1}

M_{xRd} kN m
 M_{yRd} kN m
 σ_c N/mm²
 σ_s N/mm²
 ε_c ‰
 ε_s ‰
 d cm
 x x/d
 δ

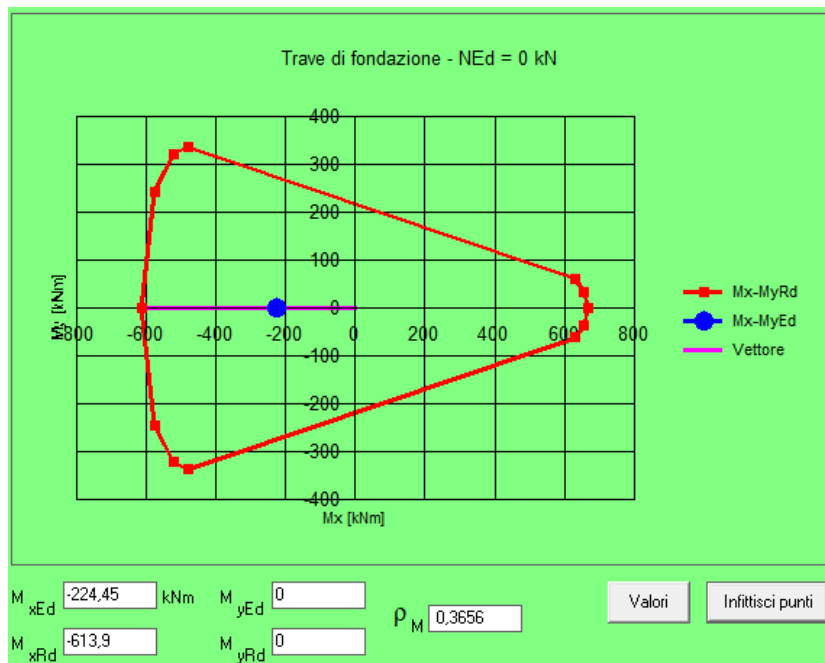
Metodo di calcolo
 S.L.U.+ S.L.U.-
 Metodo n

Tipo flessione
 Retta Deviata

N° rett.

angolo asse neutro θ°

Precompresso



M_{Rd} = -61390 daNm ≥ M_{Ed} = -22445 daNm

Rapporto di verifica: **M_{Ed}/M_{Rd} = 0.37 ≤ 1**

Verifica soddisfatta.

VERIFICA SEZIONE DI APPOGGIO
 $V_{Ed} = 21580 \text{ daN}$

 Armatura a taglio: **1+1 St.Ø10/25"**

| VERIFICA A TAGLIO PER ELEMENTI CON ARMATURE TRASVERSALI RESISTENTI A TAGLIO - §4.1.2.3.5 NTC 2018 | | | |
|--|---------------------------------|---|--|
| Lato Calcestruzzo | | | |
| H | 1700 mm | Altezza totale sezione | |
| d | 1650 mm | Altezza utile della sezione | |
| bw | 400 mm | Larghezza minima della sezione | |
| R_{ck} | 30 N/mm ² | Resistenza caratteristica cubica a compressione del cls | |
| f _{ck} | 24,9 N/mm ² | Resistenza caratteristica cilindrica a compressione | |
| f _{cd} | 14,11 N/mm ² | Resistenza di calcolo a compressione del cls | |
| f _{cd} | 7,06 N/mm ² | Resistenza a compressione ridotta del cls d'anima (=0.5 f _{cd}) | |
| α _{cc} | 0,85 | Coeff. Riduttivo per resistenze di lunga durata | |
| γ _C | 1,50 | Coefficiente di sicurezza cls | |
| α _c | 1 | Pari a 1 per membrature non compresse | |
| α | 90 ° | 1,570796 rad | Inclinazione armatura trasversale rispetto asse trave |
| Θ | 45 | 0,785398 rad | Inclinazione puntone cls rispetto asse trave [21.8° ≤ Θ ≤ 45°] |
| V_{ed} | 215800 N | Taglio sollecitante agli SLU | |
| V_{Rcd} | 2095335,00 N | Resistenza di calcolo a Taglio Compressione | |
| Lato Acciaio | | | |
| A_{sw} | 632,00 mm ² | Area armatura trasversale compresa in "s" | |
| s | 1000 mm | Interasse tra due armature trasversali consecutive | |
| f _{yk} | 450 N/mm ² | Tensione caratteristica di snervamento dell'acciaio | |
| γ _S | 1,15 | Coefficiente parziale di sicurezza dell'acciaio | |
| K _Θ | 1,00 | Coefficiente riduttivo dell'acciaio funzione della temperatura | |
| f_{yd} | 391,30 N/mm ² | Resistenza di calcolo dell'acciaio | |
| α | 90 ° | 1,570796 rad | Inclinazione armatura trasversale rispetto asse trave |
| Θ | 45 | 0,785398 rad | Inclinazione puntone cls rispetto asse trave [21.8° ≤ Θ ≤ 45°] |
| V_{Rsd} | 367246,96 N | Resistenza di calcolo a Taglio Trazione | |
| V_{Rd} | 367246,96 N | Resistenza a taglio della Trave [=MIN(V_{Rsd}; V_{Rcd})] | |

 $V_{Rd} = 36725 \text{ daN} \geq V_{Ed} = 21580 \text{ daN}$
Rapporto di verifica: $V_{Ed} / V_{Rd} = 0.59 \leq 1$
Verifica Soddisfatta.

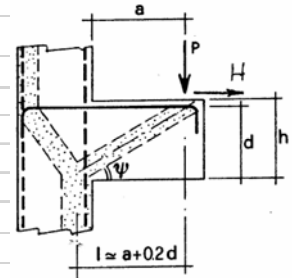
2.2.4.5 Verifica Ali travi di fondazione

Si riporta la verifica involuppo dell'aletta delle travi di fondazione con riferimento alle condizioni più gravose. In accordo con il DM17.01.2018 si applica un approccio *tirante-puntone* trattando tale elemento come una mensola tozza. Si riporta il tabulato di calcolo.

| | |
|---|--|
| Pressione massima agente (condizione involuppo) | $\sigma_d = 0.86 \text{ daN/cm}^2$ (SLU) |
| Luce max aletta (cond. involuppo) | $b = 37.5 \text{ cm}$ |
| Spessore suola | $h = 40 \text{ cm}$ |
| Risultante al metro lineare | $P_{Ed} = \sigma_d b 100 = 3225 \text{ daN/m}$ |
| Armatura | |

Si riporta il calcolo della mensola tozza.

| VERIFICA ELEMENTI TOZZI | | | APPROCCIO DA C.02.02.2009 N. 617/C.S.LL.PP. §C4.1.2.1.5 | | | |
|-------------------------|---------------------------------|--------|---|------------|-----------------|-------------------------|
| AZIONI | V_{sd} (daN) | 3225 | c: | 1,0 | | |
| | H_{sd} (daN) | 0 | L: (a+0.2d) | 42 | | |
| GEOMETRIA | H (cm) | 40 | λ : [L/(0.9d)] | 1,333 | | |
| | c (cm) | 5 | ψ (rad) | 0,64350 | | |
| | d (cm) | 35 | ψ (°) | 36,870 | | |
| | a (cm) | 35 | Armatura Tirante Superiore da Calcolo | | | |
| | B (cm) | 100 | A_{sT} : | 1,10 | cm ² | |
| CLS | R_{ck} (daN/cm ²) | 300 | Armatura Tirante Effettiva | | | |
| | f_{ck} (daN/cm ²) | 249 | n. | Φ | cm ² | |
| | γ_c | 1,5 | a) | 0 | 16 | 0,00 |
| | f_{cd} (daN/cm ²) | 141,10 | b) | 0 | 14 | 0,00 |
| ACCIAIO | Tipo | B450C | c) | 4 | 12 | 4,52 |
| | f_{yk} (daN/cm ²) | 4500 | Somma | | | |
| | γ_s | 1,15 | 4,52 | | | |
| | f_{yd} (daN/cm ²) | 3913 | Parametri Resistenti | | | |
| | | | P_{Rc} = | 71114,4 | daN | Resistenza Lato Cls |
| | | | P_{Rs} = | 13276,6437 | daN | Resistenza Lato acciaio |
| | | | P_{Rd} = | 13276,6437 | | Resistenza del Sistema |
| | | | | | | OK |



Resistenza mensola tozza: $P_{Rd} = \min (P_{Rdc} ; P_{Rds}) = 13277 \text{ daN}$

Rapporto di verifica: $P_{Ed} / P_{Rd} = 0.24 \leq 1$

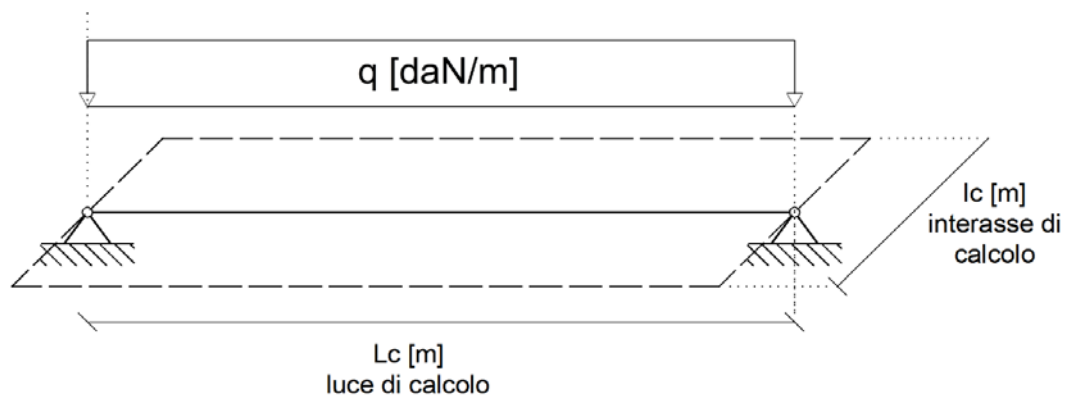
Verifica soddisfatta.

2.2.5 Verifica Copertura

Si riportano le verifiche allo Stato Limite Ultimo e agli Stati Limite di Esercizio degli elementi strutturali dei solai tipici del **piano di copertura**, con riferimento alle condizioni involuppo di carico.

2.2.5.1 Verifica Tegoli TT h40 b18 in c.a.p.

Di seguito si riportano le verifiche complete dei principali tegoli prefabbricati presenti nell'intervento in oggetto. Le analisi di seguito riportate sono comprensive degli stati sollecitativi agli SLU ed agli SLE, quindi delle rispettive verifiche, per le combinazioni di carico che forniscono le sollecitazioni massime involuppo.



Schema di calcolo

Interasse massimo di influenza carico l : 2.50 m;

Luce L : 13.10 m;

Luce di calcolo L_c : 11.85 m;

Luce sbalzo L_{sb} : 1.15 m;

Carico: uniformemente distribuito;

Schema Statico: appoggio - appoggio.

Carichi Portati

Carico distribuito q

| | | | |
|----------------------------------|---|---|-------------------|
| Peso Proprio Tegoli G_1 | $(260 \text{ daN/m}^2 \times 2.50\text{m})$ | = | 650 daN/m; |
| Getto collaborante G_1 | $(125 \text{ daN/m}^2 \times 2.50\text{m})$ | = | 315 daN/m; |
| Sovraccarico Permanente G_2 | $(100 \text{ daN/m}^2 \times 2.50\text{m})$ | = | 250 daN/m; |
| Sovraccarico Impianti G_2 | $(30 \text{ daN/m}^2 \times 2.50\text{m})$ | = | 75 daN/m; |
| Sovraccarico Var. (neve) Q_a | $(120 \text{ daN/m}^2 \times 2.5\text{m})$ | = | <u>300 daN/m;</u> |
| Totale carico distribuito | | = | 1590 daN/m |

Portata equivalente

376 daN/mq.

Tabulato di verifica

```

*****
STRUTTURA      : Skye H40-b.18 L13.10m I2.50m
SOVRACCARICHI  : p1=975daN/m; p2=190daN/m; qa= 300daN/m
COMMITTENTE    : Mensa Alseno
*****

... UNITA' DI MISURA  DaN , Cm ...

... NORMATIVA DI CALCOLO : NTC 2018

... CARATTERISTICHE DELL'ACCIAIO
.....

..ARMATURE PRE-TESE.. Fptk= 18600. Fp(1,0)k= 16700. EA= 2050000. GAMMA=1.15 C.OMOG= 6.00
..ARMATURE LENTE.. RM= 15. Fyk= 4500. EAL= 2100000. GAMMA=1.15
                   COPRIF. ARM. LENTE LONG.= 4.00
..SIGMA LIMITE PER LE STAFFE E PIOLI.. SAST= 3150.

... CARATTERISTICHE DEL CALCESTRUZZO
.....

..CLS TRAVE.. Fck= 465. Fckj= 296. Rck= 550. Rckj= 350. DaN / cm2
              Ec(FINALE)= 275000. Ec(INIZIALE)= 185000. PESO SPECIFICO= 2500. DaN / m3

Lembo inferiore : armature di precompressione presenti in zona tesa
Lembo superiore : armature di precompressione presenti in zona tesa

Sigma limite - ambiente poco aggressivo -
Compressione | < 28 giorni | > 28 giorni | > 28 giorni | > 28 giorni
Trazione max(1) | iniz.= 203.3 | transit.= 319.5 | quasi perman.= 205.4 | rara = 273.9
                 | iniz.= -23.6 | transit.= -37.1 | quasi perman.= -32.0 | freq. = -32.0

..CLS GETTO.. COEFF. OMOGENEIZZAZIONE GETTO = 1.00 RCKs= 300. Fcks= 249. DaN / cm2

... DESCRIZIONE GEOMETRICA DELLA TRAVE ...
.....

LUNGHEZZA TOTALE TRAVE = 1310.0 cm -- LUCE DI CALCOLO (iniziale) = 1290.0 cm

Volume 3.42 m3 | Peso 8561. DaN | Baricentro : quota 27.7 cm | ascissa 655. cm

..ASCISSE DELLE REAZIONI DI APPOGGIO

XR1 = 10.0 XR2 = 1300.0

..DESCRIZIONE A TRAPEZI DEL GETTO DI COMPLETAMENTO..

QUOTA INF.(*) misurata da estradosso trave
-SEZ.N. 1 -ASC.X= 0.0 -ALTEZZA GETTO H= 5.0 AREA GETTO= 1250. -QUOTA INF.(*)= 0.00
TRAPEZI 1
BASE INF. 250.0
BASE SUP. 250.0
ALTEZZA 5.0
-SEZ.N. 2 -ASC.X= 1310.0 -ALTEZZA GETTO H= 5.0 AREA GETTO= 1250. -QUOTA INF.(*)= 0.00
TRAPEZI 1
BASE INF. 250.0
BASE SUP. 250.0
ALTEZZA 5.0

..DESCRIZIONE A TRAPEZI DELLE SEZIONI SINGOLARI..

-SEZ.N. 1 -ASC.= 0.0 -ALTEZZA TRAVE= 40.0 -QUOTA INTRAD.= 0.0 -AREA CLS= 2614.
TRAPEZI 1 2 3
BASE INF. 36.0 36.0 250.0
BASE SUP. 36.0 88.0 250.0
ALTEZZA 31.0 4.0 5.0

-SEZ.N. 2 -ASC.= 1310.0 -ALTEZZA TRAVE= 40.0 -QUOTA INTRAD.= 0.0 -AREA CLS= 2614.
TRAPEZI 1 2 3
BASE INF. 36.0 36.0 250.0
BASE SUP. 36.0 88.0 250.0
ALTEZZA 31.0 4.0 5.0

..DESCRIZIONE A TRAPEZI DELLE SEZIONI DI CALCOLO..

-SEZ.N. 1 -ASC.= 50.0 -ALTEZZA TRAVE= 40.0 -QUOTA INTRAD.= 0.0 -AREA CLS= 2614.
TRAPEZI 1 2 3
BASE INF. 36.0 36.0 250.0
BASE SUP. 36.0 88.0 250.0
ALTEZZA 31.0 4.0 5.0

-SEZ.N. 2 -ASC.= 115.0 -ALTEZZA TRAVE= 40.0 -QUOTA INTRAD.= 0.0 -AREA CLS= 2614.
FORMA UGUALE A QUELLA DELLA SEZIONE N. 1
  
```

-SEZ.N. 3 -ASC.= 250.0 -ALTEZZA TRAVE= 40.0 -QUOTA INTRAD.= 0.0 -AREA CLS= 2614.
FORMA UGUALE A QUELLA DELLA SEZIONE N. 1

-SEZ.N. 4 -ASC.= 500.0 -ALTEZZA TRAVE= 40.0 -QUOTA INTRAD.= 0.0 -AREA CLS= 2614.
FORMA UGUALE A QUELLA DELLA SEZIONE N. 1

-SEZ.N. 5 -ASC.= 707.5 -ALTEZZA TRAVE= 40.0 -QUOTA INTRAD.= 0.0 -AREA CLS= 2614.
FORMA UGUALE A QUELLA DELLA SEZIONE N. 1

-SEZ.N. 6 -ASC.= 900.0 -ALTEZZA TRAVE= 40.0 -QUOTA INTRAD.= 0.0 -AREA CLS= 2614.
FORMA UGUALE A QUELLA DELLA SEZIONE N. 1

-SEZ.N. 7 -ASC.= 1100.0 -ALTEZZA TRAVE= 40.0 -QUOTA INTRAD.= 0.0 -AREA CLS= 2614.
FORMA UGUALE A QUELLA DELLA SEZIONE N. 1

-SEZ.N. 8 -ASC.= 1300.0 -ALTEZZA TRAVE= 40.0 -QUOTA INTRAD.= 0.0 -AREA CLS= 2614.
FORMA UGUALE A QUELLA DELLA SEZIONE N. 1

... DESCRIZIONE DELLE ARMATURE LENTE ...
.....

| ARMATURA LONGITUDINALE. Quote dal basso: | | | Nella Trave | | Nel Getto | |
|--|----------|-----------|-------------|-------|-----------|-------|
| SEZ.N. | ASC. X = | N.LIVELLO | AREA | QUOTA | AREA | QUOTA |
| SEZ.N. 1 | 50.0 | N.LIVELLO | AREA | QUOTA | AREA | QUOTA |
| SEZ.N. 2 | 115.0 | N.LIVELLO | AREA | QUOTA | AREA | QUOTA |
| | | 1 | 12.57 | 8.5 | | |
| SEZ.N. 3 | 250.0 | N.LIVELLO | AREA | QUOTA | AREA | QUOTA |
| SEZ.N. 4 | 500.0 | N.LIVELLO | AREA | QUOTA | AREA | QUOTA |
| SEZ.N. 5 | 707.5 | N.LIVELLO | AREA | QUOTA | AREA | QUOTA |
| SEZ.N. 6 | 900.0 | N.LIVELLO | AREA | QUOTA | AREA | QUOTA |
| SEZ.N. 7 | 1100.0 | N.LIVELLO | AREA | QUOTA | AREA | QUOTA |
| SEZ.N. 8 | 1300.0 | N.LIVELLO | AREA | QUOTA | AREA | QUOTA |

STAFFE ASSEGNATE

| N.Braccia | Diam | Passo | Angolo | xIniz. | xFin. | cmq/m |
|-----------|------|-------|--------|--------|--------|-------|
| 4 | 8. | 10. | 90. | 0.0 | 200.0 | 20.1 |
| 4 | 6. | 20. | 90. | 200.0 | 1210.0 | 5.7 |
| 4 | 8. | 20. | 90. | 1210.0 | 1310.0 | 10.1 |

... DESCRIZIONE DELLE ARMATURE PRE-TESE ...
.....

lunghezza dei tratti di diffusione della precompressione = 99. cm

..ARMATURE A TRACCIATO ORIZZONTALE..

| N. | AREA | SIGMA | RILAS. | QUOTA - TRATTI | INATTIVI DEI TREFOLI - | | ANC.SIN | ANC.DES | LQUAINA LQUAINA | | | |
|----|------|--------|--------|----------------|------------------------|-------|---------|---------|-----------------|----------|--------|------|
| | | | | | DA | A | | | (cm) | SINISTRA | DESTRA | |
| 1 | 0.00 | 13500. | 243. | 6.0 | 0.0 | 100.0 | 1210.0 | 1310.0 | 100. | 100. | 0. | 0. |
| 2 | 5.56 | 13500. | 243. | 6.0 | 0.0 | 200.0 | 1210.0 | 1310.0 | 100. | 100. | 100. | 0. |
| 3 | 0.00 | 13500. | 243. | 11.0 | 0.0 | 100.0 | 1210.0 | 1310.0 | 100. | 100. | 0. | 0. |
| 4 | 2.78 | 13500. | 243. | 11.0 | 0.0 | 500.0 | 910.0 | 1310.0 | 100. | 100. | 400. | 300. |
| 5 | 0.00 | 13500. | 243. | 16.0 | 0.0 | 100.0 | 1210.0 | 1310.0 | 100. | 100. | 0. | 0. |
| 6 | 0.00 | 13500. | 243. | 16.0 | 0.0 | 100.0 | 1210.0 | 1310.0 | 100. | 100. | 0. | 0. |
| 7 | 0.00 | 13500. | 243. | 21.0 | 0.0 | 100.0 | 1210.0 | 1310.0 | 100. | 100. | 0. | 0. |
| 8 | 0.00 | 13500. | 243. | 21.0 | 0.0 | 100.0 | 1210.0 | 1310.0 | 100. | 100. | 0. | 0. |
| 9 | 0.00 | 13500. | 243. | 0.0 | 0.0 | 100.0 | 1210.0 | 1310.0 | 100. | 100. | 0. | 0. |
| 10 | 0.00 | 13500. | 243. | 0.0 | 0.0 | 100.0 | 1210.0 | 1310.0 | 100. | 100. | 0. | 0. |

| TIRO TOTALE | BARIC.TIRO | TIRO RIALZATI | FORZA DEV.MAX | FORZA DEV.SIN | FORZA DEV.DES |
|-------------|------------|---------------|---------------|---------------|---------------|
| 112590. | 7.67 | 0. | 0. | 0. | 0. |

-- FASE 1 -- RILASCIO DEI TREFOLI

CARATTERISTICHE DELLE SEZIONI

| N. | ASC | YIT | YST | YSS | AREA | MOM.ENERZIA |
|----|--------|------|------|-----|-------------|-------------|
| 1 | 50.0 | 27.7 | 12.3 | | 0.26140E+04 | 0.38616E+06 |
| 2 | 115.0 | 26.4 | 13.6 | | 0.28025E+04 | 0.45103E+06 |
| 3 | 250.0 | 27.4 | 12.6 | | 0.26474E+04 | 0.40169E+06 |
| 4 | 500.0 | 27.3 | 12.7 | | 0.26640E+04 | 0.40616E+06 |
| 5 | 707.5 | 27.3 | 12.7 | | 0.26640E+04 | 0.40616E+06 |
| 6 | 900.0 | 27.3 | 12.7 | | 0.26640E+04 | 0.40616E+06 |
| 7 | 1100.0 | 27.4 | 12.6 | | 0.26474E+04 | 0.40169E+06 |
| 8 | 1300.0 | 27.7 | 12.3 | | 0.26140E+04 | 0.38616E+06 |

CARATTERISTICHE DI SOLLECITAZIONE

VALORI INCREMENTALI DELLA FASE

FRAZ.TORC.(*)=Fraz. del mom.torc. totale (di competenza di trave+getto) attribuito alla sola trave avendo lasciato al getto il 0.% del mom.torc. di sua competenza teorica (da rapporto inerzie)

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | FRAZ.TORC.(*) |
|----|------|-------------|-------------|-------------|--------------|-------------|-------------|---------------|
| 1 | 50. | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 2 | 115. | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

| | | | | | | | | |
|---|-------|-------------|--------------|-------------|-------------|-------------|-------------|-------|
| 3 | 250. | 0.73709E+05 | -0.15798E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 4 | 500. | 0.11056E+06 | -0.21741E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 5 | 707. | 0.11056E+06 | -0.21741E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 6 | 900. | 0.11056E+06 | -0.21741E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 7 | 1100. | 0.73709E+05 | -0.15798E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 8 | 1300. | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

VALORI TOTALI DOVUTI AI CARICHI

TORC.TRAVE(*)=Frazione del mom.torcente totale attribuito alla sola trave
usato per il calcolo delle TAU di torsione nella trave

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | TORC.TRAVE(*) |
|----|--------|-------------|-------------|-------------|--------------|-------------|-------------|---------------|
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

APPOGGIO DI SINISTRA XR1= 10.0 APPOGGIO DI DESTRA XR2= 1300.0

| REAZIONE FASE | REAZIONE TOTALE | REAZIONE FASE | REAZIONE TOTALE |
|---------------|-----------------|---------------|-----------------|
| 0. | 0. | 0. | 0. |

MODULO ELASTICO ATTUALE CLS 185000.
COEFF. MULTIPLICATIVO FRECCIA FASE 3.00
VARIAZIONE FRECCIE NELLA FASE E TOTALE CUMULATO

| N. | ASC | VARIAZ.FASE | CUMULATA |
|----|--------|-------------|----------|
| 1 | 50.0 | -1.4193 | -1.4193 |
| 2 | 115.0 | -3.6862 | -3.6862 |
| 3 | 250.0 | -8.2590 | -8.2590 |
| 4 | 500.0 | -14.0249 | -14.0249 |
| 5 | 707.5 | -15.2057 | -15.2057 |
| 6 | 900.0 | -12.9592 | -12.9592 |
| 7 | 1100.0 | -7.6008 | -7.6008 |
| 8 | 1300.0 | 0.0525 | 0.0525 |

| FRECCIA FASE | MASSIMA | ASC = | VALORE = |
|----------------------------|---------|-------|----------|
| FRECCIA FASE | MINIMA | 5.0 | 0.1501 |
| | | 671.5 | -15.2688 |
| FRECCIA ACCUMULATA MASSIMA | | 5.0 | 0.1501 |
| FRECCIA ACCUMULATA MINIMA | | 671.5 | -15.2688 |

LEGENDA - U.M. Forze = DaN - Momenti = DaN x cm - Sigma = DaN / cm2

Nv = Sforzo assiale dovuto a carichi esterni : >0 compressione
Myv = Momento dei carichi attorno all' asse yy verticale : >0 teso lembo sinistro
Mzv = Momento dei carichi attorno all' asse zz orizzontale : >0 teso lembo inferiore
Np = Sforzo assiale dovuto alla precompressione (comprese perdite) : >0 compressione
Myp = Momento dovuto a Np attorno all' asse yy verticale : >0 teso lembo sinistro
Mzp = Momento dovuto a Np attorno all' asse zz orizzontale : >0 teso lembo inferiore
Myt = Incremento del Momento attorno all' asse yy verticale di traslazione per Taglio : agli SLE SOLO per sezioni NON precompresse
Mzt = Incremento del Momento attorno all' asse zz orizzontale di traslazione per Taglio : agli SLE SOLO per sezioni NON precompresse
Simbolo per Sigma : P = Sezione Parzializzata - per le sezioni nella zona di diffusione

| SFORZI N. ABSC. | Totali di | | I fase ZZ | | Precompressione ZZ | | Traslaz.ZZ | Totali YY | | Precomp.YY | Traslaz.YY |
|--------------------|-----------|-------------|-------------|-------------|--------------------|-------------|-------------|-------------|-------------|-------------|------------|
| | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt | | | |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 2 | 115.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 3 | 250.0 | 0.00000E+00 | 0.00000E+00 | 0.73709E+05 | -0.15798E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 4 | 500.0 | 0.00000E+00 | 0.00000E+00 | 0.11056E+06 | -0.21741E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 5 | 707.5 | 0.00000E+00 | 0.00000E+00 | 0.11056E+06 | -0.21741E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 6 | 900.0 | 0.00000E+00 | 0.00000E+00 | 0.11056E+06 | -0.21741E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 7 | 1100.0 | 0.00000E+00 | 0.00000E+00 | 0.73709E+05 | -0.15798E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |

-- FASE 2 -- PESO PROPRIO

CARATTERISTICHE DI SOLLECITAZIONE

VALORI INCREMENTALI DELLA FASE

FRAZ.TORC.(*)=Fraz. del mom.torc. totale (di competenza di trave+getto) attribuito alla sola trave
avendo lasciato al getto il 0.% del mom.torc. di sua competenza teorica (da rapporto inerzie)

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | FRAZ.TORC.(*) |
|----|-----|-------------|-------------|-------------|--------------|-------------|-------------|---------------|
| 1 | 50. | 0.00000E+00 | 0.16305E+06 | 0.39537E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

| | | | | | | | | |
|---|-------|-------------|--------------|--------------|-------------|-------------|-------------|-------|
| 2 | 115. | 0.00000E+00 | 0.40623E+06 | 0.35289E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 3 | 250. | 0.00000E+00 | 0.82308E+06 | 0.26467E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 4 | 500. | 0.00000E+00 | 0.12805E+07 | 0.10129E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 5 | 707. | 0.00000E+00 | 0.13500E+07 | -0.34309E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 6 | 900. | 0.00000E+00 | 0.11629E+07 | -0.16011E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 7 | 1100. | 0.00000E+00 | 0.71199E+06 | -0.29081E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 8 | 1300. | 0.00000E+00 | -0.32700E+03 | 0.65350E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

VALORI TOTALI DOVUTI AI CARICHI

TORC.TRAVE(*)=Frazione del mom.torcente totale attribuito alla sola trave
usato per il calcolo delle TAU di torsione nella trave

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | TORC.TRAVE(*) |
|----|--------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50.0 | 0.00000E+00 | 0.16305E+06 | 0.39537E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | 0.40623E+06 | 0.35289E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.82308E+06 | 0.26467E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.12805E+07 | 0.10129E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.13500E+07 | -0.34309E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.11629E+07 | -0.16011E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.71199E+06 | -0.29081E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | -0.32700E+03 | 0.65350E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

APPOGGIO DI SINISTRA XR1= 10.0 APPOGGIO DI DESTRA XR2= 1300.0

REAZIONE FASE REAZIONE TOTALE REAZIONE FASE REAZIONE TOTALE
-4280. -4280. -4280. -4280.

MODULO ELASTICO ATTUALE CLS 185000.
COEFF. MOLTIPLICATIVO FRECCIA FASE 3.00
VARIAZIONE FRECCIE NELLA FASE E TOTALE CUMULATO

| N. | ASC | VARIAZ.FASE | CUMULATA |
|----|--------|-------------|----------|
| 1 | 50.0 | 0.9374 | -0.4819 |
| 2 | 115.0 | 2.4079 | -1.2784 |
| 3 | 250.0 | 5.2281 | -3.0309 |
| 4 | 500.0 | 8.7505 | -5.2743 |
| 5 | 707.5 | 9.3215 | -5.8842 |
| 6 | 900.0 | 7.8082 | -5.1510 |
| 7 | 1100.0 | 4.4464 | -3.1544 |
| 8 | 1300.0 | -0.0307 | 0.0219 |

FRECCIA FASE MASSIMA ASC = 671.5 VALORE = 9.3886
FRECCIA FASE MINIMA ASC = 5.0 VALORE = -0.0993
FRECCIA ACCUMULATA MASSIMA ASC = 5.0 VALORE = 0.0508
FRECCIA ACCUMULATA MINIMA ASC = 707.5 VALORE = -5.8842

VERIFICHE FLESSIONALI

LEGENDA - U.M. Forze = DaN - Momenti = DaN x cm - Sigma = DaN / cm2
Nv = Sforzo assiale dovuto a carichi esterni : >0 compressione
Myv = Momento dei carichi attorno all' asse yy verticale : >0 teso lembo sinistro
Mzv = Momento dei carichi attorno all' asse zz orizzontale : >0 teso lembo inferiore
Np = Sforzo assiale dovuto alla precompressione (comprese perdite) : >0 compressione
Myp = Momento dovuto a Np attorno all' asse yy verticale : >0 teso lembo sinistro
Mzp = Momento dovuto a Np attorno all' asse zz orizzontale : >0 teso lembo inferiore
Myt = Incremento del Momento attorno all' asse yy verticale di traslazione per Taglio : agli SLE SOLO per sezioni NON precompresse
Mzt = Incremento del Momento attorno all' asse zz orizzontale di traslazione per Taglio : agli SLE SOLO per sezioni NON precompresse
Simbolo per Sigma : P = Sezione Parzializzata - per le sezioni nella zona di diffusione

| N. ABSC. | Totali di | | I fase ZZ | | Precompressione ZZ | | Traslaz.ZZ | Totali YY | | Precomp.YY | Traslaz.YY |
|----------|-----------|-------------|-------------|-------------|--------------------|-------------|-------------|-------------|-------------|-------------|------------|
| | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt | | | |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 2 | 115.0 | 0.00000E+00 | 0.40623E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 3 | 250.0 | 0.00000E+00 | 0.82308E+06 | 0.73709E+05 | -0.15798E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 4 | 500.0 | 0.00000E+00 | 0.12805E+07 | 0.11056E+06 | -0.21741E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 5 | 707.5 | 0.00000E+00 | 0.13500E+07 | 0.11056E+06 | -0.21741E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 6 | 900.0 | 0.00000E+00 | 0.11629E+07 | 0.11056E+06 | -0.21741E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 7 | 1100.0 | 0.00000E+00 | 0.71199E+06 | 0.73709E+05 | -0.15798E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | |

| N. ASC. | sigma c trave | | variazione | | Barre trave | | Sigma Trefoli | | sigma c getto | | Barre getto | |
|---------|---------------|------|------------|------|-------------|--------|---------------|--------|---------------|------|-------------|--------|
| | SUP. | INF. | SUP. | INF. | traz. | compr. | totale | incr. | SUP. | INF. | traz. | compr. |
| 1 | 50.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0 | 0 |
| 2 | 115.0 | 18.1 | -23.8F | 18.1 | -23.8 | -1095 | 0 | -13520 | 585 | 0.0 | 0.0 | 0 |
| 3 | 250.0 | 4.2 | 79.5 | 25.7 | -56.2 | 0 | 0 | -12814 | -239 | 0.0 | 0.0 | 0 |
| 4 | 500.0 | 13.6 | 101.6 | 39.9 | -86.2 | 0 | 0 | -12642 | -332 | 0.0 | 0.0 | 0 |
| 5 | 707.5 | 15.8 | 97.0 | 42.1 | -90.8 | 0 | 0 | -12654 | -326 | 0.0 | 0.0 | 0 |
| 6 | 900.0 | 10.0 | 109.5 | 36.3 | -78.3 | 0 | 0 | -12622 | -343 | 0.0 | 0.0 | 0 |

| | | | | | | | | | | | | | |
|---|--------|-----|------|------|-------|---|---|--------|------|-----|-----|---|---|
| 7 | 1100.0 | 0.7 | 87.1 | 22.3 | -48.6 | 0 | 0 | -12794 | -250 | 0.0 | 0.0 | 0 | 0 |
| 8 | 1300.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0 | 0 |

-- FASE 3 -- PRIMA FASE PERDITE (50 %)

PERDITE PER RILASSAMENTO DELLE ARMATURE PRETESE

COEFF. C = 9.0 CADUTA A 1000 ORE = 297.0 CADUTA A T > DI 2000 ORE = 337.5

PERDITE PER VISCOSITA' - COEFF = 2.30

PERDITE PER RITIRO - COEFF=0.00030

FRAZIONI DELLE PERDITE SCONTATE NELLA FASE

RILASS RITIRO VISCOS

ARMATURE
PRETESE 0.50 0.50 0.50

CARATTERISTICHE DI SOLLECITAZIONE

VALORI INCREMENTALI DELLA FASE

FRAZ.TORC.(*)=Fraz. del mom.torc. totale (di competenza di trave+getto) attribuito alla sola trave avendo lasciato al getto il 0.% del mom.torc. di sua competenza teorica (da rapporto inerzie)

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | FRAZ.TORC.(*) |
|----|-------|--------------|-------------|-------------|--------------|-------------|-------------|---------------|
| 1 | 50. | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 2 | 115. | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 3 | 250. | -0.72602E+04 | 0.15561E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 4 | 500. | -0.12595E+05 | 0.24892E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 5 | 707. | -0.12248E+05 | 0.24201E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 6 | 900. | -0.13182E+05 | 0.26063E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 7 | 1100. | -0.76674E+04 | 0.16434E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 8 | 1300. | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

VALORI TOTALI DOVUTI AI CARICHI

TORC.TRAVE(*)=Frazione del mom.torcente totale attribuito alla sola trave usato per il calcolo delle TAU di torsione nella trave

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | TORC.TRAVE(*) |
|----|--------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50.0 | 0.00000E+00 | 0.16305E+06 | 0.39537E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | 0.40623E+06 | 0.35289E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.82308E+06 | 0.26467E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.12805E+07 | 0.10129E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.13500E+07 | -0.34309E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.11629E+07 | -0.16011E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.71199E+06 | -0.29081E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | -0.32700E+03 | 0.65350E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

APPOGGIO DI SINISTRA XR1= 10.0 APPOGGIO DI DESTRA XR2= 1300.0

| REAZIONE FASE | REAZIONE TOTALE | REAZIONE FASE | REAZIONE TOTALE |
|---------------|-----------------|---------------|-----------------|
| 0. | -4280. | 0. | -4280. |

MODULO ELASTICO ATTUALE CLS 185000.
COEFF. MOLTIPLICATIVO FRECCIA FASE 3.00
VARIAZIONE FRECCIE NELLA FASE E TOTALE CUMULATO

| N. | ASC | VARIAZ.FASE | CUMULATA |
|----|--------|-------------|----------|
| 1 | 50.0 | 0.1441 | -0.3378 |
| 2 | 115.0 | 0.3743 | -0.9041 |
| 3 | 250.0 | 0.8401 | -2.1909 |
| 4 | 500.0 | 1.4577 | -3.8166 |
| 5 | 707.5 | 1.6070 | -4.2772 |
| 6 | 900.0 | 1.3702 | -3.7808 |
| 7 | 1100.0 | 0.8003 | -2.3541 |
| 8 | 1300.0 | -0.0056 | 0.0163 |

| FRECCIA FASE | MASSIMA | ASC = | VALORE = |
|--------------|---------|-------|----------|
| FRECCIA FASE | MINIMA | 5.0 | 1.6109 |
| | | | -0.0152 |

| FRECCIA ACCUMULATA | MASSIMA | ASC = | VALORE = |
|--------------------|---------|-------|----------|
| FRECCIA ACCUMULATA | MINIMA | 707.5 | 0.0355 |
| | | | -4.2772 |

VERIFICHE FLESSIONALI

LEGENDA - U.M. Forze = DaN - Momenti = DaN x cm - Sigma = DaN / cm2
Nv = Sforzo assiale dovuto a carichi esterni : >0 compressione
Myv = Momento dei carichi attorno all' asse yy verticale : >0 teso lembo sinistro

Mzv = Momento dei carichi attorno all' asse zz orizzontale : >0 teso lembo inferiore
 Np = Sforzo assiale dovuto alla precompressione (comprese perdite) : >0 compressione
 Myp = Momento dovuto a Np attorno all' asse yy verticale : >0 teso lembo sinistro
 Mzp = Momento dovuto a Np attorno all' asse zz orizzontale : >0 teso lembo inferiore
 Myt = Incremento del Momento attorno all' asse yy verticale di traslazione per Taglio : agli SLE SOLO per sezioni NON precomprese
 Mzt = Incremento del Momento attorno all' asse zz orizzontale di traslazione per Taglio : agli SLE SOLO per sezioni NON precomprese
 Simbolo per Sigma : P = Sezione Parzializzata - per le sezioni nella zona di diffusione

| SFORZI | Totali di | I fase ZZ | Precompressione ZZ | | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-----------|-------------|--------------------|-------------|--------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | 0.40623E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.82308E+06 | 0.66449E+05 | -0.14242E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.12805E+07 | 0.97969E+05 | -0.19252E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.13500E+07 | 0.98315E+05 | -0.19321E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.11629E+07 | 0.97382E+05 | -0.19135E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.71199E+06 | 0.66041E+05 | -0.14155E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| TENSIONI | sigma c trave | variazione | Barre trave | Sigma Trefoli | sigmac getto | Barre getto |
|----------|---------------|-------------|--------------|---------------|--------------|--------------|
| N. ASC. | SUP. INF. | SUP. INF. | traz. compr. | totale incr. | SUP. INF. | traz. compr. |
| 1 | 50.0 | 0.0 0.0 | 0.0 0.0 | 0 0 | 0 0 | 0 0 |
| 2 | 115.0 | 18.1 -23.8F | 0.0 0.0 | -1095 0 | -13351 585 | 0.0 0.0 |
| 3 | 250.0 | 6.3 66.2 | 2.1 -13.4 | 0 0 | -11915 -208 | 0.0 0.0 |
| 4 | 500.0 | 16.7 80.2 | 3.0 -21.5 | 0 0 | -11590 -280 | 0.0 0.0 |
| 5 | 707.5 | 18.7 76.1 | 3.0 -20.9 | 0 0 | -11613 -275 | 0.0 0.0 |
| 6 | 900.0 | 13.1 87.1 | 3.2 -22.5 | 0 0 | -11551 -289 | 0.0 0.0 |
| 7 | 1100.0 | 2.9 73.0 | 2.2 -14.1 | 0 0 | -11877 -217 | 0.0 0.0 |
| 8 | 1300.0 | 0.0 0.0 | 0.0 0.0 | 0 0 | 0 0 | 0.0 0.0 |

-- FASE 4 -- SOLLEVAMENTO

ASCISSE CENTRI DI APPOGGIO/SOLLEVAMENTO -
XR1 = 100.0 XR2 =1210.0

DESCRIZIONE CARICHI VERTICALI EQUIVALENTI

| ASCISSA | VALORE |
|---------|----------|
| 100.00 | -4280.42 |
| 1210.00 | -4280.42 |

CARATTERISTICHE DI SOLLECITAZIONE

VALORI INCREMENTALI DELLA FASE

FRAZ.TORC.(*)=Fraz. del mom.torc. totale (di competenza di trave+getto) attribuito alla sola trave avendo lasciato al getto il 0.% del mom.torc. di sua competenza teorica (da rapporto inerzie)

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | FRAZ.TORC.(*) |
|----|-------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50. | 0.00000E+00 | -0.17122E+06 | -0.42804E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 2 | 115. | 0.00000E+00 | -0.38524E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 3 | 250. | 0.00000E+00 | -0.38524E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 4 | 500. | 0.00000E+00 | -0.38524E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 5 | 707.5 | 0.00000E+00 | -0.38524E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 6 | 900. | 0.00000E+00 | -0.38524E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 7 | 1100. | 0.00000E+00 | -0.38524E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 8 | 1300. | 0.00000E+00 | 0.19531E-02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

VALORI TOTALI DOVUTI AI CARICHI

TORC.TRAVE(*)=Frazione del mom.torc. totale attribuito alla sola trave usato per il calcolo delle TAU di torsione nella trave

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | TORC.TRAVE(*) |
|----|--------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50.0 | 0.00000E+00 | -0.81688E+04 | -0.32675E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | 0.20994E+05 | 0.35289E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.43784E+06 | 0.26467E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.89529E+06 | 0.10129E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.96479E+06 | -0.34309E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.77766E+06 | -0.16011E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.32675E+06 | -0.29081E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | -0.32700E+03 | 0.65350E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

APPOGGIO DI SINISTRA XR1= 10.0 APPOGGIO DI DESTRA XR2= 1300.0

REAZIONE FASE REAZIONE TOTALE REAZIONE FASE REAZIONE TOTALE
4280. 0. 4280. 0.
COEFFICIENTE DINAMICO = 1.000

VERIFICHE FLESSIONALI

LEGENDA - U.M. Forze = DaN - Momenti = DaN x cm - Sigma = DaN / cm2
 Nv = Sforzo assiale dovuto a carichi esterni : >0 compressione
 Myv = Momento dei carichi attorno all' asse yy verticale : >0 teso lembo sinistro
 Mzv = Momento dei carichi attorno all' asse zz orizzontale : >0 teso lembo inferiore
 Np = Sforzo assiale dovuto alla precompressione (comprese perdite) : >0 compressione
 Myp = Momento dovuto a Np attorno all' asse yy verticale : >0 teso lembo sinistro
 Mzp = Momento dovuto a Np attorno all' asse zz orizzontale : >0 teso lembo inferiore
 Myt = Incremento del Momento attorno all' asse yy verticale di traslazione per Taglio : agli SLE SOLO per sezioni NON precomprese
 Mzt = Incremento del Momento attorno all' asse zz orizzontale di traslazione per Taglio : agli SLE SOLO per sezioni NON precomprese
 Simbolo per Sigma : P = Sezione Parzializzata - per le sezioni nella zona di diffusione

| SFORZI | Totali di | I fase ZZ | Precompressione ZZ | | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-------------|-------------|--------------------|--------------|-------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt |
| 1 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 115.0 | 0.00000E+00 | 0.20994E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 250.0 | 0.00000E+00 | 0.43785E+06 | 0.66449E+05 | -0.14242E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 500.0 | 0.00000E+00 | 0.89529E+06 | 0.97969E+05 | -0.19252E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 707.5 | 0.00000E+00 | 0.96479E+06 | 0.98315E+05 | -0.19321E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 900.0 | 0.00000E+00 | 0.77766E+06 | 0.97382E+05 | -0.19135E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 1100.0 | 0.00000E+00 | 0.32675E+06 | 0.66041E+05 | -0.14155E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| TENSIONI | sigma c trave | | variazione | | Barre trave | | Sigma Trefoli | sigmac getto | | Barre getto | | |
|----------|---------------|-------|------------|------|-------------|--------|---------------|--------------|------|-------------|-------|--------|
| N. ASC. | SUP. | INF. | SUP. | INF. | traz. | compr. | totale | incr. | SUP. | INF. | traz. | compr. |
| 1 50.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0 | 0 |
| 2 115.0 | 0.6 | -1.2 | -17.5 | 22.6 | -12 | 0 | -13101 | 7 | 0.0 | 0.0 | 0 | 0 |
| 3 250.0 | -5.8 | 92.5 | -12.1 | 26.3 | 0 | 0 | -11847 | -245 | 0.0 | 0.0 | 0 | 0 |
| 4 500.0 | 4.6 | 106.1 | -12.0 | 25.9 | 0 | 0 | -11523 | -316 | 0.0 | 0.0 | 0 | 0 |
| 5 707.5 | 6.7 | 102.0 | -12.0 | 25.9 | 0 | 0 | -11546 | -311 | 0.0 | 0.0 | 0 | 0 |
| 6 900.0 | 1.1 | 113.0 | -12.0 | 25.9 | 0 | 0 | -11485 | -325 | 0.0 | 0.0 | 0 | 0 |
| 7 1100.0 | -9.1 | 99.3 | -12.1 | 26.3 | 0 | 0 | -11808 | -254 | 0.0 | 0.0 | 0 | 0 |
| 8 1300.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0 | 0 |

-- FASE 5 -- Trasporto ralla 1° caso

ASCISSE CENTRI DI APPOGGIO/SOLLEVAMENTO -
XR1 = 100.0 XR2 =1210.0

DESCRIZIONE CARICHI VERTICALI EQUIVALENTI

| ASCISSA | VALORE |
|---------|----------|
| 100.00 | -4280.42 |
| 1210.00 | -4280.42 |

CARATTERISTICHE DI SOLLECITAZIONE

VALORI INCREMENTALI DELLA FASE

FRAZ.TORC.(*)=Fraz. del mom.torc. totale (di competenza di trave+getto) attribuito alla sola trave avendo lasciato al getto il 0.% del mom.torc. di sua competenza teorica (da rapporto inerzie)

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | FRAZ.TORC.(*) |
|----|-------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50. | 0.00000E+00 | -0.17122E+06 | -0.42804E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 2 | 115. | 0.00000E+00 | -0.38524E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 3 | 250. | 0.00000E+00 | -0.38524E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 4 | 500. | 0.00000E+00 | -0.38524E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 5 | 707. | 0.00000E+00 | -0.38524E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 6 | 900. | 0.00000E+00 | -0.38524E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 7 | 1100. | 0.00000E+00 | -0.38524E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 8 | 1300. | 0.00000E+00 | 0.19531E-02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

VALORI TOTALI DOVUTI AI CARICHI

TORC.TRAVE(*)=Frazione del mom.torc. totale attribuito alla sola trave usato per il calcolo delle TAU di torsione nella trave

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | TORC.TRAVE(*) |
|----|--------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50.0 | 0.00000E+00 | -0.81688E+04 | -0.32675E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | 0.20994E+05 | 0.35289E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.43784E+06 | 0.26467E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.89529E+06 | 0.10129E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.96479E+06 | -0.34309E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.77766E+06 | -0.16011E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.32675E+06 | -0.29081E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | -0.32700E+03 | 0.65350E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

APPOGGIO DI SINISTRA XR1= 10.0 APPOGGIO DI DESTRA XR2= 1300.0

REAZIONE FASE REAZIONE TOTALE REAZIONE FASE REAZIONE TOTALE
 4280. 0. 4280. 0.
 COEFFICIENTE DINAMICO = 1.000

VERIFICHE FLESSIONALI

LEGENDA - U.M. Forze = DaN - Momenti = DaN x cm - Sigma = DaN / cm²
 Nv = Sforzo assiale dovuto a carichi esterni : >0 compressione
 Myv = Momento dei carichi attorno all' asse yy verticale : >0 teso lembo sinistro
 Mzv = Momento dei carichi attorno all' asse zz orizzontale : >0 teso lembo inferiore
 Np = Sforzo assiale dovuto alla precompressione (comprese perdite) : >0 compressione
 Myp = Momento dovuto a Np attorno all' asse yy verticale : >0 teso lembo sinistro
 Mzp = Momento dovuto a Np attorno all' asse zz orizzontale : >0 teso lembo inferiore
 Myt = Incremento del Momento attorno all' asse yy verticale di traslazione per Taglio : agli SLE SOLO per sezioni NON precomprese
 Mzt = Incremento del Momento attorno all' asse zz orizzontale di traslazione per Taglio : agli SLE SOLO per sezioni NON precomprese
 Simbolo per Sigma : P = Sezione Parzializzata - per le sezioni nella zona di diffusione

| SFORZI | Totali di | I fase | ZZ | Precompressione | ZZ | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-----------|-------------|-------------|-----------------|--------------|-------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt | |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | 0.20994E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.43785E+06 | 0.66449E+05 | -0.14242E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.89529E+06 | 0.97969E+05 | -0.19252E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.96479E+06 | 0.98315E+05 | -0.19321E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.77766E+06 | 0.97382E+05 | -0.19135E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.32675E+06 | 0.66041E+05 | -0.14155E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| TENSIONI | sigma c trave | variazione | Barre trave | Sigma Trefoli | sigmac getto | Barre getto |
|----------|------------------|------------|--------------|---------------|--------------|--------------|
| N. ASC. | SUP. INF. | SUP. INF. | traz. compr. | totale incr. | SUP. INF. | traz. compr. |
| 1 | 50.0 0.0 0.0 | 0.0 0.0 | 0 0 | 0 0 | 0.0 0.0 | 0 0 |
| 2 | 115.0 0.6 -1.2 | 0.0 0.0 | -12 0 | -13101 7 | 0.0 0.0 | 0 0 |
| 3 | 250.0 -5.8 92.5 | 0.0 0.0 | 0 0 | -11847 -245 | 0.0 0.0 | 0 0 |
| 4 | 500.0 4.6 106.1 | 0.0 0.0 | 0 0 | -11523 -316 | 0.0 0.0 | 0 0 |
| 5 | 707.5 6.7 102.0 | 0.0 0.0 | 0 0 | -11546 -311 | 0.0 0.0 | 0 0 |
| 6 | 900.0 1.1 113.0 | 0.0 0.0 | 0 0 | -11485 -325 | 0.0 0.0 | 0 0 |
| 7 | 1100.0 -9.1 99.3 | 0.0 0.0 | 0 0 | -11808 -254 | 0.0 0.0 | 0 0 |
| 8 | 1300.0 0.0 0.0 | 0.0 0.0 | 0 0 | 0 0 | 0.0 0.0 | 0 0 |

-- FASE 6 -- Cambio Appoggi

ASCISSE NUOVI PUNTI DI APPOGGIO -
 XR1 = 115.0 XR2 =1300.0

CARATTERISTICHE DI SOLLECITAZIONE

VALORI INCREMENTALI DELLA FASE

FRAZ.TORC.(*)=Fraz. del mom.torc. totale (di competenza di trave+getto) attribuito alla sola trave avendo lasciato al getto il 0.% del mom.torc. di sua competenza teorica (da rapporto inerzie)

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | FRAZ.TORC.(*) |
|----|-------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50. | 0.00000E+00 | -0.17122E+06 | -0.42804E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 2 | 115. | 0.00000E+00 | -0.44944E+06 | -0.42804E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 3 | 250. | 0.00000E+00 | -0.39824E+06 | 0.37928E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 4 | 500. | 0.00000E+00 | -0.30342E+06 | 0.37928E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 5 | 707. | 0.00000E+00 | -0.22472E+06 | 0.37928E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 6 | 900. | 0.00000E+00 | -0.15171E+06 | 0.37928E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 7 | 1100. | 0.00000E+00 | -0.75855E+05 | 0.37928E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 8 | 1300. | 0.00000E+00 | 0.20312E+00 | 0.42804E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

VALORI TOTALI DOVUTI AI CARICHI

TORC.TRAVE(*)=Frazione del mom.torc. totale attribuito alla sola trave usato per il calcolo delle TAU di torsione nella trave

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | TORC.TRAVE(*) |
|----|--------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50.0 | 0.00000E+00 | -0.81688E+04 | -0.32675E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.43213E+05 | -0.75152E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.42484E+06 | 0.30260E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.97711E+06 | 0.13922E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.11253E+07 | 0.36191E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.10112E+07 | -0.12218E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.63613E+06 | -0.25288E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | -0.32680E+03 | 0.43458E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

APPOGGIO DI SINISTRA XR1= 115.0 APPOGGIO DI DESTRA XR2= 1300.0

REAZIONE FASE REAZIONE TOTALE REAZIONE FASE REAZIONE TOTALE

-4660. -4660. -3901. -3901.

MODULO ELASTICO ATTUALE CLS 275000.
COEFF. MOLTIPLICATIVO FRECCIA FASE 3.00
VARIAZIONE FRECCIE NELLA FASE E TOTALE CUMULATO

| N. | ASC | VARIAZ.FASE | CUMULATA |
|----|--------|-------------|----------|
| 1 | 50.0 | 0.3209 | 0.9367 |
| 2 | 115.0 | 0.0000 | 0.0000 |
| 3 | 250.0 | -0.5325 | -1.9223 |
| 4 | 500.0 | -1.0357 | -4.2419 |
| 5 | 707.5 | -1.0573 | -4.8825 |
| 6 | 900.0 | -0.8431 | -4.3187 |
| 7 | 1100.0 | -0.4609 | -2.6625 |
| 8 | 1300.0 | 0.0037 | 0.0200 |

| | | | | |
|----------------------------|-------|-------|----------|---------|
| FRECCIA FASE MASSIMA | ASC = | 5.0 | VALORE = | 0.5564 |
| FRECCIA FASE MINIMA | ASC = | 602.5 | VALORE = | -1.0846 |
| FRECCIA ACCUMULATA MASSIMA | ASC = | 5.0 | VALORE = | 1.5799 |
| FRECCIA ACCUMULATA MINIMA | ASC = | 707.5 | VALORE = | -4.8825 |

VERIFICHE FLESSIONALI

LEGENDA - U.M. Forze = DaN - Momenti = DaN x cm - Sigma = DaN / cm2
 Nv = Sforzo assiale dovuto a carichi esterni : >0 compressione
 Myv = Momento dei carichi attorno all' asse yy verticale : >0 teso lembo sinistro
 Mzv = Momento dei carichi attorno all' asse zz orizzontale : >0 teso lembo inferiore
 Np = Sforzo assiale dovuto alla precompressione (compresse perdite) : >0 compressione
 Myp = Momento dovuto a Np attorno all' asse yy verticale : >0 teso lembo sinistro
 Mzp = Momento dovuto a Np attorno all' asse zz orizzontale : >0 teso lembo inferiore
 Myt = Incremento del Momento attorno all' asse yy verticale di traslazione per Taglio : agli SLE SOLO per sezioni NON precompresse
 Mzt = Incremento del Momento attorno all' asse zz orizzontale di traslazione per Taglio : agli SLE SOLO per sezioni NON precompresse
 Simbolo per Sigma : P = Sezione Parzializzata - per le sezioni nella zona di diffusione

| SFORZI N. ABSC. | Totali di I fase ZZ | | Precompressione ZZ | | Traslaz.ZZ | Totali YY | | Precomp.YY | Traslaz.YY |
|--------------------|---------------------|-------------|--------------------|-------------|--------------|-------------|-------------|-------------|-------------|
| | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt | |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.43213E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.42484E+06 | 0.66449E+05 | -0.14242E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.97711E+06 | 0.97969E+05 | -0.19252E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.11253E+07 | 0.98315E+05 | -0.19321E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.10112E+07 | 0.97382E+05 | -0.19135E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.63613E+06 | 0.66041E+05 | -0.14155E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| TENSIONI N. ASC. | sigma c trave | | variazione | | Barre trave | | Sigma totale | Trefoli incr. | sigmac getto | | Barre getto | | |
|---------------------|---------------|--------|------------|------|-------------|--------|--------------|---------------|--------------|------|-------------|--------|---|
| | SUP. | INF. | SUP. | INF. | traz. | compr. | | | SUP. | INF. | traz. | compr. | |
| 1 | 50.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0.0 | 0.0 | 0 | 0 | |
| 2 | 115.0 | -1.3 * | 2.5 | -1.9 | 3.8 | 0 | 25 | -13155 | -15 | 0.0 | 0.0 | 0 | 0 |
| 3 | 250.0 | -6.2 * | 93.4 | -0.4 | 0.9 | 0 | 0 | -11867 | -246 | 0.0 | 0.0 | 0 | 0 |
| 4 | 500.0 | 7.2 | 100.6 | 2.6 | -5.5 | 0 | 0 | -11555 | -309 | 0.0 | 0.0 | 0 | 0 |
| 5 | 707.5 | 11.7 | 91.2 | 5.0 | -10.8 | 0 | 0 | -11587 | -296 | 0.0 | 0.0 | 0 | 0 |
| 6 | 900.0 | 8.4 | 97.3 | 7.3 | -15.7 | 0 | 0 | -11534 | -303 | 0.0 | 0.0 | 0 | 0 |
| 7 | 1100.0 | 0.6 | 78.2 | 9.7 | -21.1 | 0 | 0 | -11867 | -224 | 0.0 | 0.0 | 0 | 0 |
| 8 | 1300.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0 | 0 |

-- FASE 7 -- carico perm. 1a fase calda

| N. | TIPO | X INIZIO | X FINE | VALORE_INI. | VALORE_FINE | ECCENT.Z | QUOTA_Y | DIREZIONE |
|----|-------------------|----------|--------|-------------|-------------|----------|---------|-----------|
| 1 | FORZA DISTRIBUITA | 140.0 | 1295.0 | 3.15 | 3.15 | 0.00 | 0.00 | VERTICALE |

CARATTERISTICHE DI SOLLECITAZIONE

VALORI INCREMENTALI DELLA FASE

FRAZ.TORC.(*)=Fraz. del mom.torc. totale (di competenza di trave+getto) attribuito alla sola trave avendo lasciato al getto il 0.% del mom.torc. di sua competenza teorica (da rapporto inerzie)

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | FRAZ.TORC.(*) |
|----|-------|-------------|-------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50. | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 2 | 115. | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 3 | 250. | 0.00000E+00 | 0.22238E+06 | 0.14419E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 4 | 500. | 0.00000E+00 | 0.48442E+06 | 0.65442E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 5 | 707. | 0.00000E+00 | 0.55240E+06 | 0.79749E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 6 | 900. | 0.00000E+00 | 0.49419E+06 | -0.60558E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 7 | 1100. | 0.00000E+00 | 0.31008E+06 | -0.12356E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 8 | 1300. | 0.00000E+00 | 0.14514E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

VALORI TOTALI DOVUTI AI CARICHI

TORC.TRAVE(*)=Frazione del mom.torcente totale attribuito alla sola trave
usato per il calcolo delle TAU di torsione nella trave

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | TORC.TRAVE(*) |
|----|--------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50.0 | 0.00000E+00 | -0.81688E+04 | -0.32675E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.43213E+05 | -0.75152E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.64722E+06 | 0.44679E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.14615E+07 | 0.20466E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.16777E+07 | 0.36988E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.15054E+07 | -0.18274E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.94621E+06 | -0.37644E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | -0.32665E+03 | 0.43458E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

APPOGGIO DI SINISTRA XR1= 115.0 APPOGGIO DI DESTRA XR2= 1300.0

| REAZIONE FASE | REAZIONE TOTALE | REAZIONE FASE | REAZIONE TOTALE |
|---------------|-----------------|---------------|-----------------|
| -1788. | -6448. | -1850. | -5751. |

MODULO ELASTICO ATTUALE CLS 275000.
COEFF. MOLTIPLICATIVO FRECCIA FASE 3.00
VARIAZIONE FRECCIE NELLA FASE E TOTALE CUMULATO

| N. | ASC | VARIAZ.FASE | CUMULATA |
|----|--------|-------------|----------|
| 1 | 50.0 | -0.3791 | 0.5576 |
| 2 | 115.0 | 0.0000 | 0.0000 |
| 3 | 250.0 | 0.7704 | -1.1519 |
| 4 | 500.0 | 1.8571 | -2.3848 |
| 5 | 707.5 | 2.1696 | -2.7130 |
| 6 | 900.0 | 1.8995 | -2.4192 |
| 7 | 1100.0 | 1.1084 | -1.5541 |
| 8 | 1300.0 | -0.0083 | 0.0116 |

| FRECCIA | FASE | MASSIMA | ASC = | VALORE = |
|---------|------|---------|-------|----------|
| FRECCIA | FASE | MINIMA | 707.5 | 2.1696 |
| | | | 5.0 | -0.6416 |

| FRECCIA ACCUMULATA | MASSIMA | ASC = | VALORE = |
|--------------------|---------|-------|----------|
| FRECCIA ACCUMULATA | MINIMA | 5.0 | 0.9383 |
| | | 707.5 | -2.7130 |

LEGENDA - U.M. Forze = DaN - Momenti = DaN x cm - Sigma = DaN / cm2

Nv = Sforzo assiale dovuto a carichi esterni : >0 compressione
Myv = Momento dei carichi attorno all' asse yy verticale : >0 teso lembo sinistro
Mzv = Momento dei carichi attorno all' asse zz orizzontale : >0 teso lembo inferiore
Np = Sforzo assiale dovuto alla precompressione (comprese perdite) : >0 compressione
Myp = Momento dovuto a Np attorno all' asse yy verticale : >0 teso lembo sinistro
Mzp = Momento dovuto a Np attorno all' asse zz orizzontale : >0 teso lembo inferiore
Myt = Incremento del Momento attorno all' asse yy verticale di traslazione per Taglio : agli SLE SOLO per sezioni NON precompresse
Mzt = Incremento del Momento attorno all' asse zz orizzontale di traslazione per Taglio : agli SLE SOLO per sezioni NON precompresse
Simbolo per Sigma : P = Sezione Parzializzata - per le sezioni nella zona di diffusione

| SFORZI | Totali di | I fase | ZZ | Precompressione | ZZ | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-----------|-------------|--------------|-----------------|--------------|-------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt | |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.43213E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.64722E+06 | 0.66449E+05 | -0.14242E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.14615E+07 | 0.97969E+05 | -0.19252E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.16777E+07 | 0.98315E+05 | -0.19321E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.15054E+07 | 0.97382E+05 | -0.19135E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.94621E+06 | 0.66041E+05 | -0.14155E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

-- FASE 8 -- carico perm. fase II qperm. 190 daN/m

| N. | TIPO | X INIZIO | X FINE | VALORE_INI | VALORE_FINE | ECCENT.Z | QUOTA_Y | DIREZIONE |
|----|-------------------|----------|--------|------------|-------------|----------|---------|-----------|
| 1 | FORZA DISTRIBUITA | 0.0 | 1310.0 | 2.50 | 2.50 | 0.00 | 0.00 | VERTICALE |
| 2 | FORZA DISTRIBUITA | 140.0 | 1295.0 | 0.75 | 0.75 | 0.00 | 0.00 | VERTICALE |

| CARATTERISTICHE DELLE SEZIONI | | | | | | | |
|-------------------------------|--------|------|-----|------|-------------|--------------|--|
| N. | ASC | YIT | YST | YSS | AREA | MOM. INERZIA | |
| 1 | 50.0 | 32.5 | 7.5 | 12.5 | 0.38640E+04 | 0.57382E+06 | |
| 2 | 115.0 | 31.4 | 8.6 | 13.6 | 0.40525E+04 | 0.67728E+06 | |
| 3 | 250.0 | 32.3 | 7.7 | 12.7 | 0.38974E+04 | 0.59703E+06 | |
| 4 | 500.0 | 32.2 | 7.8 | 12.8 | 0.39140E+04 | 0.60454E+06 | |
| 5 | 707.5 | 32.2 | 7.8 | 12.8 | 0.39140E+04 | 0.60454E+06 | |
| 6 | 900.0 | 32.2 | 7.8 | 12.8 | 0.39140E+04 | 0.60454E+06 | |
| 7 | 1100.0 | 32.3 | 7.7 | 12.7 | 0.38974E+04 | 0.59703E+06 | |
| 8 | 1300.0 | 32.5 | 7.5 | 12.5 | 0.38640E+04 | 0.57382E+06 | |

CARATTERISTICHE DI SOLLECITAZIONE

VALORI INCREMENTALI DELLA FASE

FRAZ.TORC.(*)=Fraz. del mom.torc. totale (di competenza di trave+getto) attribuito alla sola trave avendo lasciato al getto il 0.% del mom.torc. di sua competenza teorica (da rapporto inerzie)

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | FRAZ.TORC.(*) |
|----|-------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50. | 0.00000E+00 | -0.31250E+04 | -0.12500E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 2 | 115. | 0.00000E+00 | -0.16531E+05 | -0.28750E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 3 | 250. | 0.00000E+00 | 0.21547E+06 | 0.15009E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 4 | 500. | 0.00000E+00 | 0.48914E+06 | 0.68841E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 5 | 707. | 0.00000E+00 | 0.56202E+06 | 0.14035E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 6 | 900. | 0.00000E+00 | 0.50450E+06 | -0.61159E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 7 | 1100. | 0.00000E+00 | 0.31718E+06 | -0.12616E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 8 | 1300. | 0.00000E+00 | -0.12475E+03 | 0.25000E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

VALORI TOTALI DOVUTI AI CARICHI

TORC.TRAVE(*)=Frazione del mom.torcente totale attribuito alla sola trave usato per il calcolo delle TAU di torsione nella trave

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | TORC.TRAVE(*) |
|----|--------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50.0 | 0.00000E+00 | -0.11294E+05 | -0.45175E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.59744E+05 | -0.10390E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.86269E+06 | 0.59688E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.19507E+07 | 0.27350E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.22397E+07 | 0.51023E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.20099E+07 | -0.24390E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.12634E+07 | -0.50260E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | -0.45141E+03 | 0.43708E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

APPOGGIO DI SINISTRA XR1= 115.0 APPOGGIO DI DESTRA XR2= 1300.0

| REAZIONE FASE | REAZIONE TOTALE | REAZIONE FASE | REAZIONE TOTALE |
|---------------|-----------------|---------------|-----------------|
| -2208. | -8657. | -1933. | -7684. |

MODULO ELASTICO ATTUALE CLS 275000.
COEFF. MOLTIPLICATIVO FRECCIA FASE 3.00
VARIAZIONE FRECCIE NELLA FASE E TOTALE CUMULATO

| N. | ASC | VARIAZ.FASE | CUMULATA |
|----|--------|-------------|----------|
| 1 | 50.0 | -0.2553 | 0.3023 |
| 2 | 115.0 | 0.0000 | 0.0000 |
| 3 | 250.0 | 0.5216 | -0.6303 |
| 4 | 500.0 | 1.2634 | -1.1214 |
| 5 | 707.5 | 1.4794 | -1.2335 |
| 6 | 900.0 | 1.2973 | -1.1218 |
| 7 | 1100.0 | 0.7578 | -0.7963 |
| 8 | 1300.0 | -0.0057 | 0.0059 |

FRECCIA FASE MASSIMA ASC = 707.5 VALORE = 1.4794
FRECCIA FASE MINIMA ASC = 5.0 VALORE = -0.4319

FRECCIA ACCUMULATA MASSIMA ASC = 5.0 VALORE = 0.5064
FRECCIA ACCUMULATA MINIMA ASC = 707.5 VALORE = -1.2335

LEGENDA - U.M. Forze = DaN - Momenti = DaN x cm - Sigma = DaN / cm2

Nv = Sforzo assiale dovuto a carichi esterni : >0 compressione
Myv = Momento dei carichi attorno all' asse yy verticale : >0 teso lembo sinistro
Mzv = Momento dei carichi attorno all' asse zz orizzontale : >0 teso lembo inferiore
Np = Sforzo assiale dovuto alla precompressione (comprese perdite) : >0 compressione
Myp = Momento dovuto a Np attorno all' asse yy verticale : >0 teso lembo sinistro
Mzp = Momento dovuto a Np attorno all' asse zz orizzontale : >0 teso lembo inferiore
Myt = Incremento del Momento attorno all' asse yy verticale di traslazione per Taglio : agli SLE SOLO per sezioni NON precomprese
Mzt = Incremento del Momento attorno all' asse zz orizzontale di traslazione per Taglio : agli SLE SOLO per sezioni NON precomprese
Simbolo per Sigma : P = Sezione Parzializzata - per le sezioni nella zona di diffusione

| SFORZI | Totali di | I fase ZZ | Precompressione ZZ | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-----------|-------------|--------------------|-------------|--------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Myv | Myp | Myt |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.43213E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.64722E+06 | 0.66449E+05 | -0.14242E+07 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.14615E+07 | 0.97969E+05 | -0.19252E+07 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.16777E+07 | 0.98315E+05 | -0.19321E+07 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.15054E+07 | 0.97382E+05 | -0.19135E+07 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.94621E+06 | 0.66041E+05 | -0.14155E+07 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| SFORZI | Totali di | II fase ZZ | Precompressione ZZ | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-----------|-------------|--------------------|-------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Myv | Myp | Myt |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.16531E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.21547E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.48914E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.56202E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

6 900.0 0.00000E+00 0.50450E+06 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
71100.0 0.00000E+00 0.31718E+06 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
81300.0 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00

-- FASE 9 -- SECONDA FASE PERDITE (50%)

PERDITE PER RILASSAMENTO DELLE ARMATURE PRETESE

COEFF. C = 9.0 CADUTA A 1000 ORE = 297.0 CADUTA A T > DI 2000 ORE = 337.5

PERDITE PER VISCOSITA' - COEFF = 2.30

PERDITE PER RITIRO - COEFF=0.00030

FRAZIONI DELLE PERDITE SCONTATE NELLA FASE

RILASS RITIRO VISCOS

ARMATURE

PRETESE 0.50 0.50 0.50

CARATTERISTICHE DI SOLLECITAZIONE

VALORI INCREMENTALI DELLA FASE

FRAZ.TORC.(*)=Fraz. del mom.torc. totale (di competenza di trave+getto) attribuito alla sola trave avendo lasciato al getto il 0.% del mom.torc. di sua competenza teorica (da rapporto inerzie)

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | FRAZ.TORC.(*) |
|----|-------|--------------|-------------|-------------|--------------|-------------|-------------|---------------|
| 1 | 50. | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 2 | 115. | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 3 | 250. | -0.52118E+04 | 0.13689E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 4 | 500. | -0.65916E+04 | 0.16168E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 5 | 707. | -0.56936E+04 | 0.13942E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 6 | 900. | -0.63467E+04 | 0.15561E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 7 | 1100. | -0.42391E+04 | 0.11134E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 8 | 1300. | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

VALORI TOTALI DOVUTI AI CARICHI

TORC.TRAVE(*)=Frazione del mom.torc. totale attribuito alla sola trave usato per il calcolo delle TAU di torsione nella trave

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | TORC.TRAVE(*) |
|----|--------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50.0 | 0.00000E+00 | -0.11294E+05 | -0.45175E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.59744E+05 | -0.10390E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.86269E+06 | 0.59688E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.19507E+07 | 0.27350E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.22397E+07 | 0.51023E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.20099E+07 | -0.24390E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.12634E+07 | -0.50260E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | -0.45141E+03 | 0.43708E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

APPOGGIO DI SINISTRA XR1= 115.0 APPOGGIO DI DESTRA XR2= 1300.0

| REAZIONE FASE | REAZIONE TOTALE | REAZIONE FASE | REAZIONE TOTALE |
|---------------|-----------------|---------------|-----------------|
| 0. | -8657. | 0. | -7684. |

MODULO ELASTICO ATTUALE CLS 275000.

COEFF. MULTIPLICATIVO FRECCIA FASE 3.00

VARIAZIONE FRECCIE NELLA FASE E TOTALE CUMULATO

| N. | ASC | VARIAZ.FASE | CUMULATA |
|----|--------|-------------|----------|
| 1 | 50.0 | -0.0764 | 0.2259 |
| 2 | 115.0 | 0.0000 | 0.0000 |
| 3 | 250.0 | 0.1533 | -0.4770 |
| 4 | 500.0 | 0.3453 | -0.7761 |
| 5 | 707.5 | 0.3976 | -0.8360 |
| 6 | 900.0 | 0.3469 | -0.7750 |
| 7 | 1100.0 | 0.2084 | -0.5878 |
| 8 | 1300.0 | -0.0016 | 0.0043 |

| FRECCIA | FASE | MASSIMA | ASC = | VALORE = |
|---------|------|---------|-------|----------|
| FRECCIA | FASE | MINIMA | 707.5 | 0.3976 |
| | | | 5.0 | -0.1292 |

| FRECCIA ACCUMULATA | MASSIMA | ASC = | VALORE = |
|--------------------|---------|-------|----------|
| FRECCIA ACCUMULATA | MINIMA | 5.0 | 0.3772 |
| | | 707.5 | -0.8360 |

VERIFICHE FLESSIONALI

LEGENDA - U.M. Forze = DaN - Momenti = DaN x cm - Sigma = DaN / cm2
Nv = Sforzo assiale dovuto a carichi esterni : >0 compressione

Myv = Momento dei carichi attorno all' asse yy verticale : >0 teso lembo sinistro
Mzv = Momento dei carichi attorno all' asse zz orizzontale : >0 teso lembo inferiore
Np = Sforzo assiale dovuto alla precompressione (comprese perdite) : >0 compressione
Myp = Momento dovuto a Np attorno all' asse yy verticale : >0 teso lembo sinistro
Mzp = Momento dovuto a Np attorno all' asse zz orizzontale : >0 teso lembo inferiore
Myt = Incremento del Momento attorno all' asse yy verticale di traslazione per Taglio : agli SLE SOLO per sezioni NON precompresse
Mzt = Incremento del Momento attorno all' asse zz orizzontale di traslazione per Taglio : agli SLE SOLO per sezioni NON precompresse
Simbolo per Sigma : P = Sezione Parzializzata - per le sezioni nella zona di diffusione

| SFORZI | Totali di | I fase ZZ | Precompressione ZZ | | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-----------|-------------|--------------------|-------------|--------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.43213E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.64722E+06 | 0.66449E+05 | -0.14242E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.14615E+07 | 0.97969E+05 | -0.19252E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.16777E+07 | 0.98315E+05 | -0.19321E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.15054E+07 | 0.97382E+05 | -0.19135E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.94621E+06 | 0.66041E+05 | -0.14155E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| SFORZI | Totali di | II fase ZZ | Precompressione ZZ | | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-----------|--------------|--------------------|-------------|-------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.16531E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | -0.52118E+04 | 0.35236E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | -0.65916E+04 | 0.65082E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | -0.56936E+04 | 0.70144E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | -0.63467E+04 | 0.66012E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | -0.42391E+04 | 0.42853E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| TENSIONI | sigma c trave | | variazione | | Barre trave | | Sigma Trefoli | | sigmac getto | | Barre getto | |
|----------|---------------|--------|------------|------|-------------|--------|---------------|-------|--------------|------|-------------|--------|
| N. ASC. | SUP. | INF. | SUP. | INF. | traz. | compr. | totale | incr. | SUP. | INF. | traz. | compr. |
| 1 | 50.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0 | 0 |
| 2 | 115.0 | -1.5 * | 3.3 | 0.0 | 0 | 34 | -12659 | -19 | -0.3 | -0.2 | 0 | 0 |
| 3 | 250.0 | 4.0 | 57.8 | 0.4 | -8.7 | 0 | -11212 | -177 | 6.2 | 3.2 | 0 | 0 |
| 4 | 500.0 | 29.1 | 31.7 | 0.4 | -10.3 | 0 | -10960 | -181 | 12.1 | 6.7 | 0 | 0 |
| 5 | 707.5 | 36.6 | 15.2 | 0.3 | -8.9 | 0 | -11042 | -158 | 13.4 | 7.6 | 0 | 0 |
| 6 | 900.0 | 30.7 | 27.3 | 0.4 | -9.9 | 0 | -10952 | -174 | 12.4 | 6.9 | 0 | 0 |
| 7 | 1100.0 | 14.7 | 32.8 | 0.4 | -7.1 | 0 | -11290 | -139 | 8.1 | 4.5 | 0 | 0 |
| 8 | 1300.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0 | 0.0 | 0.0 | 0 | 0 |

-- FASE 10 -- carico acc. 300 daN/m

| N. | TIPO | X INIZIO | X FINE | VALORE_INI. | VALORE_FINE | ECCENT.Z | QUOTA_Y | DIREZIONE |
|----|-------------------|----------|--------|-------------|-------------|----------|---------|-----------|
| 1 | FORZA DISTRIBUITA | 0.0 | 1310.0 | 3.00 | 3.00 | 0.00 | 0.00 | VERTICALE |

CARATTERISTICHE DI SOLLECITAZIONE

-combinazione di carico quasi permanente

coeff. psi dei variabili per la combinazione = 0.20

VALORI INCREMENTALI DELLA FASE

FRAZ.TORC.(*)=Fraz. del mom.torc. totale (di competenza di trave+getto) attribuito alla sola trave avendo lasciato al getto il 0.% del mom.torc. di sua competenza teorica (da rapporto inerzie)

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | FRAZ.TORC.(*) |
|----|-------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50. | 0.00000E+00 | -0.75000E+03 | -0.30000E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 2 | 115. | 0.00000E+00 | -0.39675E+04 | -0.69000E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 3 | 250. | 0.00000E+00 | 0.39006E+05 | 0.27782E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 4 | 500. | 0.00000E+00 | 0.89712E+05 | 0.12782E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 5 | 707.5 | 0.00000E+00 | 0.10332E+06 | 0.33228E+01 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 6 | 900. | 0.00000E+00 | 0.92841E+05 | -0.11218E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 7 | 1100. | 0.00000E+00 | 0.58405E+05 | -0.23218E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 8 | 1300. | 0.00000E+00 | -0.29979E+02 | 0.60000E+01 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

VALORI TOTALI DOVUTI AI CARICHI

TORC.TRAVE(*)=Frazione del mom.torc. totale attribuito alla sola trave usato per il calcolo delle TAU di torsione nella trave

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | TORC.TRAVE(*) |
|----|--------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50.0 | 0.00000E+00 | -0.12044E+05 | -0.48175E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.63711E+05 | -0.11080E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.90170E+06 | 0.62466E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.20404E+07 | 0.28629E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.23430E+07 | 0.54346E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.21027E+07 | -0.25511E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.13218E+07 | -0.52581E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | -0.48139E+03 | 0.43768E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

APPOGGIO DI SINISTRA XR1= 115.0 APPOGGIO DI DESTRA XR2= 1300.0

REAZIONE FASE REAZIONE TOTALE REAZIONE FASE REAZIONE TOTALE
-428. -9084. -358. -8042.

MODULO ELASTICO ATTUALE CLS 275000.
COEFF. MOLTIPLICATIVO FRECCIA FASE 2.10
VARIAZIONE FRECCIE NELLA FASE E TOTALE CUMULATO
N. ASC VARIAZ.FASE CUMULATA

| | | | |
|---|--------|---------|---------|
| 1 | 50.0 | -0.0327 | 0.1932 |
| 2 | 115.0 | 0.0000 | 0.0000 |
| 3 | 250.0 | 0.0669 | -0.4101 |
| 4 | 500.0 | 0.1623 | -0.6138 |
| 5 | 707.5 | 0.1902 | -0.6457 |
| 6 | 900.0 | 0.1669 | -0.6081 |
| 7 | 1100.0 | 0.0975 | -0.4903 |
| 8 | 1300.0 | -0.0007 | 0.0036 |

FRECCIA FASE MASSIMA ASC = 707.5 VALORE = 0.1902
FRECCIA FASE MINIMA ASC = 5.0 VALORE = -0.0553

FRECCIA ACCUMULATA MASSIMA ASC = 5.0 VALORE = 0.3219
FRECCIA ACCUMULATA MINIMA ASC = 671.5 VALORE = -0.6463

VERIFICHE FLESSIONALI

LEGENDA - U.M. Forze = DaN - Momenti = DaN x cm - Sigma = DaN / cm2
Nv = Sforzo assiale dovuto a carichi esterni : >0 compressione
Myv = Momento dei carichi attorno all' asse yy verticale : >0 teso lembo sinistro
Mzv = Momento dei carichi attorno all' asse zz orizzontale : >0 teso lembo inferiore
Np = Sforzo assiale dovuto alla precompressione (comprese perdite) : >0 compressione
Myp = Momento dovuto a Np attorno all' asse yy verticale : >0 teso lembo sinistro
Mzp = Momento dovuto a Np attorno all' asse zz orizzontale : >0 teso lembo inferiore
Myt = Incremento del Momento attorno all' asse yy verticale di traslazione per Taglio : agli SLE SOLO per sezioni NON precompresse
Mzt = Incremento del Momento attorno all' asse zz orizzontale di traslazione per Taglio : agli SLE SOLO per sezioni NON precompresse
Simbolo per Sigma : P = Sezione Parzializzata - per le sezioni nella zona di diffusione

| SFORZI | Totali di | I fase | ZZ | Precompressione | ZZ | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-----------|-------------|--------------|-----------------|--------------|-------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt | |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.43213E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.64722E+06 | 0.66449E+05 | -0.14242E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.14615E+07 | 0.97969E+05 | -0.19252E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.16777E+07 | 0.98315E+05 | -0.19321E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.15054E+07 | 0.97382E+05 | -0.19135E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.94621E+06 | 0.66041E+05 | -0.14155E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| SFORZI | Totali di | II fase | ZZ | Precompressione | ZZ | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-----------|--------------|--------------|-----------------|-------------|-------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt | |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.20499E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | -0.52118E+04 | 0.39137E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | -0.65916E+04 | 0.74053E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | -0.56936E+04 | 0.80476E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | -0.63467E+04 | 0.75296E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | -0.42391E+04 | 0.48693E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| TENSIONI | sigma c trave | variazione | Barre trave | Sigma Trefoli | sigmac getto | Barre getto |
|----------|---------------|------------|--------------|---------------|--------------|--------------|
| N. ASC. | SUP. INF. | SUP. INF. | traz. compr. | totale incr. | SUP. INF. | traz. compr. |
| 1 | 50.0 | 0.0 0.0 | 0.0 0.0 | 0 0 | 0.0 0.0 | 0 0 |
| 2 | 115.0 | -1.6 3.5 | -0.1 0.2 | 0 36 | -12657 -20 | -0.4 -0.3 |
| 3 | 250.0 | 4.5 55.7 | 0.5 -2.1 | 0 0 | -11218 -172 | 7.0 3.7 |
| 4 | 500.0 | 30.2 26.9 | 1.2 -4.8 | 0 0 | -10972 -171 | 14.0 7.9 |
| 5 | 707.5 | 37.9 9.7 | 1.3 -5.5 | 0 0 | -11056 -147 | 15.6 9.0 |
| 6 | 900.0 | 31.9 22.3 | 1.2 -4.9 | 0 0 | -10965 -164 | 14.4 8.1 |
| 7 | 1100.0 | 15.5 29.6 | 0.8 -3.2 | 0 0 | -11298 -133 | 9.3 5.2 |
| 8 | 1300.0 | 0.0 0.0 | 0.0 0.0 | 0 0 | 0.0 0.0 | 0.0 0.0 |

VERIFICA ALLA FESSURAZIONE

ambiente poco aggressivo - Sigma fessurazione (DaN/cm2) : cls trave = -32.0 - cls getto = -33.0

| SEZ | ASC. | MOM.FES | MOM.CAR | KFESS | |
|-----|--------|--------------|--------------|-------|--|
| 2 | 115.0 | -0.15886E+07 | -0.63711E+05 | 3.00 | lembo superiore getto : Mom. fessur. di Formazione Fessure |
| 3 | 250.0 | 0.25232E+07 | 0.90170E+06 | 2.80 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |
| 4 | 500.0 | 0.31458E+07 | 0.20404E+07 | 1.54 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |
| 5 | 707.5 | 0.31264E+07 | 0.23430E+07 | 1.33 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |
| 6 | 900.0 | 0.31225E+07 | 0.21027E+07 | 1.48 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |
| 7 | 1100.0 | 0.24607E+07 | 0.13218E+07 | 1.86 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |

CARATTERISTICHE DI SOLLECITAZIONE

-combinazione di carico frequente

coeff. psi dei variabili per la combinazione = 0.50

VALORI INCREMENTALI DELLA FASE

FRAZ.TORC.(*)=Fraz. del mom.torc. totale (di competenza di trave+getto) attribuito alla sola trave avendo lasciato al getto il 0.% del mom.torc. di sua competenza teorica (da rapporto inerzie)

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | FRAZ.TORC.(*) |
|----|-------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50. | 0.00000E+00 | -0.18750E+04 | -0.75000E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 2 | 115. | 0.00000E+00 | -0.99188E+04 | -0.17250E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 3 | 250. | 0.00000E+00 | 0.97515E+05 | 0.69456E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 4 | 500. | 0.00000E+00 | 0.22428E+06 | 0.31956E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 5 | 707. | 0.00000E+00 | 0.25830E+06 | 0.83070E+01 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 6 | 900. | 0.00000E+00 | 0.23210E+06 | -0.28044E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 7 | 1100. | 0.00000E+00 | 0.14601E+06 | -0.58044E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 8 | 1300. | 0.00000E+00 | -0.74947E+02 | 0.15000E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

VALORI TOTALI DOVUTI AI CARICHI

TORC.TRAVE(*)=Frazione del mom.torc. totale attribuito alla sola trave usato per il calcolo delle TAU di torsione nella trave

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | TORC.TRAVE(*) |
|----|--------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50.0 | 0.00000E+00 | -0.13169E+05 | -0.52675E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.69663E+05 | -0.12115E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.96021E+06 | 0.66633E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.21750E+07 | 0.30546E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.24980E+07 | 0.59330E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.22420E+07 | -0.27194E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.14094E+07 | -0.56064E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | -0.52635E+03 | 0.43858E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

APPOGGIO DI SINISTRA XR1= 115.0 APPOGGIO DI DESTRA XR2= 1300.0

| REAZIONE FASE | REAZIONE TOTALE | REAZIONE FASE | REAZIONE TOTALE |
|---------------|-----------------|---------------|-----------------|
| -1070. | -9726. | -895. | -8579. |

MODULO ELASTICO ATTUALE CLS 275000.
COEFF. MOLTIPLICATIVO FRECCIA FASE 1.50
VARIAZIONE FRECCIE NELLA FASE E TOTALE CUMULATO

| N. | ASC | VARIAZ.FASE | CUMULATA |
|----|--------|-------------|----------|
| 1 | 50.0 | -0.0350 | 0.1582 |
| 2 | 115.0 | 0.0000 | 0.0000 |
| 3 | 250.0 | 0.0717 | -0.3384 |
| 4 | 500.0 | 0.1739 | -0.4399 |
| 5 | 707.5 | 0.2038 | -0.4419 |
| 6 | 900.0 | 0.1788 | -0.4293 |
| 7 | 1100.0 | 0.1045 | -0.3859 |
| 8 | 1300.0 | -0.0008 | 0.0028 |

FRECCIA FASE MASSIMA ASC = 707.5 VALORE = 0.2038
FRECCIA FASE MINIMA ASC = 5.0 VALORE = -0.0593

FRECCIA ACCUMULATA MASSIMA ASC = 5.0 VALORE = 0.2627
FRECCIA ACCUMULATA MINIMA ASC = 602.5 VALORE = -0.4481

VERIFICHE FLESSIONALI
.....

| SFORZI | Totali di | I fase | ZZ | Precompressione | ZZ | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-----------|-------------|--------------|-----------------|--------------|-------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Mzt | Myv | Myt | Myt | Myt |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.43213E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.64722E+06 | 0.66449E+05 | -0.14242E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.14615E+07 | 0.97969E+05 | -0.19252E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.16777E+07 | 0.98315E+05 | -0.19321E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.15054E+07 | 0.97382E+05 | -0.19135E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.94621E+06 | 0.66041E+05 | -0.14155E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| SFORZI | Totali di II fase ZZ | | Precompressione ZZ | | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|----------------------|--------------|--------------------|-------------|-------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.26450E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | -0.52118E+04 | 0.44988E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | -0.65916E+04 | 0.87509E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | -0.56936E+04 | 0.95974E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | -0.63467E+04 | 0.89222E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | -0.42391E+04 | 0.57454E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| TENSIONI | sigma c trave | | variazione | | Barre trave | | Sigma Trefoli | | sigmac getto | | Barre getto | | |
|----------|---------------|------|------------|------|-------------|--------|---------------|--------|--------------|------|-------------|--------|---|
| N. ASC. | SUP. | INF. | SUP. | INF. | traz. | compr. | totale | incr. | SUP. | INF. | traz. | compr. | |
| 1 | 50.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0 | 0 | |
| 2 | 115.0 | -1.6 | 3.8 | -0.1 | 0.3 | 0 | 39 | -12655 | -22 | -0.5 | -0.3 | 0 | 0 |
| 3 | 250.0 | 5.3 | 52.5 | 0.8 | -3.2 | 0 | 0 | -11226 | -166 | 8.3 | 4.5 | 0 | 0 |
| 4 | 500.0 | 32.0 | 19.7 | 1.7 | -7.2 | 0 | 0 | -10991 | -156 | 16.9 | 9.6 | 0 | 0 |
| 5 | 707.5 | 39.9 | 1.5 | 2.0 | -8.2 | 0 | 0 | -11078 | -130 | 18.9 | 11.0 | 0 | 0 |
| 6 | 900.0 | 33.8 | 14.9 | 1.8 | -7.4 | 0 | 0 | -10984 | -148 | 17.3 | 9.9 | 0 | 0 |
| 7 | 1100.0 | 16.6 | 24.9 | 1.1 | -4.7 | 0 | 0 | -11310 | -123 | 11.2 | 6.4 | 0 | 0 |
| 8 | 1300.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0.0 | 0.0 | 0 | 0 |

VERIFICA ALLA FESSURAZIONE

ambiente poco aggressivo - Sigma fessurazione (DaN/cm2) : cls trave = -32.0 - cls getto = -33.0

| SEZ | ASC. | MOM.FES | MOM.CAR | KFESS | |
|-----|--------|--------------|--------------|-------|--|
| 2 | 115.0 | -0.15886E+07 | -0.69663E+05 | 3.00 | lembo superiore getto : Mom. fessur. di Formazione Fessure |
| 3 | 250.0 | 0.25232E+07 | 0.96021E+06 | 2.63 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |
| 4 | 500.0 | 0.31458E+07 | 0.21750E+07 | 1.45 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |
| 5 | 707.5 | 0.31264E+07 | 0.24980E+07 | 1.25 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |
| 6 | 900.0 | 0.31225E+07 | 0.22420E+07 | 1.39 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |
| 7 | 1100.0 | 0.24607E+07 | 0.14094E+07 | 1.75 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |

CARATTERISTICHE DI SOLLECITAZIONE

-combinazione di carico rara

coeff. psi dei variabili per la combinazione = 1.00

VALORI INCREMENTALI DELLA FASE

FRAZ.TORC.(*)=Fraz. del mom.torc. totale (di competenza di trave+getto) attribuito alla sola trave avendo lasciato al getto il 0.% del mom.torc. di sua competenza teorica (da rapporto inerzie)

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | FRAZ.TORC.(*) |
|----|-------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50. | 0.00000E+00 | -0.37500E+04 | -0.15000E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 2 | 115. | 0.00000E+00 | -0.19837E+05 | -0.34500E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 3 | 250. | 0.00000E+00 | 0.19503E+06 | 0.13891E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 4 | 500. | 0.00000E+00 | 0.44856E+06 | 0.63911E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 5 | 707. | 0.00000E+00 | 0.51659E+06 | 0.16614E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 6 | 900. | 0.00000E+00 | 0.46420E+06 | -0.56089E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 7 | 1100. | 0.00000E+00 | 0.29203E+06 | -0.11609E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |
| 8 | 1300. | 0.00000E+00 | -0.14989E+03 | 0.30000E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 1.000 |

VALORI TOTALI DOVUTI AI CARICHI

TORC.TRAVE(*)=Frazione del mom.torc. totale attribuito alla sola trave usato per il calcolo delle TAU di torsione nella trave

| N. | ASC | AZ.ASSIALE | MOM.FLETT.Y | TAGLIO Y | MOM.TORCENTE | MOM.FLETT.X | TAGLIO X | TORC.TRAVE(*) |
|----|--------|-------------|--------------|--------------|--------------|-------------|-------------|---------------|
| 1 | 50.0 | 0.00000E+00 | -0.15044E+05 | -0.60175E+03 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.79581E+05 | -0.13840E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.10577E+07 | 0.73579E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.23992E+07 | 0.33741E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.27563E+07 | 0.67637E+02 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.24741E+07 | -0.29999E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.15554E+07 | -0.61869E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | -0.60130E+03 | 0.44008E+04 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

APPOGGIO DI SINISTRA XR1= 115.0 APPOGGIO DI DESTRA XR2= 1300.0

| REAZIONE FASE | REAZIONE TOTALE | REAZIONE FASE | REAZIONE TOTALE |
|---------------|-----------------|---------------|-----------------|
| -2139. | -10796. | -1791. | -9475. |

MODULO ELASTICO ATTUALE CLS 275000.
COEFF. MOLTIPLICATIVO FRECCIA FASE 1.00
VARIAZIONE FRECCIE NELLA FASE E TOTALE CUMULATO

| N. | ASC | VARIAZ.FASE | CUMULATA |
|----|------|-------------|----------|
| 1 | 50.0 | -0.0389 | 0.1192 |

| | | | |
|---|--------|---------|---------|
| 2 | 115.0 | 0.0000 | 0.0000 |
| 3 | 250.0 | 0.0797 | -0.2587 |
| 4 | 500.0 | 0.1932 | -0.2467 |
| 5 | 707.5 | 0.2265 | -0.2155 |
| 6 | 900.0 | 0.1987 | -0.2306 |
| 7 | 1100.0 | 0.1161 | -0.2698 |
| 8 | 1300.0 | -0.0009 | 0.0020 |

| | | | | | | |
|--------------------|---------|---------|-------|----------|----------|---------|
| FRECCIA | FASE | MASSIMA | ASC = | 707.5 | VALORE = | 0.2265 |
| FRECCIA | FASE | MINIMA | ASC = | 5.0 | VALORE = | -0.0658 |
| FRECCIA ACCUMULATA | MASSIMA | ASC = | 5.0 | VALORE = | 0.1968 | |
| FRECCIA ACCUMULATA | MINIMA | ASC = | 286.0 | VALORE = | -0.2818 | |

VERIFICHE FLESSIONALI

| SFORZI | Totali di | I fase | ZZ | Precompressione | ZZ | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-----------|-------------|--------------|-----------------|--------------|-------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt | |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.43213E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | 0.00000E+00 | 0.64722E+06 | 0.66449E+05 | -0.14242E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | 0.00000E+00 | 0.14615E+07 | 0.97969E+05 | -0.19252E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | 0.00000E+00 | 0.16777E+07 | 0.98315E+05 | -0.19321E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | 0.00000E+00 | 0.15054E+07 | 0.97382E+05 | -0.19135E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | 0.00000E+00 | 0.94621E+06 | 0.66041E+05 | -0.14155E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| SFORZI | Totali di | II fase | ZZ | Precompressione | ZZ | Traslaz.ZZ | Totali YY | Precomp.YY | Traslaz.YY |
|----------|-----------|--------------|--------------|-----------------|-------------|-------------|-------------|-------------|-------------|
| N. ABSC. | Nv | Mzv | Np | Mzp | Mzt | Myv | Myp | Myt | |
| 1 | 50.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 2 | 115.0 | 0.00000E+00 | -0.36369E+05 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 3 | 250.0 | -0.52118E+04 | 0.54739E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 4 | 500.0 | -0.65916E+04 | 0.10994E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 5 | 707.5 | -0.56936E+04 | 0.12180E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 6 | 900.0 | -0.63467E+04 | 0.11243E+07 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 7 | 1100.0 | -0.42391E+04 | 0.72056E+06 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |
| 8 | 1300.0 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 | 0.00000E+00 |

| TENSIONI | sigma c trave | variazione | Barre trave | Sigma Trefoli | sigmac getto | Barre getto |
|----------|---------------|------------|--------------|---------------|--------------|---------------|
| N. ASC. | SUP. INF. | SUP. INF. | traz. compr. | totale incr. | SUP. INF. | traz. compr. |
| 1 | 50.0 | 0.0 0.0 | 0.0 0.0 | 0 0 | 0 0 | 0 0 |
| 2 | 115.0 | -1.8 4.2 | -0.1 0.5 | 0 44 | -12652 -25 | -0.7 -0.5 0 0 |
| 3 | 250.0 | 6.5 47.2 | 1.3 -5.3 | 0 0 | -11240 -155 | 10.3 5.8 0 0 |
| 4 | 500.0 | 34.9 7.8 | 2.9 -11.9 | 0 0 | -11021 -131 | 21.6 12.5 0 0 |
| 5 | 707.5 | 43.3 -12.3 | 3.3 -13.7 | 0 0 | -11113 -101 | 24.4 14.3 0 0 |
| 6 | 900.0 | 36.8 2.6 | 3.0 -12.4 | 0 0 | -11016 -123 | 22.2 12.9 0 0 |
| 7 | 1100.0 | 18.5 17.0 | 1.9 -7.9 | 0 0 | -11331 -106 | 14.3 8.2 0 0 |
| 8 | 1300.0 | 0.0 0.0 | 0.0 0.0 | 0 0 | 0 0 | 0.0 0.0 0 0 |

VERIFICA ALLA FESSURAZIONE

ambiente poco aggressivo - Sigma fessurazione (DaN/cm2) : cls trave = -32.0 - cls getto = -33.0

| SEZ | ASC. | MOM.FES | MOM.CAR | KFESS | |
|-----|--------|--------------|--------------|-------|--|
| 2 | 115.0 | -0.15886E+07 | -0.79581E+05 | 3.00 | lembo superiore getto : Mom. fessur. di Formazione Fessure |
| 3 | 250.0 | 0.25232E+07 | 0.10577E+07 | 2.39 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |
| 4 | 500.0 | 0.31458E+07 | 0.23992E+07 | 1.31 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |
| 5 | 707.5 | 0.31264E+07 | 0.27563E+07 | 1.13 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |
| 6 | 900.0 | 0.31225E+07 | 0.24741E+07 | 1.26 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |
| 7 | 1100.0 | 0.24607E+07 | 0.15554E+07 | 1.58 | lembo inferiore trave : Mom. fessur. di Formazione Fessure |

VALORI DI PROGETTO PER LA VERIFICA SCORRIMENTO TRAVE-GETTO

INCREMENTI DEGLI SFORZI E DELLE TENSIONI ALLO SLU DOPO LA SOLIDARIZZAZIONE DEL GETTO - DaN, DaNcm, DaN/cmq
DSST: SIGMA ESTRADOSSO TRAVE - DSIT: SIGMA INTRADOSSO GETTO - DSSS: SIGMA ESTRADOSSO GETTO

| N. | Asc.X. | ASSIALE Ned | MOMENTO Med | TAGLIO Ved | SCORRIMENTO | vEdi | DSST | Limite | DSIS | DSSS | Limite ? |
|----|--------|-------------|--------------|--------------|--------------|-------|-------|---------|------|------|------------|
| 9 | 50.0 | 0.00000E+00 | -0.10312E+05 | -0.41250E+03 | -0.89925E+01 | -0.04 | -0.13 | < 273.9 | -0.1 | -0.2 | < 273.9 OK |
| 14 | 115.0 | 0.00000E+00 | -0.54553E+05 | -0.94875E+03 | -0.19478E+02 | -0.08 | -0.69 | < 273.9 | -0.7 | -1.1 | < 273.9 OK |
| 20 | 250.0 | 0.00000E+00 | 0.61575E+06 | 0.43350E+04 | 0.92888E+02 | 0.37 | 7.98 | < 273.9 | 8.0 | 13.1 | < 273.9 OK |
| 25 | 500.0 | 0.00000E+00 | 0.14065E+07 | 0.19913E+04 | 0.42511E+02 | 0.17 | 18.21 | < 273.9 | 18.2 | 29.8 | < 273.9 OK |
| 30 | 707.5 | 0.00000E+00 | 0.16179E+07 | 0.45973E+02 | 0.98146E+00 | 0.00 | 20.94 | < 273.9 | 20.9 | 34.3 | < 273.9 OK |
| 36 | 900.0 | 0.00000E+00 | 0.14531E+07 | -0.17587E+04 | -0.37546E+02 | -0.15 | 18.81 | < 273.9 | 18.8 | 30.8 | < 273.9 OK |
| 44 | 1100.0 | 0.00000E+00 | 0.91382E+06 | -0.36337E+04 | -0.77861E+02 | -0.31 | 11.84 | < 273.9 | 11.8 | 19.5 | < 273.9 OK |
| 62 | 1300.0 | 0.00000E+00 | -0.41197E+03 | 0.82500E+02 | 0.17985E+01 | 0.01 | -0.01 | < 273.9 | 0.0 | 0.0 | < 273.9 OK |

VERIFICA ALLO SCORRIMENTO ALL' INTERFACCIA CON IL GETTO

FATTORE C=0.00 - FATTORE MU =0.00 - % RIDUZIONE CARICHI DINAMICI= 0%
ARMATURA CONNESSIONE= 0.00 cm2/m DA 0.0 A 150.0 - DA 1160.0 A 1310.0 cm

| N. | ASC. | VEd | C*F'ctd | scpn*mu | vAs | vEdi | vRdi | ? | VAs necessaria | VAs presente (cmq/m) |
|----|--------|--------|---------|---------|------|-------|------|----|----------------|----------------------|
| 9 | 50.0 | -412. | 0.00 | 0.00 | 0.00 | -0.04 | 0.00 | VE | 0.23 | 0.00 |
| 14 | 115.0 | -949. | 0.00 | 0.00 | 0.00 | -0.08 | 0.00 | VE | 0.50 | 0.00 |
| 20 | 250.0 | 4335. | 0.00 | 0.00 | 0.00 | 0.37 | 0.00 | VE | 2.37 | 0.00 |
| 25 | 500.0 | 1991. | 0.00 | 0.00 | 0.00 | 0.17 | 0.00 | VE | 1.09 | 0.00 |
| 30 | 707.5 | 46. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | VE | 0.02 | 0.00 |
| 36 | 900.0 | -1759. | 0.00 | 0.00 | 0.00 | -0.15 | 0.00 | VE | 0.96 | 0.00 |
| 44 | 1100.0 | -3634. | 0.00 | 0.00 | 0.00 | -0.31 | 0.00 | VE | 1.99 | 0.00 |
| 62 | 1300.0 | 82. | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 | VE | 0.05 | 0.00 |

VERIFICA A TAGLIO ALLO STATO ULTIMO DI ROTTURA

METODO NORMALE

Angolo staffe (in gradi sull'orizzontale)= 90.0
 OK = taglio verificato | NO = taglio NON verificato
 NO 1 : area staffe < minimo prescritto dalla Normativa
 NO 2 : area staffe insufficiente < area necessaria totale
 NO 3 : resistenza biella insufficiente

| Dx da X | biella a X | l.concio +/- | Astaffe reali cm2/m | Astaffe minima cm2/m | D/C | Apioli minima cm2/m | cot(teta) biella | Forza tirante DaN | VEd(max) concio DaN | VRcd DaN | VRsd DaN | VRcd VEd | VRsd VEd | VRd VEd | ? |
|---------|------------|--------------|---------------------|----------------------|-----|---------------------|------------------|-------------------|---------------------|----------|----------|----------|----------|---------|----|
| 115. | 156. | 41. | 18.98 | > 5.40 | M | 0.5 | 1.0 | 6478. | 12956. | 85913. | 27412. | 6.63 | 2.12 | 2.12 | OK |
| 116. | 157. | 41. | 18.97 | > 5.40 | M | 2.9 | 1.0 | 6478. | 12956. | 85913. | 27390. | 6.63 | 2.11 | 2.11 | OK |
| 119. | 160. | 41. | 18.94 | > 5.40 | M | 2.9 | 1.0 | 6457. | 12914. | 85913. | 27345. | 6.65 | 2.12 | 2.12 | OK |
| 151. | 192. | 41. | 17.79 | > 5.40 | M | 2.8 | 1.0 | 6159. | 12318. | 85913. | 25695. | 6.97 | 2.09 | 2.09 | OK |
| 210. | 251. | 41. | 5.90 | > 5.40 | M | 2.4 | 1.3 | 7127. | 11022. | 91389. | 11022. | 8.29 | 1.00 | 1.00 | OK |
| 214. | 255. | 41. | 5.65 | > 5.40 | M | 2.4 | 1.3 | 7321. | 10934. | 90546. | 10934. | 8.28 | 1.00 | 1.00 | OK |
| 250. | 291. | 41. | 5.65 | > 5.40 | M | 2.4 | 1.2 | 6300. | 10143. | 92177. | 10143. | 9.09 | 1.00 | 1.00 | OK |
| 286. | 327. | 41. | 5.65 | > 5.40 | M | 2.2 | 1.1 | 5356. | 9353. | 93534. | 9353. | 9.99 | 1.00 | 1.00 | OK |
| 348. | 389. | 41. | 5.65 | > 5.40 | M | 1.9 | 1.0 | 3995. | 7991. | 94461. | 8165. | 9.99 | 1.02 | 1.02 | OK |
| 410. | 451. | 41. | 5.65 | > 5.40 | M | 1.6 | 1.0 | 3314. | 6629. | 94513. | 8165. | 9.99 | 1.23 | 1.23 | OK |
| 464. | 505. | 41. | 5.65 | > 5.40 | M | 1.3 | 1.0 | 2721. | 5443. | 94549. | 8165. | 9.99 | 1.50 | 1.50 | OK |
| 500. | 541. | 41. | 5.65 | > 5.40 | M | 1.1 | 1.0 | 2326. | 4652. | 98360. | 8165. | 9.99 | 1.76 | 1.76 | OK |
| 536. | 577. | 41. | 5.65 | > 5.40 | M | 0.9 | 1.0 | 1930. | 3861. | 98380. | 8165. | 9.99 | 2.11 | 2.11 | OK |
| 602. | 643. | 41. | 5.65 | > 5.40 | M | 0.6 | 1.0 | 1200. | 2400. | 98404. | 8165. | 9.99 | 3.40 | 3.40 | OK |
| 638. | 679. | 41. | 5.65 | > 5.40 | M | 0.4 | 1.0 | 805. | 1610. | 98409. | 8165. | 9.99 | 5.07 | 5.07 | OK |
| 671. | 712. | 41. | 5.65 | > 5.40 | M | 0.2 | 1.0 | 442. | 885. | 98409. | 8165. | 9.99 | 9.23 | 9.23 | OK |
| 666. | 707. | -41. | 5.65 | > 5.40 | M | 0.0 | 1.0 | 223. | 446. | 98404. | 8165. | 9.99 | 9.99 | 9.99 | OK |
| 702. | 743. | -41. | 5.65 | > 5.40 | M | 0.2 | 1.0 | 376. | 752. | 98393. | 8165. | 9.99 | 9.99 | 9.99 | OK |
| 733. | 774. | -41. | 5.65 | > 5.40 | M | 0.3 | 1.0 | 683. | 1367. | 98380. | 8165. | 9.99 | 5.97 | 5.97 | OK |
| 769. | 810. | -41. | 5.65 | > 5.40 | M | 0.5 | 1.0 | 1079. | 2157. | 98360. | 8165. | 9.99 | 3.78 | 3.78 | OK |
| 805. | 846. | -41. | 5.65 | > 5.40 | M | 0.7 | 1.0 | 1474. | 2948. | 98334. | 8165. | 9.99 | 2.77 | 2.77 | OK |
| 823. | 864. | -41. | 5.65 | > 5.40 | M | 0.8 | 1.0 | 1672. | 3344. | 98319. | 8165. | 9.99 | 2.44 | 2.44 | OK |
| 859. | 900. | -41. | 5.65 | > 5.40 | M | 1.0 | 1.0 | 2067. | 4134. | 98285. | 8165. | 9.99 | 1.98 | 1.98 | OK |
| 895. | 936. | -41. | 5.65 | > 5.40 | M | 1.1 | 1.0 | 2462. | 4925. | 94485. | 8165. | 9.99 | 1.66 | 1.66 | OK |
| 921. | 962. | -41. | 5.65 | > 5.40 | M | 1.3 | 1.0 | 2748. | 5496. | 94461. | 8165. | 9.99 | 1.49 | 1.49 | OK |
| 957. | 998. | -41. | 5.65 | > 5.40 | M | 1.5 | 1.0 | 3143. | 6287. | 94426. | 8165. | 9.99 | 1.30 | 1.30 | OK |
| 983. | 1024. | -41. | 5.65 | > 5.40 | M | 1.6 | 1.0 | 3429. | 6858. | 94398. | 8165. | 9.99 | 1.19 | 1.19 | OK |
| 1019. | 1060. | -41. | 5.65 | > 5.40 | M | 1.8 | 1.0 | 3824. | 7649. | 94355. | 8165. | 9.99 | 1.07 | 1.07 | OK |
| 1023. | 1064. | -41. | 5.65 | > 5.40 | M | 1.8 | 1.0 | 3868. | 7737. | 94350. | 8165. | 9.99 | 1.06 | 1.06 | OK |
| 1055. | 1096. | -41. | 5.65 | > 5.40 | M | 2.0 | 1.0 | 4361. | 8440. | 94257. | 8440. | 9.99 | 1.00 | 1.00 | OK |
| 1059. | 1100. | -41. | 5.65 | > 5.40 | M | 2.0 | 1.0 | 4453. | 8527. | 94215. | 8527. | 9.99 | 1.00 | 1.00 | OK |
| 1095. | 1136. | -41. | 5.65 | > 5.40 | M | 2.2 | 1.1 | 5317. | 9318. | 93436. | 9318. | 9.99 | 1.00 | 1.00 | OK |
| 1118. | 1159. | -41. | 5.65 | > 5.40 | M | 2.3 | 1.2 | 5909. | 9823. | 92630. | 9823. | 9.43 | 1.00 | 1.00 | OK |
| 1150. | 1191. | -41. | 5.74 | > 5.40 | M | 2.5 | 1.3 | 6691. | 10531. | 91525. | 10531. | 8.69 | 1.00 | 1.00 | OK |
| 1153. | 1194. | -41. | 5.78 | > 5.40 | M | 2.5 | 1.3 | 6710. | 10586. | 91573. | 10586. | 8.65 | 1.00 | 1.00 | OK |
| 1154. | 1195. | -41. | 5.81 | > 5.40 | M | 2.5 | 1.3 | 6718. | 10614. | 91601. | 10614. | 8.63 | 1.00 | 1.00 | OK |
| 1155. | 1196. | -41. | 6.69 | > 5.40 | M | 2.5 | 1.1 | 5847. | 10629. | 93732. | 10629. | 8.82 | 1.00 | 1.00 | OK |
| 1183. | 1224. | -41. | 7.94 | > 5.40 | M | 2.7 | 1.0 | 5625. | 11251. | 85913. | 11460. | 7.64 | 1.02 | 1.02 | OK |
| 1190. | 1231. | -41. | 8.81 | > 5.40 | M | 2.7 | 1.0 | 5702. | 11405. | 85913. | 12722. | 7.53 | 1.12 | 1.12 | OK |
| 1218. | 1259. | -41. | 9.85 | > 5.40 | M | 2.9 | 1.0 | 6010. | 12020. | 85913. | 14223. | 7.15 | 1.18 | 1.18 | OK |
| 1219. | 1260. | -41. | 9.86 | > 5.40 | M | 2.9 | 1.0 | 6021. | 12042. | 85913. | 14231. | 7.13 | 1.18 | 1.18 | OK |
| 1220. | 1261. | -41. | 9.87 | > 5.40 | M | 2.9 | 1.0 | 6032. | 12064. | 85913. | 14252. | 7.12 | 1.18 | 1.18 | OK |
| 1223. | 1264. | -41. | 9.91 | > 5.40 | M | 2.9 | 1.0 | 6065. | 12130. | 85913. | 14314. | 7.08 | 1.18 | 1.18 | OK |
| 1235. | 1276. | -41. | 10.05 | > 5.40 | M | 2.9 | 1.0 | 6199. | 12398. | 85913. | 14516. | 6.93 | 1.17 | 1.17 | OK |
| 1236. | 1277. | -41. | 10.05 | > 5.40 | M | 2.9 | 1.0 | 6210. | 12420. | 85913. | 14516. | 6.92 | 1.17 | 1.17 | OK |
| 1237. | 1278. | -41. | 10.05 | > 5.40 | M | 3.0 | 1.0 | 6221. | 12442. | 85913. | 14516. | 6.91 | 1.17 | 1.17 | OK |
| 1255. | 1296. | -41. | 10.05 | > 5.40 | M | 3.0 | 1.0 | 6413. | 12827. | 85913. | 14516. | 6.70 | 1.13 | 1.13 | OK |
| 1258. | 1299. | -41. | 10.05 | > 5.40 | M | 3.1 | 1.0 | 6436. | 12873. | 85913. | 14516. | 6.67 | 1.13 | 1.13 | OK |

VERIFICA FLESSIONALE ALLO STATO ULTIMO DI ROTTURA

LEGENDA

Sez. = n° della sezione
 Asc. = ascissa della sezione
 Comb. = n° della combinazione delle azioni

Msd+/- = momento di calcolo positivo/negativo NB. valori massimi fra tutte le fasi fino alla corrente
Mrd+/- = momento resistente di calcolo positivo/negativo
Kr+ = Mrd+/Msd+
Kr- = Mrd-/Msd-
x = distanza asse neutro dal lembo compresso
gammas = fattore di sicurezza parziale delle azioni a sfavore di sicurezza
gammaf = fattore di sicurezza parziale delle azioni a favore di sicurezza
psi = coefficienti di combinazione delle azioni
gammap = fattore di sicurezza parziale per la precompressione
PF = precompressione favorevole
PS = precompressione sfavorevole
Msdfase= momento di calcolo alla fase corrente

COMBINAZIONE DI AZIONI

n. combinazioni = 1
1

| IDFA | tipo fase | gammas | gammaf | psi | n.fase |
|------|------------|--------|--------|------|--------|
| 0 | p.proprio | 1.30 | 1.00 | 1.00 | 2 |
| 2 | permanenti | 1.30 | 1.00 | 1.00 | 6 |
| 3 | permanenti | 1.30 | 1.00 | 1.00 | 7 |
| 4 | permanenti | 1.50 | 1.00 | 1.00 | 8 |
| 1 | variabili | 1.50 | 0.00 | 1.00 | 10 |

Precompressione Sfavorevole (PS):gammap trefoli = 1.00 gammap cavi = 1.00

Precompressione Favorevole (PF) :gammap trefoli = 1.00 gammap cavi = 1.00

Valori gamma : Calcestruzzo | Arm.lente | Arm.Pretese | Arm.Postese
1.50 1.15 1.15 1.15

MOMENTI RESISTENTI DI CALCOLO POSITIVI E NEGATIVI

| Sez. | Asc. | PS/PF | Mrd+/- | x | tipo di crisi |
|------|--------|-------|------------|-------|--------------------|
| 1 | 50.0 | PS | 0.0000E+00 | 0.00 | armat. prec. -tref |
| | | PS | 0.0000E+00 | 0.00 | cls soletta |
| 2 | 115.0 | PS | 0.1776E+07 | 0.95 | armat. prec. -tref |
| | | PS | -.2666E+06 | 5.79 | cls soletta |
| 3 | 250.0 | PS | 0.3445E+07 | 1.74 | armat. prec. -tref |
| | | PS | -.1670E+06 | 7.21 | cls soletta |
| 4 | 500.0 | PS | 0.4896E+07 | 2.61 | armat. prec. -tref |
| | | PS | -.3072E+06 | 10.07 | cls soletta |
| 5 | 707.5 | PS | 0.4896E+07 | 2.61 | armat. prec. -tref |
| | | PS | -.3084E+06 | 10.17 | cls soletta |
| 6 | 900.0 | PS | 0.4896E+07 | 2.61 | armat. prec. -tref |
| | | PS | -.3103E+06 | 10.03 | cls soletta |
| 7 | 1100.0 | PS | 0.3445E+07 | 1.74 | armat. prec. -tref |
| | | PS | -.1674E+06 | 7.23 | cls soletta |
| 8 | 1300.0 | PS | 0.0000E+00 | 0.00 | |
| | | PS | 0.0000E+00 | 0.00 | |

MOMENTI DI PROGETTO E RAPPORTI CON I MOMENTI RESISTENTI DI CALCOLO

| Sez. | Asc. | Comb. | Msd+ | Mrd+ | kr+ | Msd- | Mrd- | kr- | Msdfase |
|------|--------|-------|------------|------------|-------|---------------|------------|-------|---------------|
| 1 | 50.0 | 1 | 0.4665E+06 | 0.0000E+00 | 0.00 | PF -.1107E+06 | 0.0000E+00 | 0.00 | PF -.2093E+05 |
| 2 | 115.0 | 1 | 0.7702E+06 | 0.1776E+07 | 2.31 | PF -.1107E+06 | -.2666E+06 | 2.41 | PF -.1107E+06 |
| 3 | 250.0 | 1 | 0.1666E+07 | 0.3445E+07 | 2.07 | PF 0.2086E+06 | -.1670E+06 | 99.00 | PF 0.1457E+07 |
| 4 | 500.0 | 1 | 0.3365E+07 | 0.4896E+07 | 1.45 | PF 0.5868E+05 | -.3072E+06 | 99.00 | PF 0.3307E+07 |
| 5 | 707.5 | 1 | 0.3799E+07 | 0.4896E+07 | 1.29 | PF 0.4167E+04 | -.3084E+06 | 99.00 | PF 0.3799E+07 |
| 6 | 900.0 | 1 | 0.3436E+07 | 0.4896E+07 | 1.42 | PF 0.2608E+05 | -.3103E+06 | 99.00 | PF 0.3410E+07 |
| 7 | 1100.0 | 1 | 0.2172E+07 | 0.3445E+07 | 1.59 | PF 0.2809E+05 | -.1674E+06 | 99.00 | PF 0.2144E+07 |
| 8 | 1300.0 | 1 | 0.0000E+00 | 0.0000E+00 | 99.00 | PF -.8367E+03 | 0.0000E+00 | 0.00 | PF -.8366E+03 |

Tagli massimi , Reazioni e Area di ferro necessaria agli appoggi

App.Sinistro : x= 115.0

SLU : Taglio.max= 12956. Af inferiore= 1.7 sigma Af= 3913.
SLE : Reazione q.perman.= -9084. frequente= -9726. rara= -10796.
SLU : Reazione Massima = -14904.
SLU : Forza Tirante orizzontale Ftd = 6478.

App.Destro : x= 1300.0

SLU : Taglio.max= 12873. Af inferiore= 1.6 sigma Af= 3913.
SLE : Reazione q.perman.= -8042. frequente= -8579. rara= -9475.
SLU : Reazione Massima = -13062.
SLU : Forza Tirante orizzontale Ftd = 6436.

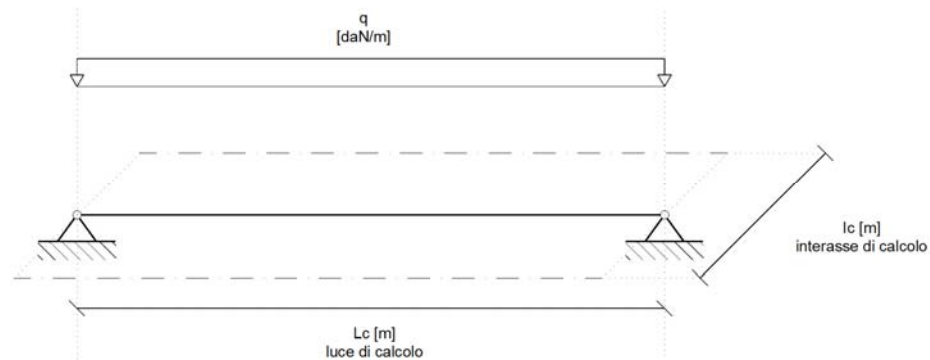
Verifica a taglio SLU NTC 2018 §4.1.2.3.5.2

| VERIFICA A TAGLIO PER ELEMENTI CON ARMATURE TRASVERSALI RESISTENTI A TAGLIO - §4.1.2.3.5 NTC 2018 | | |
|---|--------------------------------|--|
| Lato Calcestruzzo | [4.1.28] | |
| H | 400 mm | Altezza totale sezione |
| d | 340 mm | Altezza utile della sezione |
| bw | 360 mm | Larghezza minima della sezione |
| R_{ck} | 55 N/mm² | Resistenza caratteristica cubica a compressione del cls |
| f _{ck} | 45,65 N/mm ² | Resistenza caratteristica cilindrica a compressione |
| f _{cd} | 25,87 N/mm ² | Resistenza di calcolo a compressione del cls |
| v | 0,50 | |
| f _{cd} | 12,93 N/mm ² | Resistenza a compressione ridotta del cls d'anima (=0.5 f _{cd}) |
| α _{cc} | 0,85 | Coeff. Riduttivo per resistenze di lunga durata |
| γ _C | 1,50 | Coefficiente di sicurezza cls |
| α _c | 1 | Pari a 1 per membrature non compresse |
| α | 90 ° | 1,570796 rad Inclinazione armatura trasversale rispetto asse trave |
| θ | 26 | 0,453786 rad Inclinazione puntone cls rispetto asse trave [21.8° ≤ θ ≤ 45°] |
| V_{ed} | 129560 N | Taglio sollecitante agli SLU |
| V_{Rcd} | 561389,81 N | Resistenza di calcolo a Taglio Compressione [4.1.28] |
| Lato Acciaio | [4.1.27] | |
| A_{sw} | 560,00 mm² | Area armatura trasversale compresa in "s" |
| s | 1000 mm | Interasse tra due armature trasversali consecutive |
| f _{yk} | 450 N/mm ² | Tensione caratteristica di snervamento dell'acciaio |
| γ _s | 1,15 | Coefficiente parziale di sicurezza dell'acciaio |
| K _θ | 1,00 | Coefficiente riduttivo dell'acciaio funzione della temperatura |
| f_{yd} | 391,30 N/mm² | Resistenza di calcolo dell'acciaio |
| α | 90 ° | 1,570796 rad Inclinazione armatura trasversale rispetto asse trave |
| θ | 26 | 0,453786 rad Inclinazione puntone cls rispetto asse trave [21.8° ≤ θ ≤ 45°] |
| V_{Rsd} | 137480,90 N | Resistenza di calcolo a Taglio Trazione [4.1.27] |
| V_{Rd} | 137480,90 N | Resistenza a taglio della Trave [=MIN(V_{Rsd}; V_{Rcd})] [4.1.29] |
| Definizione del Tirante Longitudinale per effetto del solo Taglio - Secondo EC2 §4.3.2.4.4 | | |
| T_d | 132818,68 N | Forza di trazione nelle armature longitudinali tese |
| A_{sL} | 339,43 mm² | Armatura tirante per effetto del solo taglio |

2.2.5.2 Travetti 16x36 L9.00m Ic1.28m

Dati geometrici e caratteristiche del materiale

| | |
|-----------------|------------------------|
| Schema statico | appoggio-appoggio |
| Luce di calcolo | $L_c = 9.00 \text{ m}$ |
| Larghezza base | $b = 16 \text{ cm}$ |
| Altezza | $h = 36 \text{ cm}$ |
| Interasse | $l_c = 128 \text{ cm}$ |
| Inclinazione | $\alpha = 11^\circ$ |
| Materiale | Legno lamellare GL24h |



Analisi dei carichi

| | | |
|--|---|------------------|
| Peso proprio G_1 | | 25 daN/m |
| Permanenti portati G_2 | $90 \text{ daN/m}^2 \times 1.28 \text{ m}$ | 115 daN/m |
| Sovraccarico variabile Q_a | $120 \text{ daN/m}^2 \times 1.28 \text{ m}$ | <u>155 daN/m</u> |
| Totale carico caratteristico distribuito q | | 295 daN/m |

Sollecitazioni di verifica

| Combinazione | Sollecitazioni | |
|--------------|------------------------------|-----------------------------|
| SLE rara | $M_k = 2987 \text{ daNm}$ | $V_k = 1326 \text{ daN}$ |
| SLU | $M_{Ed} = 4430 \text{ daNm}$ | $V_{Ed} = 1970 \text{ daN}$ |

Condizione di verifica

| | |
|------------------------------------|-----------------|
| Classe di servizio | 1 |
| Condizione di carico significativa | Breve durata |
| Coefficiente di durata del carico | $k_{mod} = 0.9$ |

Tabulato di calcolo

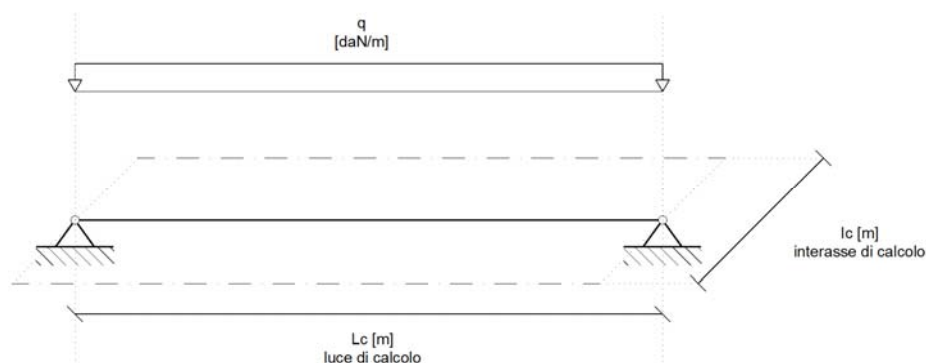
| TRAVI IN LEGNO | | |
|---|-------------------------------|--|
| Caratteristiche meccaniche del legno | | |
| GL 24h | | Classe del legno |
| $\rho_k =$ | 385 kg/m ³ | massa volumica caratteristica |
| $\rho_{mean} =$ | 420 kg/m ³ | massa volumica media |
| $f_{m,k} =$ | 24 MPa | resistenza caratteristica a flessione |
| $f_{t,0,k} =$ | 19,2 MPa | resistenza caratteristica a trazione parallela alle fibre |
| $f_{t,90,k} =$ | 0,5 MPa | resistenza caratteristica a trazione perpendicolare alle fibre |
| $f_{c,0,k} =$ | 24 MPa | resistenza caratteristica a compressione parallela alle fibre |
| $f_{c,90,k} =$ | 2,5 MPa | resistenza caratteristica a compressione perpendicolare alle fibre |
| $f_{v,k} =$ | 3,5 MPa | resistenza caratteristica a taglio |
| $E_{0,mean} =$ | 11500 MPa | modulo di elasticità medio parallelo alle fibre |
| $E_{90,mean} =$ | 300 MPa | modulo di elasticità medio perpendicolare alle fibre |
| $G_{mean} =$ | 650 MPa | modulo di elasticità tangenziale medio |
| $k_{mod} =$ | 0,90 | coeff. funzione delle condizioni ambientali |
| $\gamma_m =$ | 1,45 | coefficiente di sicurezza del legno |
| $k_h =$ | 1,05 | coefficiente di forma |
| $f_{m,d} =$ | 15,6 MPa | resistenza di progetto a flessione |
| $f_{t,0,d} =$ | 12,5 MPa | resistenza di progetto a trazione parallela alle fibre |
| $f_{t,90,d} =$ | 0,3 MPa | resistenza di progetto a trazione perpendicolare alle fibre |
| $f_{c,0,d} =$ | 15,6 MPa | resistenza di progetto a compressione parallela alle fibre |
| $f_{c,90,d} =$ | 1,6 MPa | resistenza di progetto a compressione perpendicolare alle fibre |
| $f_{v,d} =$ | 2,3 MPa | resistenza di progetto a taglio |
| Carichi applicati | | |
| $g_{k1} =$ | 0,00 kN/m ² | carico caratteristico permanente |
| $g_{k2} =$ | 0,90 kN/m ² | carico caratteristico permanente portato |
| $q_k =$ | 1,20 kN/m ² | carico caratteristico variabile |
| $i =$ | 1,280 m | interasse |
| $g_{k1} =$ | 0,288 kN/m | carico caratteristico permanente |
| $g_{k2} =$ | 1,15 kN/m | carico caratteristico permanente portato |
| $q_k =$ | 1,54 kN/m | carico caratteristico variabile |
| SLU: | | |
| $\gamma_{G1} =$ | 1,30 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,50 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,50 | coefficiente parziale per carichi variabili |
| $F_d =$ | 4,41 | carico uniforme di progetto |
| SLE - combinazione rara: | | |
| $\gamma_{G1} =$ | 1,00 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,00 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,00 | coefficiente parziale per carichi variabili |
| $\psi_{01} =$ | 1,00 | coefficiente di combinazione |
| $F_d =$ | 2,98 | carico uniforme di progetto |
| SLE - combinazione frequente: | | |
| $\gamma_{G1} =$ | 1,00 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,00 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,00 | coefficiente parziale per carichi variabili |
| $\psi_{11} =$ | 0,50 | coefficiente di combinazione |
| $F_d =$ | 0,00 | carico uniforme di progetto |
| SLE - combinazione quasi permanente | | |
| $\gamma_{G1} =$ | 1,00 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,00 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,00 | coefficiente parziale per carichi variabili |
| $\psi_{21} =$ | 0,30 | coefficiente di combinazione |
| $F_d =$ | 1,90 | carico uniforme di progetto |

| Caratteristiche geometriche | | | | |
|-----------------------------|----------|-----------------|------------|---|
| b = | 160 | mm | | base della sezione reagente |
| h = | 360 | mm | | altezza della sezione reagente |
| A = | 5,76E+04 | mm ² | | area della sezione reagente |
| W = | 3,46E+06 | mm ³ | | modulo di resistenza della sezione |
| I = | 6,22E+08 | mm ⁴ | | momento d'inerzia della sezione |
| L = | 9.000 | mm | | lunghezza della trave |
| b _y = | 150 | mm | | lunghezza appoggio |
| S = | 2,40E+04 | mm ² | | superficie di appoggio della trave |
| Verifiche SLU | | | | |
| M _{SLU} = | 44,615 | kNm | | momento flettente a SLU |
| V _{SLU} = | 19,829 | kN | | sforzo di taglio a SLU |
| σ _{m,0,d} = | 12,9 | MPa | < 15,6 MPa | Verificato tensione normale a SLU |
| k _{cr} = | 0,71 | | | coefficiente correttivo per larghezza efficace |
| τ _d = | 0,73 | MPa | < 2,3 MPa | Verificato tensione tangenziale a SLU |
| σ _{c,90,d} = | 0,8 | MPa | < 1,6 MPa | Verificato tensione ortogonale alla fibratura a SLU |
| Verifiche SLE | | | | |
| k _{def} = | 0,60 | | | |
| f _g = | 15,50 | mm | | freccia dovuta ai carichi permanenti |
| f _q = | 17,20 | mm | | freccia dovuta ai carichi variabili |
| f _{q,t=0} = | 17,20 | mm | | freccia a tempo zero dovuta ai soli carichi variabili |
| f _{lim=L/300} = | 30,0 | mm | | freccia limite a tempo zero |
| f _{t=inf} = | 45,09 | mm | | freccia a tempo infinito - COMBINAZIONE QUASI PERMANENTE |
| f _{lim=L/200} = | 45,00 | mm | | freccia limite a tempo infinito |

2.2.5.3 Travetti 16x30 L4.60m lc1.28m

Dati geometrici e caratteristiche del materiale

| | |
|-----------------|-----------------------|
| Schema statico | appoggio-appoggio |
| Luce di calcolo | $L_c = 4.60$ m |
| Larghezza base | $b = 16$ cm |
| Altezza | $h = 30$ cm |
| Interasse | $l_c = 128$ cm |
| Inclinazione | $\alpha = 11^\circ$ |
| Materiale | Legno lamellare GL24h |



Analisi dei carichi

| | | |
|--|---|------------------|
| Peso proprio G_1 | | 25 daN/m |
| Permanenti portati G_2 | $90 \text{ daN/m}^2 \times 1.28 \text{ m}$ | 115 daN/m |
| Sovraccarico variabile Q_a | $120 \text{ daN/m}^2 \times 1.28 \text{ m}$ | <u>155 daN/m</u> |
| Totale carico caratteristico distribuito q | | 295 daN/m |

Sollecitazioni di verifica

| Combinazione | Sollecitazioni | |
|--------------|----------------------|---------------------|
| SLE rara | $M_k = 780$ daNm | $V_k = 680$ daN |
| SLU | $M_{Ed} = 1160$ daNm | $V_{Ed} = 1006$ daN |

Condizione di verifica

| | |
|------------------------------------|-----------------|
| Classe di servizio | 1 |
| Condizione di carico significativa | Breve durata |
| Coefficiente di durata del carico | $k_{mod} = 0.9$ |

Tabulato di calcolo

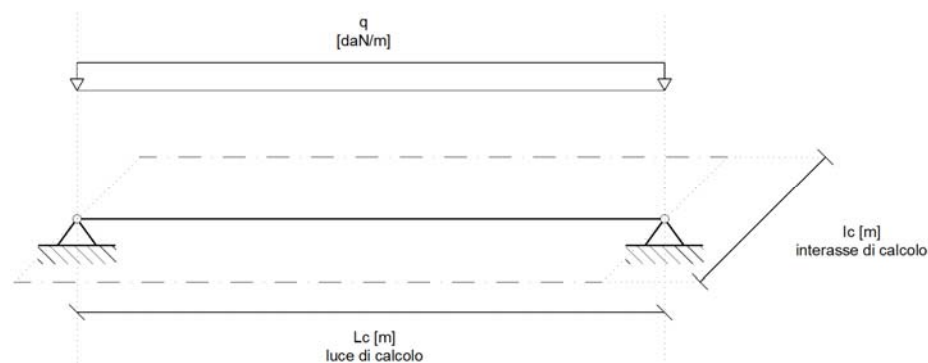
| TRAVI IN LEGNO | | |
|---|-------------------------------|--|
| <i>Caratteristiche meccaniche del legno</i> | | |
| GL 24h | | <i>Classe del legno</i> |
| $\rho_k =$ | 385 kg/m ³ | massa volumica caratteristica |
| $\rho_{mean} =$ | 420 kg/m ³ | massa volumica media |
| $f_{m,k} =$ | 24 MPa | resistenza caratteristica a flessione |
| $f_{t,0,k} =$ | 19,2 MPa | resistenza caratteristica a trazione parallela alle fibre |
| $f_{t,90,k} =$ | 0,5 MPa | resistenza caratteristica a trazione perpendicolare alle fibre |
| $f_{c,0,k} =$ | 24 MPa | resistenza caratteristica a compressione parallela alle fibre |
| $f_{c,90,k} =$ | 2,5 MPa | resistenza caratteristica a compressione perpendicolare alle fibre |
| $f_{v,k} =$ | 3,5 MPa | resistenza caratteristica a taglio |
| $E_{0,mean} =$ | 11500 MPa | modulo di elasticità medio parallelo alle fibre |
| $E_{90,mean} =$ | 300 MPa | modulo di elasticità medio perpendicolare alle fibre |
| $G_{mean} =$ | 650 MPa | modulo di elasticità tangenziale medio |
| $K_{mod} =$ | 0,90 | coeff. funzione delle condizioni ambientali |
| $\gamma_m =$ | 1,45 | coefficiente di sicurezza del legno |
| $K_h =$ | 1,05 | coefficiente di forma |
| $f_{m,d} =$ | 15,6 MPa | resistenza di progetto a flessione |
| $f_{t,0,d} =$ | 12,5 MPa | resistenza di progetto a trazione parallela alle fibre |
| $f_{t,90,d} =$ | 0,3 MPa | resistenza di progetto a trazione perpendicolare alle fibre |
| $f_{c,0,d} =$ | 15,6 MPa | resistenza di progetto a compressione parallela alle fibre |
| $f_{c,90,d} =$ | 1,6 MPa | resistenza di progetto a compressione perpendicolare alle fibre |
| $f_{v,d} =$ | 2,3 MPa | resistenza di progetto a taglio |
| <i>Carichi applicati</i> | | |
| $g_{k1} =$ | 0,00 kN/m ² | carico caratteristico permanente |
| $g_{k2} =$ | 0,90 kN/m ² | carico caratteristico permanente portato |
| $q_k =$ | 1,30 kN/m ² | carico caratteristico variabile |
| $i =$ | 1,28 m | interasse |
| $g_{k1} =$ | 0,240 kN/m | carico caratteristico permanente |
| $g_{k2} =$ | 1,15 kN/m | carico caratteristico permanente portato |
| $q_k =$ | 1,66 kN/m | carico caratteristico variabile |
| SLU: | | |
| $\gamma_{G1} =$ | 1,30 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,50 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,50 | coefficiente parziale per carichi variabili |
| $F_d =$ | 4,54 | carico uniforme di progetto |
| SLE - combinazione rara: | | |
| $\gamma_{G1} =$ | 1,00 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,00 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,00 | coefficiente parziale per carichi variabili |
| $\psi_{01} =$ | 1,00 | coefficiente di combinazione |
| $F_d =$ | 3,06 | carico uniforme di progetto |
| SLE - combinazione frequente: | | |
| $\gamma_{G1} =$ | 1,00 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,00 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,00 | coefficiente parziale per carichi variabili |
| $\psi_{11} =$ | 0,50 | coefficiente di combinazione |
| $F_d =$ | 0,00 | carico uniforme di progetto |
| SLE - combinazione quasi permanente | | |
| $\gamma_{G1} =$ | 1,00 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,00 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,00 | coefficiente parziale per carichi variabili |
| $\psi_{21} =$ | 0,30 | coefficiente di combinazione |
| $F_d =$ | 1,89 | carico uniforme di progetto |

| Caratteristiche geometriche | | | | |
|------------------------------------|---------------|-----------------|-------------------|---|
| b = | 160 | mm | | base della sezione reagente |
| h = | 300 | mm | | altezza della sezione reagente |
| A = | 4,80E+04 | mm ² | | area della sezione reagente |
| W = | 2,40E+06 | mm ³ | | modulo di resistenza della sezione |
| I = | 3,60E+08 | mm ⁴ | | momento d'inerzia della sezione |
| L = | 4.600 | mm | | lunghezza della trave |
| b _y = | 150 | mm | | lunghezza appoggio |
| S = | 2,40E+04 | mm ² | | superficie di appoggio della trave |
| Verifiche SLU | | | | |
| M _{SLU} = | 11,998 | kNm | | momento flettente a SLU |
| V _{SLU} = | 10,433 | kN | | sforzo di taglio a SLU |
| σ _{m,0,d} = | 5,0 | MPa | < 15,6 MPa | Verificato tensione normale a SLU |
| k _{cr} = | 0,71 | | | coefficiente correttivo per larghezza efficace |
| τ _d = | 0,46 | MPa | < 2,3 MPa | Verificato tensione tangenziale a SLU |
| σ _{c,90,d} = | 0,4 | MPa | < 1,6 MPa | Verificato tensione ortogonale alla fibratura a SLU |
| Verifiche SLE | | | | |
| k _{def} = | 0,60 | | | |
| f _g = | 1,96 | mm | | freccia dovuta ai carichi permanenti |
| f _q = | 2,34 | mm | | freccia dovuta ai carichi variabili |
| f _{q,t=0} = | 2,34 | mm | | freccia a tempo zero dovuta ai soli carichi variabili |
| f _{lim=L/300} = | 15,3 | mm | Verificato | freccia limite a tempo zero |
| f _{t=inf} = | 5,90 | mm | | freccia a tempo infinito - COMBINAZIONE QUASI PERMANENTE |
| f _{lim=L/200} = | 23,00 | mm | Verificato | freccia limite a tempo infinito |

2.2.5.4 Trave di colmo 40x92 L15.60m lc 6.80m

Dati geometrici e caratteristiche del materiale

| | |
|-----------------|-------------------------|
| Schema statico | appoggio-appoggio |
| Luce di calcolo | $L_c = 15.60 \text{ m}$ |
| Larghezza base | $b = 40 \text{ cm}$ |
| Altezza | $h = 92 \text{ cm}$ |
| Interasse | $l_c = 680 \text{ cm}$ |
| Materiale | Legno lamellare GL24h |



Analisi dei carichi

| | | |
|--|---|-------------------|
| Peso proprio G_1 | | 155 daN/m |
| Peso proprio travetti G_1 | $(20 \text{ daN/m} / 1.28\text{m}) \times 6.80 \text{ m}$ | 135 daN/m |
| Permanenti portati G_2 | $90 \text{ daN/m}^2 \times 6.80 \text{ m}$ | 615 daN/m |
| Sovraccarico variabile Q_a | $120 \text{ daN/m}^2 \times 6.80 \text{ m}$ | <u>815 daN/m</u> |
| Totale carico caratteristico distribuito q | | 1720 daN/m |

Sollecitazioni di verifica

| Combinazione | Sollecitazioni | |
|--------------|-------------------------------|------------------------------|
| SLE rara | $M_k = 52322 \text{ daNm}$ | $V_k = 13416 \text{ daN}$ |
| SLU | $M_{Ed} = 76720 \text{ daNm}$ | $V_{Ed} = 19762 \text{ daN}$ |

Condizione di verifica

| | |
|------------------------------------|-----------------|
| Classe di servizio | 1 |
| Condizione di carico significativa | Breve durata |
| Coefficiente di durata del carico | $k_{mod} = 0.9$ |

Tabulato di calcolo

| TRAVI IN LEGNO | | |
|---|-------------------------------|--|
| <i>Caratteristiche meccaniche del legno</i> | | |
| GL 24h | | <i>Classe del legno</i> |
| $\rho_k =$ | 385 kg/m ³ | massa volumica caratteristica |
| $\rho_{mean} =$ | 420 kg/m ³ | massa volumica media |
| $f_{m,k} =$ | 24 MPa | resistenza caratteristica a flessione |
| $f_{t,0,k} =$ | 19,2 MPa | resistenza caratteristica a trazione parallela alle fibre |
| $f_{t,90,k} =$ | 0,5 MPa | resistenza caratteristica a trazione perpendicolare alle fibre |
| $f_{c,0,k} =$ | 24 MPa | resistenza caratteristica a compressione parallela alle fibre |
| $f_{c,90,k} =$ | 2,5 MPa | resistenza caratteristica a compressione perpendicolare alle fibre |
| $f_{v,k} =$ | 3,5 MPa | resistenza caratteristica a taglio |
| $E_{0,mean} =$ | 11500 MPa | modulo di elasticità medio parallelo alle fibre |
| $E_{90,mean} =$ | 300 MPa | modulo di elasticità medio perpendicolare alle fibre |
| $G_{mean} =$ | 650 MPa | modulo di elasticità tangenziale medio |
| $K_{mod} =$ | 0,90 | coeff. funzione delle condizioni ambientali |
| $\gamma_m =$ | 1,45 | coefficiente di sicurezza del legno |
| $K_h =$ | 1,00 | coefficiente di forma |
| $f_{m,d} =$ | 14,9 MPa | resistenza di progetto a flessione |
| $f_{t,0,d} =$ | 11,9 MPa | resistenza di progetto a trazione parallela alle fibre |
| $f_{t,90,d} =$ | 0,3 MPa | resistenza di progetto a trazione perpendicolare alle fibre |
| $f_{c,0,d} =$ | 14,9 MPa | resistenza di progetto a compressione parallela alle fibre |
| $f_{c,90,d} =$ | 1,6 MPa | resistenza di progetto a compressione perpendicolare alle fibre |
| $f_{v,d} =$ | 2,2 MPa | resistenza di progetto a taglio |
| <i>Carichi applicati</i> | | |
| $g_{k1} =$ | 0,20 kN/m ² | carico caratteristico permanente |
| $g_{k2} =$ | 0,90 kN/m ² | carico caratteristico permanente portato |
| $q_k =$ | 1,20 kN/m ² | carico caratteristico variabile |
| $i =$ | 6,80 m | interasse |
| $g_{k1} =$ | 3,200 kN/m | carico caratteristico permanente |
| $g_{k2} =$ | 6,12 kN/m | carico caratteristico permanente portato |
| $q_k =$ | 8,16 kN/m | carico caratteristico variabile |
| SLU: | | |
| $\gamma_{G1} =$ | 1,30 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,50 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,50 | coefficiente parziale per carichi variabili |
| $F_d =$ | 25,58 | carico uniforme di progetto |
| SLE - combinazione rara: | | |
| $\gamma_{G1} =$ | 1,00 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,00 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,00 | coefficiente parziale per carichi variabili |
| $\psi_{01} =$ | 1,00 | coefficiente di combinazione |
| $F_d =$ | 17,48 | carico uniforme di progetto |
| SLE - combinazione frequente: | | |
| $\gamma_{G1} =$ | 1,00 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,00 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,00 | coefficiente parziale per carichi variabili |
| $\psi_{11} =$ | 0,50 | coefficiente di combinazione |
| $F_d =$ | 0,00 | carico uniforme di progetto |
| SLE - combinazione quasi permanente | | |
| $\gamma_{G1} =$ | 1,00 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,00 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,00 | coefficiente parziale per carichi variabili |
| $\psi_{21} =$ | 0,30 | coefficiente di combinazione |
| $F_d =$ | 11,77 | carico uniforme di progetto |

| Caratteristiche geometriche | | | | |
|-----------------------------|----------|-----------------|------------|---|
| b = | 400 | mm | | base della sezione reagente |
| h = | 920 | mm | | altezza della sezione reagente |
| A = | 3,68E+05 | mm ² | | area della sezione reagente |
| W = | 5,64E+07 | mm ³ | | modulo di resistenza della sezione |
| I = | 2,60E+10 | mm ⁴ | | momento d'inerzia della sezione |
| L = | 15.600 | mm | | lunghezza della trave |
| b _y = | 350 | mm | | lunghezza appoggio |
| S = | 1,40E+05 | mm ² | | superficie di appoggio della trave |
| Verifiche SLU | | | | |
| M _{SLU} = | 778,144 | kNm | | momento flettente a SLU |
| V _{SLU} = | 199,524 | kN | | sforzo di taglio a SLU |
| σ _{m,0,d} = | 13,8 | MPa | < 14,9 MPa | Verificato tensione normale a SLU |
| k _{cr} = | 0,71 | | | coefficiente correttivo per larghezza efficace |
| τ _d = | 1,15 | MPa | < 2,2 MPa | Verificato tensione tangenziale a SLU |
| σ _{c,90,d} = | 1,4 | MPa | < 1,6 MPa | Verificato tensione ortogonale alla fibratura a SLU |
| Verifiche SLE | | | | |
| k _{def} = | 0,60 | | | |
| f _g = | 24,08 | mm | | freccia dovuta ai carichi permanenti |
| f _q = | 21,08 | mm | | freccia dovuta ai carichi variabili |
| f _{q,t=0} = | 21,08 | mm | | freccia a tempo zero dovuta ai soli carichi variabili |
| f _{lim=L/300} = | 52,0 | mm | | Verificato freccia limite a tempo zero |
| f _{t=inf} = | 63,40 | mm | | freccia a tempo infinito - COMBINAZIONE QUASI PERMANENTE |
| f _{lim=L/200} = | 78,00 | mm | | Verificato freccia limite a tempo infinito |

VERIFICA SBALZO SU PORTICATO

Dati geometrici e caratteristiche del materiale

| | |
|-----------------|-------------------------|
| Schema statico | Mensola |
| Luce di calcolo | L _c = 2.70 m |
| Larghezza base | b= 40 cm |
| Altezza | h= 40 cm |
| Interasse | l _c = 680 cm |
| Materiale | Legno lamellare GL24h |

Analisi dei carichi

| | | |
|---|---------------------------------|-------------------|
| Peso proprio G ₁ | | 155 daN/m |
| Peso proprio travetti G ₁ | (20 daN/m / 1.28m) x 6.80 m | 135 daN/m |
| Permanenti portati G ₂ | 90 daN/m ² x 6.80 m | 615 daN/m |
| Sovraccarico variabile Q _a | 120 daN/m ² x 6.80 m | <u>815 daN/m</u> |
| Totale carico caratteristico distribuito q | | 1720 daN/m |

Sollecitazioni di verifica

| Combinazione | Sollecitazioni | |
|--------------|----------------------------|----------------------------|
| SLE rara | M _k = 6270 daNm | V _k = 4644 daN |
| SLU | M _{Ed} =9193 daNm | V _{Ed} = 6810 daN |

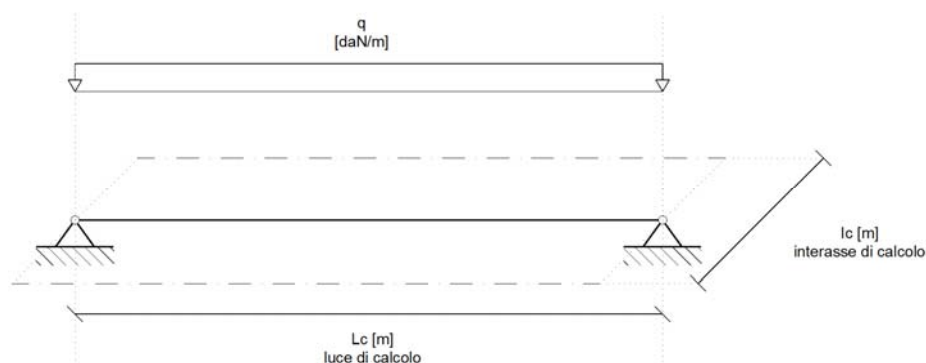
Tabulato di calcolo

| Carichi applicati | | | | |
|--|---------------|-------------------|-------------------|---|
| g_{k1} | 0,20 | kN/m ² | | carico caratteristico permanente |
| g_{k2} | 0,90 | kN/m ² | | carico caratteristico permanente portato |
| q_k | 1,20 | kN/m ² | | carico caratteristico variabile |
| i | 6,800 | m | | interasse |
| g_{k1} | 2,160 | kN/m | | carico caratteristico permanente |
| g_{k2} | 6,12 | kN/m | | carico caratteristico permanente portato |
| q_k | 8,16 | kN/m | | carico caratteristico variabile |
| SLU: | | | | |
| γ_{G1} | 1,30 | | | coefficiente parziale per carichi permanenti |
| γ_{G2} | 1,50 | | | coefficiente parziale per carichi permanenti portati |
| γ_Q | 1,50 | | | coefficiente parziale per carichi variabili |
| F_d | 24,23 | | | carico uniforme di progetto |
| SLE - combinazione rara: | | | | |
| γ_{G1} | 1,00 | | | coefficiente parziale per carichi permanenti |
| γ_{G2} | 1,00 | | | coefficiente parziale per carichi permanenti portati |
| γ_Q | 1,00 | | | coefficiente parziale per carichi variabili |
| ψ_{01} | 1,00 | | | coefficiente di combinazione |
| F_d | 16,44 | | | carico uniforme di progetto |
| SLE - combinazione frequente: | | | | |
| γ_{G1} | 1,00 | | | coefficiente parziale per carichi permanenti |
| γ_{G2} | 1,00 | | | coefficiente parziale per carichi permanenti portati |
| γ_Q | 1,00 | | | coefficiente parziale per carichi variabili |
| ψ_{11} | 0,50 | | | coefficiente di combinazione |
| F_d | 0,00 | | | carico uniforme di progetto |
| SLE - combinazione quasi permanente | | | | |
| γ_{G1} | 1,00 | | | coefficiente parziale per carichi permanenti |
| γ_{G2} | 1,00 | | | coefficiente parziale per carichi permanenti portati |
| γ_Q | 1,00 | | | coefficiente parziale per carichi variabili |
| ψ_{21} | 0,30 | | | coefficiente di combinazione |
| F_d | 10,73 | | | carico uniforme di progetto |
| Caratteristiche geometriche | | | | |
| b | 400 | mm | | base della sezione reagente |
| h | 400 | mm | | altezza della sezione reagente |
| A | 1,60E+05 | mm ² | | area della sezione reagente |
| W | 1,07E+07 | mm ³ | | modulo di resistenza della sezione |
| I | 2,13E+09 | mm ⁴ | | momento d'inerzia della sezione |
| L | 2.700 | mm | | lunghezza della trave |
| b_y | 150 | mm | | lunghezza appoggio |
| S | 6,00E+04 | mm ² | | superficie di appoggio della trave |
| Verifiche SLU | | | | |
| M_{SLU} | 88,311 | kNm | | momento flettente a SLU |
| V_{SLU} | 65,416 | kN | | sforzamento di taglio a SLU |
| $\sigma_{m,0,d}$ | 8,3 | MPa | < 14,9 MPa | Verificato tensione normale a SLU |
| k_{cr} | 0,71 | | | coefficiente correttivo per larghezza efficace |
| τ_d | 0,86 | MPa | < 2,2 MPa | Verificato tensione tangenziale a SLU |
| $\sigma_{c,90,d}$ | 1,1 | MPa | < 1,6 MPa | Verificato tensione ortogonale alla fibratura a SLU |
| Verifiche SLE | | | | |
| k_{def} | 0,60 | | | |
| f_g | 2,24 | mm | | freccia dovuta ai carichi permanenti |
| f_q | 2,21 | mm | | freccia dovuta ai carichi variabili |
| $f_{q,t=0}$ | 2,21 | mm | | freccia a tempo zero dovuta ai soli carichi variabili |
| $f_{lim=L/300}$ | 18,0 | mm | Verificato | freccia limite a tempo zero |
| $f_{t=inf}$ | 6,19 | mm | | freccia a tempo infinito - COMBINAZIONE QUASI PERMANENTE |
| $f_{lim=L/200}$ | 27,00 | mm | Verificato | freccia limite a tempo infinito |

2.2.5.5 Travetti 10x12 L4.60m lc1.28m

Dati geometrici e caratteristiche del materiale

| | |
|-----------------|-----------------------|
| Schema statico | appoggio-appoggio |
| Luce di calcolo | $L_c = 2.50$ m |
| Larghezza base | $b = 10$ cm |
| Altezza | $h = 12$ cm |
| Interasse | $l_c = 125$ cm |
| Inclinazione | $\alpha = 11^\circ$ |
| Materiale | Legno lamellare GL24h |



Analisi dei carichi

| | | |
|--|---|------------------|
| Peso proprio G_1 | | 5 daN/m |
| Permanenti portati G_2 | $90 \text{ daN/m}^2 \times 1.25 \text{ m}$ | 115 daN/m |
| Sovraccarico variabile Q_a | $120 \text{ daN/m}^2 \times 1.25 \text{ m}$ | <u>150 daN/m</u> |
| Totale carico caratteristico distribuito q | | 270 daN/m |

Sollecitazioni di verifica

| Combinazione | Sollecitazioni | |
|--------------|-----------------------------|----------------------------|
| SLE rara | $M_k = 211 \text{ daNm}$ | $V_k = 340 \text{ daN}$ |
| SLU | $M_{Ed} = 316 \text{ daNm}$ | $V_{Ed} = 505 \text{ daN}$ |

Condizione di verifica

| | |
|------------------------------------|-----------------|
| Classe di servizio | 1 |
| Condizione di carico significativa | Breve durata |
| Coefficiente di durata del carico | $k_{mod} = 0.9$ |

Tabulato di calcolo

| TRAVI IN LEGNO | | |
|---|-------------------------------|--|
| Caratteristiche meccaniche del legno | | |
| GL 24h | | Classe del legno |
| $\rho_k =$ | 385 kg/m ³ | massa volumica caratteristica |
| $\rho_{mean} =$ | 420 kg/m ³ | massa volumica media |
| $f_{m,k} =$ | 24 MPa | resistenza caratteristica a flessione |
| $f_{t,0,k} =$ | 19,2 MPa | resistenza caratteristica a trazione parallela alle fibre |
| $f_{t,90,k} =$ | 0,5 MPa | resistenza caratteristica a trazione perpendicolare alle fibre |
| $f_{c,0,k} =$ | 24 MPa | resistenza caratteristica a compressione parallela alle fibre |
| $f_{c,90,k} =$ | 2,5 MPa | resistenza caratteristica a compressione perpendicolare alle fibre |
| $f_{v,k} =$ | 3,5 MPa | resistenza caratteristica a taglio |
| $E_{0,mean} =$ | 11500 MPa | modulo di elasticità medio parallelo alle fibre |
| $E_{90,mean} =$ | 300 MPa | modulo di elasticità medio perpendicolare alle fibre |
| $G_{mean} =$ | 650 MPa | modulo di elasticità tangenziale medio |
| $K_{mod} =$ | 0,90 | coeff. funzione delle condizioni ambientali |
| $\gamma_m =$ | 1,45 | coefficiente di sicurezza del legno |
| $K_h =$ | 1,06 | coefficiente di forma |
| $f_{m,d} =$ | 15,8 MPa | resistenza di progetto a flessione |
| $f_{t,0,d} =$ | 12,6 MPa | resistenza di progetto a trazione parallela alle fibre |
| $f_{t,90,d} =$ | 0,3 MPa | resistenza di progetto a trazione perpendicolare alle fibre |
| $f_{c,0,d} =$ | 15,8 MPa | resistenza di progetto a compressione parallela alle fibre |
| $f_{c,90,d} =$ | 1,6 MPa | resistenza di progetto a compressione perpendicolare alle fibre |
| $f_{v,d} =$ | 2,3 MPa | resistenza di progetto a taglio |
| Carichi applicati | | |
| $g_{k1} =$ | 0,00 kN/m ² | carico caratteristico permanente |
| $g_{k2} =$ | 0,90 kN/m ² | carico caratteristico permanente portato |
| $q_k =$ | 1,20 kN/m ² | carico caratteristico variabile |
| $i =$ | 1,250 m | interasse |
| $g_{k1} =$ | 0,060 kN/m | carico caratteristico permanente |
| $g_{k2} =$ | 1,13 kN/m | carico caratteristico permanente portato |
| $q_k =$ | 1,50 kN/m | carico caratteristico variabile |
| SLU: | | |
| $\gamma_{G1} =$ | 1,30 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,50 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,50 | coefficiente parziale per carichi variabili |
| $F_d =$ | 4,02 | carico uniforme di progetto |
| SLE - combinazione rara: | | |
| $\gamma_{G1} =$ | 1,00 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,00 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,00 | coefficiente parziale per carichi variabili |
| $\Psi_{01} =$ | 1,00 | coefficiente di combinazione |
| $F_d =$ | 2,69 | carico uniforme di progetto |
| SLE - combinazione frequente: | | |
| $\gamma_{G1} =$ | 1,00 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,00 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,00 | coefficiente parziale per carichi variabili |
| $\Psi_{11} =$ | 0,50 | coefficiente di combinazione |
| $F_d =$ | 0,00 | carico uniforme di progetto |
| SLE - combinazione quasi permanente | | |
| $\gamma_{G1} =$ | 1,00 | coefficiente parziale per carichi permanenti |
| $\gamma_{G2} =$ | 1,00 | coefficiente parziale per carichi permanenti portati |
| $\gamma_Q =$ | 1,00 | coefficiente parziale per carichi variabili |
| $\Psi_{21} =$ | 0,30 | coefficiente di combinazione |
| $F_d =$ | 1,64 | carico uniforme di progetto |

| Caratteristiche geometriche | | | | |
|------------------------------------|--------------|-----------------|------------|---|
| b = | 100 | mm | | base della sezione reagente |
| h = | 120 | mm | | altezza della sezione reagente |
| A = | 1,20E+04 | mm ² | | area della sezione reagente |
| W = | 2,40E+05 | mm ³ | | modulo di resistenza della sezione |
| I = | 1,44E+07 | mm ⁴ | | momento d'inerzia della sezione |
| L = | 2.500 | mm | | lunghezza della trave |
| b _y = | 150 | mm | | lunghezza appoggio |
| S = | 1,50E+04 | mm ² | | superficie di appoggio della trave |
| Verifiche SLU | | | | |
| M _{SLU} = | 3,137 | kNm | | momento flettente a SLU |
| V _{SLU} = | 5,019 | kN | | sforzo di taglio a SLU |
| σ _{m,0,d} = | 13,1 | MPa | < 15,8 MPa | Verificato tensione normale a SLU |
| k _{cr} = | 0,71 | | | coefficiente correttivo per larghezza efficace |
| τ _d = | 0,88 | MPa | < 2,3 MPa | Verificato tensione tangenziale a SLU |
| σ _{c,90,d} = | 0,3 | MPa | < 1,6 MPa | Verificato tensione ortogonale alla fibratura a SLU |
| Verifiche SLE | | | | |
| k _{def} = | 0,60 | | | |
| f _g = | 3,64 | mm | | freccia dovuta ai carichi permanenti |
| f _q = | 4,61 | mm | | freccia dovuta ai carichi variabili |
| f _{q,t=0} = | 4,61 | mm | | freccia a tempo zero dovuta ai soli carichi variabili |
| f _{lim=L/300} = | 8,3 | mm | | Verificato freccia limite a tempo zero |
| f _{t=inf} = | 11,26 | mm | | freccia a tempo infinito - COMBINAZIONE QUASI PERMANENTE |
| f _{lim=L/200} = | 12,50 | mm | | Verificato freccia limite a tempo infinito |

2.2.5.6 Verifica nodo tipico Travetto – Trave colmo

Si riporta la verifica del nodo tipico tra travetto e trave di colmo. Il collegamento è realizzato mediante viti a tutto filetto incrociate.

Ancoraggio travetti-trave di colmo

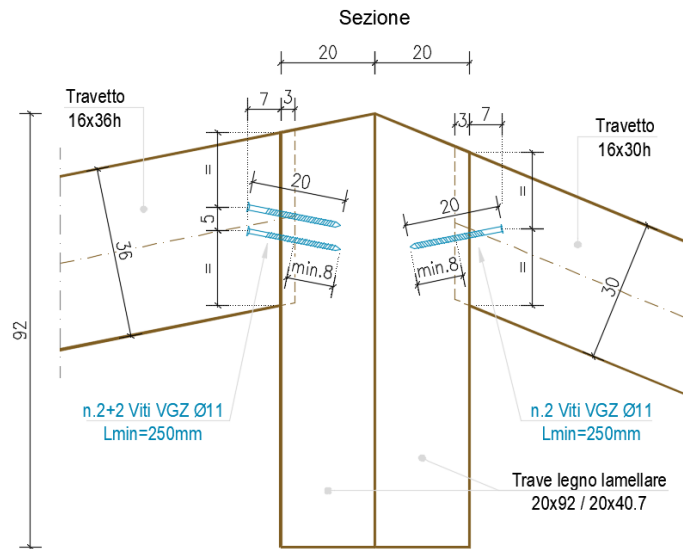


Fig 194. Schema di calcolo di riferimento della connessione.

| | |
|--------------------------------|-----------|
| Sezione travetto | 16x36 |
| Luce di calcolo travetto L_c | 9.00 m |
| Interasse di carico | 1.28 m |
| Carico distribuito SLU q_d | 436 daN/m |

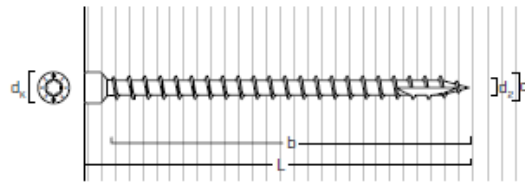
SOLLECITAZIONI DI VERIFICA

Reazione all'appoggio $V_{Ed} = 436 \times 9.00/2 = 1962 \text{ daN}$

CARATTERISTICHE CONNESSIONE

| | |
|--|---|
| Tipologia | Viti incrociate a tutto filetto |
| Viti | 2 coppie di viti VGZ Ø11 L250 Rothoblaas (o equivalente) |
| Resistenza caratteristica a snervamento f_{yk} | 1000 N/mm^2 |

Si riporta l'estratto dalla scheda tecnica del produttore.



| Diametro nominale | d ₁ | [mm] | 5,3 | 5,6 | 7 | 9 | 11 |
|---|---------------------|----------------------|------|------|------|-------|-------|
| Diametro testa | d _x | [mm] | 8,00 | 8,00 | 9,50 | 11,50 | 13,50 |
| Diametro nocciolo | d ₂ | [mm] | 3,60 | 3,80 | 4,60 | 5,90 | 6,60 |
| Diametro preforo ⁽¹⁾ | d _y | [mm] | 3,5 | 3,5 | 4,0 | 5,0 | 6,0 |
| Momento caratteristico di snervamento | M _{y,k} | [Nm] | 9,2 | 10,6 | 14,2 | 27,2 | 45,9 |
| Parametro caratteristico di resistenza ad estrazione ⁽²⁾ | f _{ax,k} | [N/mm ²] | 11,7 | 11,7 | 11,7 | 11,7 | 11,7 |
| Densità associata | ρ _a | [kg/m ³] | 350 | 350 | 350 | 350 | 350 |
| Parametro caratteristico di resistenza ad estrazione ⁽³⁾ | f _{ax,k} | [N/mm ²] | 15,0 | 15,0 | 15,0 | 15,0 | 15,0 |
| Densità associata | ρ _a | [kg/m ³] | 500 | 500 | 500 | 500 | 500 |
| Resistenza caratteristica a trazione | f _{tens,k} | [kN] | 11,0 | 12,3 | 15,4 | 25,4 | 38,0 |
| Resistenza caratteristica a snervamento | f _{y,k} | [N/mm ²] | 1000 | 1000 | 1000 | 1000 | 1000 |

⁽¹⁾ Preforo valido per legno di conifera (softwood).

⁽²⁾ Valido per legno di conifera (softwood) - densità massima 440 kg/m³.

⁽³⁾ Valido per LVL in legno di conifera (softwood) - densità massima 550 kg/m³.

Per applicazioni con materiali differenti o con densità elevata si rimanda a ETA-11/0030.

Fig 195. Caratteristiche della vite utilizzata.

Si prevede di impiegare n. 2+2 viti ROTHOBLOSS VGZ φ 11 L 250 incrociate.

Da scheda tecnica si ottiene la resistenza caratteristica per singola vite:

$$R_{V1k} = 835 \text{ daN}$$

$$R_{Vd} = 835 \times 0,9/1,5 = 501 \text{ daN}$$

La resistenza della connessione realizzata con n. 4 viti è quindi $R_d = 501 \times 4 = 2004$.

| geometria | | | TAGLID | | SCORRIMENTO | | |
|----------------|-----|----------------|------------------|------------------|----------------------------|------------------|------------------|
| | | | legno-legno | | legno-legno ⁽³⁾ | | |
| | | | | | | | |
| d ₁ | L | S _g | A _{min} | R _{V,k} | A _{min} | B _{min} | R _{V,k} |
| 11 | 250 | 110 | 125 | 8,35 | 95 | 110 | 10,80 |
| | 300 | 135 | 150 | 9,06 | 115 | 125 | 13,26 |
| | 350 | 160 | 175 | 9,06 | 130 | 145 | 15,71 |
| | 400 | 185 | 200 | 9,06 | 150 | 160 | 18,17 |
| | 450 | 210 | 225 | 9,06 | 165 | 180 | 20,63 |
| | 500 | 235 | 250 | 9,06 | 185 | 195 | 23,08 |
| | 550 | 260 | 275 | 9,06 | 200 | 215 | 25,54 |
| 600 | 285 | 300 | 9,06 | 220 | 230 | 26,87 | |

$$V_{Ed} = 1962 \text{ daN} > R_d$$

Rapporto di verifica

$$V_{Ed} / R_{vd} = 0.98 \leq 1$$

Verifica soddisfatta.

| | |
|--------------------------------|-----------|
| Sezione travetto | 16x30 |
| Luce di calcolo travetto L_c | 4.60 m |
| Interasse di carico | 1.25 m |
| Carico distribuito SLU q_d | 426 daN/m |

SOLLECITAZIONI DI VERIFICA

Reazione all'appoggio $V_{Ed} = 426 \times 4.60/2 = 980 \text{ daN}$

CARATTERISTICHE CONNESSIONE

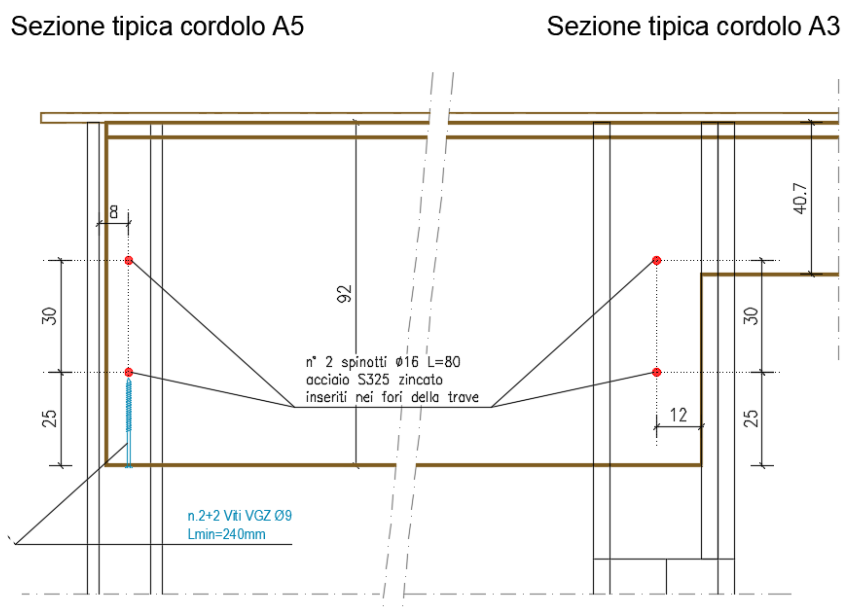
| | |
|--|--|
| Tipologia | Viti incrociate a tutto filetto |
| Viti | 1 coppia di viti VGZ Ø11 L250 Rothoblaas (o equivalente) |
| Resistenza caratteristica a snervamento f_{yk} | $f_{yk} = 1000 \text{ N/mm}^2$ |

La resistenza della connessione realizzata con n. 2 viti è quindi $R_d = 501 \times 2 = 1002 > V_{ed}$.

Verifica soddisfatta.

2.2.5.7 Verifica connessione trave di colmo - cordoli

Si riportano le verifiche delle connessioni trave di colmo – cordoli in c.a.. Per i dettagli si rimanda sempre agli Elaborati Grafici Esecutivi da consultarsi unitamente alla presente.



Sollecitazioni di verifica

Sforzo normale massimo inviluppo da modello di calcolo: $N_{ed} = 3445 \text{ daN}$

Unione realizzata mediante barre di acciaio $2\phi 16$ S355. La resistenza dell'unione si determina con riferimento alla tipologia di unione legno-acciaio in piastra spessa.

| UNIONE A TAGLIO CON BULLONI e SPINOTTI - CNR 206 - R1/2018 | | | |
|---|-------------|-------------------|---|
| <i>Unione con bulloni: momento plastico</i> | | | |
| d = | 16,0 | mm | diametro del mezzo di unione |
| f _{uk} = | 510 | MPa | resistenza ultima dell'acciaio |
| ζ _p = | 0,59 | | fattore riduttivo del momento plastico |
| W _{pl,b} = | 683 | mm ³ | modulo plastico del mezzo di unione (valido per gambo cilindrico) |
| M _{y,k} = | 0,207 | kNm | momento plastico del mezzo di unione |
| <i>Unione LEGNO - LEGNO per d ≤ 30 mm</i> | | | |
| d = | 16,0 | mm | diametro del mezzo di unione |
| ρ _k = | 350 | kg/m ³ | massa volumica caratteristica |
| f _{h,0,k} = | 24,11 | MPa | resistenza caratteristica a rifollamento per α = 0 |

| VERIFICA CONNESSIONE LEGNO / ACCIAIO - CNR 206/2007 | | | |
|--|--------|-----|--|
| Caratteristiche geometriche dell'unione | | | |
| Un piano di taglio | | | |
| | | | |
| Due piani di taglio | | | |
| | | | |
| $t_1 =$ | 0,0 | mm | spessore dell'elemento in legno 1 |
| $t_2 =$ | 400,0 | mm | spessore dell'elemento in legno 2 |
| $t =$ | 200,0 | mm | spessore della piastra |
| $d =$ | 16,0 | mm | diametro del mezzo di unione |
| $d_0 =$ | 16,0 | mm | diametro del foro nella piastra |
| $\Delta d =$ | 0,0 | mm | gioco foro nella piastra - gambo |
| $t_{sottile} =$ | 8,0 | mm | limite piastra sottile |
| $t_{spessa} =$ | 16,0 | mm | limite piastra spessa |
| tipo piastra | SPESSA | | tipo di piastra |
| Capacità portante dell'unione a due piani di taglio con piastre laterali spesse (§8.3.7.1.3) | | | |
| $f_{h,k} =$ | 24,11 | MPa | resistenza caratteristica a rifollamento del legno |
| $M_{y,Rk} =$ | 0,207 | kNm | momento di snervamento del mezzo di unione |
| $F_{ax,Rk} =$ | 0,00 | kN | contributo dell'effetto tirante |
| $F_{v,Rk}(l) =$ | 77,2 | kN | capacità portante dell'unione (l) |
| $F_{v,Rk}(k) =$ | 20,6 | kN | capacità portante dell'unione (m) |
| $F_{v,Rk} =$ | 20,6 | kN | capacità portante dell'unione |
| $F_{v,Rk} = \min \left\{ \begin{array}{l} 0.5 f_{h,2k} t_2 d \quad (l) \\ 2.3 \sqrt{M_{y,k} f_{h,2k} d} + \frac{F_{ax,Rk}}{4} \quad (m) \end{array} \right.$ | | | |
| Verifica di resistenza dell'unione | | | |
| $\gamma_M =$ | 1,50 | | coefficiente di sicurezza per le connessioni |
| $k_{mod} =$ | 0,90 | | |
| tipo unione | 5 | | tipo di unione (1, 2, 3, 4, 5) |
| $F_{v,Rk} =$ | 20,6 | kN | resistenza caratteristica dell'unione |
| $F_{v,Rd} =$ | 12,3 | kN | resistenza di progetto dell'unione |

$N_{ed,1} = 13445 / 2 = 1773 \text{ daN}$ (per singolo piano di taglio)

Verifica: $F_{v,Rd} = 2 \times 1230 = 2460 \text{ daN}$

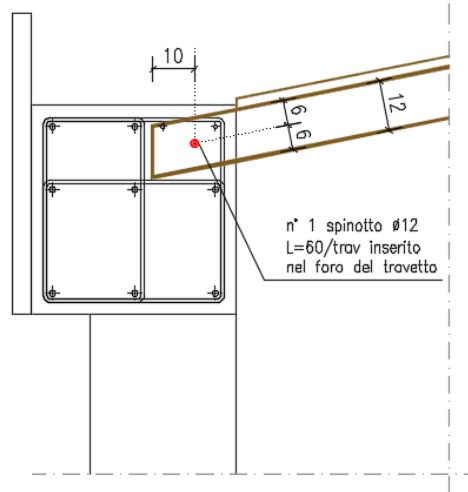
Rapporto di verifica: $\rho = 0.72 \leq 1$

Verificata soddisfatta.

2.2.5.8 Verifica connessione travetti porticato - trave in c.a.

Si riporta la verifica della connessione tra travetti 10x12 del porticato e la trave in c.a.. Per maggiori dettagli si rimanda agli elaborati grafici.

Sezione tipica trave T1



Condizione massima involucro

Combinazione SLU

$q_d = 405 \text{ daN/m}$

Reazione massima parallela

$F_{//} = q_d \times \sin 20^\circ \times L = 265 \text{ daN}$

Numero sezioni di taglio

2

Unione realizzata mediante barra di acciaio $\phi 12$ B450C. La resistenza dell'unione si determina con riferimento alla tipologia di unione legno-acciaio in piastra spessa.

| UNIONE A TAGLIO CON BULLONI e SPINOTTI - CNR 206 - R1/2018 | | | |
|---|------------|-------------------|---|
| Unione con bulloni: momento plastico | | | |
| d = | 12,0 | mm | diametro del mezzo di unione |
| $f_{uk} =$ | 540 | MPa | resistenza ultima dell'acciaio |
| $\zeta_p =$ | 0,67 | | fattore riduttivo del momento plastico |
| $W_{pl,b} =$ | 288 | mm ³ | modulo plastico del mezzo di unione (valido per gambo cilindrico) |
| $M_{y,k} =$ | 0,104 | kNm | momento plastico del mezzo di unione |
| Unione LEGNO - LEGNO per $d \leq 30 \text{ mm}$ | | | |
| d = | 12,0 | mm | diametro del mezzo di unione |
| $\rho_k =$ | 350 | kg/m ³ | massa volumica caratteristica |
| $f_{h,0,k} =$ | 25,26 | MPa | resistenza caratteristica a rifollamento per $\alpha = 0$ |
| | tipo legno | k_{90} | Legenda: |
| | LC | 1,53 | legno di conifere massiccio e lamellare |
| | LVL | 1,48 | legno LVL |
| | LL | 1,08 | legno di latifoglie massiccio e lamellare |
| tipo | LL | | tipo di legno utilizzato (LC; LVL; LL) |
| $k_{90} =$ | 1,08 | MPa | resistenza caratteristica a rifollamento con preforo |
| $\alpha =$ | 12 | deg | angolo dello sforzo rispetto alla direzione delle fibre |
| | 0,209 | rad | |
| $f_{h,\alpha,k} =$ | 25,17 | MPa | resistenza caratteristica a rifollamento |

| VERIFICA CONNESSIONE LEGNO / ACCIAIO - CNR 206/2007 | | | |
|---|----------|-----|--|
| Caratteristiche geometriche dell'unione | | | |
| Un piano di taglio | | | |
| | | | |
| Due piani di taglio | | | |
| | | | |
| $t_1 =$ | 0,0 | mm | spessore dell'elemento in legno 1 |
| $t_2 =$ | 100,0 | mm | spessore dell'elemento in legno 2 |
| $t =$ | 200,0 | mm | spessore della piastra |
| $d =$ | 12,0 | mm | diametro del mezzo di unione |
| $d_0 =$ | 12,0 | mm | diametro del foro nella piastra |
| $\Delta d =$ | 0,0 | mm | gioco foro nella piastra - gambo |
| $t_{sottile} =$ | 6,0 | mm | limite piastra sottile |
| $t_{spessa} =$ | 12,0 | mm | limite piastra spessa |
| tipo piastra | SPESSA | | tipo di piastra |
| Capacità portante dell'unione a due piani di taglio con piastre laterali spesse (§8.3.7.1.3) | | | |
| $f_{h,k} =$ | 25,17 | MPa | resistenza caratteristica a rifollamento del legno |
| $M_{y,Rk} =$ | 0,104 | kNm | momento di snervamento del mezzo di unione |
| $F_{ax,Rk} =$ | 0,00 | kN | contributo dell'effetto tirante |
| $F_{v,Rk}(j) =$ | 15,1 | kN | capacità portante dell'unione (l) |
| $F_{v,Rk}(k) =$ | 12,9 | kN | capacità portante dell'unione (m) |
| $F_{v,Rk} =$ | 12,9 | kN | capacità portante dell'unione 5 |
| $F_{v,Rk} = \min \begin{cases} 0.5 f_{h,2k} t_2 d & (l) \\ 2.3 \sqrt{M_{y,k} f_{h,2k} d} + \frac{F_{ax,Rk}}{4} & (m) \end{cases}$ | | | |
| Verifica di resistenza dell'unione | | | |
| $\gamma_M =$ | 1,50 | | coefficiente di sicurezza per le connessioni |
| $k_{mod} =$ | 0,90 | | |
| tipo unione | 5 | | tipo di unione (1, 2, 3, 4, 5) |
| $F_{v,Rk} =$ | 12,9 | kN | resistenza caratteristica dell'unione |
| $F_{v,Rd} =$ | 7,7 | kN | resistenza di progetto dell'unione |

$N_{ed} = 265 \text{ daN}$

Verifica: $F_{v,Rd} = 2 \times 770 = 1540 \text{ daN}$

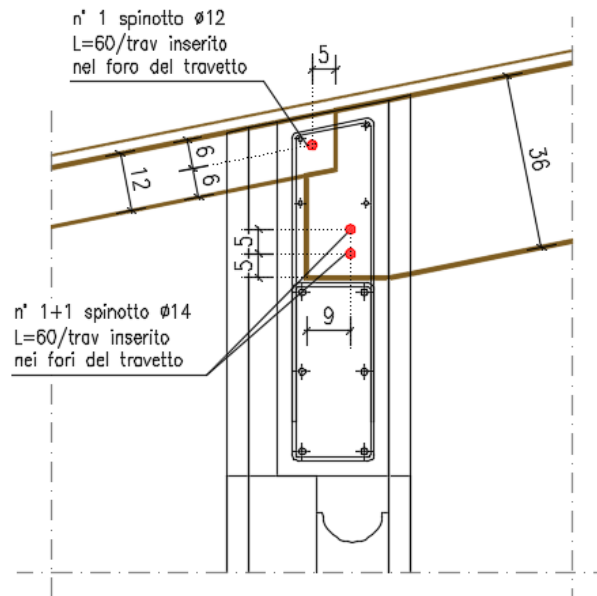
Rapporto di verifica: $\rho = 0.17 \leq 1$

Verificata soddisfatta.

2.2.5.9 Verifica connessioni trvetti cordoli

Si riporta la verifica della connessione tra travetti e i cordoli in c.a.. Per maggiori dettagli si rimanda agli elaborati grafici.

Sezione tipica cordolo A1



Condizione massima inviluppo

Combinazione SLU

$$q_d = 438 \text{ daN/m}$$

Reazione massima parallela

$$F_{//} = q_d \times \text{sen}20^\circ \times L = 1020 \text{ daN}$$

Numero sezioni di taglio

2

Unione realizzata mediante n° 2 barre di acciaio ϕ 14 B450C. La resistenza dell'unione si determina con riferimento alla tipologia di unione legno-acciaio in piastra spessa.

| UNIONE A TAGLIO CON BULLONI e SPINOTTI - CNR 206 - R1/2018 | | | |
|--|------------|-------------------|---|
| Unione con bulloni: momento plastico | | | |
| d = | 14,0 | mm | diametro del mezzo di unione |
| f _{uk} = | 540 | MPa | resistenza ultima dell'acciaio |
| ζ_p = | 0,63 | | fattore riduttivo del momento plastico |
| W _{pl,b} = | 457 | mm ³ | modulo plastico del mezzo di unione (valido per gambo cilindrico) |
| M _{y,k} = | 0,155 | kNm | momento plastico del mezzo di unione |
| Unione LEGNO - LEGNO per d ≤ 30 mm | | | |
| d = | 14,0 | mm | diametro del mezzo di unione |
| ρ_k = | 350 | kg/m ³ | massa volumica caratteristica |
| f _{h,0,k} = | 24,68 | MPa | resistenza caratteristica a rifollamento per $\alpha = 0$ |
| | tipo legno | k ₉₀ | Legenda: |
| | LC | 1,56 | legno di conifere massiccio e lamellare |
| | LVL | 1,51 | legno LVL |
| | LL | 1,11 | legno di latifoglie massiccio e lamellare |
| tipo | LL | | tipo di legno utilizzato (LC; LVL; LL) |
| k ₉₀ = | 1,11 | MPa | resistenza caratteristica a rifollamento con preforo |
| α = | 12 | deg | angolo dello sforzo rispetto alla direzione delle fibre |
| | 0,209 | rad | |
| f _{h,α,k} = | 24,57 | MPa | resistenza caratteristica a rifollamento |

| VERIFICA CONNESSIONE LEGNO / ACCIAIO - CNR 206/2007 | | | |
|---|--------|-----|--|
| Caratteristiche geometriche dell'unione | | | |
| Un piano di taglio | | | |
| | | | |
| Due piani di taglio | | | |
| | | | |
| $t_1 =$ | 0,0 | mm | spessore dell'elemento in legno 1 |
| $t_2 =$ | 160,0 | mm | spessore dell'elemento in legno 2 |
| $t =$ | 200,0 | mm | spessore della piastra |
| $d =$ | 14,0 | mm | diametro del mezzo di unione |
| $d_0 =$ | 14,0 | mm | diametro del foro nella piastra |
| $\Delta d =$ | 0,0 | mm | gioco foro nella piastra - gambo |
| $t_{sottile} =$ | 7,0 | mm | limite piastra sottile |
| $t_{spessa} =$ | 14,0 | mm | limite piastra spessa |
| tipo piastra | SPESSA | | tipo di piastra |
| Capacità portante dell'unione a due piani di taglio con piastre laterali spesse (§8.3.7.1.3) | | | |
| $f_{h,k} =$ | 24,57 | MPa | resistenza caratteristica a rifollamento del legno |
| $M_{y,Rk} =$ | 0,155 | kNm | momento di snervamento del mezzo di unione |
| $F_{ax,Rk} =$ | 0,00 | kN | contributo dell'effetto tirante |
| $F_{v,Rk}(j) =$ | 27,5 | kN | capacità portante dell'unione (l) |
| $F_{v,Rk}(k) =$ | 16,8 | kN | capacità portante dell'unione (m) |
| $F_{v,Rk} =$ | 16,8 | kN | capacità portante dell'unione 5 |
| $F_{v,Rk} = \min \begin{cases} 0.5 f_{h,2k} t_2 d & (l) \\ 2.3 \sqrt{M_{y,k} f_{h,2k} d} + \frac{F_{ax,Rk}}{4} & (m) \end{cases}$ | | | |
| Verifica di resistenza dell'unione | | | |
| $\gamma_M =$ | 1,50 | | coefficiente di sicurezza per le connessioni |
| $k_{mod} =$ | 0,90 | | |
| tipo unione | 5 | | tipo di unione (1, 2, 3, 4, 5) |
| $F_{v,Rk} =$ | 16,8 | kN | resistenza caratteristica dell'unione |
| $F_{v,Rd} =$ | 10,1 | kN | resistenza di progetto dell'unione |

$F_{//} = 1020 \text{ daN}$

Verifica: $F_{v,Rd} = 2 \times 1010 = 2020 \text{ daN}$

Rapporto di verifica: $\rho = 0.51 \leq 1$

Verificata soddisfatta.

2.2.6 Verifiche Pilastrì

2.2.6.1 Pilastrì 25x35 h330 - porticato

Dati geometrici

| | |
|-------------------|---|
| Schema statico | Mensola – Incastro al piede (a favore di sicurezza) |
| Altezza pilastro | H= 3.30 m |
| Sezione | 25x35 cm |
| Area di influenza | $A_i = 4.05 \text{ m} \times 1.20 \text{ m} = 4.86 \text{ m}^2$ |

Analisi dei carichi

| | | | |
|--|---|---|----------------|
| Peso proprio G_1 | $(0.087 \text{ m}^2 \times 2500 \text{ daN/m}^3 \times 3.30\text{m})$ | = | 725 daN |
| P.P. Trave | $(0.5\text{m} \times 0.5\text{m} \times 2500 \text{ daN/m}^3 \times 4.05 \text{ m})$ | = | 2530 daN |
| P.P.travetti | $(0.10\text{m} \times 0.12\text{m} \times 420 \text{ daN/m}^3 \times 1.2\text{m} \times (4.05\text{m}/1.23))$ | = | 20 daN |
| Pacchetto copertura | $(90 \text{ daN/m}^2 \times 4.86 \text{ m}^2)$ | = | 440 daN |
| Sovraccarico neve | $(120 \text{ daN/m}^2 \times 4.86 \text{ m}^2)$ | = | <u>585 daN</u> |
| Totale carico concentrato caratteristico | | | 4300 daN |

Sollecitazioni di verifica

| Combinazione | Sollecitazioni | | |
|--------------|-----------------------------|---------------------------|--|
| SLE – Rara | $N_k = 4300 \text{ daN}$ | $M_k = 0 \text{ daNm}$ | |
| SLE – QPERM | $N_{QP} = 3715 \text{ daN}$ | $M_{QP} = 0 \text{ daNm}$ | |
| SLU | $N_{Ed} = 5760 \text{ daN}$ | $M_{Ed} = 0 \text{ daNm}$ | |

Per individuare le sollecitazioni sismiche sul pilastro si considera un $S_e = 0.31g$, considerando un comportamento **non dissipativo** ($q=1.5$). Si hanno le seguenti sollecitazioni involuppo nella combinazione sismica.

| | | |
|-----|--|---|
| SLV | $N_{SLV} = 3715 \text{ daN}$ | $V_{SLV} = 1155 \text{ daN}$ |
| | $M_{SLV} = 3715 \cdot 0.31 \cdot 3.30 = 3815 \text{ daNm}$ | $M_{\perp SLV} = 0.30 \cdot 3815 = 1145 \text{ daNm}$ |

Armature longitudinali

| | |
|-------------------|---|
| Armatura minima | $A_{s,min} = 0.003 A_c = 2.625 \text{ cm}^2$ |
| Armatura prevista | 2+2Ø16 Acciaio B450C $A_s = 8.04 \text{ cm}^2$ |

Verifica a Pressoflessione - SLU

Essendo il pilastro soggetto prevalentemente a sforzo assiale, viene svolta la verifica a compressione.

| | |
|---------------------------------------|--|
| Area calcestruzzo | $A_c = 875 \text{ cm}^2$ |
| Resistenza di progetto a compressione | $f_{cd} = 142 \text{ daN/cm}^2$ |
| Tensione assiale | $\sigma_d = N_{Ed}/A_c = 6.585 \text{ daN/cm}^2$ |

rapporto di verifica $p: \sigma_d / f_{cd} = 0.05 < 1$

Verifica soddisfatta.

Verifica a Pressoflessione – Condizioni Sismiche SLV

Verifica a Taglio

| VERIFICA A TAGLIO PER ELEMENTI CON ARMATURE TRASVERSALI RESISTENTI A TAGLIO - §4.1.2.3.5 NTC 2018 | | | |
|---|--------------------------|---|--|
| Lato Calcestruzzo | | | |
| H | 350 mm | Altezza totale sezione | |
| d | 300 mm | Altezza utile della sezione | |
| bw | 250 mm | Larghezza minima della sezione | |
| R _{ck} | 30 N/mm ² | Resistenza caratteristica cubica a compressione del cls | |
| f _{ck} | 24,9 N/mm ² | Resistenza caratteristica cilindrica a compressione | |
| f _{cd} | 14,11 N/mm ² | Resistenza di calcolo a compressione del cls | |
| f _{cd} | 7,06 N/mm ² | Resistenza a compressione ridotta del cls d'anima (=0.5 f _{cd}) | |
| α _{cc} | 0,85 | Coeff. Riduttivo per resistenze di lunga durata | |
| γ _C | 1,50 | Coefficiente di sicurezza cls | |
| α _c | 1 | Pari a 1 per membrature non compresse | |
| α | 90 ° | 1,570796 rad | Inclinazione armatura trasversale rispetto asse trave |
| Θ | 45 | 0,785398 rad | Inclinazione puntone cls rispetto asse trave [21.8° ≤ Θ ≤ 45°] |
| V _{Ed} | 11550 N | Taglio sollecitante agli SLU | |
| V _{Rcd} | 238106,25 N | Resistenza di calcolo a Taglio Compressione | |
| Lato Acciaio | | | |
| A _{sw} | 667,00 mm ² | Area armatura trasversale compresa in "s" | |
| s | 1000 mm | Interasse tra due armature trasversali consecutive | |
| f _{yk} | 450 N/mm ² | Tensione caratteristica di snervamento dell'acciaio | |
| γ _S | 1,15 | Coefficiente parziale di sicurezza dell'acciaio | |
| K _θ | 1,00 | Coefficiente riduttivo dell'acciaio funzione della temperatura | |
| f _{yd} | 391,30 N/mm ² | Resistenza di calcolo dell'acciaio | |
| α | 90 ° | 1,570796 rad | Inclinazione armatura trasversale rispetto asse trave |
| Θ | 45 | 0,785398 rad | Inclinazione puntone cls rispetto asse trave [21.8° ≤ Θ ≤ 45°] |
| V _{Rsd} | 70470,00 N | Resistenza di calcolo a Taglio Trazione | |
| V _{Rd} | 70470,00 N | Resistenza a taglio della Trave [=MIN(V_{Rsd}; V_{Rcd})] | |

Armatura a taglio prevista

St.Ø8/15" 2br.

A_{sw} = 6.67cm²/m

V_{Ed} = 1155 daN < V_{Rd} = 7047 daN

Verifica a taglio soddisfatta

2.2.6.2 Pilastri 30x67 h330 - porticato

Dati geometrici

| | |
|-------------------|---|
| Schema statico | Mensola – Incastro al piede (a favore di sicurezza) |
| Altezza pilastro | H= 3.30 m |
| Sezione | 30x67 cm |
| Area di influenza | $A_i = 1.60 \text{ m} \times 1.20 \text{ m} = 1.95 \text{ m}^2$ |

Analisi dei carichi

| | | | |
|--|---|---|----------------|
| Peso proprio G_1 | $(0.2 \text{ m}^2 \times 2500 \text{ daN/m}^3 \times 3.30\text{m})$ | = | 1685 daN |
| P.P. Trave | $(0.5\text{m} \times 0.5\text{m} \times 2500 \text{ daN/m}^3 \times 1.60 \text{ m})$ | = | 1000 daN |
| P.P.travetti | $(0.10\text{m} \times 0.12\text{m} \times 420 \text{ daN/m}^3 \times 1.2\text{m} \times (1.60\text{m}/1.20))$ | = | 10 daN |
| Pacchetto copertura | $(90 \text{ daN/m}^2 \times 1.95\text{m}^2)$ | = | 175 daN |
| Sovraccarico neve | $(120 \text{ daN/m}^2 \times 1.95 \text{ m}^2)$ | = | <u>235 daN</u> |
| Totale carico concentrato caratteristico | | | 3105 daN |

Sollecitazioni di verifica

| Combinazione | Sollecitazioni | | |
|--------------|-----------------------------|---------------------------|--|
| SLE – Rara | $N_k = 3105 \text{ daN}$ | $M_k = 0 \text{ daNm}$ | |
| SLE – QPERM | $N_{QP} = 2870 \text{ daN}$ | $M_{QP} = 0 \text{ daNm}$ | |
| SLU | $N_{Ed} = 4125 \text{ daN}$ | $M_{Ed} = 0 \text{ daNm}$ | |

Per individuare le sollecitazioni sismiche sul pilastro si considera un $S_e = 0.31g$, considerando un comportamento **non dissipativo** ($q=1.5$). Si hanno le seguenti sollecitazioni iniluppo nella combinazione sismica.

| | | |
|-----|-------------------------------|------------------------------------|
| SLV | $N_{SLV} = 2780 \text{ daN}$ | $V_{SLV} = 890 \text{ daN}$ |
| | $M_{SLV} = 2940 \text{ daNm}$ | $M_{\perp SLV} = 885 \text{ daNm}$ |

Armature longitudinali

| | |
|-------------------|---|
| Armatura minima | $A_{s,min} = 0.003 A_c = 5.83 \text{ cm}^2$ |
| Armatura prevista | 2+2Ø16 Acciaio B450C $A_s = 8.04 \text{ cm}^2$ |

Verifica a Pressoflessione - SLU

Essendo il pilastro soggetto prevalentemente a sforzo assiale, viene svolta la verifica a compressione.

| | |
|--|--|
| Area calcestruzzo | $A_c = 1943 \text{ cm}^2$ |
| Resistenza di progetto a compressione | $f_{cd} = 142 \text{ daN/cm}^2$ |
| Tensione assiale | $\sigma_d = N_{Ed}/A_c = 1.5 \text{ daN/cm}^2$ |
| rapporto di verifica p: $\sigma_d / f_{cd} = 0.01 < 1$ | Verifica soddisfatta. |

Verifica a Pressoflessione – Condizioni Sismiche SLV

Titolo : Pil 29x67 porticato

N° Vertici **Zoom** **N° barre** **Zoom**

| N° | x [cm] | y [cm] |
|----|--------|--------|
| 1 | 0 | 0 |
| 2 | 30 | 0 |
| 3 | 30 | 67 |
| 4 | 0 | 67 |

| N° | As [cm²] | x [cm] | y [cm] |
|----|----------|--------|--------|
| 1 | 2,01 | 5 | 5 |
| 2 | 2,01 | 5 | 62 |
| 3 | 2,01 | 25 | 5 |
| 4 | 2,01 | 25 | 62 |

Tipo Sezione
 Rettan.re Trapezi
 a T Circolare
 Rettangoli Coord.

Sollecitazioni
 S.L.U. **Metodo n**

N_{Ed} **0** kN
M_{xEd} **0** kNm
M_{yEd} **0**

P.to applicazione N
 Centro Baricentro cls
 Coord.[cm] xN yN

Tipo rottura
 Lato calcestruzzo - Acciaio snervato

Metodo di calcolo
 S.L.U.+ S.L.U.-
 Metodo n

Tipo flessione
 Retta Deviata

N° rett.

Calcola MRd **Dominio Mx-My**

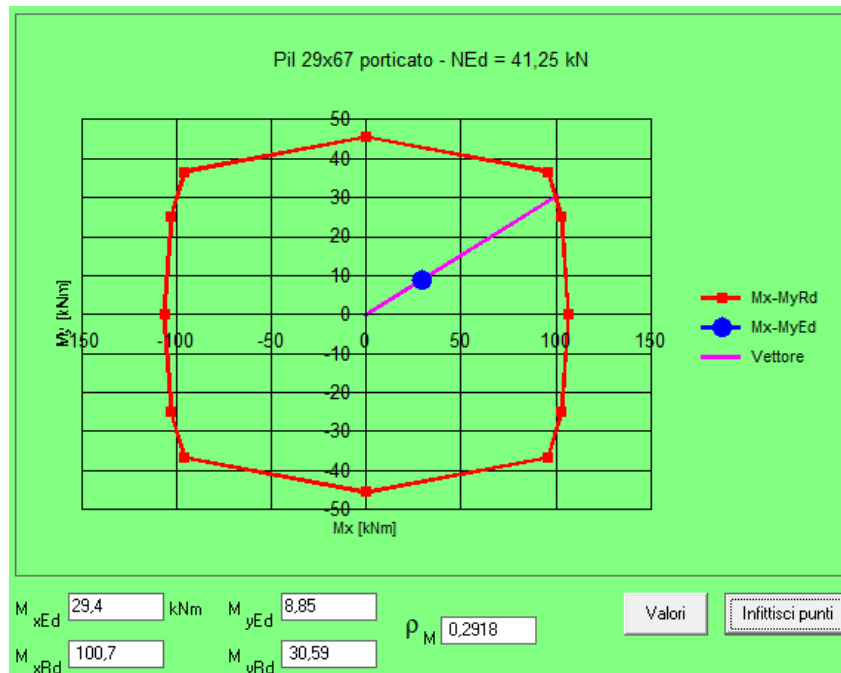
angolo asse neutro θ°

Precompresso

Materiali

 ϵ_{su} ‰ ϵ_{c2} ‰
 f_{yd} N/mm² ϵ_{cu} ‰
 E_s N/mm² f_{cd} ‰
 E_s/E_c f_{cc}/f_{cd} [?]
 ϵ_{syd} ‰ $\sigma_{c,adm}$
 $\sigma_{s,adm}$ N/mm² τ_{co}
 τ_{c1}

M_{xRd} kN m
M_{yRd} kN m
 σ_c N/mm²
 σ_s N/mm²
 ϵ_c ‰
 ϵ_s ‰
d cm
x **w/d**
 δ



Rapporto di verifica: $\rho = 0.29 \leq 1$

Verifica soddisfatta.

Verifica a Taglio

| VERIFICA A TAGLIO PER ELEMENTI CON ARMATURE TRASVERSALI RESISTENTI A TAGLIO - §4.1.2.3.5 NTC 2018 | | | |
|---|--------------------------|---|--|
| Lato Calcestruzzo | | | |
| H | 670 mm | Altezza totale sezione | |
| d | 620 mm | Altezza utile della sezione | |
| bw | 300 mm | Larghezza minima della sezione | |
| R _{ck} | 30 N/mm ² | Resistenza caratteristica cubica a compressione del cls | |
| f _{ck} | 24,9 N/mm ² | Resistenza caratteristica cilindrica a compressione | |
| f _{cd} | 14,11 N/mm ² | Resistenza di calcolo a compressione del cls | |
| f _{cd} | 7,06 N/mm ² | Resistenza a compressione ridotta del cls d'anima (=0.5 f _{cd}) | |
| α _{cc} | 0,85 | Coeff. Riduttivo per resistenze di lunga durata | |
| γ _C | 1,50 | Coefficiente di sicurezza cls | |
| α _c | 1 | Pari a 1 per membrature non compresse | |
| α | 90 ° | 1,570796 rad | Inclinazione armatura trasversale rispetto asse trave |
| Θ | 45 | 0,785398 rad | Inclinazione puntone cls rispetto asse trave [21.8° ≤ Θ ≤ 45°] |
| V _{ed} | 8900 N | Taglio sollecitante agli SLU | |
| V _{Rcd} | 590503,50 N | Resistenza di calcolo a Taglio Compressione | |
| Lato Acciaio | | | |
| A _{sw} | 667,00 mm ² | Area armatura trasversale compresa in "s" | |
| s | 1000 mm | Interasse tra due armature trasversali consecutive | |
| f _{yk} | 450 N/mm ² | Tensione caratteristica di snervamento dell'acciaio | |
| γ _S | 1,15 | Coefficiente parziale di sicurezza dell'acciaio | |
| K _θ | 1,00 | Coefficiente riduttivo dell'acciaio funzione della temperatura | |
| f _{yd} | 391,30 N/mm ² | Resistenza di calcolo dell'acciaio | |
| α | 90 ° | 1,570796 rad | Inclinazione armatura trasversale rispetto asse trave |
| Θ | 45 | 0,785398 rad | Inclinazione puntone cls rispetto asse trave [21.8° ≤ Θ ≤ 45°] |
| V _{Rsd} | 145638,00 N | Resistenza di calcolo a Taglio Trazione | |
| V _{Rd} | 145638,00 N | Resistenza a taglio della Trave [=MIN(V_{Rsd}; V_{Rcd})] | |

Armatura a taglio prevista

St.Ø8/15" 2br.

A_{sw} = 6.67cm²/m

V_{Ed} = 890 daN < V_{Rd} = 14564 daN

Verifica a taglio soddisfatta

2.2.6.3 Pilastri L h350 - porticato

Dati geometrici

| | |
|-------------------|--|
| Schema statico | Mensola – Incastro al piede (a favore di sicurezza) |
| Altezza pilastro | H= 3.50 m |
| Sezione | L 38-49-38 cm |
| Area di influenza | $A_i = 1.25 \text{ m} \times (4.6 \text{ m} + 1.20 \text{ m})$ |

Analisi dei carichi

| | | | |
|--|--|---|----------------|
| Peso proprio G_1 | $(0.365 \text{ m}^2 \times 2500 \text{ daN/m}^3 \times 3.50 \text{ m})$ | = | 3195 daN |
| Muratura | $(1.85 \text{ m}/2 \times 0.75 \text{ m} \times 470 \text{ daN/m}^2)$ | = | 326 daN |
| Cordolo | $(0.75 \times 0.25 \text{ m}^2 \times 2500 \text{ daN/m}^3 \times 1.25 \text{ m})$ | = | 585 daN |
| P.. strutt. Cop. (travi e travetti) | | = | 237 daN |
| Pacchetto copertura | $(90 \text{ daN/m}^2 \times A_i)$ | = | 655 daN |
| Sovraccarico neve | $(120 \text{ daN/m}^2 \times A_i)$ | = | <u>870 daN</u> |
| Totale carico concentrato caratteristico | | | 5868 daN |

Sollecitazioni di verifica

| Combinazione | Sollecitazioni | | |
|--------------|-----------------------------|---------------------------|--|
| SLE – Rara | $N_k = 5868 \text{ daN}$ | $M_k = 0 \text{ daNm}$ | |
| SLE – QPERM | $N_{QP} = 5000 \text{ daN}$ | $M_{QP} = 0 \text{ daNm}$ | |
| SLU | $N_{Ed} = 8115 \text{ daN}$ | $M_{Ed} = 0 \text{ daNm}$ | |

Per individuare le sollecitazioni sismiche sul pilastro si considera un $S_e = 0.31g$, considerando un comportamento **non dissipativo** ($q=1.5$). Si hanno le seguenti sollecitazioni involuppo nella combinazione sismica.

| | | |
|-----|-------------------------------|-------------------------------------|
| SLV | $N_{SLV} = 5000 \text{ daN}$ | $V_{SLV} = 1550 \text{ daN}$ |
| | $M_{SLV} = 5425 \text{ daNm}$ | $M_{\perp SLV} = 1630 \text{ daNm}$ |

Armature longitudinali

| | |
|-------------------|--|
| Armatura minima | $A_{s,min} = 0.003 A_c = 10.95 \text{ cm}^2$ |
| Armatura prevista | 3+3+2Ø16 Acciaio B450C $A_s = 16.08 \text{ cm}^2$ |

Verifica a Pressoflessione - SLU

Essendo il pilastro soggetto prevalentemente a sforzo assiale, viene svolta la verifica a compressione.

| | |
|---------------------------------------|--|
| Area calcestruzzo | $A_c = 3650 \text{ cm}^2$ |
| Resistenza di progetto a compressione | $f_{cd} = 142 \text{ daN/cm}^2$ |
| Tensione assiale | $\sigma_d = N_{Ed}/A_c = 2.2 \text{ daN/cm}^2$ |

rapporto di verifica $\rho: \sigma_d / f_{cd} = 0.015 < 1$

Verifica soddisfatta.

Verifica a Pressoflessione – Condizioni Sismiche SLV

A favore di sicurezza la verifica viene svolta considerando la sezione ridotta superiore.

Titolo : Pil 29x67 porticato

N° Vertici 6 **Zoom** **N° barre** 8 **Zoom**

| N° | x [cm] | y [cm] |
|----|--------|--------|
| 1 | 0 | 0 |
| 2 | 72 | 0 |
| 3 | 72 | 38 |
| 4 | 38 | 38 |
| 5 | 38 | 62 |
| 6 | 0 | 62 |

| N° | As [cm²] | x [cm] | y [cm] |
|----|----------|--------|--------|
| 1 | 2,01 | 5 | 5 |
| 2 | 2,01 | 5 | 57 |
| 3 | 2,01 | 33 | 5 |
| 4 | 2,01 | 67 | 5 |
| 5 | 2,01 | 33 | 57 |
| 6 | 2,01 | 33 | 33 |

Sollecitazioni
S.L.U. **Metodo n**

N_{Ed} 44,15 **44,15** kN
M_{xEd} 47,95 **47,95** kNm
M_{yEd} 14,4 **14,4**

P.to applicazione N
 Centro Baricentro cls
 Coord.[cm] xN 0 yN 0

Tipo rottura
Lato calcestruzzo - Acciaio snervato

Metodo di calcolo
 S.L.U.+ S.L.U.-
 Metodo n

Tipo flessione
 Retta Deviata

N° rett. 100

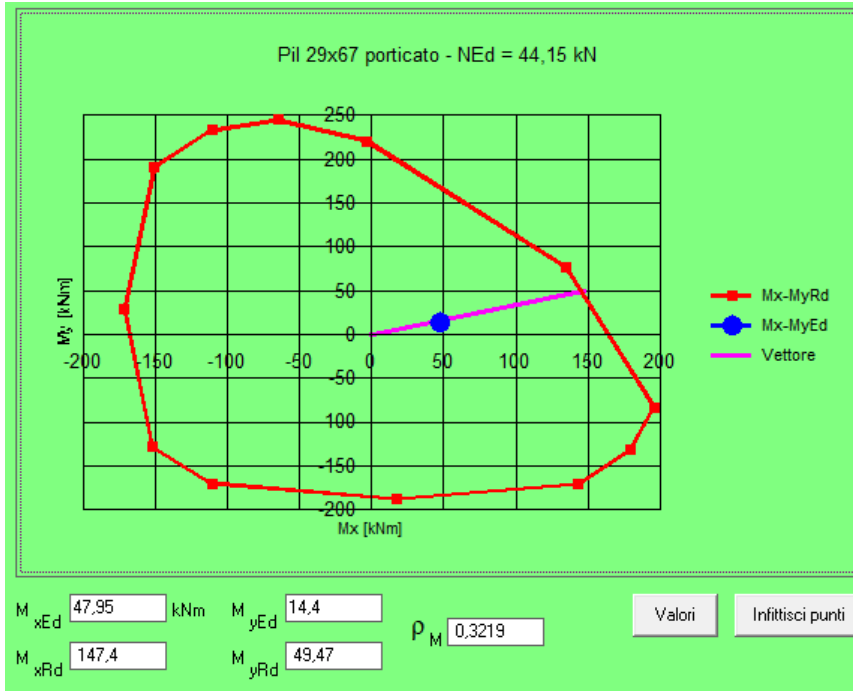
Calcola MRd **Dominio Mx-My**

angolo asse neutro θ° 333

Precompresso

Materiali
B450C C25/30
ε_{su} 67,5 % ε_{c2} 2 %
f_{yd} 391,3 N/mm² ε_{cu} 3,5
E_s 200.000 N/mm² f_{cd} 14,17
E_s/E_c 15 f_{cc}/f_{cd} 0,8
ε_{syd} 1,957 % σ_{c,adm} 9,75
σ_{s,adm} 255 N/mm² τ_{co} 0,6
τ_{c1} 1,829

M_{xRd} 147,4 kN m
M_{yRd} 49,47 kN m
σ_c -14,17 N/mm²
σ_s 391,3 N/mm²
ε_c 3,5 %
ε_s 11,34 %
d 65,77 cm
x 15,51 x/d 0,2359
δ 0,7348



Rapporto di verifica: $\rho = 0.32 \leq 1$

Verifica soddisfatta.

Verifica a Taglio

| VERIFICA A TAGLIO PER ELEMENTI CON ARMATURE TRASVERSALI RESISTENTI A TAGLIO - §4.1.2.3.5 NTC 2018 | | | |
|---|--------------------------|---|--|
| Lato Calcestruzzo | | | |
| H | 620 mm | Altezza totale sezione | |
| d | 570 mm | Altezza utile della sezione | |
| bw | 380 mm | Larghezza minima della sezione | |
| R _{ck} | 30 N/mm ² | Resistenza caratteristica cubica a compressione del cls | |
| f _{ck} | 24,9 N/mm ² | Resistenza caratteristica cilindrica a compressione | |
| f _{cd} | 14,11 N/mm ² | Resistenza di calcolo a compressione del cls | |
| f _{cd} | 7,06 N/mm ² | Resistenza a compressione ridotta del cls d'anima (=0.5 f _{cd}) | |
| α _{cc} | 0,85 | Coeff. Riduttivo per resistenze di lunga durata | |
| γ _C | 1,50 | Coefficiente di sicurezza cls | |
| α _c | 1 | Pari a 1 per membrature non compresse | |
| α | 90 ° | 1,570796 rad | Inclinazione armatura trasversale rispetto asse trave |
| Θ | 45 | 0,785398 rad | Inclinazione puntone cls rispetto asse trave [21.8° ≤ Θ ≤ 45°] |
| V _{Ed} | 15500 N | Taglio sollecitante agli SLU | |
| V _{Rcd} | 687650,85 N | Resistenza di calcolo a Taglio Compressione | |
| Lato Acciaio | | | |
| A _{sw} | 667,00 mm ² | Area armatura trasversale compresa in "s" | |
| s | 1000 mm | Interasse tra due armature trasversali consecutive | |
| f _{yk} | 450 N/mm ² | Tensione caratteristica di snervamento dell'acciaio | |
| γ _S | 1,15 | Coefficiente parziale di sicurezza dell'acciaio | |
| K _θ | 1,00 | Coefficiente riduttivo dell'acciaio funzione della temperatura | |
| f _{yd} | 391,30 N/mm ² | Resistenza di calcolo dell'acciaio | |
| α | 90 ° | 1,570796 rad | Inclinazione armatura trasversale rispetto asse trave |
| Θ | 45 | 0,785398 rad | Inclinazione puntone cls rispetto asse trave [21.8° ≤ Θ ≤ 45°] |
| V _{Rsd} | 133893,00 N | Resistenza di calcolo a Taglio Trazione | |
| V _{Rd} | 133893,00 N | Resistenza a taglio della Trave [=MIN(V_{Rsd}; V_{Rcd})] | |

Armatura a taglio prevista

St.Ø8/15" 2br.

A_{sw} = 6.67cm²/m

V_{Ed} = 1550 daN < V_{Rd} = 13389 daN

Verifica a taglio soddisfatta

2.2.6.4 Pilastri 20x30

Dati geometrici

| | |
|-------------------|---|
| Schema statico | Mensola – Incastro al piede (a favore di sicurezza) |
| Altezza pilastro | H= 2.75 m |
| Sezione | 20x30 cm |
| Area di influenza | $A_i = 4.05 \text{ m} \times 1.20 \text{ m} = 4.86 \text{ m}^2$ |

Sollecitazioni di verifica

| Combinazione | Sollecitazioni |
|--------------|-----------------------------|
| SLE – Rara | $N_k = 6820 \text{ daN}$ |
| SLE – QPERM | $N_{QP} = 5765 \text{ daN}$ |
| SLU | $N_{Ed} = 9390 \text{ daN}$ |

Per individuare le sollecitazioni sismiche sul pilastro si considera un $S_e = 0.31g$, considerando un comportamento **non dissipativo** ($q=1.5$). Si hanno le seguenti sollecitazioni involuppo nella combinazione sismica.

| | | |
|-----|-------------------------------|-------------------------------------|
| SLV | $N_{SLV} = 5765 \text{ daN}$ | $V_{SLV} = 1787 \text{ daN}$ |
| | $M_{SLV} = 4933 \text{ daNm}$ | $M_{\perp SLV} = 1480 \text{ daNm}$ |

Armature longitudinali

| | |
|-------------------|---|
| Armatura minima | $A_{s,min} = 0.003 A_c = 1.8 \text{ cm}^2$ |
| Armatura prevista | 2+2Ø16 Acciaio B450C $A_s = 8.04 \text{ cm}^2$ |

Verifica a Pressoflessione - SLU

Essendo il pilastro soggetto prevalentemente a sforzo assiale, viene svolta la verifica a compressione.

| | |
|--|--|
| Area calcestruzzo | $A_c = 600 \text{ cm}^2$ |
| Resistenza di progetto a compressione | $f_{cd} = 142 \text{ daN/cm}^2$ |
| Tensione assiale | $\sigma_d = N_{Ed}/A_c = 15.65 \text{ daN/cm}^2$ |
| rapporto di verifica $\rho: \sigma_d / f_{cd} = 0.11 < 1$ | Verifica soddisfatta. |

Verifica a Pressoflessione – Condizioni Sismiche SLV

Titolo : Pil 20x30 interno

N° Vertici **Zoom** **N° barre** **Zoom**

| N° | x [cm] | y [cm] |
|----|--------|--------|
| 1 | 0 | 0 |
| 2 | 20 | 0 |
| 3 | 20 | 30 |
| 4 | 0 | 30 |

| N° | As [cm²] | x [cm] | y [cm] |
|----|----------|--------|--------|
| 1 | 2,01 | 5 | 5 |
| 2 | 2,01 | 5 | 25 |
| 3 | 2,01 | 15 | 5 |
| 4 | 2,01 | 15 | 25 |

Tipo Sezione
 Rettan.re Trapezi
 a T Circolare
 Rettangoli Coord.

Sollecitazioni
 S.L.U. Metodo n

N Ed **0** kN
M xEd **0** kNm
M yEd **0**

P.to applicazione N
 Centro Baricentro cls
 Coord.[cm] xN yN

Tipo rottura
 Lato calcestruzzo - Acciaio snervato

Metodo di calcolo
 S.L.U.+ S.L.U.-
 Metodo n

Tipo flessione
 Retta Deviata

N° rett.
Calcola MRd **Dominio Mx-My**

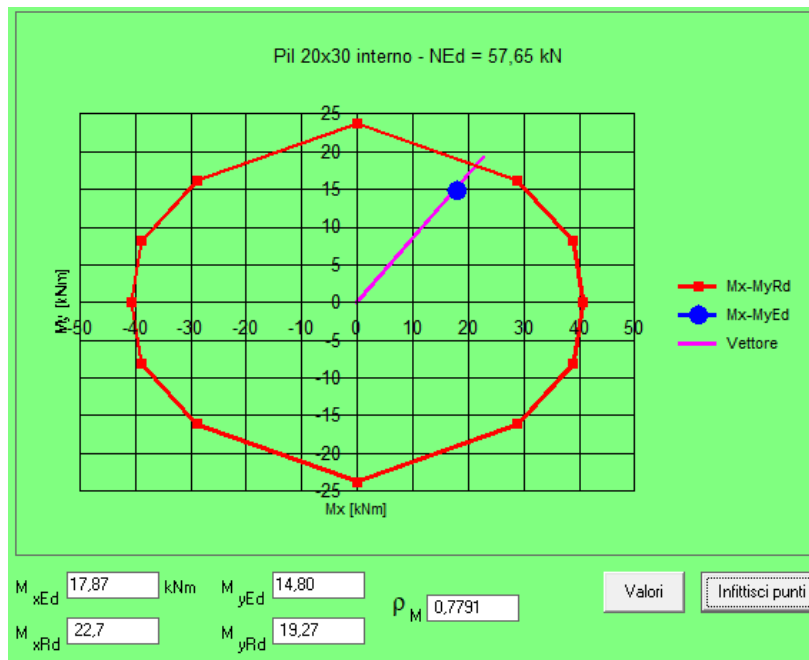
angolo asse neutro θ°

Precompresso

Materiali

 ϵ_{su} ‰ ϵ_{c2} ‰
 f_{yd} N/mm² ϵ_{cu}
 E_s N/mm² f_{cd}
 E_s/E_c f_{cc}/f_{cd} ?
 ϵ_{syd} ‰ $\sigma_{c,adm}$
 $\sigma_{s,adm}$ N/mm² τ_{co}
 τ_{c1}

M xRd kN m
M yRd kN m
 σ_c N/mm²
 σ_s N/mm²
 ϵ_c ‰
 ϵ_s ‰
 d cm
 x x/d
 δ



Rapporto di verifica: $\rho = 0.78 \leq 1$

Verifica soddisfatta.

Verifica a Taglio

| VERIFICA A TAGLIO PER ELEMENTI CON ARMATURE TRASVERSALI RESISTENTI A TAGLIO - §4.1.2.3.5 NTC 2018 | | | |
|---|--------------------------|---|--|
| Lato Calcestruzzo | | | |
| H | 300 mm | Altezza totale sezione | |
| d | 250 mm | Altezza utile della sezione | |
| bw | 200 mm | Larghezza minima della sezione | |
| R _{ck} | 30 N/mm ² | Resistenza caratteristica cubica a compressione del cls | |
| f _{ck} | 24,9 N/mm ² | Resistenza caratteristica cilindrica a compressione | |
| f _{cd} | 14,11 N/mm ² | Resistenza di calcolo a compressione del cls | |
| f _{cd} | 7,06 N/mm ² | Resistenza a compressione ridotta del cls d'anima (=0.5 f _{cd}) | |
| α _{cc} | 0,85 | Coeff. Riduttivo per resistenze di lunga durata | |
| γ _C | 1,50 | Coefficiente di sicurezza cls | |
| α _c | 1 | Pari a 1 per membrature non compresse | |
| α | 90 ° | 1,570796 rad | Inclinazione armatura trasversale rispetto asse trave |
| Θ | 45 | 0,785398 rad | Inclinazione puntone cls rispetto asse trave [21.8° ≤ Θ ≤ 45°] |
| V _{Ed} | 17870 N | Taglio sollecitante agli SLU | |
| V _{Rcd} | 158737,50 N | Resistenza di calcolo a Taglio Compressione | |
| Lato Acciaio | | | |
| A _{sw} | 667,00 mm ² | Area armatura trasversale compresa in "s" | |
| s | 1000 mm | Interasse tra due armature trasversali consecutive | |
| f _{yk} | 450 N/mm ² | Tensione caratteristica di snervamento dell'acciaio | |
| γ _S | 1,15 | Coefficiente parziale di sicurezza dell'acciaio | |
| K _θ | 1,00 | Coefficiente riduttivo dell'acciaio funzione della temperatura | |
| f _{yd} | 391,30 N/mm ² | Resistenza di calcolo dell'acciaio | |
| α | 90 ° | 1,570796 rad | Inclinazione armatura trasversale rispetto asse trave |
| Θ | 45 | 0,785398 rad | Inclinazione puntone cls rispetto asse trave [21.8° ≤ Θ ≤ 45°] |
| V _{Rsd} | 58725,00 N | Resistenza di calcolo a Taglio Trazione | |
| V _{Rd} | 58725,00 N | Resistenza a taglio della Trave [=MIN(V_{Rsd}; V_{Rcd})] | |

Armatura a taglio prevista

St.Ø8/15" 2br.

A_{sw} = 6.67cm²/m

V_{Ed} = 1787 daN < V_{Rd} = 5872 daN

Verifica a taglio soddisfatta

2.2.7 Verifica Trave porticato

Si riportano le verifiche analitiche allo stato limite Ultimo e agli stati limite di Esercizio degli elementi trave con riferimento alle condizione involuppo più gravose in accordo con il DM17.01.2018.

Si riporta di seguito la sezione dell'elemento strutturale oggetto di verifica, per maggiore dettaglio si rimanda agli Elaborati Grafici Progettuali.

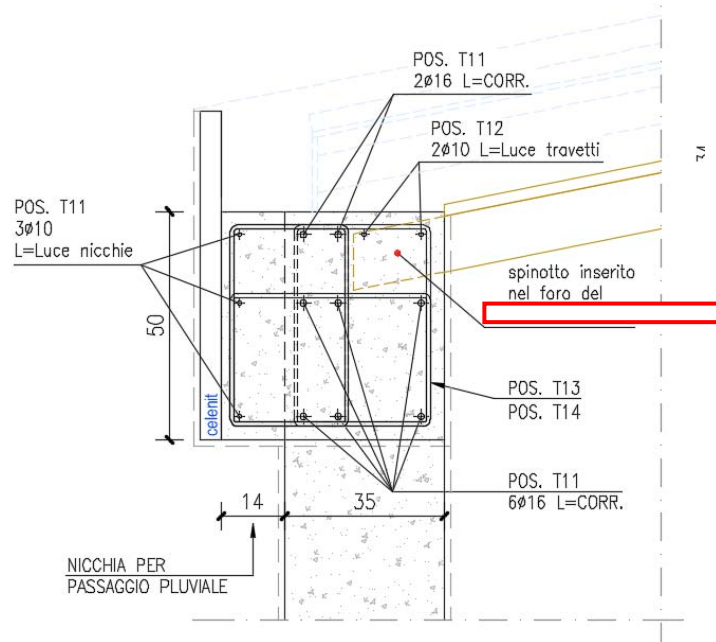
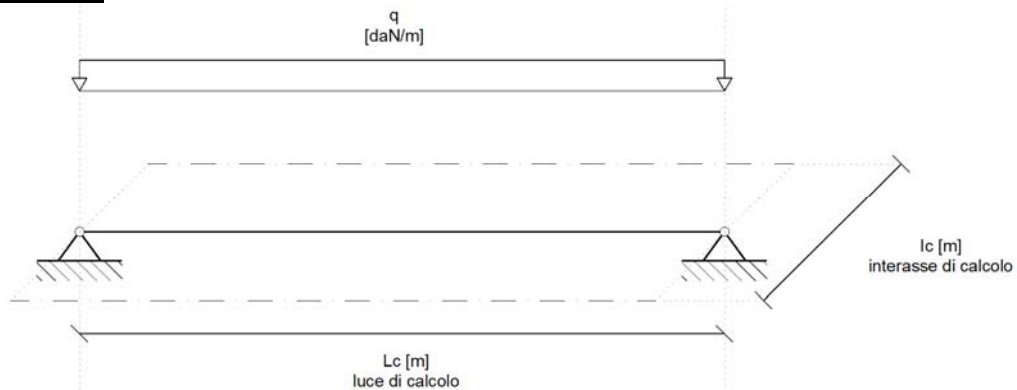


Fig 196. Sezione resistente di verifica

SCHEMA DI CALCOLO



| | |
|--------------------------------------|------------------------------------|
| Luce di calcolo L_c : | 4.05 m; |
| Schema Statico: | appoggio - appoggio; |
| Interasse di influenza carico solaio | l_c : 1.50 m; |
| Sezione di verifica | 35 x 50 cm (a favore di sicurezza) |

CARICHI PORTATI

| | | | |
|---|-----------------------------------|----------|------------------|
| Peso proprio strutturale G_1 | = | 625 | daN/m; |
| Peso proprio travetti G_1 | = | 10 | daN/m; |
| Permanente Copertura G_2 | (90 daN/m ² x 1.50 m) | = | 135 daN/m; |
| Sovraccarico neve Q_a | (120 daN/m ² x 1.50 m) | = | 180 daN/m; |
| Totale carico distribuito q | | = | 950 daN/m |

SOLLECITAZIONI DI VERIFICA

| COMBINAZIONE | SOLLECITAZIONI | |
|------------------|---------------------------|--------------------------|
| SLU FONDAMENTALE | $M_{Ed,SLU} = 2850$ daNm | $V_{Ed,SLU} = 2815$ daN |
| SLE - RARA | $M_{Ed,RARA} = 1950$ daNm | $V_{Ed,RARA} = 1925$ daN |

Armatura di calcolo

3+3Ø16 correnti

Acciaio B450C

Verifica a pressoflessione - SLU

Titolo: Trave T1 porticato

N° Vertici: 4 Zoom N° barre: 9 Zoom

| N° | x [cm] | y [cm] |
|----|--------|--------|
| 1 | 0 | 0 |
| 2 | 35 | 0 |
| 3 | 35 | 50 |
| 4 | 0 | 50 |

| N° | As [cm²] | x [cm] | y [cm] |
|----|----------|--------|--------|
| 1 | 2,01 | 5 | 31 |
| 2 | 2,01 | 15 | 31 |
| 3 | 2,01 | 30 | 31 |
| 4 | 2,01 | 5 | 5 |
| 5 | 2,01 | 15 | 5 |
| 6 | 2,01 | 30 | 5 |

Sollecitazioni
S.L.U. Metodo n

| | |
|----------------|----------|
| N_{Ed} 0 | 0 kN |
| M_{xEd} 28,5 | 19,5 kNm |
| M_{yEd} 0 | 0 |

P.to applicazione N
 Centro Baricentro cls
 Coord.[cm] xN 0 yN 0

Tipo rottura
Lato calcestruzzo - Acciaio snervato

Materiali

| | |
|--|-----------------------|
| B450C | C25/30 |
| ϵ_{su} 67,5 ‰ | ϵ_{c2} 2 ‰ |
| f_{yd} 391,3 N/mm ² | ϵ_{cu} 3,5 ‰ |
| E_s 200.000 N/mm ² | f_{cd} 14,17 |
| E_s/E_c 15 | f_{cc}/f_{cd} 0,8 |
| ϵ_{syd} 1,957 ‰ | $\sigma_{c,adm}$ 9,75 |
| $\sigma_{s,adm}$ 255 N/mm ² | τ_{co} 0,6 |
| | τ_{c1} 1,829 |

M_{xRd} 132,5 kN m

σ_c -14,17 N/mm²

σ_s 391,3 N/mm²

ϵ_c 3,5 ‰

ϵ_s 15,31 ‰

d 45 cm

x 8,371 x/d 0,186

δ 0,7

Tipo Sezione
 Rettan.re Trapezi
 a T Circolare
 Rettangoli Coord.

Metodo di calcolo
 S.L.U.+ S.L.U.-
 Metodo n

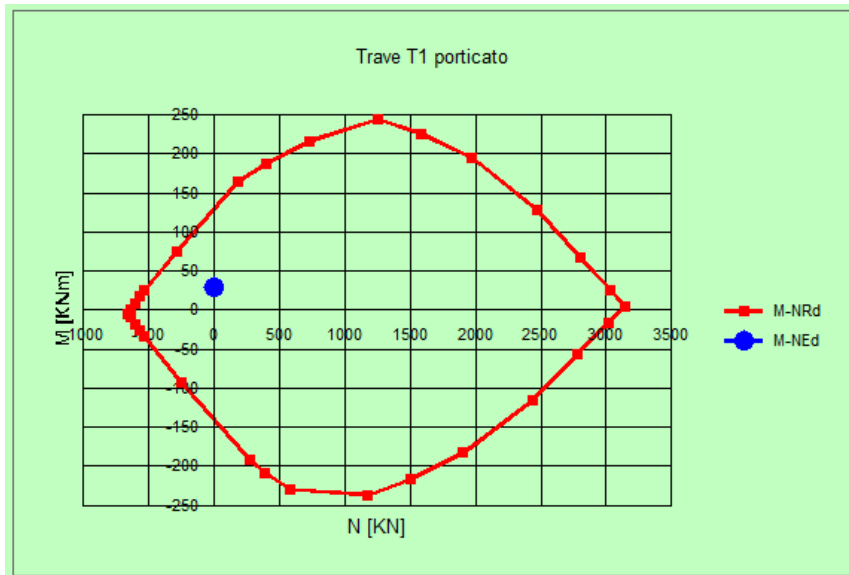
Tipo flessione
 Retta Deviata

N° rett. 100

Calcola MRd Dominio M-N

L_0 0 cm Col. modello

Precompresso



$M_{Rd} = 13250 \text{ daNm} \geq M_{Ed} = 2850 \text{ daNm}$

Rapporto di verifica: $M_{Ed}/M_{Rd} = 0.22 \leq 1$ Verifica soddisfatta.

Verifiche Stato Tensionale SLE

Combinazione SLE Rara

Titolo: Trave T1 porticato

N° Vertici: Zoom N° barre: Zoom

| N° | x [cm] | y [cm] |
|----|--------|--------|
| 1 | 0 | 0 |
| 2 | 35 | 0 |
| 3 | 35 | 50 |
| 4 | 0 | 50 |

| N° | As [cm²] | x [cm] | y [cm] |
|----|----------|--------|--------|
| 1 | 2,01 | 5 | 31 |
| 2 | 2,01 | 15 | 31 |
| 3 | 2,01 | 30 | 31 |
| 4 | 2,01 | 5 | 5 |
| 5 | 2,01 | 15 | 5 |
| 6 | 2,01 | 30 | 5 |

Sollecitazioni
S.L.U. Metodo n

N_{Ed} kN
 M_{xEd} kNm
 M_{yEd}

P.to applicazione N
 Centro Baricentro cls
 Coord. [cm] x_N
 y_N

Tipo Sezione
 Rettan.re Trapezi
 a T Circolare
 Rettangoli Coord.

Metodo di calcolo
 S.L.U.+ S.L.U.-
 Metodo n

Materiali

| B450C | | C25/30 | |
|------------------|--|------------------|------------------------------------|
| ϵ_{su} | <input type="text" value="67,5"/> ‰ | ϵ_{c2} | <input type="text" value="2"/> ‰ |
| f_{yd} | <input type="text" value="391,3"/> N/mm² | ϵ_{cu} | <input type="text" value="3,5"/> ‰ |
| E_s | <input type="text" value="200.000"/> N/mm² | f_{cd} | <input type="text" value="14,17"/> |
| E_s/E_c | <input type="text" value="15"/> | f_{cc}/f_{cd} | <input type="text" value="0,8"/> |
| ϵ_{syd} | <input type="text" value="1,957"/> ‰ | $\sigma_{c,adm}$ | <input type="text" value="9,75"/> |
| $\sigma_{s,adm}$ | <input type="text" value="255"/> N/mm² | τ_{co} | <input type="text" value="0,6"/> |
| | | τ_{c1} | <input type="text" value="1,829"/> |

σ_c N/mm²
 σ_s N/mm²
 ϵ_s ‰
d cm
x x/d
 δ

Verifica
N° iterazioni:

Precompresso

Verifica Tensionale (§4.1.2.2.5.1 e §4.1.2.2.5.2 NTC 2018)

$$\sigma_{C.RARA} = 20 \text{ daN/cm}^2 \leq 0.45 f_{ck} = 112 \text{ daN/cm}^2$$

VERIFICA SODDISFATTA

$$\sigma_{S.RARA} = 747.5 \text{ daN/cm}^2 \leq 0.8 f_{yk} = 3600 \text{ daN/cm}^2$$

VERIFICA SODDISFATTA

Verifica a Fessurazione

L'elemento in questione è sottoposto a *condizioni ambientali ordinarie*, le armature rientrano nella categoria "*poco sensibili*". Pertanto lo stato limite di apertura delle fessure da garantire è pari a

- $w \leq w_3$ per combinazione **frequente**,

- $w \leq w_2$ per combinazione **quasi permanente**. (cfr. **tabella 4.1.IV da N.T.C. 2018**)

Essendo lo Stato Tensionale massimo in cmb. SLE delle armature tese:

$$\sigma_{s,max,rara} = 748 \text{ daN/cm}^2 \leq 2400 \text{ daN/cm}^2 \quad (\text{cfr. Tab. C4.1.II / C4.1.III da C. 21.01.2019 n.7 C.S.LL.PP}).$$

In riferimento alla "*Circolare Esplicativa 21.01.2019 n.7 C.S.LL.PP. par C4.1.2.2.4.5, Verifica della fessurazione senza calcolo diretto*" la **VERIFICA** risulta **SODDISFATTA**.

Valutazione della freccia massima

Ipotesi di calcolo

- Momento d'inerzia : $J = 126113 \text{ cm}^4$ (sezione parzializzata)
- Modulo elastico cls: $E_{cls} = 314000 \text{ daN/cm}^2$
- Coeff. di def. viscosa $\varphi = 2.3$

Freccia istantanea massima in combinazione Rara :

$$- f_{\max,ist,tot} = 5/384 qL^4/EJ = 0.08 \text{ cm}$$

Freccia a lungo termine in combinazione Rara:

$$- f_{\text{MAX},\infty,tot} = \varphi f_{\max,ist} = 0.2 \text{ cm} \leq L/250 = 1.62 \text{ cm}$$

Verifica Soddisfatta.

VERIFICA A TAGLIO SEZIONE DI APPOGGIO

| VERIFICA A TAGLIO PER ELEMENTI CON ARMATURE TRASVERSALI RESISTENTI A TAGLIO - §4.1.2.3.5 NTC 2018 | | |
|---|--------------------------|--|
| Lato Calcestruzzo | | |
| H | 500 mm | Altezza totale sezione |
| d | 450 mm | Altezza utile della sezione |
| b _w | 450 mm | Larghezza minima della sezione |
| R _{ck} | 30 N/mm ² | Resistenza caratteristica cubica a compressione del cls |
| f _{ck} | 24,9 N/mm ² | Resistenza caratteristica cilindrica a compressione |
| f _{cd} | 14,11 N/mm ² | Resistenza di calcolo a compressione del cls |
| f _{cd} | 7,06 N/mm ² | Resistenza a compressione ridotta del cls d'anima (=0.5 f _{cd}) |
| α _{cc} | 0,85 | Coeff. Riduttivo per resistenze di lunga durata |
| γ _C | 1,50 | Coefficiente di sicurezza cls |
| α _c | 1 | Pari a 1 per membrature non compresse |
| α | 90 ° | 1,570796 rad Inclinazione armatura trasversale rispetto asse trave |
| Θ | 40 | 0,698132 rad Inclinazione puntone cls rispetto asse trave [21.8° ≤ Θ ≤ 45°] |
| V _{ed} | 28150 N | Taglio sollecitante agli SLU |
| V _{Rcd} | 633119,98 N | Resistenza di calcolo a Taglio Compressione |
| Lato Acciaio | | |
| A _{sw} | 500,00 mm ² | Area armatura trasversale compresa in "s" |
| s | 1000 mm | Interasse tra due armature trasversali consecutive |
| f _{yk} | 450 N/mm ² | Tensione caratteristica di snervamento dell'acciaio |
| γ _s | 1,15 | Coefficiente parziale di sicurezza dell'acciaio |
| K _θ | 1,00 | Coefficiente riduttivo dell'acciaio funzione della temperatura |
| f _{yd} | 391,30 N/mm ² | Resistenza di calcolo dell'acciaio |
| α | 90 ° | 1,570796 rad Inclinazione armatura trasversale rispetto asse trave |
| Θ | 40 | 0,698132 rad Inclinazione puntone cls rispetto asse trave [21.8° ≤ Θ ≤ 45°] |
| V _{Rsd} | 94433,52 N | Resistenza di calcolo a Taglio Trazione |
| V _{Rd} | 94433,52 N | Resistenza a taglio della Trave [=MIN(V _{Rsd} ; V _{Rcd})] |
| Definizione del Tirante Longitudinale per effetto del solo Taglio - Secondo EC2 §4.3.2.4.4 | | |
| T _d | 16773,93 N | Forza di trazione nelle armature longitudinali tese |
| A _{sL} | 42,87 mm ² | Armatura tirante per effetto del solo taglio |

Armatura a taglio:

St.Ø8/20" 2br. o equivalente

 A_{sw} = 5.00 cm²/m

 V_{Rd} = 9443 daN ≥ V_{Ed} = 2815 daN

Rapporto di verifica: ρ = 0.30 ≤ 1

Verifica soddisfatta

2.2.8 Verifica Struttura pareti in cartongesso

Si riportano di seguito le verifiche dei tubolari metallici costituenti la struttura delle pareti in cartongesso

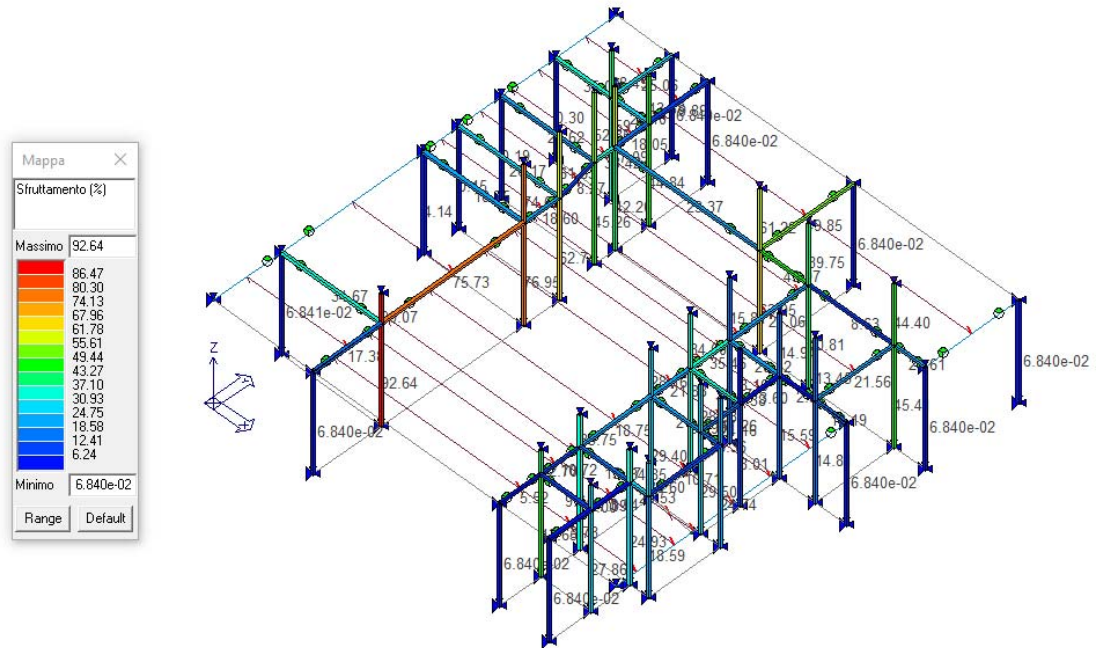


Fig 197. Massimo Sfruttamento del materiale [% ≤ 100 Verifica Soddisfatta].

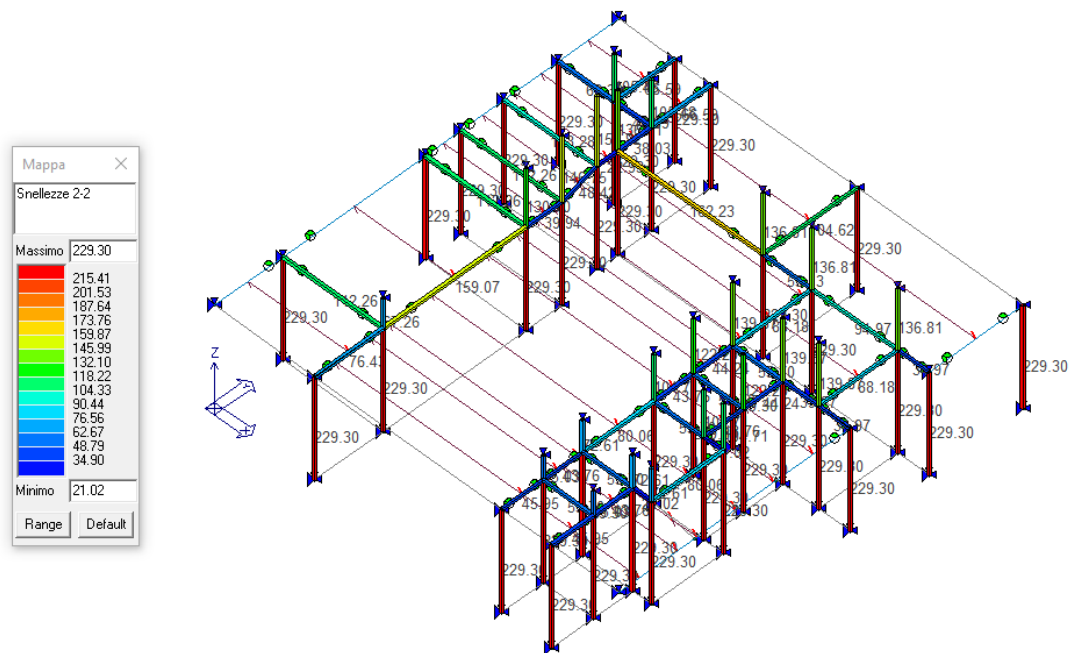
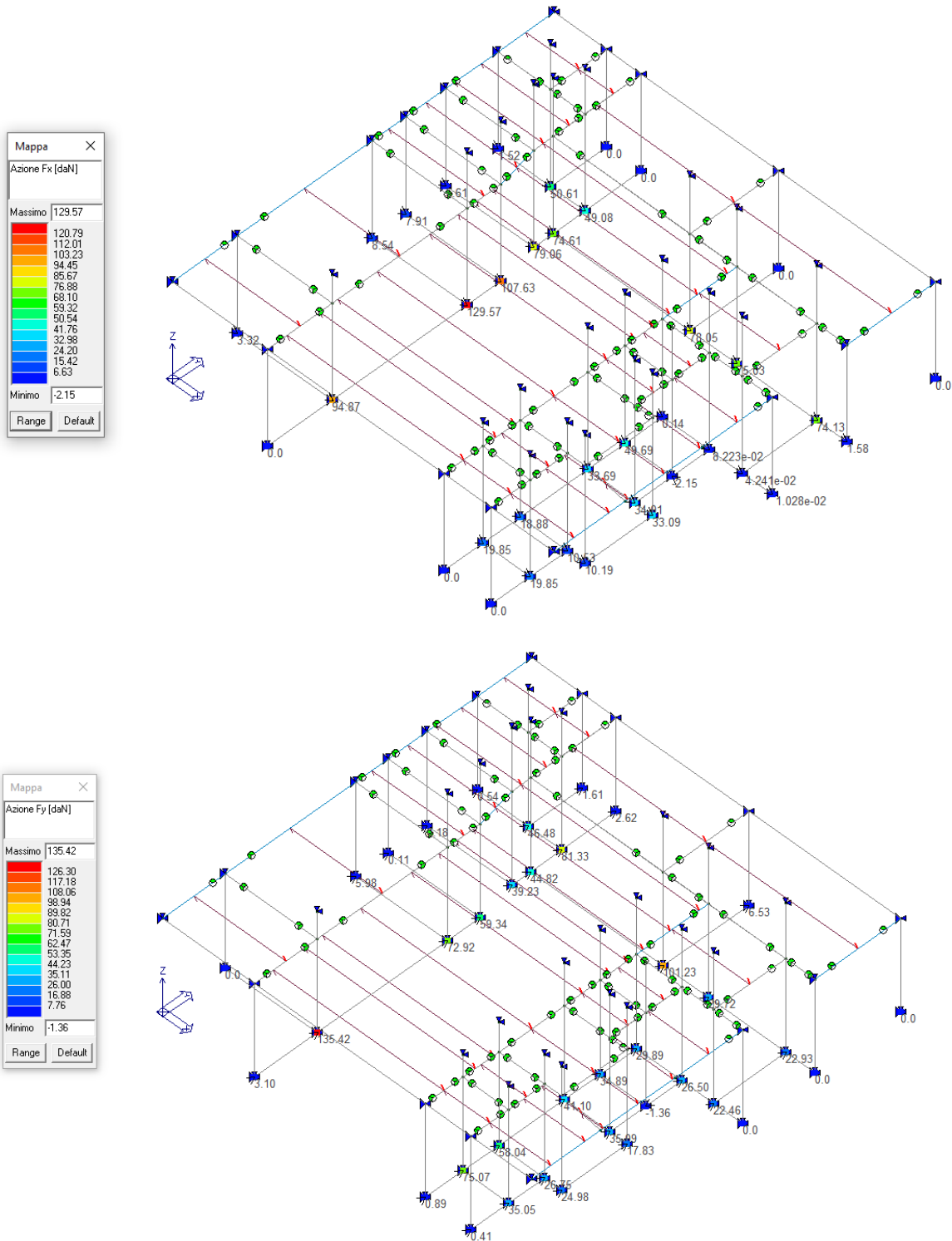


Fig 198. $\lambda < 250$ per membrature secondarie (NTC 2.018 par. 4.2.4.1.3.1) Verifica soddisfatta

1.1.1.2 Verifica unioni

- **Verifica fissaggi base dei pilastri**

Sollecitazioni base pilastri



$F_{Ris} = 188$ daN su 2 barre filettate HAS Hilti8 con ancoraggio chimico.

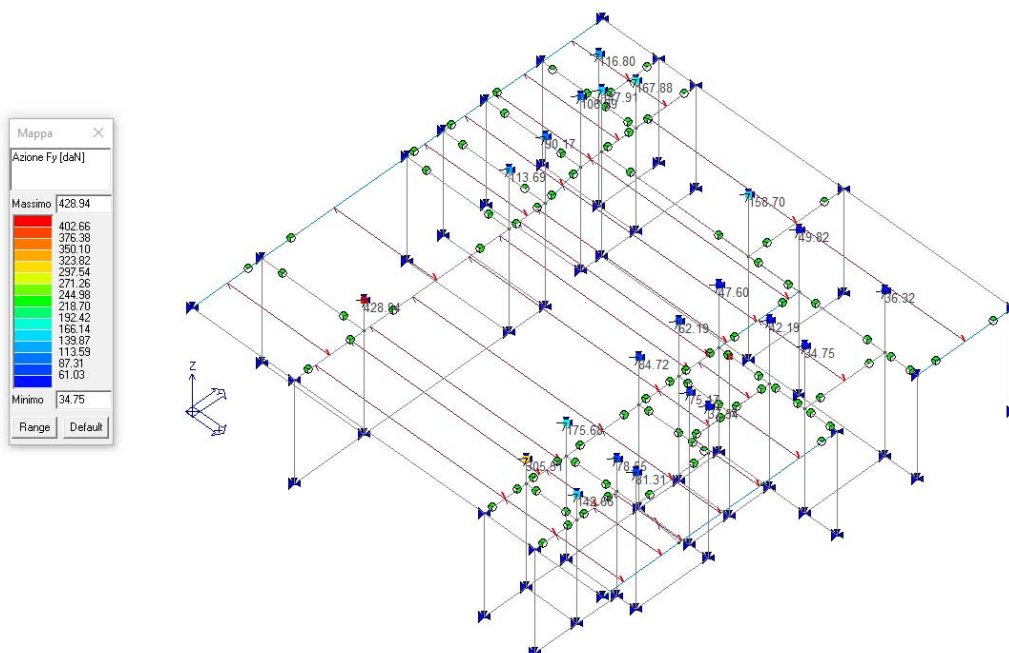
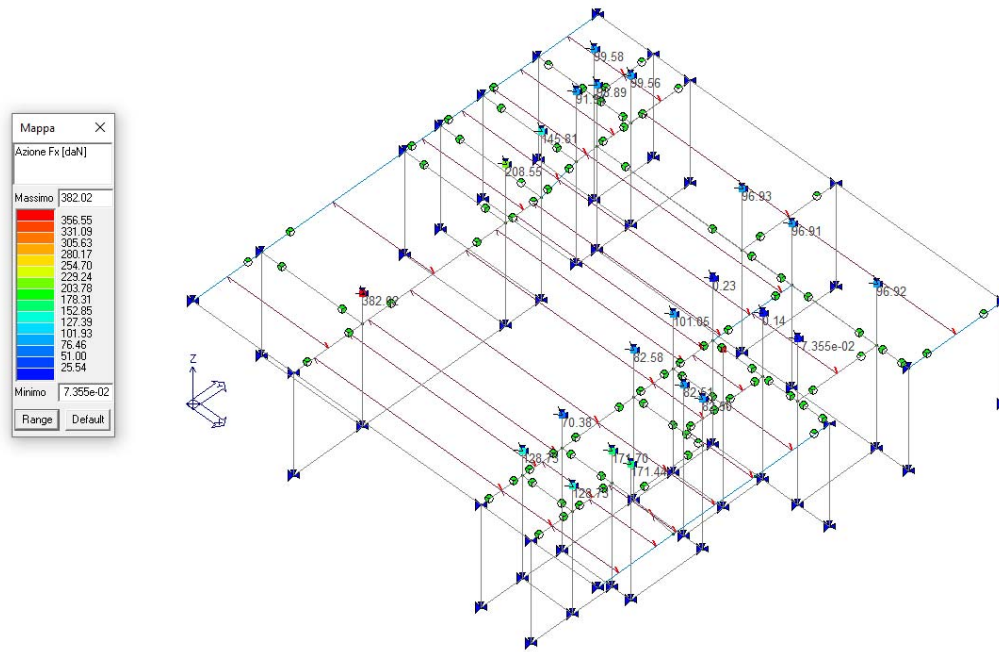
Per singola barra di ancoraggio a taglio $F_{ED} = 94$ daN

$F_{RD} = 490$ daN

Rapporto di verifica: $F_{Ed}/F_{Rd} = 0.19 \leq 1$

Verifica soddisfatta.

Sollecitazioni sommità pilastri



Verifica fissaggi base dei pilastri

$F_{Ris} = 575$ daN su 2 barre filettate HAS Hilti8 con ancoraggio chimico.

Per singola barra di ancoraggio a taglio $F_{ED} = 287$ daN

$F_{RD} = 490$ daN

Rapporto di verifica: $F_{Ed}/F_{Rd} = 0.58 \leq 1$

Verifica soddisfatta.

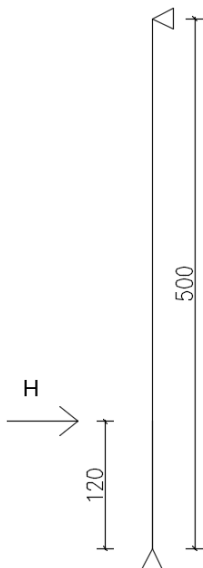
1.1.1.3 Verifica montanti

La verifica dei montanti della parete in cartongesso è stata effettuata sul montante più sollecitato, cioè quello di lunghezza maggiore pari a 5,00m.

La verifica del montante risulta soddisfatta adottando un profilo 50x75x50 spessore 0,8mm interasse 50 cm.

La sollecitazione più gravosa risulta quella dovuta al sovraccarico orizzontale applicato a 1,20 m dalla quota del pavimento.

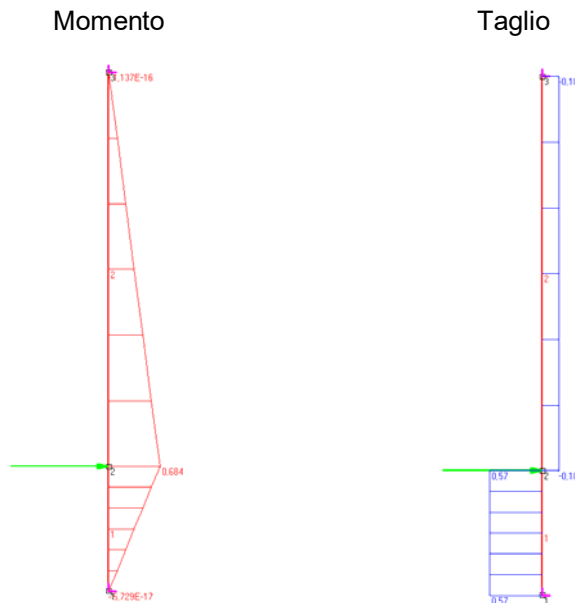
Schema statico



Combinazione di carico: Spinta della folla

$$S_f = H_k \cdot i \cdot \gamma_q = 100 \cdot 0.5 \cdot 1.5 = 75 \text{ daN}$$

Sollecitazioni

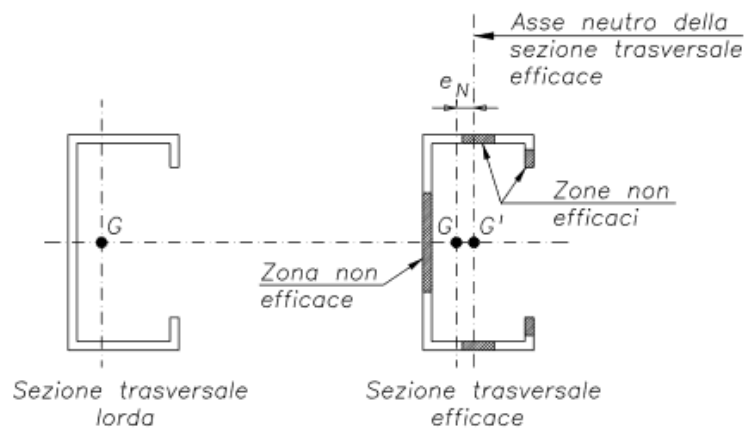


Momento massimo sollecitante $M_{Ed} = 68 \text{ daNm}$

Taglio massimo sollecitante $V_{Ed} = 57 \text{ daN}$

Verifica

Per il calcolo del Momento resistente del singolo montante si tiene conto del fatto che il profilo, per la sua geometria, ricade in classe 4, ovvero entra nel caso delle sezioni denominate “sezioni snelle” per le quali è necessario mettere in conto gli effetti dell’instabilità locale nel determinare il loro momento resistente, che sarà inferiore al momento al limite elastico, o la loro resistenza a compressione, che sarà inferiore alla forza che provoca la completa plasticizzazione della sezione. Per tener conto di quanto sopra il momento resistente viene determinato considerando un “modulo di resistenza efficace” calcolato sulla base delle sole zone della sezione che si possono ritenere efficaci, come rappresentato in figura.



Di seguito si riportano le grandezze inerziali efficaci relative al montante a C 75x50x0,8 mm :

- J_{eff} 130259 mm⁴ Momento di inerzia della sezione efficace
- W_{eff} 3286 mm³ Modulo di resistenza della sezione efficace

Considerando il profilo realizzato con acciaio tipo S235 si ha:

$$\text{Momento resistente: } M_{Rd} = \frac{(W_{eff} \cdot f_{yk})}{\gamma_s} = \left(\frac{3286 \cdot 235}{1,05} \right) \cdot 10^{-6} = 0,74 \text{ kNm}$$

$$\text{Taglio resistente: } V_{Rd} = \frac{f_{yk} \cdot A_{eff}}{\sqrt{3}} \cdot \frac{I_{eff} \cdot b}{S_x} = \frac{235 \cdot 1,05}{1,73} \cdot \frac{130259 \cdot 0,8}{1500} \cdot 10^{-3} = 9,0 \text{ kN}$$

Verifica Momento: $M_{Ed}/M_{Rd} = 68/74 = 0,92 < 1$ **verificato**

Verifica Taglio: $V_{Ed}/V_{Rd} = 57/900 = 0,06 < 1$ **verificato**

Verifica Profili Controsoffitto In Cartongesso Autoportante

profilo a C 50x100x50 spessore 0,8mm

Interasse: 0,50 m

Luce massima di calcolo: 5,45 m

Carico distribuito dovuto al peso del controsoffitto: 0,25 kN/mq

Carico sul singolo profilo (comb. SLU): $q = 1,5 \times (0,25 \times 0,50) = 0,19 \text{ kN/m}$

$M_{Ed} = 0,70 \text{ kNm}$

$M_{Rd} = 1,00 \text{ kNm}$

$M_{Ed} < M_{Rd}$

verificato

2.2.9 Verifica vasca di laminazione

Si riportano le verifiche a SLU delle pareti.

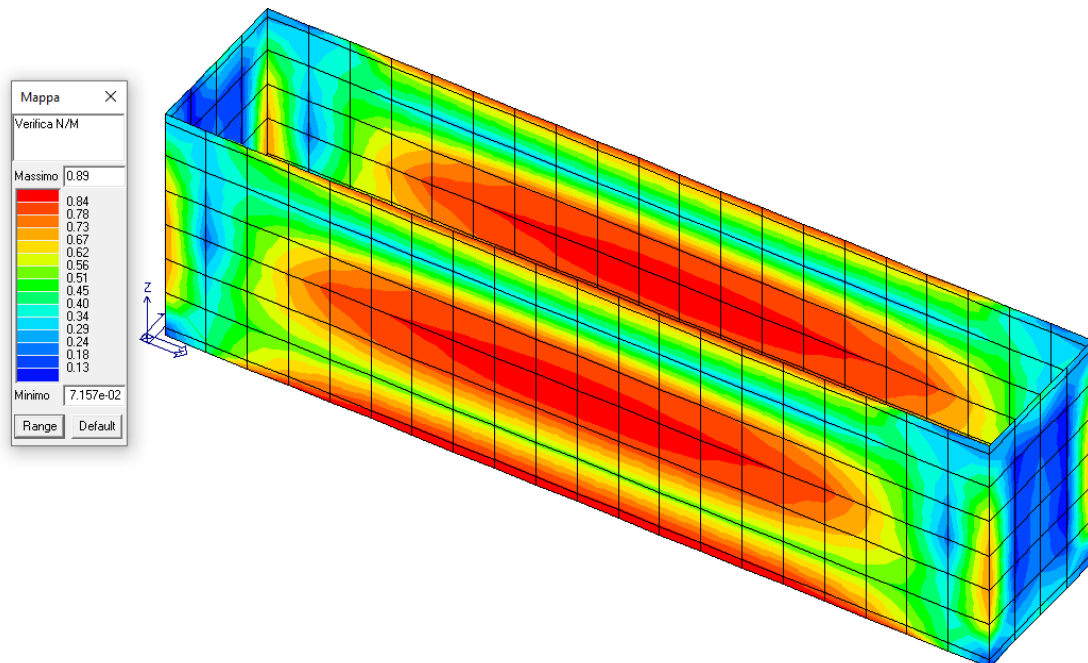


Fig 199. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

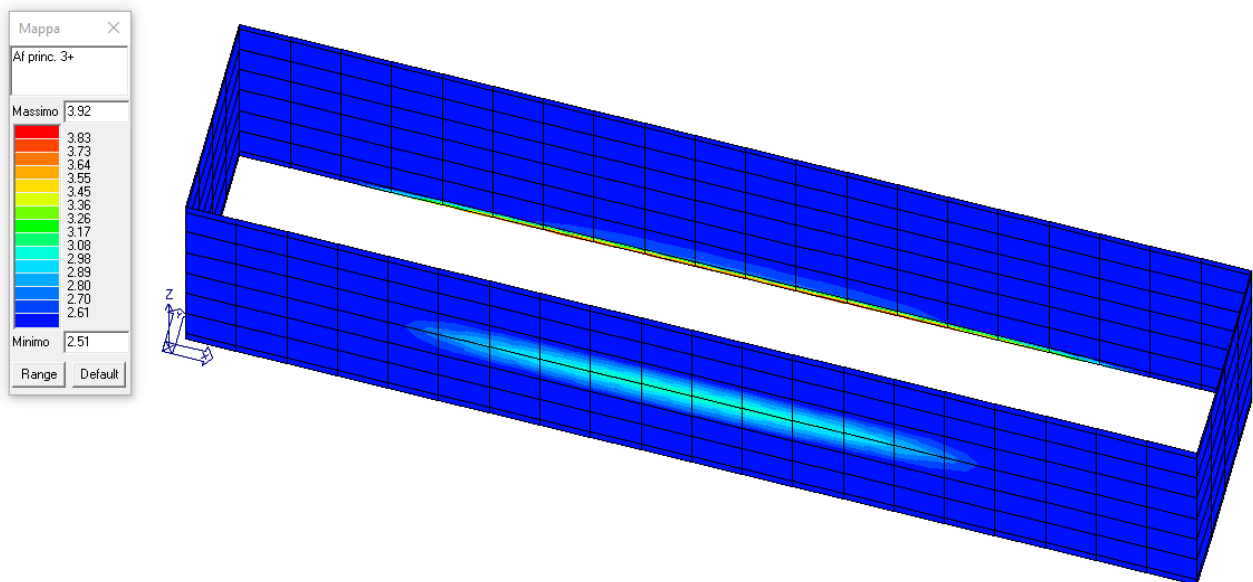


Fig 200. Mappa Armatura Verticale Faccia Positiva da Calcolo [cm^2/m]. .

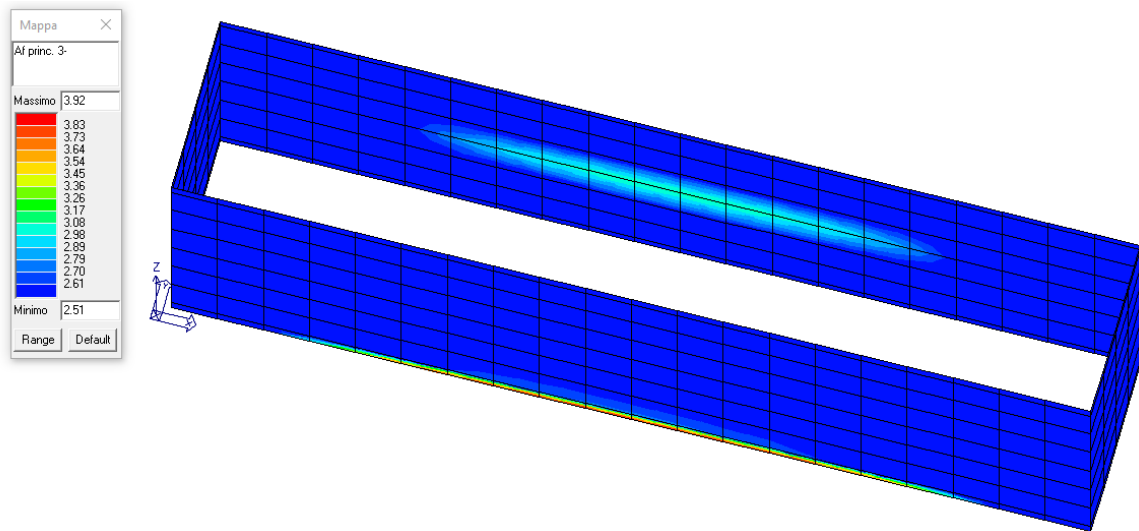


Fig 201. Mappa Armatura Verticale Faccia Negativa da Calcolo [cm²/m]. .

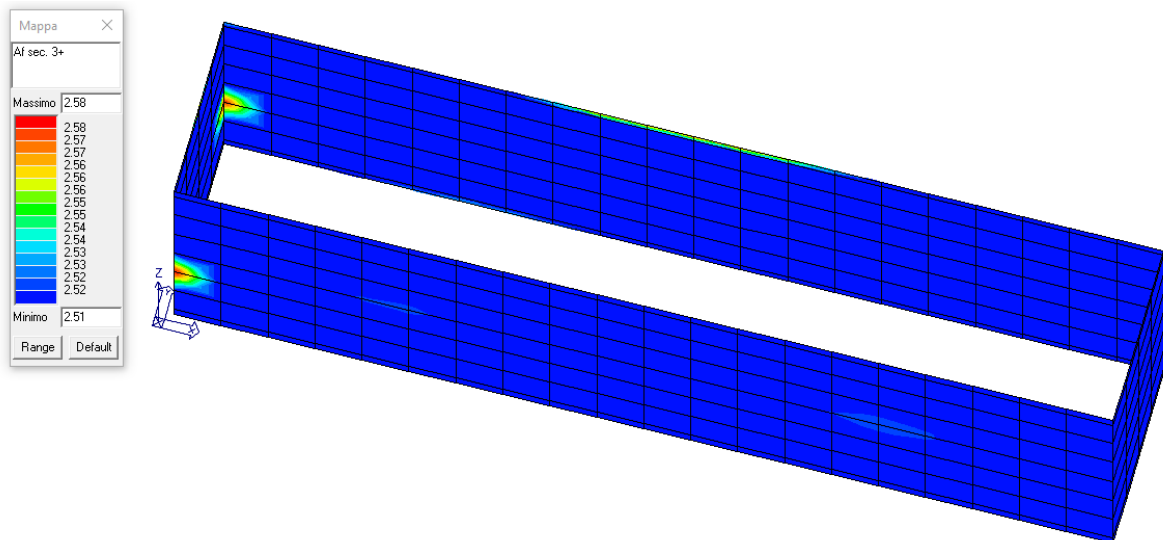


Fig 202. Mappa Armatura Orizzontale Faccia Positiva da Calcolo [cm²/m]. .

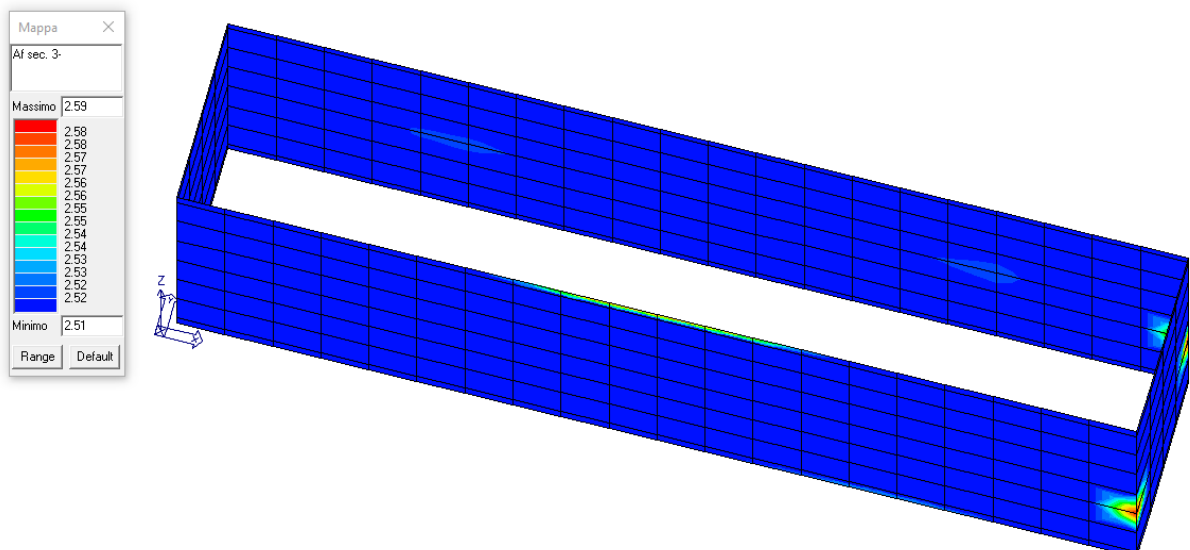


Fig 203. Mappa Armatura Orizzontale Faccia Negativa da Calcolo [cm²/m]. .

Si riportano le verifiche a SLU della soletta e della platea.

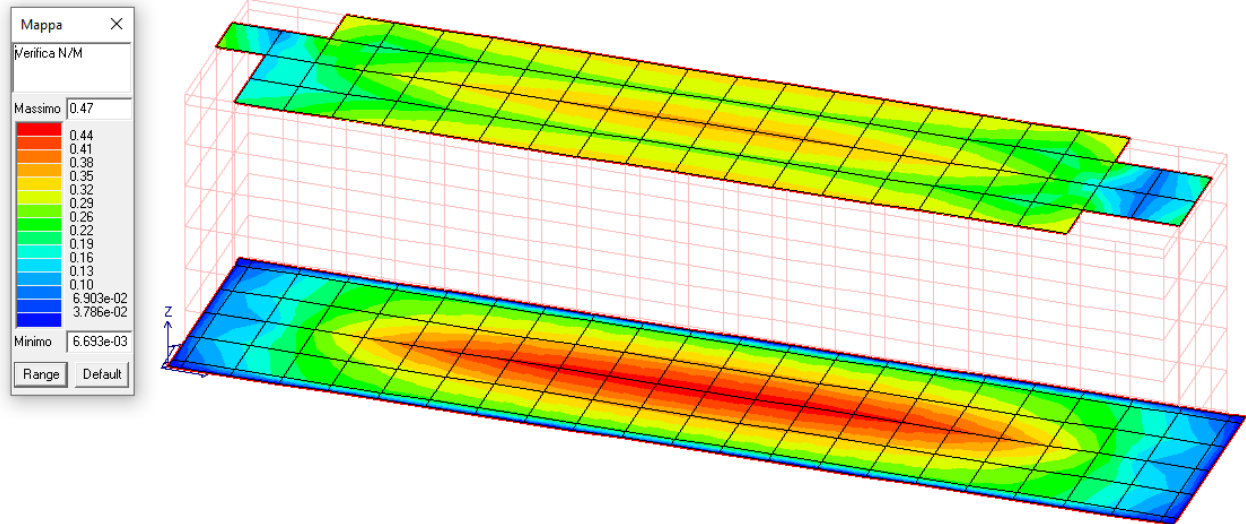


Fig 204. SLU: Mappa di verifica N/M – Verifiche soddisfatte ($\rho \leq 1$).

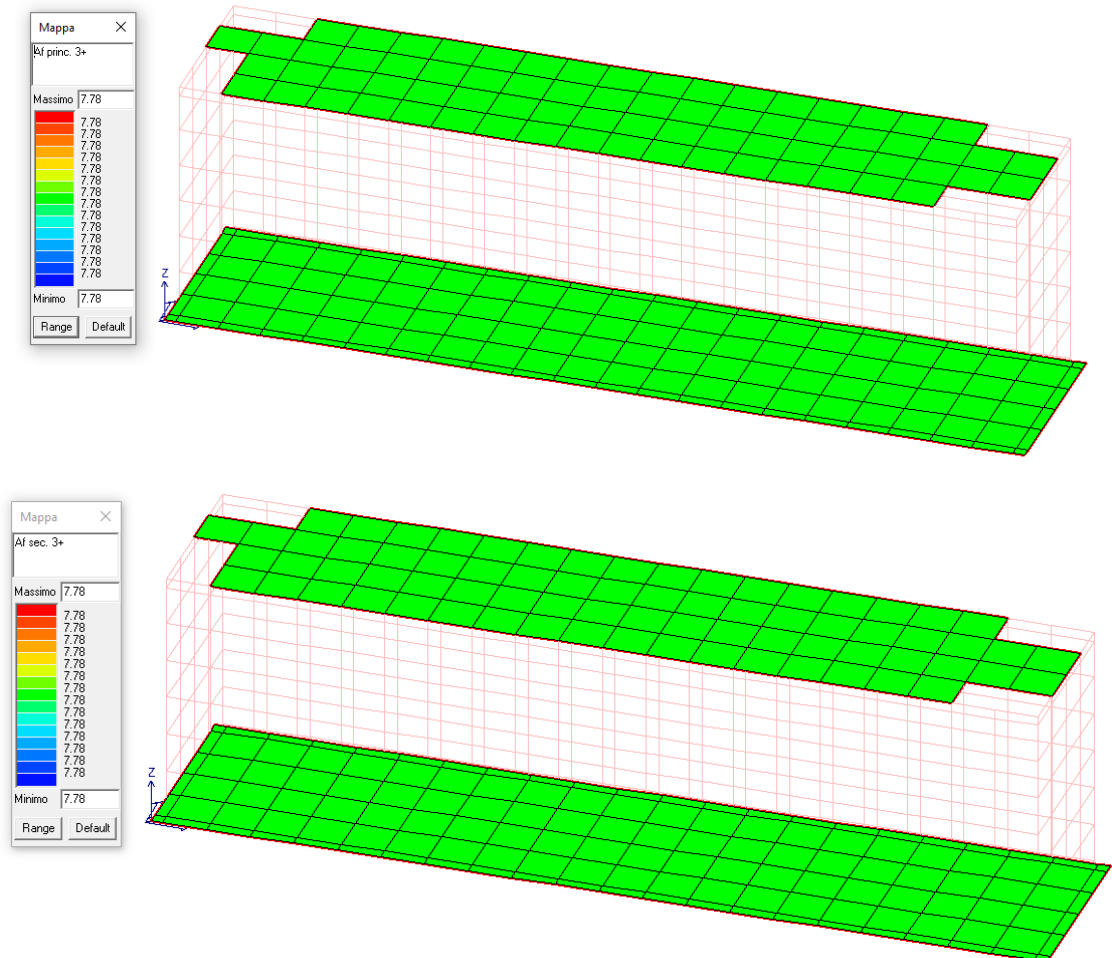


Fig 205. Soletta e platea in c.a.: Armatura superiore (dir. X e dir Y)

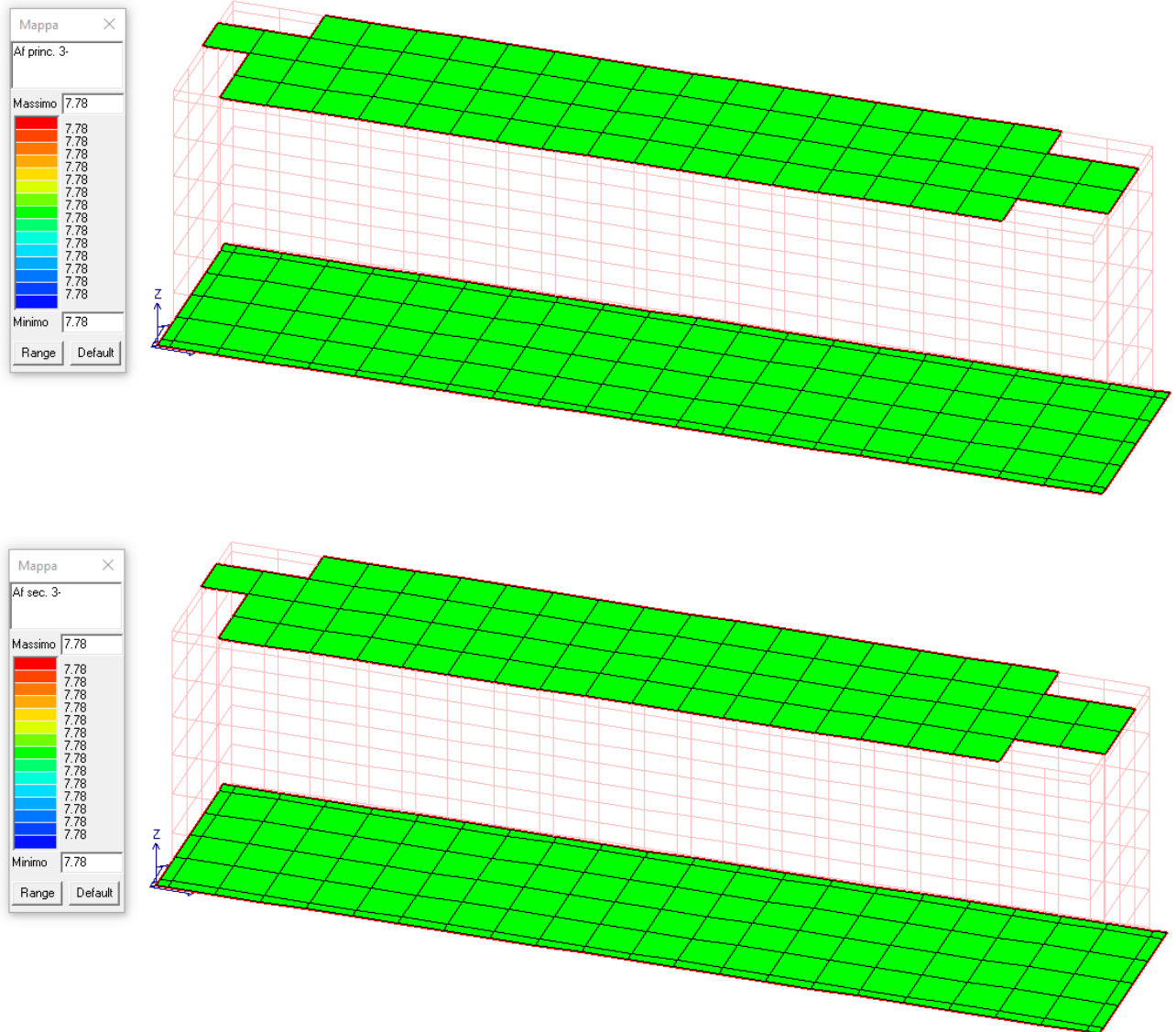


Fig 206. Soletta e platea in c.a.: Armatura inferiore (dir. X e dir Y)

Tutte le armature previste in progetto sono tutte uguali o maggiori rispetto a quanto richiesto da modello di calcolo.

Fig 207.

2.3 Verifiche agli Stati Limite di Esercizio

2.3.1 Verifica degli Spostamenti Relativi come da da §7.3.6.1 D.M.17.01.2018

2.3.1.1 Verifiche agli SLD

Per le costruzioni ricadenti in **Classe d’Uso I e II** si deve verificare che l’azione sismica di progetto non produca agli elementi costruttivi senza funzione strutturale danni tali da rendere la costruzione temporaneamente inagibile.

Nel caso delle costruzioni civili ed industriali, qualora la temporanea inagibilità sia dovuta a spostamenti eccessivi di interpiano, questa condizione si può ritenere soddisfatta quando gli spostamenti di interpiano ottenuti dall’analisi in presenza dell’azione sismica di progetto relativa allo SLD siano inferiori, nel caso in esame, ai limiti indicati di seguito:

nel caso in esame, la Struttura in c.a. da realizzare in opera è stata dimensionata e verificata per considerando un limite di spostamento relativo di interpiano d_{rp} allo SLD di **0.002h** come da punto **[7.3.13] §7.3.6.1 DM17.01.2018**, in accordo con il §7.5 delle *Linee Guida per Sistemi Costruttivi a Pannelli Portanti basati sull’impiego di blocchi cassero e calcestruzzo debolmente armato gettato in opera (luglio 2011)*.

Pertanto affinché la verifica sia soddisfatta occorre che:

$$d_{rp} \leq 0.002h;$$

dove:

d_{rp} : è lo spostamento di interpiano, ovvero la differenza tra gli spostamenti al solaio superiore ed inferiore;

h : altezza di interpiano.

Verifica [RIG]

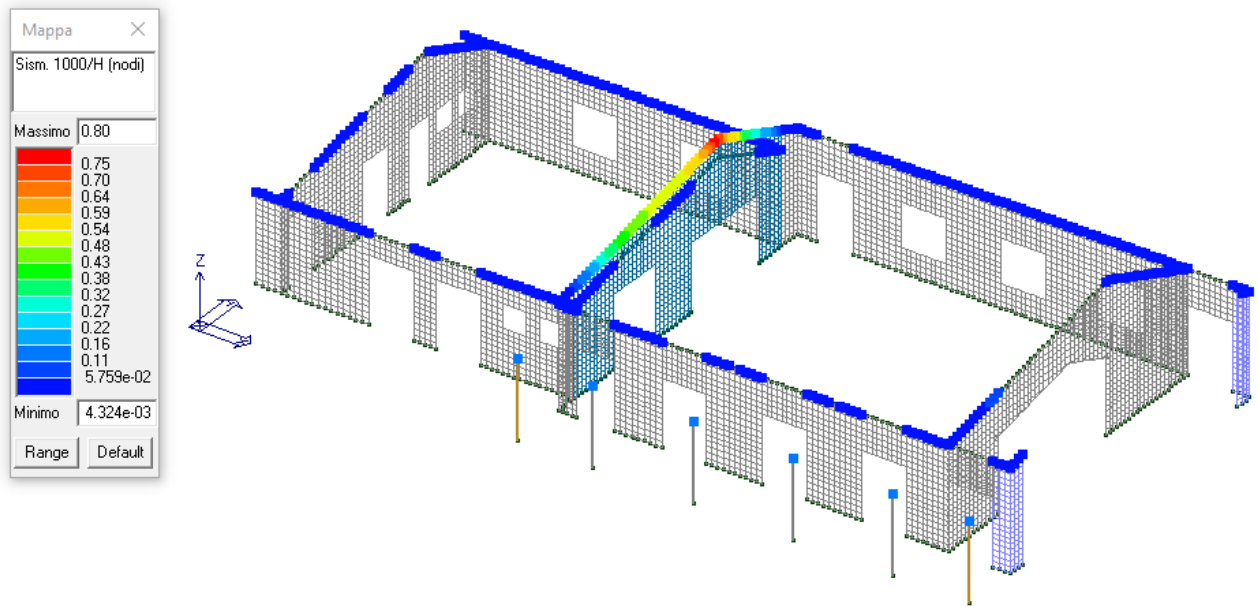


Fig 208. Spostamenti relativi d'interpiano massimi "d_r" per SLD valutati sui pilastri.

$d_{rp,SLD} = 0.0008 h \leq 0.002h$

Verifica soddisfatta.

2.3.2 Verifica Pareti ISOTEX agli SLE

Vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

In particolare vengono riportati i risultati relativi alle tre categorie di combinazione considerate:

- Combinazioni Rare
- Combinazioni Frequenti
- Combinazioni Quasi Permanenti.

Le tensioni in esercizio sono state limitate ai seguenti valori:

Calcestruzzo $\sigma_{c,lim} = 0.45 \times f_{ck} = 112.5 \text{ MPa}$ comb. permanente [4.1.16]

$\sigma_{c,lim} = 0.60 \times f_{ck} = 150 \text{ MPa}$ comb. rara [4.1.15]

Acciaio $\sigma_{s,lim} = 0.80 \times f_{yk} = 360 \text{ MPa}$ comb. rara [4.1.17]

I valori di interesse sono i seguenti:

rRfck rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni rare [normalizzato a 1]

rRfyk rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni rare [normalizzato a 1]

rPfck rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni quasi permanenti [normalizzato a 1].

Lo stato limite di fessurazione è stato condotto con riferimento al metodo tabellare, assumendo le seguenti condizioni:

- ambiente ordinario
- armatura poco sensibile alla corrosione
- apertura di fessura limite $w_{lim} = w_3 = 0.40 \text{ mm}$ comb. Frequente
 $w_{lim} = w_2 = 0.30 \text{ mm}$ comb. Quasi Permanente

Tab. 4.1.IV - Criteri di scelta dello stato limite di fessurazione

| Gruppi di Esigenze | Condizioni ambientali | Combinazione di azioni | Armatura | | | |
|--------------------|-----------------------|------------------------|--------------------|------------|------------------|------------|
| | | | Sensibile | | Poco sensibile | |
| | | | Stato limite | w_k | Stato limite | w_k |
| A | Ordinarie | frequente | apertura fessure | $\leq w_2$ | apertura fessure | $\leq w_3$ |
| | | quasi permanente | apertura fessure | $\leq w_1$ | apertura fessure | $\leq w_2$ |
| B | Aggressive | frequente | apertura fessure | $\leq w_1$ | apertura fessure | $\leq w_2$ |
| | | quasi permanente | decompressione | - | apertura fessure | $\leq w_1$ |
| C | Molto aggressive | frequente | formazione fessure | - | apertura fessure | $\leq w_1$ |
| | | quasi permanente | decompressione | - | apertura fessure | $\leq w_1$ |

Di seguito si riporta la modellazione dei setti oggetto di verifica:

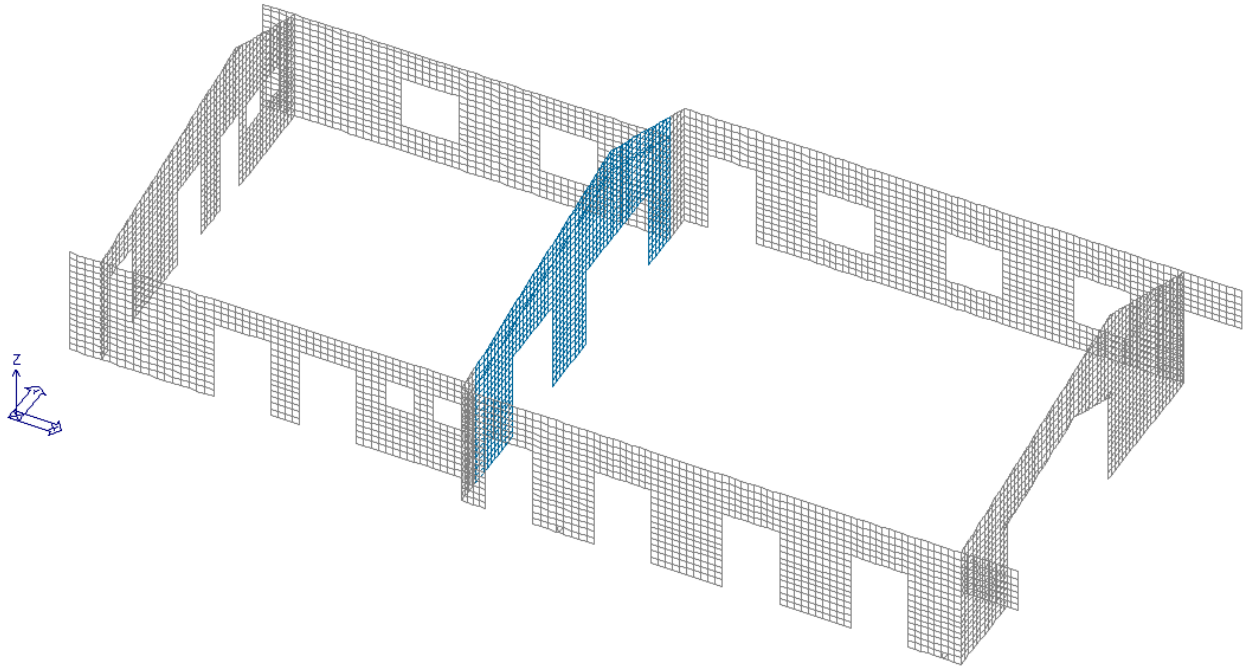


Fig 209. Modellazione Setti oggetto di verifica.

Verifica Apertura di Fessura

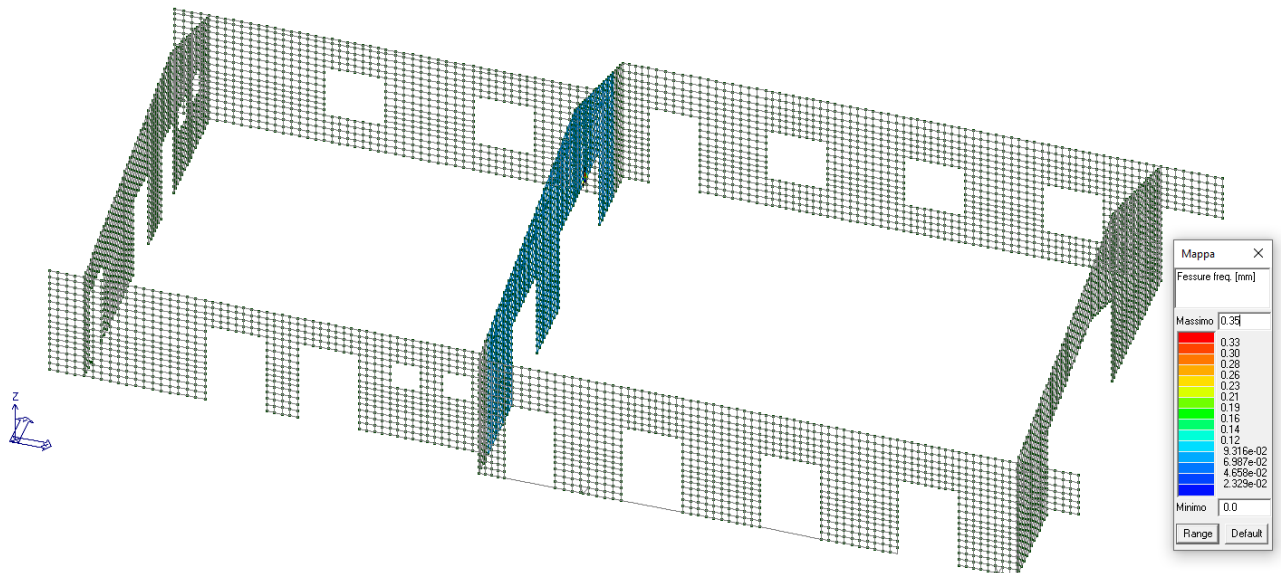


Fig 210. Cmb. SLE Frequente: Verifica Apertura di Fessura [$w_{max} = 0.0 \text{ mm} < w_3 = 0.4 \text{ mm}$].

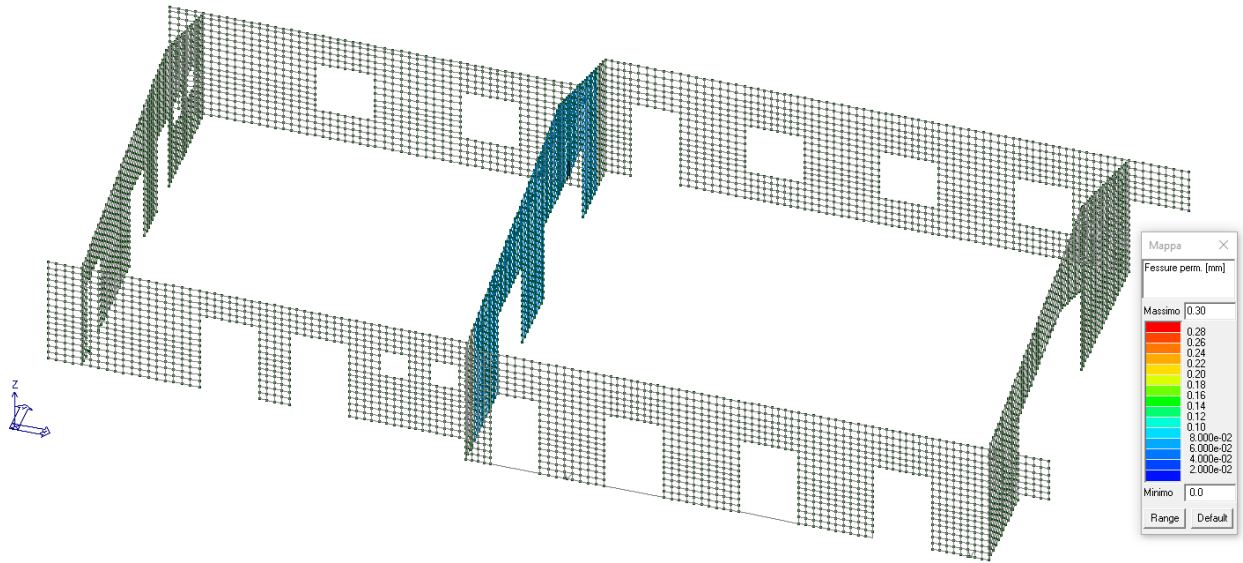


Fig 211. Cmb. SLE Quasi Perm.: Verifica Apertura di Fessura [$w_{max}= 0.0 \text{ mm} < w_3= 0.3 \text{ mm}$].

Verifica Apertura di Fessura Soddisfatta.

Mappe Cromatiche di verifica

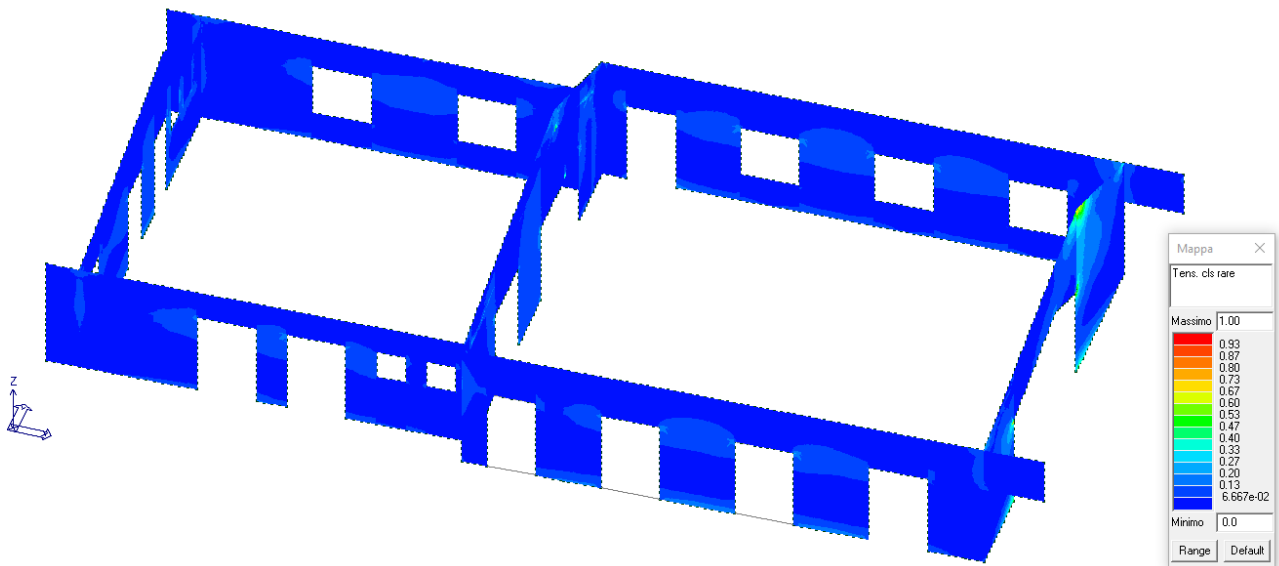


Fig 212. Verifiche SLE: Mappa verifica tensioni cls Cmb. Rare [$0.52 \leq 1.0$].

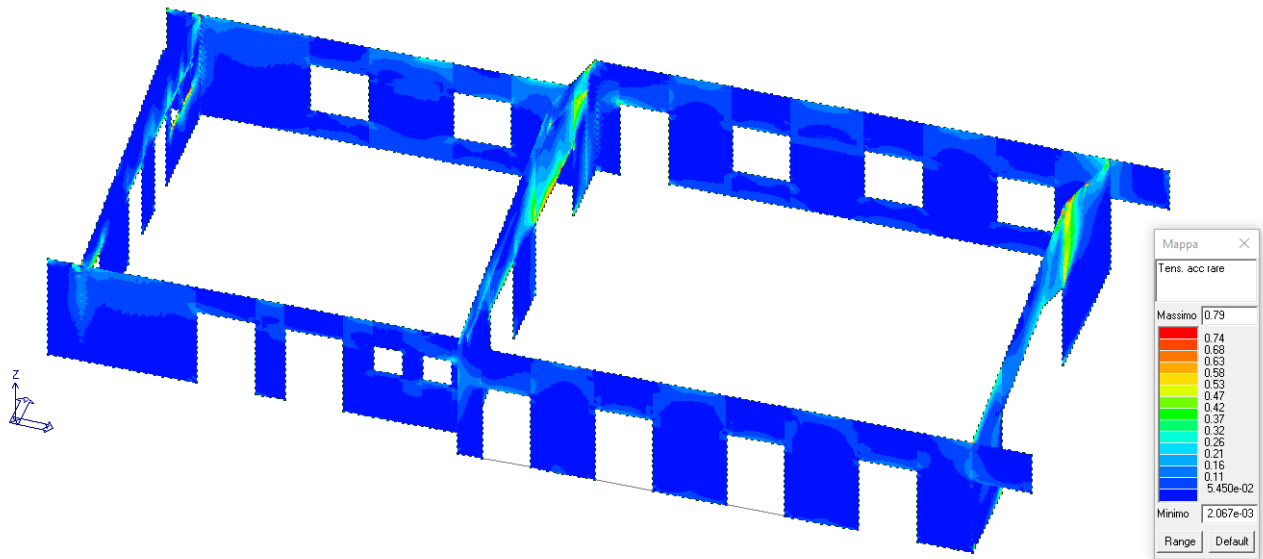


Fig 213. Verifiche SLE: Mappa Verifica Tensioni acciaio Cmb. Rare [$0.75 \leq 1.0$].

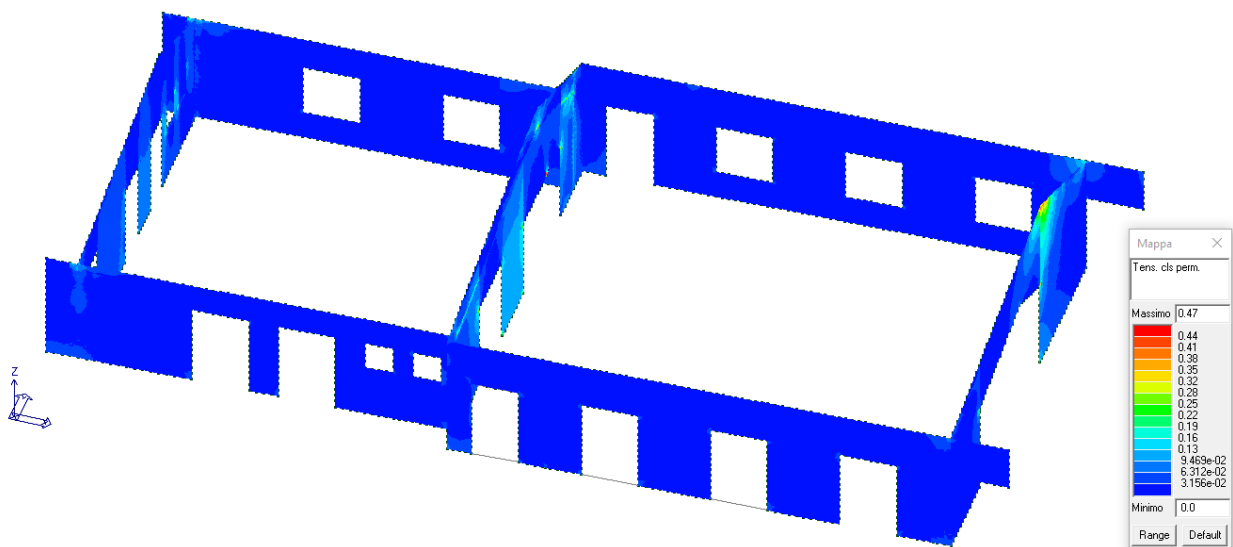


Fig 214. Verifiche SLE: Mappa Verifica Tensioni cls. Cmb. Quasi Permanenti [$0.47 \leq 1.0$].

Verifica Stato Tensionale Massimo dei materiali Soddisfatto.

2.3.3 Verifica Cordoli Spiccato Elevazioni agli SLE

Vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

In particolare vengono riportati i risultati relativi alle tre categorie di combinazione considerate:

- Combinazioni Rare
- Combinazioni Frequenti
- Combinazioni Quasi Permanenti.

Le tensioni in esercizio sono state limitate ai seguenti valori:

| | | | |
|--------------|---|------------------|----------|
| Calcestruzzo | $\sigma_{c,lim} = 0.45 \times f_{ck} = 112.5 \text{ MPa}$ | comb. permanente | [4.1.16] |
| | $\sigma_{c,lim} = 0.60 \times f_{ck} = 150 \text{ MPa}$ | comb. rara | [4.1.15] |
| Acciaio | $\sigma_{s,lim} = 0.80 \times f_{yk} = 360 \text{ MPa}$ | comb. rara | [4.1.17] |

I valori di interesse sono i seguenti:

rRfck rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni rare [normalizzato a 1]

rRfyk rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni rare [normalizzato a 1]

rPfck rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni quasi permanenti [normalizzato a 1].

Lo stato limite di fessurazione è stato condotto con riferimento al metodo tabellare, assumendo le seguenti condizioni:

- ambiente ordinario
- armatura poco sensibile alla corrosione
- apertura di fessura limite $w_{lim} = w_3 = 0.40 \text{ mm}$ comb. Frequente
 $w_{lim} = w_2 = 0.30 \text{ mm}$ comb. Quasi Permanente

Tab. 4.1.IV • Criteri di scelta dello stato limite di fessurazione

| Gruppi di Esigenze | Condizioni ambientali | Combinazione di azioni | Armatura | | | |
|--------------------|-----------------------|------------------------|--------------------|------------|------------------|------------|
| | | | Sensibile | | Poco sensibile | |
| | | | Stato limite | w_k | Stato limite | w_k |
| A | Ordinarie | frequente | apertura fessure | $\leq w_2$ | apertura fessure | $\leq w_3$ |
| | | quasi permanente | apertura fessure | $\leq w_1$ | apertura fessure | $\leq w_2$ |
| B | Aggressive | frequente | apertura fessure | $\leq w_1$ | apertura fessure | $\leq w_2$ |
| | | quasi permanente | decompressione | - | apertura fessure | $\leq w_1$ |
| C | Molto aggressive | frequente | formazione fessure | - | apertura fessure | $\leq w_1$ |
| | | quasi permanente | decompressione | - | apertura fessure | $\leq w_1$ |

Verifica Apertura di Fessura

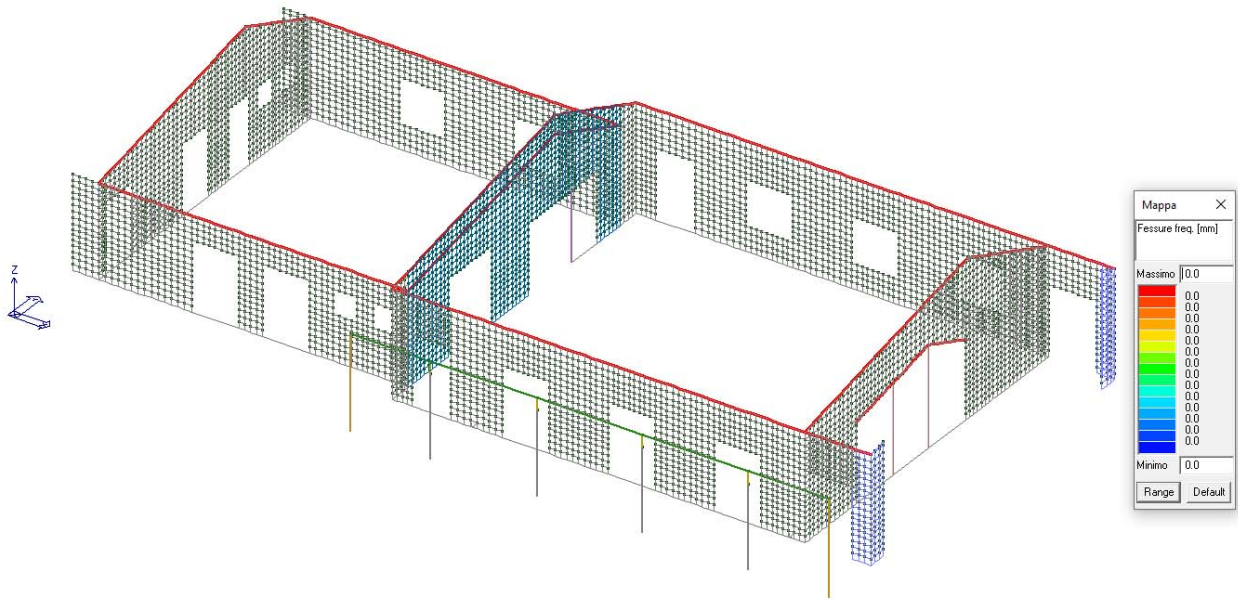


Fig 215. Cmb. SLE Frequente: Verifica Apertura di Fessura [$w_{max}= 0.0 \text{ mm} < w_3= 0.4 \text{ mm}$].

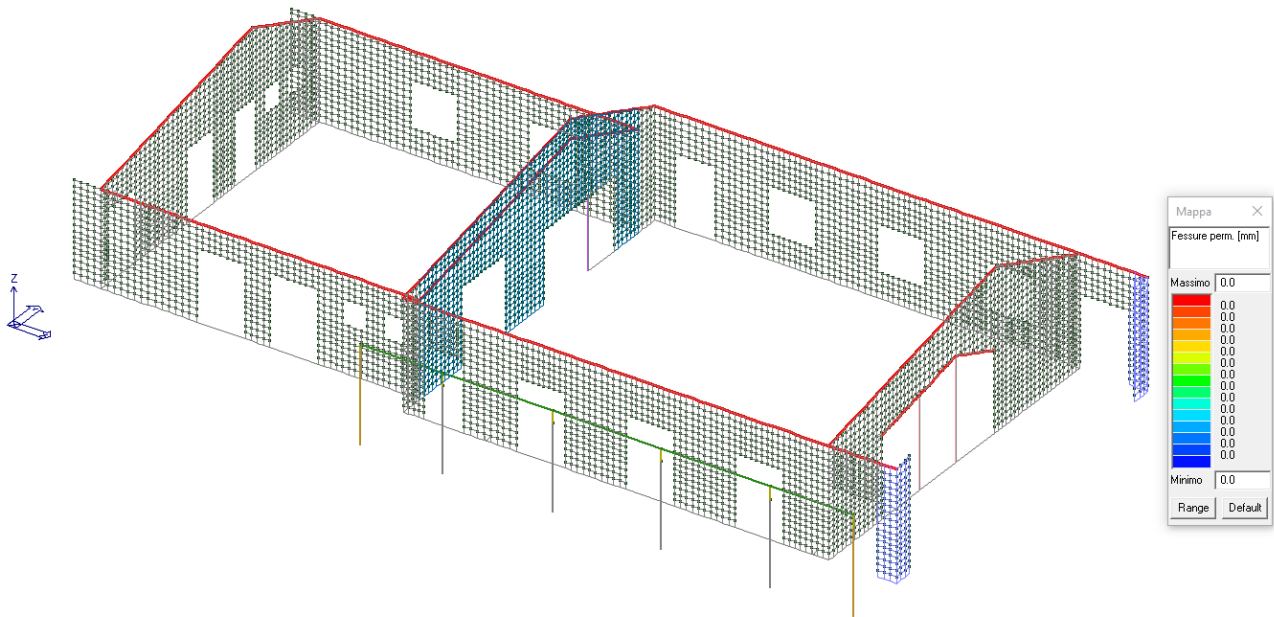


Fig 216. Cmb. SLE Quasi Perm.: Verifica Apertura di Fessura [$w_{max}= 0.0 \text{ mm} < w_3= 0.3 \text{ mm}$].

Verifica Apertura di Fessura Soddisfatta.

Verifica Stato Tensionale

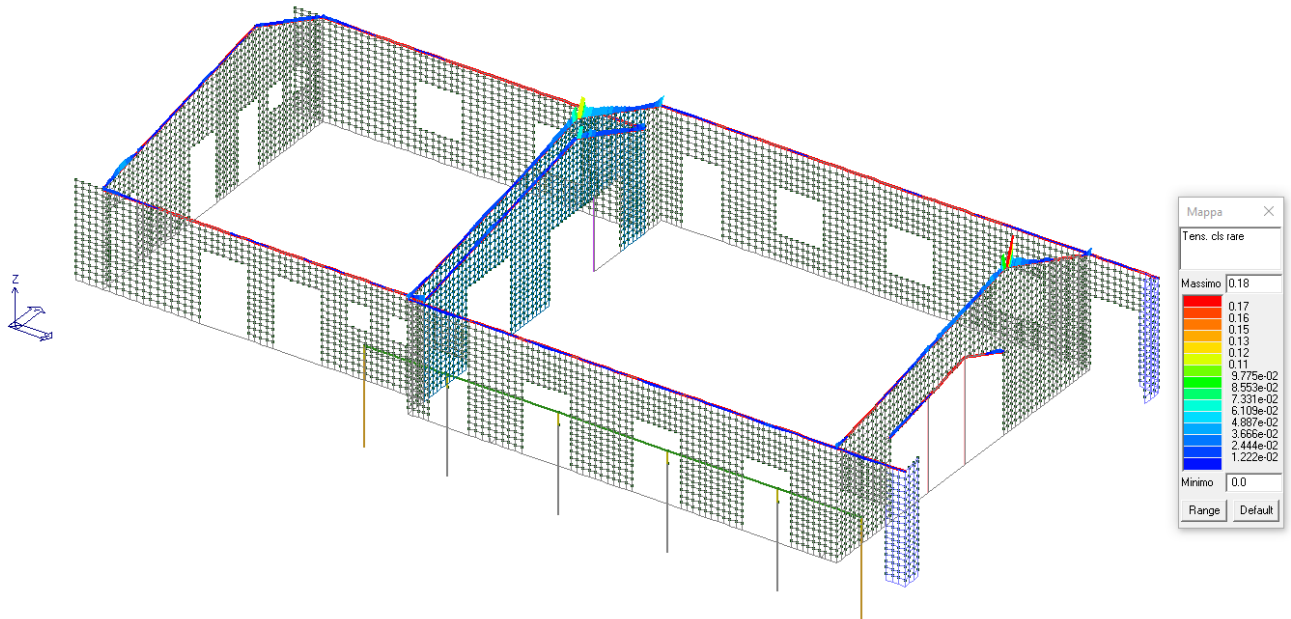


Fig 217. Cmb. SLE Rara: Rapporto di Verifica Stato tensionale max del cls [$0.18 \leq 1.0$ Verifica soddisfatta].

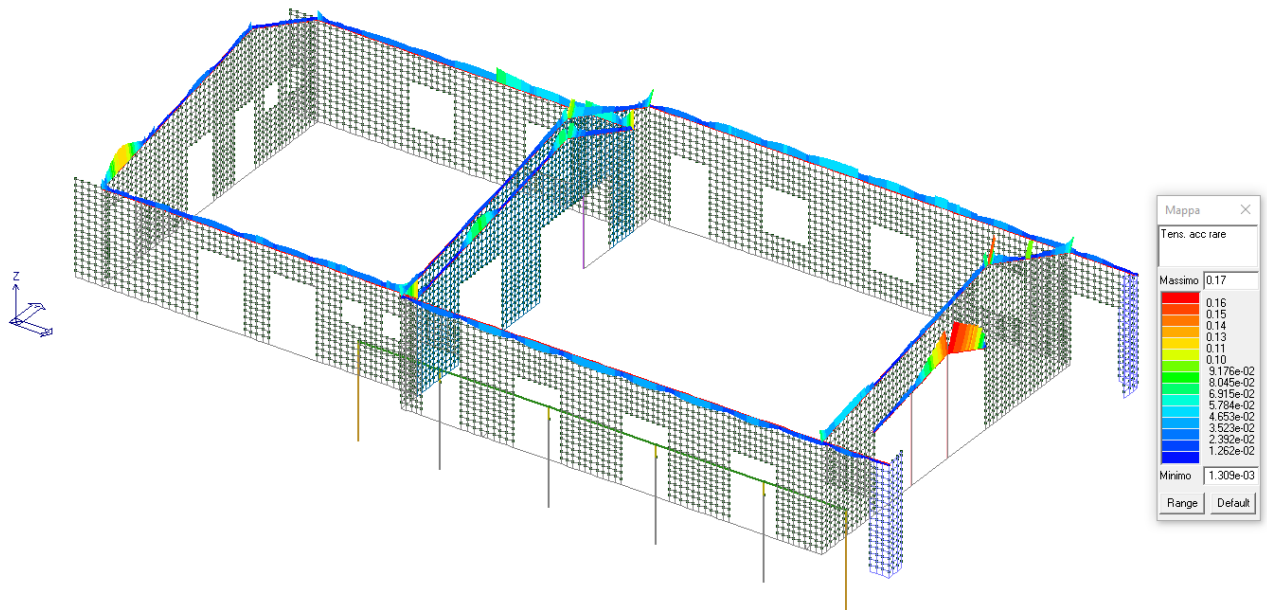


Fig 218. Cmb. SLE Rara: Rapporto di Verifica Stato tensionale max dell'acciaio [$0.17 \leq 1.0$ Verifica soddisfatta].

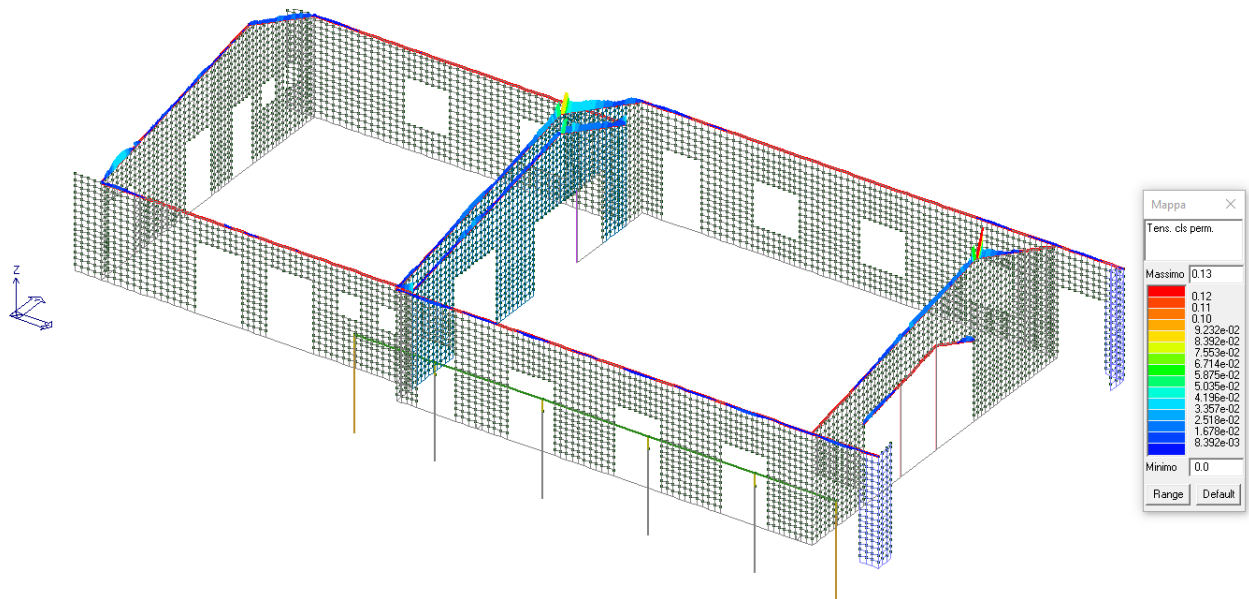


Fig 219. Cmb. SLE Quasi Perm.: Rapporto di Verifica Stato tensionale max del cls [0.14 ≤ 1.0 Verifica soddisfatta].

Verifica Stato tensionale massimo dei materiali Soddisfatta.

2.3.4 Verifica Setti in c.a. di fondazione agli SLE

Vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

In particolare vengono riportati i risultati relativi alle tre categorie di combinazione considerate:

- Combinazioni Rare
- Combinazioni Frequenti
- Combinazioni Quasi Permanenti.

Le tensioni in esercizio sono state limitate ai seguenti valori:

| | | | |
|--------------|--|------------------|----------|
| Calcestruzzo | $\sigma_{c,lim} = 0.45 \times f_{ck} = 11.2 \text{ MPa}$ | comb. permanente | [4.1.16] |
| | $\sigma_{c,lim} = 0.60 \times f_{ck} = 14.9 \text{ MPa}$ | comb. rara | [4.1.15] |
| Acciaio | $\sigma_{s,lim} = 0.80 \times f_{yk} = 360 \text{ MPa}$ | comb. rara | [4.1.17] |

I valori di interesse sono i seguenti:

rRfck rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni rare [normalizzato a 1]

rRfyk rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni rare [normalizzato a 1]

rPfck rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni quasi permanenti [normalizzato a 1].

Verifica Stato Tensionale

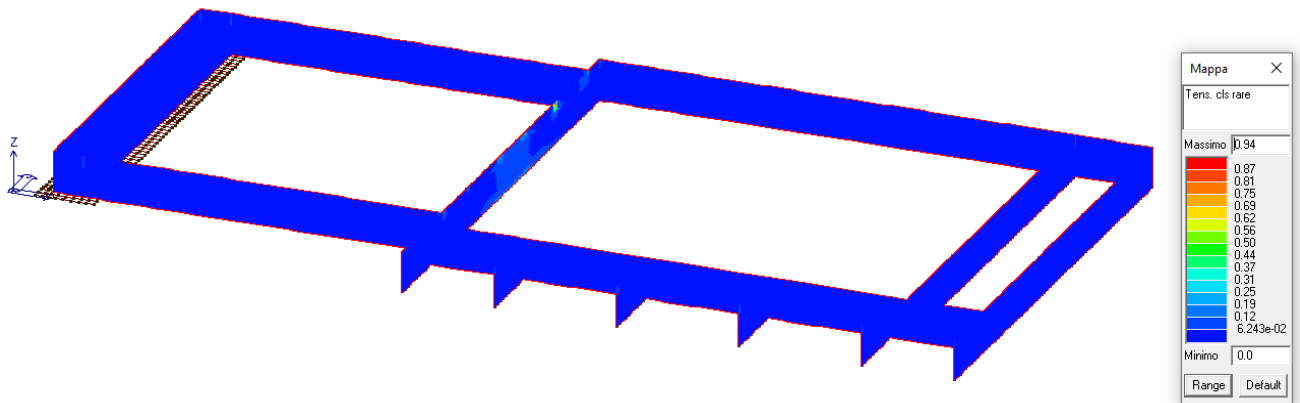


Fig 220. Cmb. SLE Rara: Rapporto di Verifica Stato tensionale max del cls [0.94 ≤ 1.0 Verifica soddisfatta].

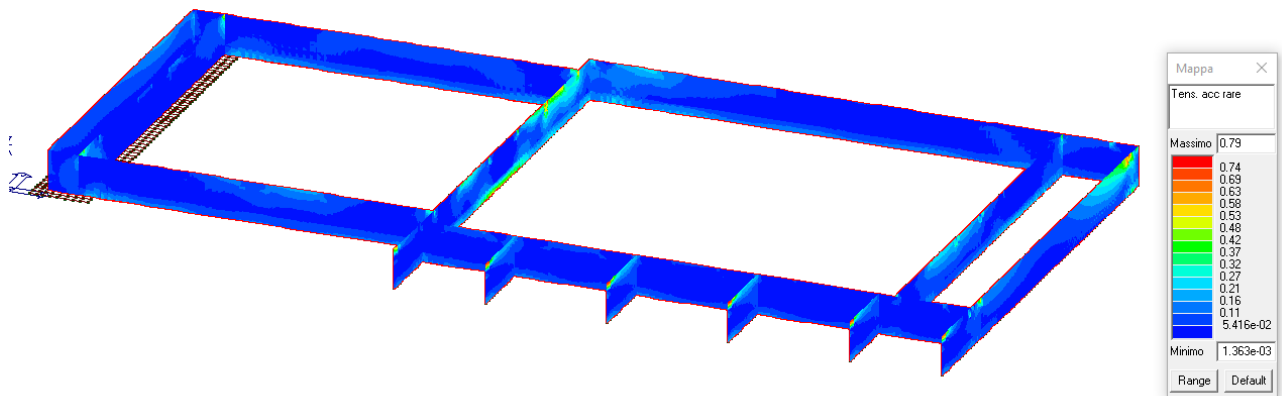


Fig 221. Cmb. SLE Rara: Rapporto di Verifica Stato tensionale max dell'acciaio [0.79 ≤ 1.0 Verifica soddisfatta].

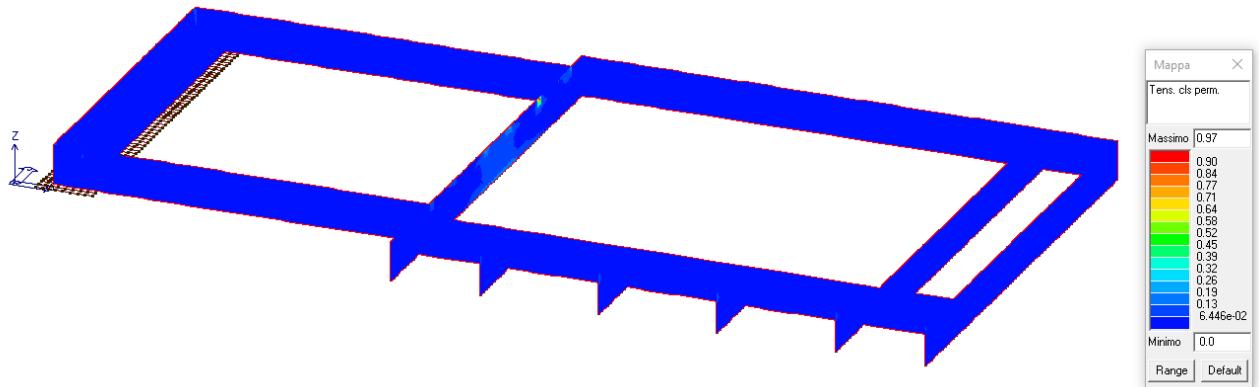


Fig 222. Cmb. SLE Quasi Perm.: Rapporto di Verifica Stato tensionale max del cls [$0.97 \leq 1.0$ Verifica soddisfatta].

Verifica Stato tensionale massimo dei materiali Soddisfatta.

2.3.5 Verifica Travi di Fondazione agli SLE

Vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

In particolare vengono riportati i risultati relativi alle tre categorie di combinazione considerate:

- Combinazioni Rare
- Combinazioni Frequenti
- Combinazioni Quasi Permanenti.

Le tensioni in esercizio sono state limitate ai seguenti valori:

| | | | |
|--------------|--|------------------|----------|
| Calcestruzzo | $\sigma_{c,lim} = 0.45 \times f_{ck} = 11.2 \text{ MPa}$ | comb. permanente | [4.1.16] |
| | $\sigma_{c,lim} = 0.60 \times f_{ck} = 14.9 \text{ MPa}$ | comb. rara | [4.1.15] |
| Acciaio | $\sigma_{s,lim} = 0.80 \times f_{yk} = 360 \text{ MPa}$ | comb. rara | [4.1.17] |

I valori di interesse sono i seguenti:

rRfck rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni rare [normalizzato a 1]

rRfyk rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni rare [normalizzato a 1]

rPfck rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni quasi permanenti [normalizzato a 1].

Lo stato limite di fessurazione è stato condotto con riferimento al metodo tabellare, assumendo le seguenti condizioni:

- ambiente ordinario
- armatura poco sensibile alla corrosione
- apertura di fessura limite $w_{lim} = w_3 = 0.40 \text{ mm}$ comb. Frequente
 $w_{lim} = w_2 = 0.30 \text{ mm}$ comb. Quasi Permanente

Tab. 4.1.IV • Criteri di scelta dello stato limite di fessurazione

| Gruppi di Esigenze | Condizioni ambientali | Combinazione di azioni | Armatura | | | |
|--------------------|-----------------------|------------------------|--------------------|------------|------------------|------------|
| | | | Sensibile | | Poco sensibile | |
| | | | Stato limite | w_k | Stato limite | w_k |
| A | Ordinarie | frequente | apertura fessure | $\leq w_2$ | apertura fessure | $\leq w_3$ |
| | | quasi permanente | apertura fessure | $\leq w_1$ | apertura fessure | $\leq w_2$ |
| B | Aggressive | frequente | apertura fessure | $\leq w_1$ | apertura fessure | $\leq w_2$ |
| | | quasi permanente | decompressione | - | apertura fessure | $\leq w_1$ |
| C | Molto aggressive | frequente | formazione fessure | - | apertura fessure | $\leq w_1$ |
| | | quasi permanente | decompressione | - | apertura fessure | $\leq w_1$ |

Verifica Apertura di Fessura

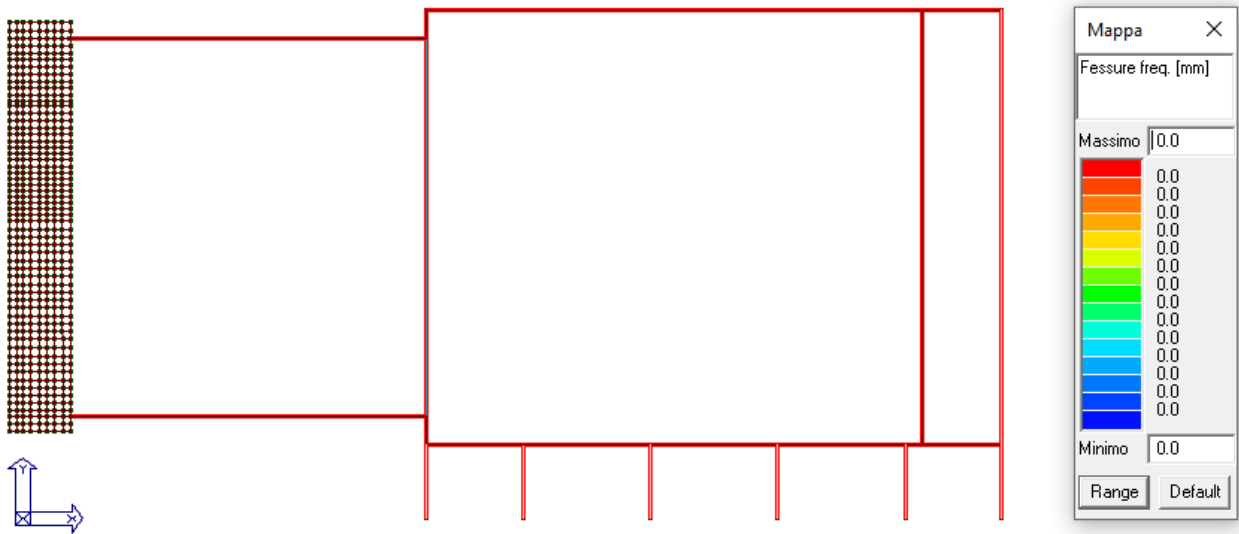


Fig 223. Cmb. SLE Frequente: Verifica Apertura di Fessura [$w_{max}= 0.0 \text{ mm} < w_3= 0.4 \text{ mm}$].

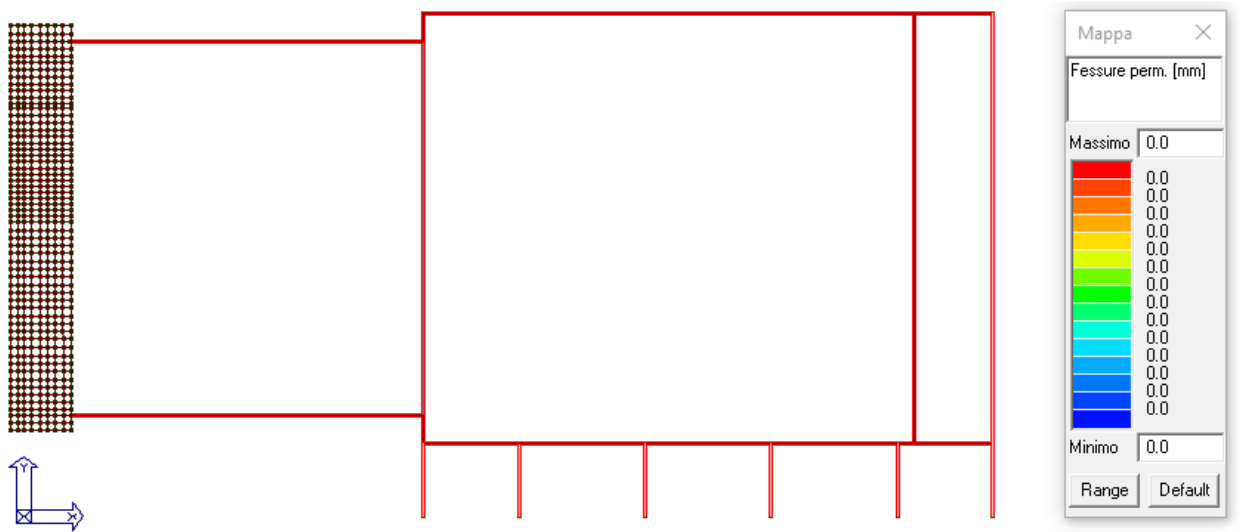


Fig 224. Cmb. SLE Quasi Perm.: Verifica Apertura di Fessura [$w_{max}= 0.0 \text{ mm} < w_3= 0.3 \text{ mm}$].

Verifica Apertura di Fessura Soddisfatta.

Verifica Stato Tensionale

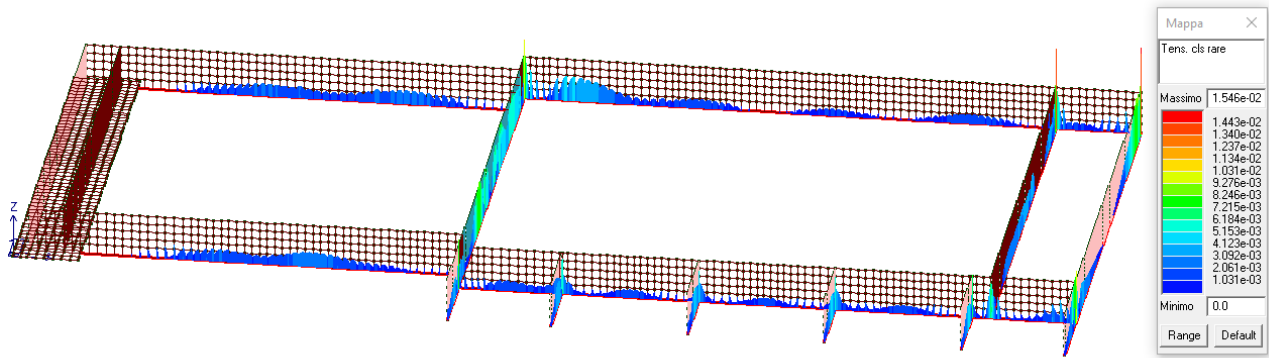


Fig 225. Cmb. SLE Rara: Rapporto di Verifica Stato tensionale max del cls [0.015 ≤ 1.0 Verifica soddisfatta].

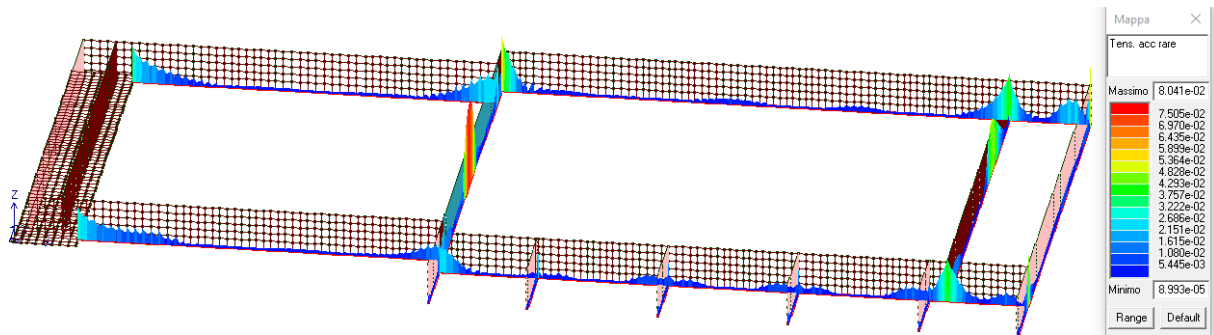


Fig 226. Cmb. SLE Rara: Rapporto di Verifica Stato tensionale max dell'acciaio [0.08 ≤ 1.0 Verifica soddisfatta].

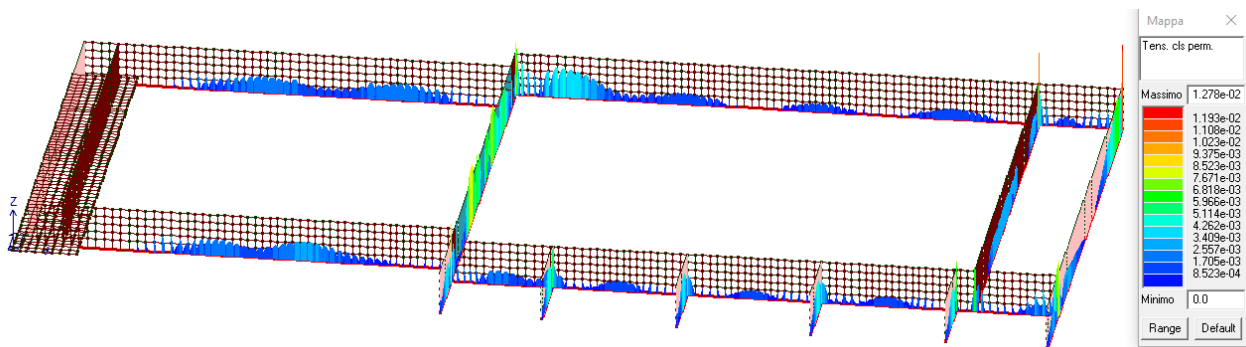


Fig 227. Cmb. SLE Quasi Perm.: Rapporto di Verifica Stato tensionale max del cls [0.013 ≤ 1.0 Verifica soddisfatta].

Verifica Stato tensionale massimo dei materiali Soddisfatta.

Verifiche Suola di Fondazione 215x40

Verifica Stato Tensionale

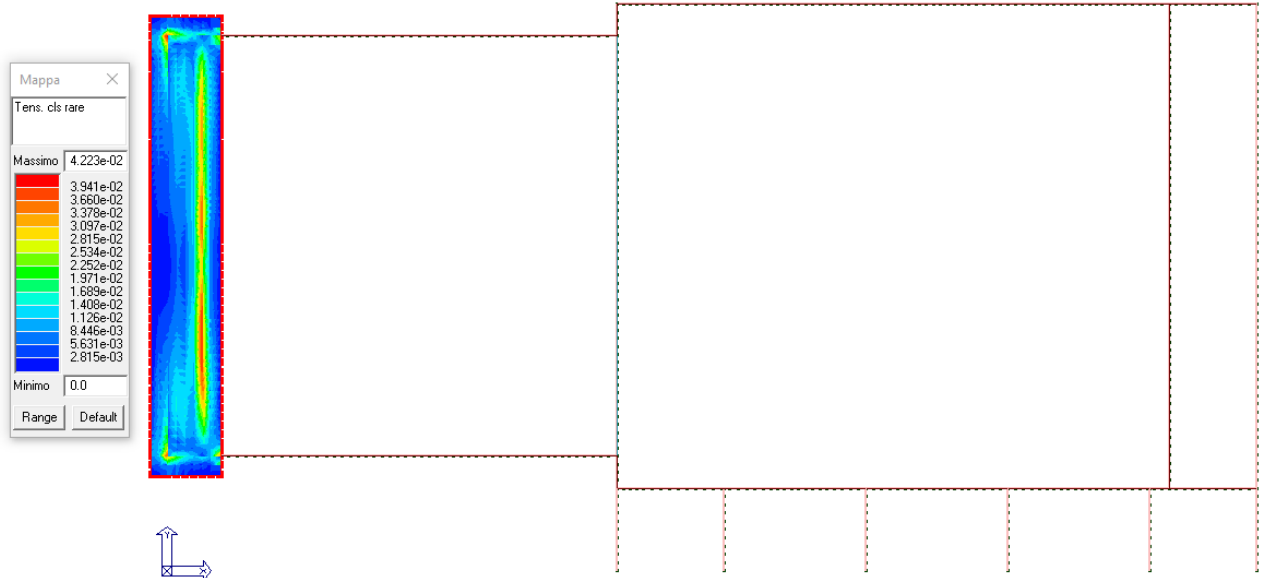


Fig 228. Cmb. SLE Rara: Rapporto di Verifica Stato tensionale max del cls [$0.04 \leq 1.0$ Verifica soddisfatta].

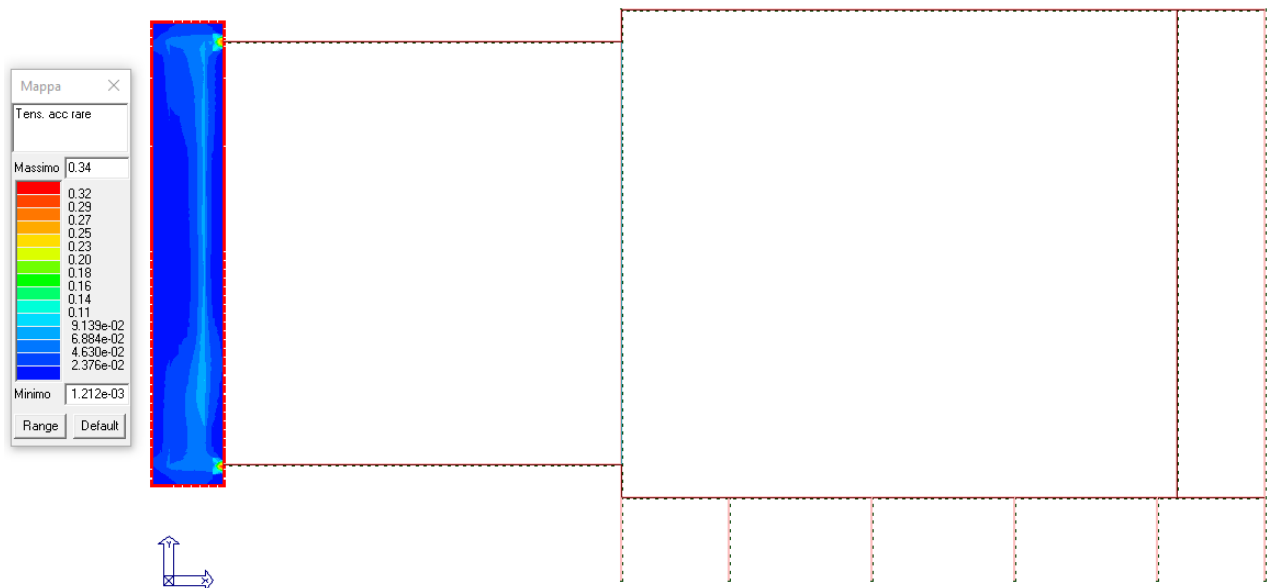


Fig 229. Cmb. SLE Rara: Rapporto di Verifica Stato tensionale max dell'acciaio [$0.34 \leq 1.0$ Verifica soddisfatta].

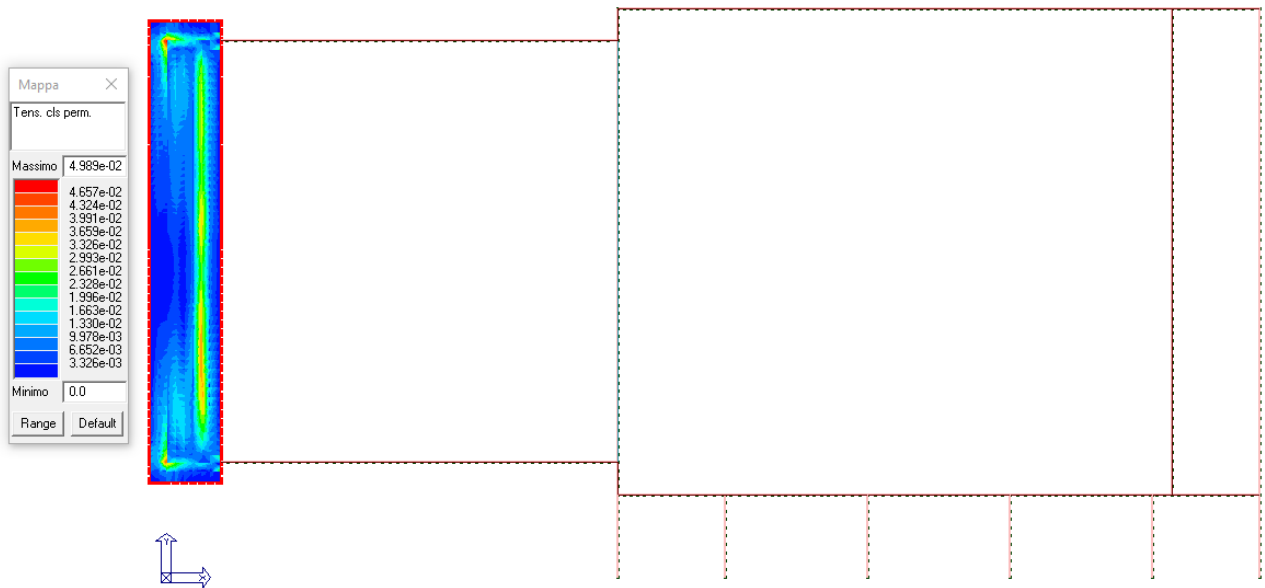


Fig 230. Cmb. SLE Quasi Perm.: Rapporto di Verifica Stato tensionale max del cls [$0.05 \leq 1.0$ Verifica soddisfatta].

Verifica Stato tensionale massimo dei materiali Soddisfatta.

2.3.6 Verifiche vasca di laminazione.

Verifica SL delle tensioni in esercizio

Le tensioni negli elementi vengono limitate ai seguenti valori:

| | |
|-------------------|--|
| Comb. Rara: | Calcestruzzo: $\sigma_c < 0.60 f_{ck}$ |
| | Acciaio: $\sigma_s < 0.80 f_{yk}$ |
| Comb. Permanente: | Calcestruzzo: $\sigma_c < 0.45 f_{ck}$ |

Si riporta la verifica dei setti.

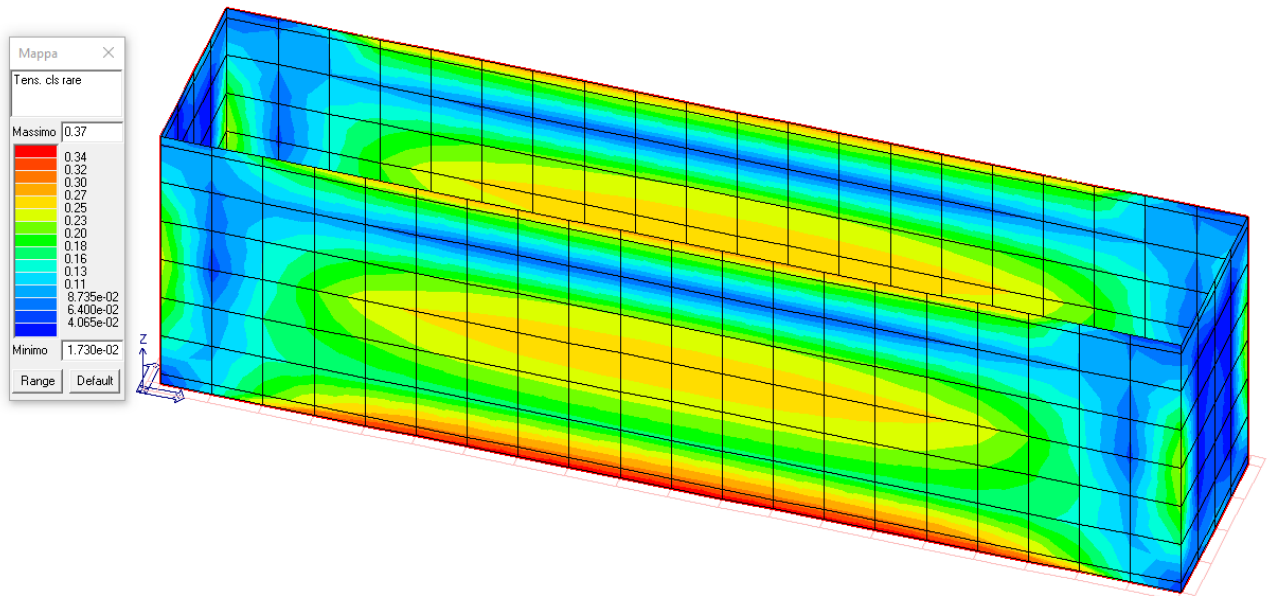


Fig 231. Cmb. SLE Rara: Rapporto di Verifica Stato tensionale max del cls [0.37 ≤ 1.0 Verifica soddisfatta].

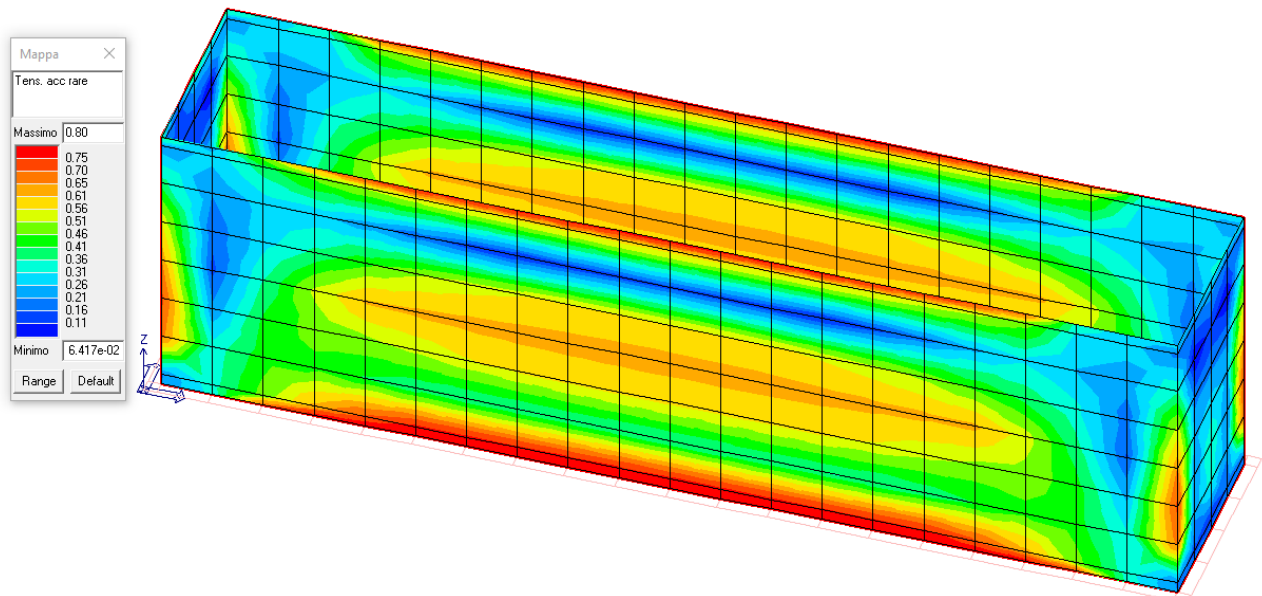


Fig 232. Cmb. SLE Rara: Rapporto di Verifica Stato tensionale max dell'acciaio [0.80 ≤ 1.0 Verifica soddisfatta].

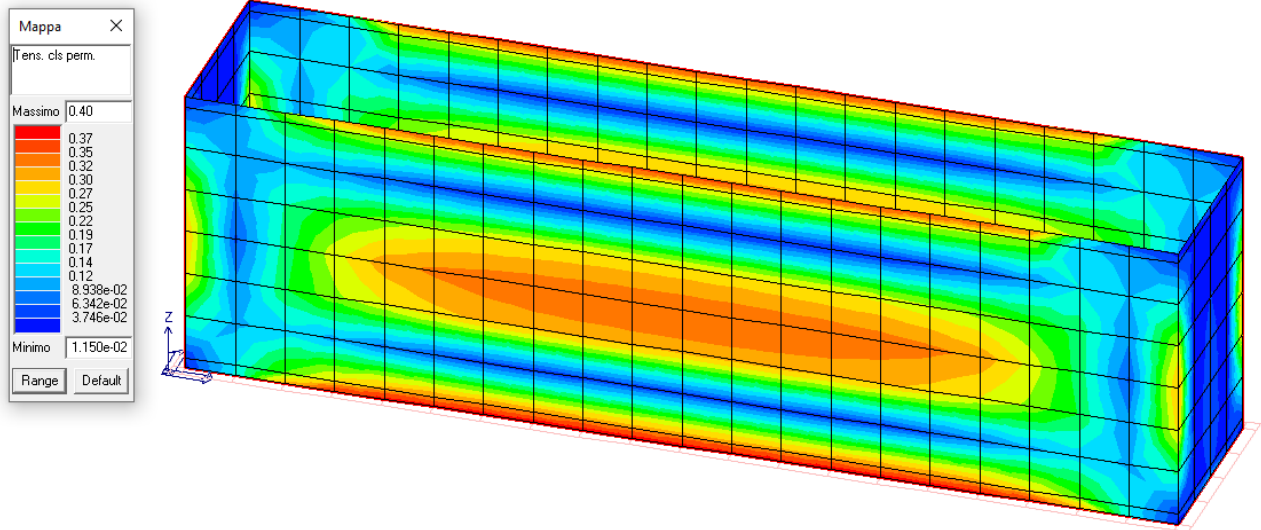


Fig 233. Cmb. SLE Quasi Perm.: Rapporto di Verifica Stato tensionale max del cls [0.40 ≤ 1.0 Verifica soddisfatta].

Si riporta la verifica delle solette.

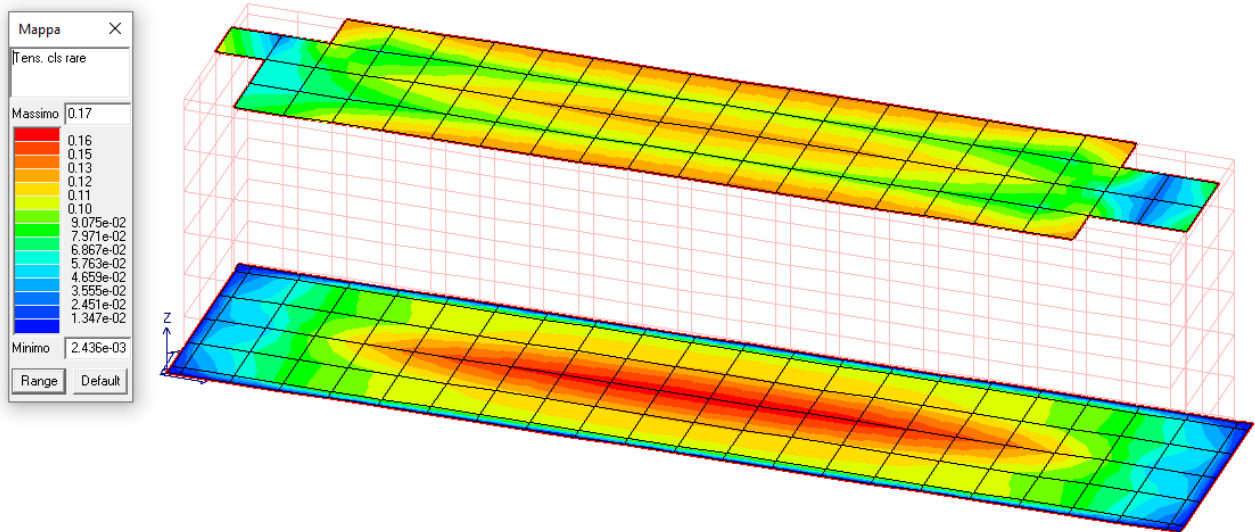


Fig 234. Cmb. SLE Rara: Rapporto di Verifica Stato tensionale max del cls [0.17 ≤ 1.0 Verifica soddisfatta].

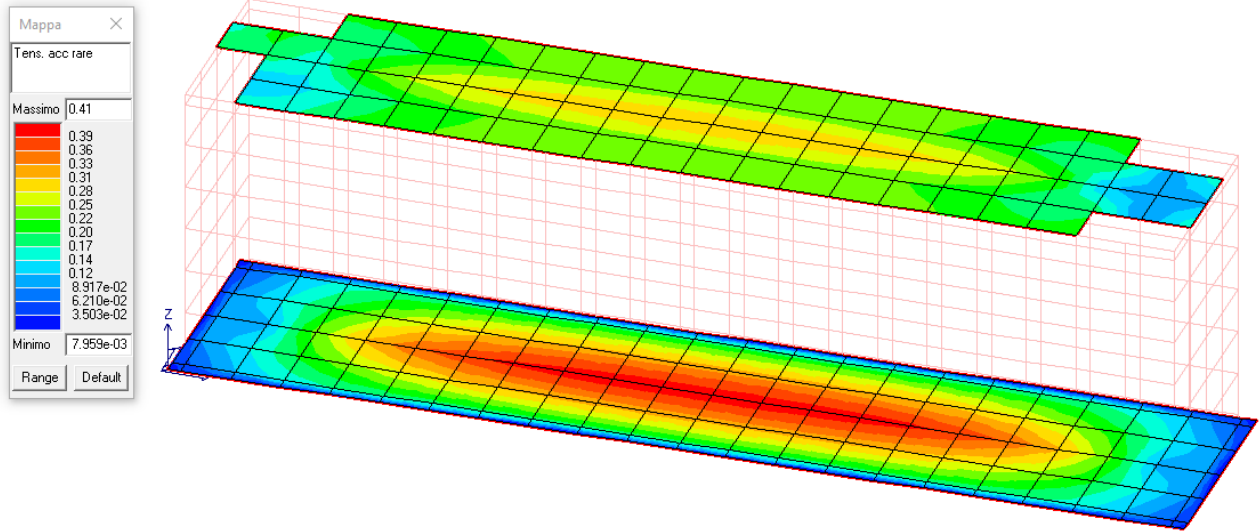


Fig 235. Cmb. SLE Rara: Rapporto di Verifica Stato tensionale max dell'acciaio [$0.41 \leq 1.0$ Verifica soddisfatta].

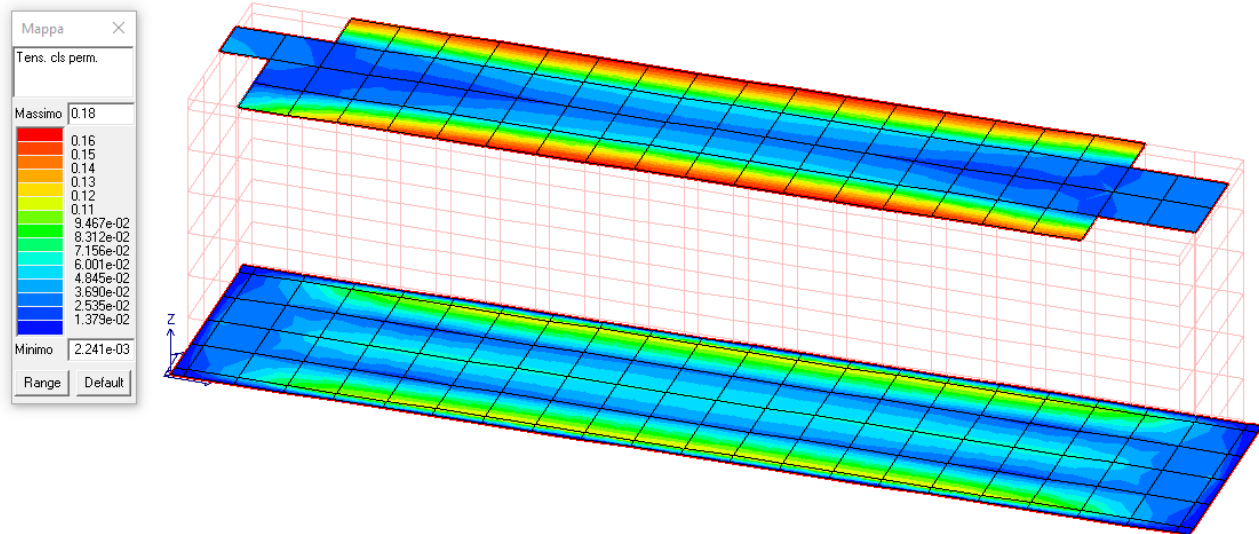


Fig 236. Cmb. SLE Quasi Perm.: Rapporto di Verifica Stato tensionale max del cls [$0.18 \leq 1.0$ Verifica soddisfatta].

IL PROGETTISTA STRUTTURALE

Per A.Ierre engineering S.r.l.

Ing. Silvio Bonati

